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Comune di Certaldo



PROGETTO:

**INTERVENTO DI ADEGUAMENTO STATICO E SISMICO
DELLA PASSERELLA PEDONALE SUL TORRENTE AGLIENA
TRA VIA TRENTO E VIA B. CIARI**

Progetto ESECUTIVO

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COLLABORATORI

COMUNE

Certaldo (FI)

DATA: Marzo 2022

LOCALITA'

Via Trento – Via B. Ciari

Il tecnico
Ing. Giovanni Corti

COMMITTENTE

Comune di Certaldo

ELABORATO

DS3.3

CALCOLI ESECUTIVI DELLE STRUTTURE
(FASCICOLO A8/9 – Campata "A")

Sez. A8-9(A)

Oggetto : INTERVENTO DI ADEGUAMENTO STATICO E SISMICO DELLA
PASSERELLA PEDONALE SUL TORRENTE AGLIENA TRA VIA
TRENTO E VIA B. CIARI – *Progetto ESECUTIVO*

Staz. Appaltante : Comune di Certaldo

Località : Via Trento / Via B. Ciari – Certaldo (FI)

Impalcato – Campata "A"

FASCICOLO DEI CALCOLI DELLE STRUTTURE

ANALISI SISMICA DINAMICA LINEARE

- DEFINIZIONE DEL MODELLO FEM DELLA STRUTTURA	PAG.	A8-9. 0001
- VERIFICHE ASTE IN ACCIAIO	PAG.	A8-9. 0143
- GRAFICI ESPLICATIVI DELLA STRUTTURA	PAG.	A8-9. 0355
- VERIFICHE PROFILI DI SOSTEGNO AGLI APPOGGI	PAG.	A8-9. 0357
- VERIFICHE DEGLI APPOGGI E DEGLI SPOSTAMENTI	PAG.	A8-9. 0389

Impalcato "A" – Definizione del modello F.E.M. (campata isolata)

Introduzione

Sistemi di riferimento

Le coordinate, i carichi concentrati, i cedimenti, le reazioni vincolari e gli spostamenti dei NODI sono riferiti ad una terna destra cartesiana globale con l'asse Z verticale rivolto verso l'alto.

I carichi in coordinate locali e le sollecitazioni delle ASTE sono riferite ad una terna destra cartesiana locale così definita:

- origine nel nodo iniziale dell'asta;
 - asse X coincidente con l'asse dell'asta e con verso dal nodo iniziale al nodo finale;
 - immaginando la trave a sezione rettangolare l'asse Y è parallelo alla base e l'asse Z è parallelo all'altezza.
- La rotazione dell'asta comporta quindi una rotazione di tutta la terna locale.

Si può immaginare la terna locale di un'asta comunque disposta nello spazio come derivante da quella globale dopo una serie di trasformazioni:

- una rotazione intorno all'asse Z che porti l'asse X a coincidere con la proiezione dell'asse dell'asta sul piano orizzontale;
- una traslazione lungo il nuovo asse X così definito in modo da portare l'origine a coincidere con la proiezione del nodo iniziale dell'asta sul piano orizzontale;
- una traslazione lungo l'asse Z che porti l'origine a coincidere con il nodo iniziale dell'asta;
- una rotazione intorno all'asse Y così definito che porti l'asse X a coincidere con l'asse dell'asta;
- una rotazione intorno all'asse X così definito pari alla rotazione dell'asta.

In pratica le travi prive di rotazione avranno sempre l'asse Z rivolto verso l'alto e l'asse Y nel piano del solaio, mentre i pilastri privi di rotazione avranno l'asse Y parallelo all'asse Y globale e l'asse Z parallelo ma controverso all'asse X globale. Da notare quindi che per i pilastri la "base" è il lato parallelo a Y.

Le sollecitazioni ed i carichi in coordinate locali negli ELEMENTI BIDIMENSIONALI e nei MURI sono riferiti ad una terna destra cartesiana locale così definita:

- origine nel primo nodo dell'elemento;
- asse X coincidente con la congiungente il primo ed il secondo nodo dell'elemento;
- asse Y definito come prodotto vettoriale fra il versore dell'asse X e il versore della congiungente il primo e il quarto nodo. Asse Z a formare con gli altri due una terna destrorsa.

Praticamente un elemento verticale con l'asse X locale coincidente con l'asse X globale ha anche gli altri assi locali coincidenti con quelli globali.

Rotazioni e momenti

Seguendo il principio adottato per tutti i carichi che sono positivi se CONTROVERSI agli assi, anche i momenti concentrati e le rotazioni impresse in coordinate globali risultano positivi se CONTROVERSI al segno positivo delle rotazioni. Il segno positivo dei momenti e delle rotazioni è quello orario per l'osservatore posto nell'origine: X ruota su Y, Y ruota su Z, Z ruota su X. In pratica è sufficiente adottare la regola della mano destra: col pollice rivolto nella direzione dell'asse, la rotazione che porta a chiudere il palmo della mano corrisponde al segno positivo.

Normativa di riferimento

La normativa di riferimento è la seguente:

- Legge n. 64 del 2/2/1974 - Provvedimenti per le costruzioni con particolari prescrizioni per le zone sismiche.
- D.M. del 24/1/1986 - Norme tecniche relative alle costruzioni sismiche.
- Legge n. 1086 del 5/11/1971 - Norme per la disciplina delle opere di conglomerato cementizio armato, normale e precompresso ed a struttura metallica.
- D.M. del 14/2/1992 - Norme tecniche per l'esecuzione delle opere in c.a. normale e precompresso e per le strutture metalliche.
- D.M. del 9/1/1996 - Norme tecniche per l'esecuzione delle opere in c.a. normale e precompresso e per le strutture metalliche.
- D.M. del 16/1/1996 - Norme tecniche per le costruzioni in zone sismiche.
- Circolare n. 21745 del 30/7/1981 - Legge n. 219 del 14/5/1981 - Art. 10 - Istruzioni relative al rafforzamento degli edifici in muratura danneggiati dal sisma.
- Regione Autonoma Friuli Venezia Giulia - Legge Regionale n. 30 del 20/6/1977 - Documentazione tecnica per la progettazione e direzione delle opere di riparazione degli edifici - Documento Tecnico n. 2 - Raccomandazioni per la riparazione strutturale degli edifici in muratura.
- D.M. del 20/11/1987 - Norme Tecniche per la progettazione, esecuzione e collaudo degli edifici in muratura e per il loro consolidamento.
- Norme Tecniche C.N.R. n. 10011-85 del 18/4/1985 - Costruzioni di acciaio - Istruzioni per il calcolo, l'esecuzione, il collaudo e la manutenzione.

- Norme Tecniche C.N.R. n. 10025-84 del 14/12/1984 - Istruzioni per il progetto, l'esecuzione ed il controllo delle strutture prefabbricate in conglomerato cementizio e per le strutture costruite con sistemi industrializzati di acciaio - Istruzioni per il calcolo, l'esecuzione, il collaudo e la manutenzione.

- Circolare n. 65 del 10/4/1997 - Istruzioni per l'applicazione delle "Norme tecniche per le costruzioni in zone sismiche" di cui al D.M. del 16/1/1996.

- Eurocodice 5 - Progettazione delle strutture di legno.

- DIN 1052 - Metodi di verifica per il legno.

- D.M. del 17/1/2018 - Norme tecniche per le costruzioni.

- Documento Tecnico CNR-DT 200 R1/2012 - Istruzioni per la Progettazione, l'Esecuzione ed il Controllo di Interventi di Consolidamento Statico mediante l'utilizzo di Compositi Fibrorinforzati.

- Eurocodice 3 - Progettazione delle strutture in acciaio.

Unità di misura

Le unità di misura adottate sono le seguenti:

- lunghezze : m
- forze : daN
- masse : kg
- temperature : gradi centigradi
- angoli : gradi sessadecimali o radianti

Geometria

Elenco vincoli nodi

Simbologia

- Vn = Numero del vincolo nodo
- Comm. = Commento
- Sx = Spostamento in dir. X (L=libero, B=bloccato, E=elastico)
- Sy = Spostamento in dir. Y (L=libero, B=bloccato, E=elastico)
- Sz = Spostamento in dir. Z (L=libero, B=bloccato, E=elastico)
- Rx = Rotazione intorno all'asse X (L=libera, B=bloccata, E=elastica)
- Ry = Rotazione intorno all'asse Y (L=libera, B=bloccata, E=elastica)
- Rz = Rotazione intorno all'asse Z (L=libera, B=bloccata, E=elastica)
- RL = Rotazione libera
- Ly = Lunghezza (dir. Y locale)
- Lz = Larghezza (dir. Z locale)
- Kt = Coeff. di sottofondo su suolo elastico alla Winkler

Vn	Comm.	Sx	Sy	Sz	Rx	Ry	Rz	RL	Ly	Lz	Kt
									<m>	<m>	<daN/cm>
1	Libero	L	L	L	L	L	L				
8	Nodo fisso	E	E	B	B	B	B				
9	Nodo fisso (scorr. X)	E	E	B	B	B	B				
10	Nodo scorrevole (fisso X)	E	E	B	B	B	B				
11	Nodo scorrevole (scorr. X)	E	E	B	B	B	B				

Elenco costanti elastiche nodali

Simbologia

- Nodo = Numero del nodo
- Kx = Costante elastica in dir. X
- Ky = Costante elastica in dir. Y
- Kz = Costante elastica in dir. Z
- KRx = Costante elastica intorno all'asse X
- KRy = Costante elastica intorno all'asse Y

Nodo	Kx	Ky	Kz	KRx	KRy	Nodo	Kx	Ky	Kz	KRx	KRy
	<daN/cm>	<daN/cm>	<daN/cm>	<daNm/rad>	<daNm/rad>		<daN/cm>	<daN/cm>	<daN/cm>	<daNm/rad>	<daNm/rad>
1519	10000.00	10000.00	--	--	--	1520	100.00	10000.00	--	--	--
2110	10000.00	100.00	--	--	--	2111	100.00	100.00	--	--	--

Elenco nodi

Simbologia

- Nodo = Numero del nodo
- X = Coordinata X del nodo
- Y = Coordinata Y del nodo
- Z = Coordinata Z del nodo
- Imp. = Numero dell'impalcato
- Vn = Numero del vincolo nodo

Nodo	X	Y	Z	Imp.	Vn	Nodo	X	Y	Z	Imp.	Vn	Nodo	X	Y	Z	Imp.	Vn
	<m>	<m>	<m>				<m>	<m>	<m>				<m>	<m>	<m>		

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-10257	2.00	-0.05	4.52	0	1	-10256	1.83	-0.05	4.52	0	1	-10255	1.67	-0.05	4.52	0	1
-10254	1.48	-0.05	4.52	0	1	-10253	1.33	-0.05	4.52	0	1	-10252	1.19	-0.05	4.52	0	1
-10251	0.88	-0.05	4.52	0	1	-10250	0.75	-0.05	4.52	0	1	-10249	0.63	-0.05	4.52	0	1
-10248	0.32	-0.05	4.52	0	1	-10247	0.17	-0.05	4.52	0	1	-10246	0.03	-0.05	4.52	0	1
-10245	-0.17	-0.05	4.52	0	1	-10244	-0.33	-0.05	4.52	0	1	-10243	-0.50	-0.05	4.52	0	1
-10201	2.00	-0.22	4.51	0	1	-10200	1.83	-0.22	4.51	0	1	-10199	1.66	-0.22	4.51	0	1
-10198	1.49	-0.22	4.51	0	1	-10197	1.17	-0.22	4.51	0	1	-10196	0.88	-0.22	4.51	0	1
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-10134	1.83	-0.39	4.51	0	1	-10133	1.66	-0.39	4.51	0	1	-10132	1.50	-0.39	4.51	0	1
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-10128	0.88	-0.39	4.51	0	1	-10127	0.75	-0.39	4.51	0	1	-10126	0.63	-0.39	4.51	0	1
-10125	0.50	-0.39	4.51	0	1	-10124	0.33	-0.39	4.51	0	1	-10123	0.17	-0.39	4.51	0	1
-10122	0.00	-0.39	4.51	0	1	-10121	-0.16	-0.39	4.51	0	1	-10120	-0.33	-0.39	4.51	0	1
-10119	-0.50	-0.39	4.51	0	1	-10043	2.00	-0.56	4.51	0	1	-10042	1.83	-0.56	4.51	0	1
-10041	1.66	-0.56	4.51	0	1	-10040	1.50	-0.56	4.51	0	1	-10039	1.33	-0.56	4.51	0	1
-10038	1.17	-0.56	4.51	0	1	-10037	1.00	-0.56	4.51	0	1	-10036	0.88	-0.56	4.51	0	1
-10035	0.75	-0.56	4.51	0	1	-10034	0.63	-0.56	4.51	0	1	-10033	0.50	-0.56	4.51	0	1
-10032	0.33	-0.56	4.51	0	1	-10031	0.17	-0.56	4.51	0	1	-10030	0.00	-0.56	4.51	0	1
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-9745	1.67	-1.08	4.49	0	1	-9744	1.48	-1.08	4.49	0	1	-9743	1.33	-1.08	4.49	0	1
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-9435	-0.16	-1.95	4.47	0	1	-9434	-0.33	-1.95	4.47	0	1	-9433	-0.50	-1.95	4.47	0	1
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-9380	1.48	-2.12	4.47	0	1	-9379	1.33	-2.12	4.47	0	1	-9378	1.19	-2.12	4.47	0	1
-9377	1.00	-2.12	4.47	0	1	-9376	0.88	-2.12	4.47	0	1	-9375	0.75	-2.12	4.47	0	1
-9374	0.63	-2.12	4.47	0	1	-9373	0.50	-2.12	4.47	0	1	-9372	0.32	-2.12	4.47	0	1
-9371	0.17	-2.12	4.47	0	1	-9370	0.03	-2.12	4.47	0	1	-9369	-0.17	-2.12	4.47	0	1
-9368	-0.33	-2.12	4.47	0	1	-9367	-0.50	-2.12	4.47	0	1	-9292	2.00	-2.29	4.46	0	1
-9291	1.83	-2.29	4.46	0	1	-9290	1.66	-2.29	4.46	0	1	-9289	1.49	-2.29	4.46	0	1
-9288	1.33	-2.29	4.46	0	1	-9287	1.17	-2.29	4.46	0	1	-9286	1.00	-2.29	4.46	0	1
-9285	0.88	-2.29	4.46	0	1	-9284	0.75	-2.29	4.46	0	1	-9283	0.63	-2.29	4.46	0	1
-9282	0.50	-2.29	4.46	0	1	-9281	0.33	-2.29	4.46	0	1	-9280	0.17	-2.29	4.46	0	1
-9279	0.01	-2.29	4.46	0	1	-9278	-0.16	-2.29	4.46	0	1	-9277	-0.33	-2.29	4.46	0	1

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-9276	-0.50	-2.29	4.46	0	1	-9218	1.64	-1.08	4.46	0	1	-9217	-0.14	-1.08	4.46	0	1
-9216	2.00	-2.47	4.46	0	1	-9215	1.83	-2.47	4.46	0	1	-9214	1.66	-2.47	4.46	0	1
-9213	1.50	-2.47	4.46	0	1	-9212	1.33	-2.47	4.46	0	1	-9211	1.17	-2.47	4.46	0	1
-9210	1.00	-2.47	4.46	0	1	-9209	0.88	-2.47	4.46	0	1	-9208	0.75	-2.47	4.46	0	1
-9207	0.63	-2.47	4.46	0	1	-9206	0.50	-2.47	4.46	0	1	-9205	0.33	-2.47	4.46	0	1
-9204	0.17	-2.47	4.46	0	1	-9203	0.00	-2.47	4.46	0	1	-9202	-0.16	-2.47	4.46	0	1
-9201	-0.33	-2.47	4.46	0	1	-9200	-0.50	-2.47	4.46	0	1	-9158	2.00	-2.64	4.45	0	1
-9157	1.83	-2.64	4.45	0	1	-9156	1.66	-2.64	4.45	0	1	-9155	1.50	-2.64	4.45	0	1
-9154	1.33	-2.64	4.45	0	1	-9153	1.17	-2.64	4.45	0	1	-9152	1.00	-2.64	4.45	0	1
-9151	0.88	-2.64	4.45	0	1	-9150	0.75	-2.64	4.45	0	1	-9149	0.63	-2.64	4.45	0	1
-9148	0.50	-2.64	4.45	0	1	-9147	0.33	-2.64	4.45	0	1	-9146	0.17	-2.64	4.45	0	1
-9145	0.00	-2.64	4.45	0	1	-9144	-0.16	-2.64	4.45	0	1	-9143	-0.33	-2.64	4.45	0	1
-9142	-0.50	-2.64	4.45	0	1	-9100	2.00	-2.81	4.45	0	1	-9099	1.83	-2.81	4.45	0	1
-9098	1.66	-2.81	4.45	0	1	-9097	1.50	-2.81	4.45	0	1	-9096	1.33	-2.81	4.45	0	1
-9095	0.75	-2.81	4.45	0	1	-9094	0.17	-2.81	4.45	0	1	-9093	-0.33	-2.81	4.45	0	1
-9076	1.17	-2.81	4.45	0	1	-9075	1.00	-2.81	4.45	0	1	-9074	0.88	-2.81	4.45	0	1
-9073	0.63	-2.81	4.45	0	1	-9072	0.50	-2.81	4.45	0	1	-9071	0.33	-2.81	4.45	0	1
-9070	0.00	-2.81	4.45	0	1	-9069	-0.16	-2.81	4.45	0	1	-9068	-0.50	-2.81	4.45	0	1
-8991	2.00	-2.98	4.44	0	1	-8990	1.83	-2.98	4.44	0	1	-8989	1.66	-2.98	4.44	0	1
-8988	1.49	-2.98	4.44	0	1	-8987	1.33	-2.98	4.44	0	1	-8986	1.17	-2.98	4.44	0	1
-8985	1.00	-2.98	4.44	0	1	-8984	0.88	-2.98	4.44	0	1	-8983	0.75	-2.98	4.44	0	1
-8982	0.63	-2.98	4.44	0	1	-8981	0.50	-2.98	4.44	0	1	-8980	0.33	-2.98	4.44	0	1
-8979	0.17	-2.98	4.44	0	1	-8978	0.01	-2.98	4.44	0	1	-8977	-0.16	-2.98	4.44	0	1
-8976	-0.33	-2.98	4.44	0	1	-8975	-0.50	-2.98	4.44	0	1	-8919	1.48	-0.04	4.44	0	1
-8918	0.03	-0.04	4.44	0	1	-8917	2.00	-3.16	4.44	0	1	-8916	1.83	-3.16	4.44	0	1
-8915	1.67	-3.16	4.44	0	1	-8914	1.48	-3.16	4.44	0	1	-8913	1.33	-3.16	4.44	0	1
-8912	1.19	-3.16	4.44	0	1	-8911	1.00	-3.16	4.44	0	1	-8910	0.88	-3.16	4.44	0	1
-8909	0.75	-3.16	4.44	0	1	-8908	0.63	-3.16	4.44	0	1	-8907	0.50	-3.16	4.44	0	1
-8906	0.32	-3.16	4.44	0	1	-8905	0.17	-3.16	4.44	0	1	-8904	0.03	-3.16	4.44	0	1
-8903	-0.17	-3.16	4.44	0	1	-8902	-0.33	-3.16	4.44	0	1	-8901	-0.50	-3.16	4.44	0	1
-8843	1.49	-3.33	4.43	0	1	-8842	1.33	-3.33	4.43	0	1	-8841	0.88	-3.33	4.43	0	1
-8840	0.63	-3.33	4.43	0	1	-8839	0.01	-3.33	4.43	0	1	-8827	1.83	-3.33	4.43	0	1
-8826	1.66	-3.33	4.43	0	1	-8825	0.75	-3.33	4.43	0	1	-8824	0.50	-3.33	4.43	0	1
-8809	2.00	-3.33	4.43	0	1	-8808	1.00	-3.33	4.43	0	1	-8807	0.33	-3.33	4.43	0	1
-8806	0.17	-3.33	4.43	0	1	-8803	-0.16	-3.33	4.43	0	1	-8802	-0.33	-3.33	4.43	0	1
-8801	-0.50	-3.33	4.43	0	1	-8787	1.17	-3.33	4.43	0	1	-8730	1.64	-2.12	4.43	0	1
-8729	-0.14	-2.12	4.43	0	1	-8728	2.00	-3.50	4.43	0	1	-8727	1.83	-3.50	4.43	0	1
-8726	1.66	-3.50	4.43	0	1	-8725	1.50	-3.50	4.43	0	1	-8724	1.33	-3.50	4.43	0	1
-8723	1.17	-3.50	4.43	0	1	-8722	1.00	-3.50	4.43	0	1	-8721	0.88	-3.50	4.43	0	1
-8720	0.75	-3.50	4.43	0	1	-8719	0.63	-3.50	4.43	0	1	-8718	0.50	-3.50	4.43	0	1
-8717	0.33	-3.50	4.43	0	1	-8716	0.17	-3.50	4.43	0	1	-8715	0.00	-3.50	4.43	0	1
-8714	-0.16	-3.50	4.43	0	1	-8713	-0.33	-3.50	4.43	0	1	-8712	-0.50	-3.50	4.43	0	1
-8635	2.00	-3.67	4.43	0	1	-8634	1.83	-3.67	4.43	0	1	-8633	1.66	-3.67	4.43	0	1
-8632	1.50	-3.67	4.43	0	1	-8631	1.33	-3.67	4.43	0	1	-8630	1.17	-3.67	4.43	0	1
-8629	0.88	-3.67	4.43	0	1	-8628	0.63	-3.67	4.43	0	1	-8627	-0.33	-3.67	4.43	0	1
-8622	1.00	-3.67	4.43	0	1	-8621	0.75	-3.67	4.43	0	1	-8620	0.50	-3.67	4.43	0	1
-8619	0.33	-3.67	4.43	0	1	-8618	0.17	-3.67	4.43	0	1	-8617	0.00	-3.67	4.43	0	1
-8616	-0.16	-3.67	4.43	0	1	-8615	-0.50	-3.67	4.43	0	1	-8546	2.00	-3.85	4.42	0	1
-8545	1.83	-3.85	4.42	0	1	-8544	1.66	-3.85	4.42	0	1	-8543	1.50	-3.85	4.42	0	1
-8542	1.33	-3.85	4.42	0	1	-8541	1.17	-3.85	4.42	0	1	-8540	1.00	-3.85	4.42	0	1
-8539	0.88	-3.85	4.42	0	1	-8538	0.75	-3.85	4.42	0	1	-8537	0.63	-3.85	4.42	0	1
-8536	0.50	-3.85	4.42	0	1	-8535	0.33	-3.85	4.42	0	1	-8534	0.17	-3.85	4.42	0	1
-8533	0.00	-3.85	4.42	0	1	-8532	-0.16	-3.85	4.42	0	1	-8531	-0.33	-3.85	4.42	0	1
-8450	-0.50	-3.85	4.42	0	1	-8486	2.00	-4.02	4.42	0	1	-8485	1.83	-4.02	4.42	0	1
-8484	1.66	-4.02	4.42	0	1	-8483	1.49	-4.02	4.42	0	1	-8482	1.00	-4.02	4.42	0	1
-8481	0.88	-4.02	4.42	0	1	-8480	0.75	-4.02	4.42	0	1	-8479	0.63	-4.02	4.42	0	1
-8478	0.33	-4.02	4.42	0	1	-8477	-0.33	-4.02	4.42	0	1	-8474	1.33	-4.02	4.42	0	1
-8473	1.17	-4.02	4.42	0	1	-8472	0.50	-4.02	4.42	0	1	-8471	0.17	-4.02	4.42	0	1
-8470	0.01	-4.02	4.42	0	1	-8469	-0.16	-4.02	4.42	0	1	-8468	-0.50	-4.02	4.42	0	1
-8435	1.48	-1.08	4.41	0	1	-8434	0.03	-1.08	4.41	0	1	-8433	2.00	-4.19	4.41	0	1
-8432	1.83	-4.19	4.41	0	1	-8431	1.67	-4.19	4.41	0	1	-8430	1.48	-4.19	4.41	0	1
-8429	1.33	-4.19	4.41	0	1	-8428	1.19	-4.19	4.41	0	1	-8427	1.00	-4.19	4.41	0	1
-8426	0.88	-4.19	4.41	0	1	-8425	0.75	-4.19	4.41	0	1	-8424	0.63	-4.19	4.41	0	1
-8423	0.50	-4.19	4.41	0	1	-8422	0.32	-4.19	4.41	0	1	-8421	0.17	-4.19	4.41	0	1
-8420	0.03	-4.19	4.41	0	1	-8419	-0.17	-4.19	4.41	0	1	-8418	-0.33	-4.19	4.41	0	1
-8417	-0.50	-4.19	4.41	0	1	-8386	2.00	-4.37	4.41	0	1	-8385	1.83	-4.37	4.41	0	1
-8384	1.66	-4.37	4.41	0	1	-8383	1.49	-4.37	4.41	0	1	-8382	1.33	-4.37	4.41	0	1
-8381	1.17	-4.37	4.41	0	1	-8380	1.00	-4.37	4.41	0	1	-8379	0.88	-4.37	4.41	0	1
-8378	0.75	-4.37	4.41	0	1	-8377	0.63	-4.37	4.41	0	1	-8376	0.50	-4.37	4.41	0	1
-8375	0.33	-4.37	4.41	0	1	-8374	0.17	-4.37	4.41	0	1	-8373	0.01	-4.37	4.41	0	1
-8372	-0.16	-4.37	4.41	0	1	-8371	-0.33	-4.37	4.41	0	1	-8370	-0.50	-4.37	4.41	0	1
-8327	1.64	-3.16	4.40	0	1	-8326	-0.14	-3.16	4.40	0	1	-8325	2.00	-4.54	4.40	0	1
-8324	1.83	-4.54	4.40	0	1	-8323	1.66	-4.54	4.40	0	1	-8322	1.50	-4.54	4.40	0	1
-8321	1.33	-4.54	4.40	0	1	-8320	1.17	-4.54	4.40	0	1	-8319	1.00	-4.54	4.40	0	1
-8318	0.88	-4.54	4.40	0	1	-8317	0.75	-4.54	4.40	0	1	-8316	0.63	-4.54	4.40	0	1
-8315	0.50	-4.54	4.40	0	1	-8314	0.33	-4.54	4.40	0	1	-8313	0.17	-4.54	4.40	0	1
-8312	0.00	-4.54	4.40	0	1	-8311	-0.16	-4.54	4.40	0	1	-8310	-0.33	-4.54	4.40	0	1
-8309	-0.50	-4.54	4.40	0	1	-8237	2.00	-4.71	4.40	0	1	-8236	1.83	-4.71	4.40	0	1
-8235	1.66	-4.71	4.40	0	1	-8234	1.50	-4.71	4.40	0	1	-8233	1.33	-4.71	4.40	0	1

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-8232	1.17	-4.71	4.40	0	1	-8231	1.00	-4.71	4.40	0	1	-8230	0.88	-4.71	4.40	0	1
-8229	0.75	-4.71	4.40	0	1	-8228	0.63	-4.71	4.40	0	1	-8227	0.50	-4.71	4.40	0	1
-8226	0.33	-4.71	4.40	0	1	-8225	0.17	-4.71	4.40	0	1	-8224	0.00	-4.71	4.40	0	1
-8223	-0.16	-4.71	4.40	0	1	-8222	-0.33	-4.71	4.40	0	1	-8221	-0.50	-4.71	4.40	0	1
-8163	2.00	-4.88	4.39	0	1	-8162	1.83	-4.88	4.39	0	1	-8161	1.66	-4.88	4.39	0	1
-8160	1.50	-4.88	4.39	0	1	-8159	1.33	-4.88	4.39	0	1	-8158	1.17	-4.88	4.39	0	1
-8157	1.00	-4.88	4.39	0	1	-8156	0.88	-4.88	4.39	0	1	-8155	0.75	-4.88	4.39	0	1
-8154	0.63	-4.88	4.39	0	1	-8153	0.50	-4.88	4.39	0	1	-8152	0.33	-4.88	4.39	0	1
-8151	0.17	-4.88	4.39	0	1	-8150	0.00	-4.88	4.39	0	1	-8149	-0.16	-4.88	4.39	0	1
-8148	-0.33	-4.88	4.39	0	1	-8147	-0.50	-4.88	4.39	0	1	-8037	2.00	-5.06	4.39	0	1
-8036	1.83	-5.06	4.39	0	1	-8035	1.66	-5.06	4.39	0	1	-8034	1.49	-5.06	4.39	0	1
-8033	1.33	-5.06	4.39	0	1	-8032	1.17	-5.06	4.39	0	1	-8031	1.00	-5.06	4.39	0	1
-8030	0.88	-5.06	4.39	0	1	-8029	0.75	-5.06	4.39	0	1	-8028	0.63	-5.06	4.39	0	1
-8027	0.50	-5.06	4.39	0	1	-8026	0.33	-5.06	4.39	0	1	-8025	0.17	-5.06	4.39	0	1
-8024	0.01	-5.06	4.39	0	1	-8023	-0.16	-5.06	4.39	0	1	-8022	-0.33	-5.06	4.39	0	1
-8021	-0.50	-5.06	4.39	0	1	-7985	1.48	-2.12	4.39	0	1	-7984	0.03	-2.12	4.39	0	1
-7983	2.00	-5.23	4.39	0	1	-7982	1.83	-5.23	4.39	0	1	-7981	1.67	-5.23	4.39	0	1
-7980	1.48	-5.23	4.39	0	1	-7979	1.33	-5.23	4.39	0	1	-7978	1.19	-5.23	4.39	0	1
-7977	1.00	-5.23	4.39	0	1	-7976	0.88	-5.23	4.39	0	1	-7975	0.75	-5.23	4.39	0	1
-7974	0.63	-5.23	4.39	0	1	-7973	0.50	-5.23	4.39	0	1	-7972	0.32	-5.23	4.39	0	1
-7971	0.17	-5.23	4.39	0	1	-7970	0.03	-5.23	4.39	0	1	-7969	-0.17	-5.23	4.39	0	1
-7968	-0.33	-5.23	4.39	0	1	-7967	-0.50	-5.23	4.39	0	1	-7937	2.00	-5.40	4.38	0	1
-7936	1.83	-5.40	4.38	0	1	-7935	1.66	-5.40	4.38	0	1	-7934	1.49	-5.40	4.38	0	1
-7933	1.33	-5.40	4.38	0	1	-7932	1.17	-5.40	4.38	0	1	-7931	1.00	-5.40	4.38	0	1
-7930	0.88	-5.40	4.38	0	1	-7929	0.75	-5.40	4.38	0	1	-7928	0.63	-5.40	4.38	0	1
-7927	0.50	-5.40	4.38	0	1	-7926	0.33	-5.40	4.38	0	1	-7925	0.17	-5.40	4.38	0	1
-7924	0.01	-5.40	4.38	0	1	-7923	-0.16	-5.40	4.38	0	1	-7922	-0.33	-5.40	4.38	0	1
-7921	-0.50	-5.40	4.38	0	1	-7815	1.64	-4.19	4.38	0	1	-7814	-0.14	-4.19	4.38	0	1
-7813	2.00	-5.57	4.38	0	1	-7812	1.83	-5.57	4.38	0	1	-7811	1.66	-5.57	4.38	0	1
-7810	1.50	-5.57	4.38	0	1	-7809	1.33	-5.57	4.38	0	1	-7808	1.00	-5.57	4.38	0	1
-7807	0.88	-5.57	4.38	0	1	-7806	0.75	-5.57	4.38	0	1	-7805	0.63	-5.57	4.38	0	1
-7804	0.50	-5.57	4.38	0	1	-7803	0.17	-5.57	4.38	0	1	-7802	0.00	-5.57	4.38	0	1
-7801	-0.33	-5.57	4.38	0	1	-7800	-0.50	-5.57	4.38	0	1	-7781	1.17	-5.57	4.38	0	1
-7780	0.33	-5.57	4.38	0	1	-7779	-0.16	-5.57	4.38	0	1	-7728	1.31	-0.04	4.37	0	1
-7727	0.18	-0.04	4.37	0	1	-7723	2.00	-5.75	4.37	0	1	-7722	1.83	-5.75	4.37	0	1
-7721	1.33	-5.75	4.37	0	1	-7716	1.66	-5.75	4.37	0	1	-7715	1.50	-5.75	4.37	0	1
-7714	1.17	-5.75	4.37	0	1	-7713	1.00	-5.75	4.37	0	1	-7712	0.88	-5.75	4.37	0	1
-7711	0.75	-5.75	4.37	0	1	-7710	0.63	-5.75	4.37	0	1	-7709	0.50	-5.75	4.37	0	1
-7708	0.33	-5.75	4.37	0	1	-7707	0.17	-5.75	4.37	0	1	-7706	-0.16	-5.75	4.37	0	1
-7705	-0.33	-5.75	4.37	0	1	-7698	0.00	-5.75	4.37	0	1	-7697	-0.50	-5.75	4.37	0	1
-7671	2.00	-5.92	4.37	0	1	-7670	1.83	-5.92	4.37	0	1	-7669	1.66	-5.92	4.37	0	1
-7668	1.50	-5.92	4.37	0	1	-7667	1.17	-5.92	4.37	0	1	-7666	0.88	-5.92	4.37	0	1
-7663	1.00	-5.92	4.37	0	1	-7662	0.75	-5.92	4.37	0	1	-7661	0.63	-5.92	4.37	0	1
-7660	0.50	-5.92	4.37	0	1	-7659	0.33	-5.92	4.37	0	1	-7658	0.17	-5.92	4.37	0	1
-7657	0.00	-5.92	4.37	0	1	-7656	-0.16	-5.92	4.37	0	1	-7655	-0.33	-5.92	4.37	0	1
-7654	-0.50	-5.92	4.37	0	1	-7643	1.33	-5.92	4.37	0	1	-7586	2.00	-6.09	4.36	0	1
-7585	1.83	-6.09	4.36	0	1	-7584	1.66	-6.09	4.36	0	1	-7583	1.49	-6.09	4.36	0	1
-7582	1.33	-6.09	4.36	0	1	-7581	1.17	-6.09	4.36	0	1	-7580	1.00	-6.09	4.36	0	1
-7579	0.88	-6.09	4.36	0	1	-7578	0.63	-6.09	4.36	0	1	-7577	0.50	-6.09	4.36	0	1
-7576	0.17	-6.09	4.36	0	1	-7572	0.75	-6.09	4.36	0	1	-7571	0.33	-6.09	4.36	0	1
-7570	0.01	-6.09	4.36	0	1	-7569	-0.16	-6.09	4.36	0	1	-7568	-0.33	-6.09	4.36	0	1
-7567	-0.50	-6.09	4.36	0	1	-7510	1.48	-3.15	4.36	0	1	-7509	0.03	-3.15	4.36	0	1
-7508	2.00	-6.27	4.36	0	1	-7507	1.83	-6.27	4.36	0	1	-7506	1.67	-6.27	4.36	0	1
-7505	1.48	-6.27	4.36	0	1	-7504	1.33	-6.27	4.36	0	1	-7503	1.19	-6.27	4.36	0	1
-7502	1.00	-6.27	4.36	0	1	-7501	0.88	-6.27	4.36	0	1	-7500	0.75	-6.27	4.36	0	1
-7499	0.63	-6.27	4.36	0	1	-7498	0.50	-6.27	4.36	0	1	-7497	0.32	-6.27	4.36	0	1
-7496	0.17	-6.27	4.36	0	1	-7495	0.03	-6.27	4.36	0	1	-7494	-0.17	-6.27	4.36	0	1
-7493	-0.33	-6.27	4.36	0	1	-7492	-0.50	-6.27	4.36	0	1	-7472	2.00	-6.44	4.35	0	1
-7471	1.83	-6.44	4.35	0	1	-7470	1.66	-6.44	4.35	0	1	-7469	1.49	-6.44	4.35	0	1
-7468	1.33	-6.44	4.35	0	1	-7467	1.17	-6.44	4.35	0	1	-7466	1.00	-6.44	4.35	0	1
-7465	0.88	-6.44	4.35	0	1	-7464	0.75	-6.44	4.35	0	1	-7463	0.63	-6.44	4.35	0	1
-7462	0.50	-6.44	4.35	0	1	-7461	0.33	-6.44	4.35	0	1	-7460	0.17	-6.44	4.35	0	1
-7459	0.01	-6.44	4.35	0	1	-7458	-0.16	-6.44	4.35	0	1	-7457	-0.33	-6.44	4.35	0	1
-7456	-0.50	-6.44	4.35	0	1	-7358	1.64	-5.23	4.35	0	1	-7357	-0.14	-5.23	4.35	0	1
-7356	2.00	-6.61	4.35	0	1	-7355	1.83	-6.61	4.35	0	1	-7354	1.66	-6.61	4.35	0	1
-7353	1.50	-6.61	4.35	0	1	-7352	1.33	-6.61	4.35	0	1	-7351	1.17	-6.61	4.35	0	1
-7350	1.00	-6.61	4.35	0	1	-7349	0.88	-6.61	4.35	0	1	-7348	0.75	-6.61	4.35	0	1
-7347	0.63	-6.61	4.35	0	1	-7346	0.50	-6.61	4.35	0	1	-7345	0.33	-6.61	4.35	0	1
-7344	0.17	-6.61	4.35	0	1	-7343	0.00	-6.61	4.35	0	1	-7342	-0.16	-6.61	4.35	0	1
-7341	-0.33	-6.61	4.35	0	1	-7340	-0.50	-6.61	4.35	0	1	-7310	1.31	-1.08	4.35	0	1
-7309	0.18	-1.08	4.35	0	1	-7306	2.00	-6.78	4.35	0	1	-7305	1.83	-6.78	4.35	0	1
-7304	1.66	-6.78	4.35	0	1	-7303	1.50	-6.78	4.35	0	1	-7302	1.33	-6.78	4.35	0	1
-7301	1.17	-6.78	4.35	0	1	-7300	1.00	-6.78	4.35	0	1	-7299	0.88	-6.78	4.35	0	1
-7298	0.75	-6.78	4.35	0	1	-7297	0.63	-6.78	4.35	0	1	-7296	0.50	-6.78	4.35	0	1
-7295	0.33	-6.78	4.35	0	1	-7294	0.17	-6.78	4.35	0	1	-7293	0.00	-6.78	4.35	0	1
-7292	-0.16	-6.78	4.35	0	1	-7291	-0.33	-6.78	4.35	0	1	-7290	-0.50	-6.78	4.35	0	1
-7272	2.00	-6.96	4.34	0	1	-7271	1.83	-6.96	4.34	0	1	-7270	1.66	-6.96	4.34	0	1
-7269	1.50	-6.96	4.34	0	1	-7268	1.33	-6.96	4.34	0	1	-7267	1.17	-6.96	4.34	0	1
-7266	1.00	-6.96	4.34	0	1	-7265	0.88	-6.96	4.34	0	1	-7264	0.75	-6.96	4.34	0	1

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-7263	0.63	-6.96	4.34	0	1	-7262	0.50	-6.96	4.34	0	1	-7261	0.33	-6.96	4.34	0	1
-7260	0.17	-6.96	4.34	0	1	-7259	0.00	-6.96	4.34	0	1	-7258	-0.16	-6.96	4.34	0	1
-7257	-0.33	-6.96	4.34	0	1	-7256	-0.50	-6.96	4.34	0	1	-7209	2.00	-7.13	4.34	0	1
-7208	1.83	-7.13	4.34	0	1	-7207	1.66	-7.13	4.34	0	1	-7206	1.49	-7.13	4.34	0	1
-7205	1.33	-7.13	4.34	0	1	-7204	1.17	-7.13	4.34	0	1	-7203	1.00	-7.13	4.34	0	1
-7202	0.88	-7.13	4.34	0	1	-7201	0.75	-7.13	4.34	0	1	-7200	0.63	-7.13	4.34	0	1
-7199	0.50	-7.13	4.34	0	1	-7198	0.33	-7.13	4.34	0	1	-7197	0.17	-7.13	4.34	0	1
-7196	0.01	-7.13	4.34	0	1	-7195	-0.16	-7.13	4.34	0	1	-7194	-0.33	-7.13	4.34	0	1
-7193	-0.50	-7.13	4.34	0	1	-7157	1.26	-0.04	4.33	0	1	-7156	0.23	-0.04	4.33	0	1
-7148	1.48	-4.19	4.33	0	1	-7147	0.03	-4.19	4.33	0	1	-7146	2.00	-7.30	4.33	0	1
-7145	1.83	-7.30	4.33	0	1	-7144	1.67	-7.30	4.33	0	1	-7143	1.48	-7.30	4.33	0	1
-7142	1.33	-7.30	4.33	0	1	-7141	1.19	-7.30	4.33	0	1	-7140	1.00	-7.30	4.33	0	1
-7139	0.88	-7.30	4.33	0	1	-7138	0.75	-7.30	4.33	0	1	-7137	0.63	-7.30	4.33	0	1
-7136	0.50	-7.30	4.33	0	1	-7135	0.32	-7.30	4.33	0	1	-7134	0.17	-7.30	4.33	0	1
-7133	0.03	-7.30	4.33	0	1	-7132	-0.17	-7.30	4.33	0	1	-7131	-0.33	-7.30	4.33	0	1
-7130	-0.50	-7.30	4.33	0	1	-7092	1.10	-0.04	4.33	0	1	-7091	0.40	-0.04	4.33	0	1
-7066	2.00	-7.48	4.33	0	1	-7065	1.83	-7.48	4.33	0	1	-7064	1.66	-7.48	4.33	0	1
-7063	1.49	-7.48	4.33	0	1	-7062	1.33	-7.48	4.33	0	1	-7061	1.17	-7.48	4.33	0	1
-7060	1.00	-7.48	4.33	0	1	-7059	0.88	-7.48	4.33	0	1	-7058	0.75	-7.48	4.33	0	1
-7057	0.63	-7.48	4.33	0	1	-7056	0.50	-7.48	4.33	0	1	-7055	0.33	-7.48	4.33	0	1
-7054	0.17	-7.48	4.33	0	1	-7053	0.01	-7.48	4.33	0	1	-7052	-0.16	-7.48	4.33	0	1
-7051	-0.33	-7.48	4.33	0	1	-7050	-0.50	-7.48	4.33	0	1	-7022	1.19	-0.04	4.33	0	1
-7021	0.32	-0.04	4.33	0	1	-7009	1.64	-6.26	4.32	0	1	-7008	-0.14	-6.26	4.32	0	1
-7007	2.00	-7.65	4.32	0	1	-7006	1.83	-7.65	4.32	0	1	-7005	1.66	-7.65	4.32	0	1
-7004	1.50	-7.65	4.32	0	1	-7003	1.33	-7.65	4.32	0	1	-7002	1.17	-7.65	4.32	0	1
-7001	1.00	-7.65	4.32	0	1	-7000	0.88	-7.65	4.32	0	1	-6999	0.75	-7.65	4.32	0	1
-6998	0.63	-7.65	4.32	0	1	-6997	0.50	-7.65	4.32	0	1	-6996	0.33	-7.65	4.32	0	1
-6995	0.17	-7.65	4.32	0	1	-6994	0.00	-7.65	4.32	0	1	-6993	-0.16	-7.65	4.32	0	1
-6992	-0.33	-7.65	4.32	0	1	-6991	-0.50	-7.65	4.32	0	1	-6927	1.31	-2.12	4.32	0	1
-6926	0.18	-2.12	4.32	0	1	-6923	1.83	-7.82	4.32	0	1	-6922	1.66	-7.82	4.32	0	1
-6921	1.50	-7.82	4.32	0	1	-6920	1.33	-7.82	4.32	0	1	-6919	1.17	-7.82	4.32	0	1
-6918	1.00	-7.82	4.32	0	1	-6917	0.88	-7.82	4.32	0	1	-6916	0.75	-7.82	4.32	0	1
-6915	0.63	-7.82	4.32	0	1	-6914	0.50	-7.82	4.32	0	1	-6913	0.33	-7.82	4.32	0	1
-6912	0.17	-7.82	4.32	0	1	-6911	0.00	-7.82	4.32	0	1	-6910	-0.16	-7.82	4.32	0	1
-6909	-0.33	-7.82	4.32	0	1	-6901	2.00	-7.82	4.32	0	1	-6900	-0.50	-7.82	4.32	0	1
-6842	2.00	-7.99	4.31	0	1	-6841	1.83	-7.99	4.31	0	1	-6840	1.66	-7.99	4.31	0	1
-6839	1.50	-7.99	4.31	0	1	-6838	1.33	-7.99	4.31	0	1	-6837	1.17	-7.99	4.31	0	1
-6836	1.00	-7.99	4.31	0	1	-6835	0.88	-7.99	4.31	0	1	-6834	0.75	-7.99	4.31	0	1
-6833	0.63	-7.99	4.31	0	1	-6832	0.50	-7.99	4.31	0	1	-6831	0.33	-7.99	4.31	0	1
-6830	0.17	-7.99	4.31	0	1	-6829	0.00	-7.99	4.31	0	1	-6828	-0.16	-7.99	4.31	0	1
-6827	-0.33	-7.99	4.31	0	1	-6826	-0.50	-7.99	4.31	0	1	-6757	2.00	-8.17	4.31	0	1
-6756	1.83	-8.17	4.31	0	1	-6755	1.66	-8.17	4.31	0	1	-6754	1.49	-8.17	4.31	0	1
-6753	1.33	-8.17	4.31	0	1	-6752	1.17	-8.17	4.31	0	1	-6751	1.00	-8.17	4.31	0	1
-6750	0.88	-8.17	4.31	0	1	-6749	0.75	-8.17	4.31	0	1	-6748	0.63	-8.17	4.31	0	1
-6747	0.50	-8.17	4.31	0	1	-6746	0.33	-8.17	4.31	0	1	-6745	0.17	-8.17	4.31	0	1
-6744	0.01	-8.17	4.31	0	1	-6743	-0.16	-8.17	4.31	0	1	-6742	-0.33	-8.17	4.31	0	1
-6741	-0.50	-8.17	4.31	0	1	-6700	1.26	-1.08	4.31	0	1	-6699	0.23	-1.08	4.31	0	1
-6694	1.48	-5.23	4.31	0	1	-6693	2.00	-8.34	4.31	0	1	-6692	1.83	-8.34	4.31	0	1
-6691	1.67	-8.34	4.31	0	1	-6690	1.48	-8.34	4.31	0	1	-6689	0.63	-8.34	4.31	0	1
-6688	0.03	-8.34	4.31	0	1	-6687	-0.33	-8.34	4.31	0	1	-6678	1.33	-8.34	4.31	0	1
-6677	1.19	-8.34	4.31	0	1	-6674	0.03	-5.23	4.31	0	1	-6673	1.00	-8.34	4.31	0	1
-6672	0.88	-8.34	4.31	0	1	-6671	0.75	-8.34	4.31	0	1	-6670	0.50	-8.34	4.31	0	1
-6669	0.32	-8.34	4.31	0	1	-6668	0.17	-8.34	4.31	0	1	-6667	-0.17	-8.34	4.31	0	1
-6666	-0.50	-8.34	4.31	0	1	-6660	1.10	-1.08	4.30	0	1	-6659	0.40	-1.08	4.30	0	1
-6629	2.00	-8.51	4.30	0	1	-6628	1.83	-8.51	4.30	0	1	-6627	1.66	-8.51	4.30	0	1
-6626	1.49	-8.51	4.30	0	1	-6625	1.33	-8.51	4.30	0	1	-6624	1.17	-8.51	4.30	0	1
-6623	1.00	-8.51	4.30	0	1	-6622	0.88	-8.51	4.30	0	1	-6621	0.75	-8.51	4.30	0	1
-6620	0.63	-8.51	4.30	0	1	-6619	0.50	-8.51	4.30	0	1	-6618	0.33	-8.51	4.30	0	1
-6617	0.17	-8.51	4.30	0	1	-6616	0.01	-8.51	4.30	0	1	-6615	-0.16	-8.51	4.30	0	1
-6614	-0.33	-8.51	4.30	0	1	-6613	-0.50	-8.51	4.30	0	1	-6598	0.88	-0.39	4.30	0	1
-6597	0.63	-0.39	4.30	0	1	-6579	1.19	-1.08	4.30	0	1	-6578	0.32	-1.08	4.30	0	1
-6559	1.64	-7.30	4.30	0	1	-6558	-0.14	-7.30	4.30	0	1	-6556	2.00	-8.68	4.30	0	1
-6555	1.83	-8.68	4.30	0	1	-6554	1.66	-8.68	4.30	0	1	-6553	1.50	-8.68	4.30	0	1
-6552	1.33	-8.68	4.30	0	1	-6551	1.00	-8.68	4.30	0	1	-6550	0.88	-8.68	4.30	0	1
-6549	0.75	-8.68	4.30	0	1	-6548	0.63	-8.68	4.30	0	1	-6547	0.50	-8.68	4.30	0	1
-6546	0.17	-8.68	4.30	0	1	-6545	-0.16	-8.68	4.30	0	1	-6539	1.17	-8.68	4.30	0	1
-6538	0.33	-8.68	4.30	0	1	-6537	0.00	-8.68	4.30	0	1	-6536	-0.33	-8.68	4.30	0	1
-6535	-0.50	-8.68	4.30	0	1	-6505	0.88	-0.56	4.30	0	1	-6501	0.63	-0.56	4.30	0	1
-6496	0.88	-0.21	4.29	0	1	-6495	0.63	-0.21	4.29	0	1	-6494	1.31	-3.15	4.29	0	1
-6493	0.18	-3.15	4.29	0	1	-6492	2.00	-8.86	4.29	0	1	-6491	1.83	-8.86	4.29	0	1
-6490	1.66	-8.86	4.29	0	1	-6489	1.50	-8.86	4.29	0	1	-6488	1.33	-8.86	4.29	0	1
-6487	1.17	-8.86	4.29	0	1	-6486	1.00	-8.86	4.29	0	1	-6485	0.88	-8.86	4.29	0	1
-6484	0.75	-8.86	4.29	0	1	-6483	0.63	-8.86	4.29	0	1	-6482	0.50	-8.86	4.29	0	1
-6481	0.33	-8.86	4.29	0	1	-6480	0.17	-8.86	4.29	0	1	-6479	0.00	-8.86	4.29	0	1
-6478	-0.16	-8.86	4.29	0	1	-6477	-0.33	-8.86	4.29	0	1	-6476	-0.50	-8.86	4.29	0	1
-6438	0.88	-0.73	4.29	0	1	-6437	0.63	-0.73	4.29	0	1	-6382	0.88	-0.04	4.29	0	1
-6381	0.75	-0.04	4.29	0	1	-6380	0.63	-0.04	4.29	0	1	-6379	2.00	-9.03	4.29	0	1
-6378	1.83	-9.03	4.29	0	1	-6377	1.66	-9.03	4.29	0	1	-6376	1.50	-9.03	4.29	0	1
-6375	1.33	-9.03	4.29	0	1	-6374	1.17	-9.03	4.29	0	1	-6373	1.00	-9.03	4.29	0	1

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-2786	0.63	-9.02	3.89	0	1	-2779	1.19	-12.48	3.88	0	1	-2778	0.31	-12.48	3.88	0	1
-2771	0.88	-9.19	3.88	0	1	-2770	0.75	-9.19	3.88	0	1	-2769	0.63	-9.19	3.88	0	1
-2765	0.88	-9.37	3.88	0	1	-2764	0.75	-9.37	3.88	0	1	-2763	0.63	-9.37	3.88	0	1
-2759	0.88	-9.54	3.88	0	1	-2758	0.75	-9.54	3.88	0	1	-2757	0.63	-9.54	3.88	0	1
-2756	1.20	-10.40	3.88	0	1	-2755	0.30	-10.40	3.88	0	1	-2750	1.30	-3.14	3.87	0	1
-2749	0.20	-3.14	3.87	0	1	-2748	0.88	-9.71	3.87	0	1	-2747	0.75	-9.71	3.87	0	1
-2746	0.63	-9.71	3.87	0	1	-2741	0.88	-9.88	3.87	0	1	-2740	0.75	-9.88	3.87	0	1
-2739	0.63	-9.88	3.87	0	1	-2734	0.88	-10.06	3.86	0	1	-2733	0.75	-10.06	3.86	0	1
-2732	0.63	-10.06	3.86	0	1	-2722	0.88	-10.23	3.86	0	1	-2721	0.75	-10.23	3.86	0	1
-2720	0.63	-10.23	3.86	0	1	-2719	1.19	-13.51	3.86	0	1	-2718	0.31	-13.51	3.86	0	1
-2714	0.88	-10.40	3.85	0	1	-2713	0.75	-10.40	3.85	0	1	-2712	0.63	-10.40	3.85	0	1
-2711	0.88	-14.29	3.85	0	1	-2710	0.75	-14.29	3.85	0	1	-2709	0.63	-14.29	3.85	0	1
-2702	0.88	-10.57	3.85	0	1	-2701	0.75	-10.57	3.85	0	1	-2700	0.63	-10.57	3.85	0	1
-2699	1.20	-11.44	3.85	0	1	-2698	0.30	-11.44	3.85	0	1	-2697	0.20	-4.18	3.85	0	1
-2692	1.30	-4.18	3.85	0	1	-2691	0.88	-10.75	3.84	0	1	-2690	0.75	-10.75	3.84	0	1
-2689	0.63	-10.75	3.84	0	1	-2684	0.88	-10.92	3.84	0	1	-2683	0.75	-10.92	3.84	0	1
-2682	0.63	-10.92	3.84	0	1	-2677	0.88	-11.09	3.84	0	1	-2676	0.75	-11.09	3.84	0	1
-2675	0.63	-11.09	3.84	0	1	-2671	0.88	-14.10	3.83	0	1	-2670	0.75	-14.10	3.83	0	1
-2669	0.63	-14.10	3.83	0	1	-2661	0.88	-11.27	3.83	0	1	-2660	0.75	-11.27	3.83	0	1
-2659	0.63	-11.27	3.83	0	1	-2654	0.88	-11.44	3.83	0	1	-2653	0.75	-11.44	3.83	0	1
-2652	0.63	-11.44	3.83	0	1	-2647	0.88	-11.61	3.82	0	1	-2646	0.75	-11.61	3.82	0	1
-2645	0.63	-11.61	3.82	0	1	-2644	1.20	-12.48	3.82	0	1	-2643	0.30	-12.48	3.82	0	1
-2639	1.30	-5.21	3.82	0	1	-2638	0.20	-5.21	3.82	0	1	-2637	0.88	-11.78	3.82	0	1
-2636	0.75	-11.78	3.82	0	1	-2635	0.63	-11.78	3.82	0	1	-2627	0.88	-11.96	3.81	0	1
-2626	0.75	-11.96	3.81	0	1	-2625	0.63	-11.96	3.81	0	1	-2624	0.88	-13.90	3.81	0	1
-2623	0.75	-13.90	3.81	0	1	-2622	0.63	-13.90	3.81	0	1	-2618	0.88	-12.13	3.81	0	1
-2617	0.75	-12.13	3.81	0	1	-2616	0.63	-12.13	3.81	0	1	-2608	0.88	-12.30	3.80	0	1
-2607	0.75	-12.30	3.80	0	1	-2606	0.63	-12.30	3.80	0	1	-2598	0.88	-12.47	3.80	0	1
-2597	0.75	-12.47	3.80	0	1	-2596	0.63	-12.47	3.80	0	1	-2595	0.88	-12.65	3.80	0	1
-2594	0.75	-12.65	3.80	0	1	-2593	0.63	-12.65	3.80	0	1	-2592	1.20	-13.51	3.80	0	1
-2591	0.30	-13.51	3.80	0	1	-2589	1.30	-6.25	3.79	0	1	-2588	0.20	-6.25	3.79	0	1
-2587	0.88	-13.71	3.79	0	1	-2586	0.75	-13.71	3.79	0	1	-2585	0.63	-13.71	3.79	0	1
-2584	0.88	-12.82	3.79	0	1	-2583	0.75	-12.82	3.79	0	1	-2582	0.63	-12.82	3.79	0	1
-2581	0.88	-12.99	3.79	0	1	-2580	0.75	-12.99	3.79	0	1	-2579	0.63	-12.99	3.79	0	1
-2577	0.88	-13.17	3.78	0	1	-2576	0.75	-13.17	3.78	0	1	-2575	0.63	-13.17	3.78	0	1
-2574	0.88	-13.34	3.78	0	1	-2573	0.75	-13.34	3.78	0	1	-2572	0.63	-13.34	3.78	0	1
-2567	0.88	-13.51	3.77	0	1	-2566	0.75	-13.51	3.77	0	1	-2565	0.63	-13.51	3.77	0	1
-2563	1.30	-7.29	3.77	0	1	-2562	0.20	-7.29	3.77	0	1	-2555	1.30	-8.32	3.74	0	1
-2554	0.20	-8.32	3.74	0	1	-2546	1.24	-13.51	3.71	0	1	-2545	0.26	-13.51	3.71	0	1
-2543	1.30	-9.36	3.71	0	1	-2542	0.20	-9.36	3.71	0	1	-2541	0.09	-1.06	3.71	0	1
-2539	1.41	-1.06	3.71	0	1	-2521	1.30	-10.40	3.69	0	1	-2520	0.20	-10.40	3.69	0	1
-2498	1.28	-12.47	3.67	0	1	-2497	0.22	-12.47	3.67	0	1	-2496	1.30	-11.43	3.66	0	1
-2495	0.20	-11.43	3.66	0	1	-2487	1.46	-2.10	3.60	0	1	-2486	0.04	-2.10	3.60	0	1
-2478	1.32	-13.51	3.56	0	1	-2477	0.17	-13.51	3.55	0	1	-2464	1.50	-3.13	3.50	0	1
-2463	0.00	-3.13	3.49	0	1	-2442	0.09	-11.43	3.45	0	1	-2441	1.41	-11.43	3.44	0	1
-2438	1.52	-4.17	3.43	0	1	-2437	-0.02	-4.17	3.43	0	1	-2427	1.46	-10.39	3.39	0	1
-2426	0.04	-10.39	3.39	0	1	-2409	1.54	-5.20	3.36	0	1	-2408	-0.04	-5.20	3.36	0	1
-2405	1.50	-9.35	3.34	0	1	-2363	-0.00	-9.35	3.33	0	1	-2361	1.52	-8.31	3.32	0	1
-2360	-0.02	-8.31	3.32	0	1	-2357	1.54	-7.28	3.30	0	1	-2356	-0.04	-7.28	3.30	0	1
-2352	1.56	-6.24	3.30	0	1	-2351	-0.06	-6.24	3.30	0	1	1519	0.13	-12.46	3.33	0	8
1520	1.37	-12.46	3.33	0	9	1901	0.13	-12.47	3.50	0	1	1902	1.37	-12.47	3.50	0	1
2110	0.13	-0.02	3.67	0	10	2111	1.37	-0.02	3.67	0	11	2401	0.13	-0.03	3.82	0	1
2402	1.37	-0.03	3.82	0	1	2901	0.50	-12.49	4.20	0	1	2902	1.00	-12.49	4.20	0	1
3301	0.50	-0.05	4.52	0	1	3302	1.00	-0.05	4.52	0	1						

Elenco materiali

Simbologia

Mat. = Numero del materiale

Comm. = Commento

P = Peso specifico

E = Modulo elastico

G = Modulo elastico tangenziale

v = Coeff. di Poisson

α = Coeff. di dilatazione termica

Mat.	Comm.	P <daN/mc>	E <daN/cm²>	G <daN/cm²>	v	α
5	Calcestruzzo classe C25/30	2500	314472.00	142942.00	0.1	1.000000E-05
6	Calcestruzzo classe C28/35	2500	325881.00	148128.00	0.1	1.000000E-05
18	Acciaio	7850	2100000.00	800000.00	0.3	1.200000E-05
22	Calcestruzzo pila 1-4 (fuori alveo)	2500	269950.00	122700.00	0.1	1.000000E-05
23	Calcestruzzo pila 2 (in alveo lato via Ciari)	2500	312750.00	142160.00	0.1	1.000000E-05
24	Calcestruzzo pila 3 (in alveo lato via Trento)	2500	324490.00	147500.00	0.1	1.000000E-05
25	Calcestruzzo rampa via Ciari	2500	311900.00	141770.00	0.1	1.000000E-05
26	Calcestruzzo rampa via Trento	2500	281580.00	127990.00	0.1	1.000000E-05
27	Calcestruzzo travi impalcato	2500	324140.00	147340.00	0.1	1.000000E-05

Elenco sezioni aste

Simbologia

Sez. = Numero della sezione
 Comm. = Commento
 Tipo = Tipologia
 2C = Doppia C lato labbri
 2Cdx = Doppia C lato costola
 2I = Doppia I
 2L = Doppia L lato labbri
 2Ldx = Doppia L lato costole
 C = Sezione a C
 Cdx = C destra
 Cir. = Circolare
 Cir.c = Circolare cava
 I = Sezione a I
 L = Sezione a L
 Ldx = L destra
 Om. = Omega
 Pg = Pi greco
 Pr = Poligono regolare
 Prc = Poligono regolare cavo
 Pc = Per coordinate
 Ia = Inerzie assegnate
 R = Rettangolare
 Rc = Rettangolare cava
 T = Sezione a T
 U = Sezione a U
 Ur = U rovescia
 V = Sezione a V
 Vr = V rovescia
 Z = Sezione a Z
 Zdx = Z destra
 Ts = T stondata
 Ls = L stondata
 Cs = C stondata
 Is = I stondata
 Dis. = Disegnata
 Mem. = Membratura
 G = Generica
 T = Trave
 P = Pilastro
 Ver. = Verifica prevista
 N = Nessuna
 C = Cemento armato
 A = Acciaio
 L = Legno
 B = Base
 H = Altezza
 s = Spessore ala
 r = Raggio raccordo anima-ala
 rl = Raggio in testa ala
 D = Distanza
 R = Raggio
 Ma = Numero del materiale
 C = Numero del criterio di progetto
 Crit. C.I. = Criterio di progetto collegamento iniziale
 Crit. C.F. = Criterio di progetto collegamento finale

Sez.	Comm.	Tipo	Mem.	Ver.	B <cm>	H <cm>	s <cm>	r <cm>	s <cm>	rl <cm>	D <cm>	R <cm>	Ma	Crit. C.I.	Crit. C.F.
31	Tubo circolare d=114.3x6 mm - S355	Cir.c	T	A					0.60			5.71	183	6	6
32	Tubo 60x80x5 mm - S355	Rc	T	A	6.00	8.00			0.50				183	6	6
33	Tubo 60x100x5 mm - S355	Rc	T	A	6.00	10.00			0.50				183	6	6
34	Tubo 80x120x5 mm - S355	Rc	T	A	8.00	12.00			0.50				183	6	6
35	2 L80x60x8 - dist 6 mm - S275	2Ldx	T	A	8.00	6.00	0.80	1.10		0.45	0.60		181	6	6
36	Nervatura 50x6 mm - S275	Ts	T	A	5.00	5.00	0.60	0.10		0.00		0.10	181	6	6
37	2 L80x60x8 - dist 6 mm - S275	2Ldx	T	A	8.00	6.00	0.80	1.10		0.45	0.60		181	6	6
38	Tubo 80x80x4 mm - S235	Rc	T	A	8.00	8.00			0.40				182	6	6
39	Tubo circolare d=70x4 mm - S355	Cir.c	T	A					0.40			3.50	183	6	6
47	2 L80x60x8 - dist 6 mm - S275	2Ldx	T	A	8.00	6.00	0.80	1.10		0.45	0.60		181	6	6
48	Tubo circolare d=101.6x6 mm - S355	Cir.c	T	A					0.60			5.08	183	6	6
50	Tubo circolare d=90x4 mm - S355	Cir.c	T	A					0.40			4.50	183	6	6
52	T 80x80x6 mm - S275	Ts	T	A	8.00	8.00	0.60	0.10		0.00		0.10	181	6	6
53	Tubo 60x60x4 mm - S235	Rc	T	A	6.00	6.00			0.40				182	6	6
54	L80x8 mm - S275	Ls	T	A	8.00	8.00	0.80	1.00		0.50			181	6	6
58	Appoggio travi - 200x200	R	P	A	20.00	20.00							181	6	6
61	Tubo 60x120x4 mm - S235	Rc	T	A	6.00	12.00			0.40				182	6	6
68	Tubo 80x100x(2x5+6) mm - S355 (32)	Rc	T	A	8.00	10.00			0.80				183	6	6

Elenco vincoli aste

Simbologia

Va = Numero del vincolo asta
 Comm. = Commento
 Tipo = Tipologia
 SVI = Definizione di vincolamenti interni

ELA = Vincolo su suolo elastico alla Winkler
 BIE-RTC = Biella resistente a trazione e a compressione
 BIE-RC = Biella resistente solo a compressione
 BIE-RT = Biella resistente solo a trazione
 Ni = Sforzo normale nodo iniziale (0=sbloccato, 1=bloccato)
 Tyi = Taglio in dir. Y locale nodo iniziale (0=sbloccato, 1=bloccato)
 Tzi = Taglio in dir. Z locale nodo iniziale (0=sbloccato, 1=bloccato)
 Mxi = Momento intorno all'asse X locale nodo iniziale (0=sbloccato, 1=bloccato)
 Myi = Momento intorno all'asse Y locale nodo iniziale (0=sbloccato, 1=bloccato)
 Mzi = Momento intorno all'asse Z locale nodo iniziale (0=sbloccato, 1=bloccato)
 Nf = Sforzo normale nodo finale (0=sbloccato, 1=bloccato)
 Tyf = Taglio in dir. Y locale nodo finale (0=sbloccato, 1=bloccato)
 Tzf = Taglio in dir. Z locale nodo finale (0=sbloccato, 1=bloccato)
 Mxf = Momento intorno all'asse X locale nodo finale (0=sbloccato, 1=bloccato)
 Myf = Momento intorno all'asse Y locale nodo finale (0=sbloccato, 1=bloccato)
 Mzf = Momento intorno all'asse Z locale nodo finale (0=sbloccato, 1=bloccato)
 Kt = Coeff. di sottofondo su suolo elastico alla Winkler

Va	Comm.	Tipo	Ni	Tyi	Tzi	Mxi	Myi	Mzi	Nf	Tyf	Tzf	Mxf	Myf	Mzf	Kt
															<daN/cmc>
1	Inc+Inc	SVI	1	1	1	1	1	1	1	1	1	1	1	1	1
11	Inc+CerYZ	SVI	1	1	1	1	1	1	1	1	1	1	0	0	
13	CerYZ+CerYZ	SVI	1	1	1	1	0	0	1	1	1	1	0	0	

Elenco aste

Simbologia

Asta = Numero dell'asta
 N1 = Nodo iniziale
 N2 = Nodo finale
 Sez. = Numero della sezione
 Va = Numero del vincolo asta
 Par. = Numero dei parametri aggiuntivi
 Rot. = Rotazione
 FF = Filo fisso
 Dy1 = Scost. filo fisso Y1
 Dy2 = Scost. filo fisso Y2
 Dz1 = Scost. filo fisso Z1
 Dz2 = Scost. filo fisso Z2
 Kt = Coeff. di sottofondo su suolo elastico alla Winkler

Asta	N1	N2	Sez.	Va	Par.	Rot.	FF	Dy1	Dy2	Dz1	Dz2	Kt
						<grad>		<cm>	<cm>	<cm>	<cm>	<daN/cmc>
0	-2591	-2867		1		0.00	55	0.00	0.00	0.00	0.00	
0	-2867	-2912		1		0.00	55	0.00	0.00	0.00	0.00	
0	-2912	-2913		1		0.00	55	0.00	0.00	0.00	0.00	
0	-2913	-2868		1		0.00	55	0.00	0.00	0.00	0.00	
0	-4749	-4690		1		0.00	22	0.00	0.00	0.00	0.00	
0	-4806	-4749		1		0.00	22	0.00	0.00	0.00	0.00	
0	-2868	-2592		1		0.00	55	0.00	0.00	0.00	0.00	
0	-4861	-4806		1		0.00	22	0.00	0.00	0.00	0.00	
0	-4927	-4861		1		0.00	22	0.00	0.00	0.00	0.00	
0	-2643	-2950		1		0.00	55	0.00	0.00	0.00	0.00	
0	-4993	-4927		1		0.00	22	0.00	0.00	0.00	0.00	
0	-2950	-3008		1		0.00	55	0.00	0.00	0.00	0.00	
0	-3008	-3009		1		0.00	55	0.00	0.00	0.00	0.00	
0	-3009	-2951		1		0.00	55	0.00	0.00	0.00	0.00	
0	-5044	-4993		1		0.00	22	0.00	0.00	0.00	0.00	
0	-5121	-5044		1		0.00	22	0.00	0.00	0.00	0.00	
0	-5206	-5121		1		0.00	22	0.00	0.00	0.00	0.00	
0	-2951	-2644		1		0.00	55	0.00	0.00	0.00	0.00	
0	-5271	-5206		1		0.00	22	0.00	0.00	0.00	0.00	
0	-5322	-5271		1		0.00	22	0.00	0.00	0.00	0.00	
0	-2698	-3038		1		0.00	55	0.00	0.00	0.00	0.00	
0	-5376	-5322		1		0.00	22	0.00	0.00	0.00	0.00	
0	-3038	-3136		1		0.00	55	0.00	0.00	0.00	0.00	
0	-3136	-3137		1		0.00	55	0.00	0.00	0.00	0.00	
0	-3137	-3039		1		0.00	55	0.00	0.00	0.00	0.00	
0	-5438	-5376		1		0.00	22	0.00	0.00	0.00	0.00	
0	-5501	-5438		1		0.00	22	0.00	0.00	0.00	0.00	
0	-5596	-5501		1		0.00	22	0.00	0.00	0.00	0.00	
0	-3039	-2699		1		0.00	55	0.00	0.00	0.00	0.00	
0	-5665	-5596		1		0.00	22	0.00	0.00	0.00	0.00	
0	-5732	-5665		1		0.00	22	0.00	0.00	0.00	0.00	
0	-2755	-3162		1		0.00	55	0.00	0.00	0.00	0.00	
0	-5797	-5732		1		0.00	22	0.00	0.00	0.00	0.00	
0	-3162	-3251		1		0.00	55	0.00	0.00	0.00	0.00	
0	-3251	-3252		1		0.00	55	0.00	0.00	0.00	0.00	
0	-3252	-3163		1		0.00	55	0.00	0.00	0.00	0.00	
0	-5843	-5797		1		0.00	22	0.00	0.00	0.00	0.00	

0	-5885	-5843	1	0.00	22	0.00	0.00	0.00	0.00
0	-5994	-5885	1	0.00	22	0.00	0.00	0.00	0.00
0	-3163	-2756	1	0.00	55	0.00	0.00	0.00	0.00
0	-6067	-5994	1	0.00	22	0.00	0.00	0.00	0.00
0	-6135	-6067	1	0.00	22	0.00	0.00	0.00	0.00
0	-2811	-3279	1	0.00	55	0.00	0.00	0.00	0.00
0	-6192	-6135	1	0.00	22	0.00	0.00	0.00	0.00
0	-3279	-3378	1	0.00	55	0.00	0.00	0.00	0.00
0	-3378	-3379	1	0.00	55	0.00	0.00	0.00	0.00
0	-3379	-3280	1	0.00	55	0.00	0.00	0.00	0.00
0	-6245	-6192	1	0.00	22	0.00	0.00	0.00	0.00
0	-6303	-6245	1	0.00	22	0.00	0.00	0.00	0.00
0	-6371	-6303	1	0.00	22	0.00	0.00	0.00	0.00
0	-3280	-2812	1	0.00	55	0.00	0.00	0.00	0.00
0	-6484	-6371	1	0.00	22	0.00	0.00	0.00	0.00
0	-6549	-6484	1	0.00	22	0.00	0.00	0.00	0.00
0	-2879	-3405	1	0.00	55	0.00	0.00	0.00	0.00
0	-6621	-6549	1	0.00	22	0.00	0.00	0.00	0.00
0	-3405	-3536	1	0.00	55	0.00	0.00	0.00	0.00
0	-3536	-3537	1	0.00	55	0.00	0.00	0.00	0.00
0	-3537	-3406	1	0.00	55	0.00	0.00	0.00	0.00
0	-6671	-6621	1	0.00	22	0.00	0.00	0.00	0.00
0	-6749	-6671	1	0.00	22	0.00	0.00	0.00	0.00
0	-6834	-6749	1	0.00	22	0.00	0.00	0.00	0.00
0	-3406	-2880	1	0.00	55	0.00	0.00	0.00	0.00
0	-6916	-6834	1	0.00	22	0.00	0.00	0.00	0.00
0	-6999	-6916	1	0.00	22	0.00	0.00	0.00	0.00
0	-2965	-3607	1	0.00	55	0.00	0.00	0.00	0.00
0	-7058	-6999	1	0.00	22	0.00	0.00	0.00	0.00
0	-3607	-3825	1	0.00	55	0.00	0.00	0.00	0.00
0	-3825	-3826	1	0.00	55	0.00	0.00	0.00	0.00
0	-3826	-3608	1	0.00	55	0.00	0.00	0.00	0.00
0	-7138	-7058	1	0.00	22	0.00	0.00	0.00	0.00
0	-7201	-7138	1	0.00	22	0.00	0.00	0.00	0.00
0	-7264	-7201	1	0.00	22	0.00	0.00	0.00	0.00
0	-3608	-2966	1	0.00	55	0.00	0.00	0.00	0.00
0	-7298	-7264	1	0.00	22	0.00	0.00	0.00	0.00
0	-7348	-7298	1	0.00	22	0.00	0.00	0.00	0.00
0	-3064	-3906	1	0.00	55	0.00	0.00	0.00	0.00
0	-7464	-7348	1	0.00	22	0.00	0.00	0.00	0.00
0	-3906	-4104	1	0.00	55	0.00	0.00	0.00	0.00
0	-4104	-4105	1	0.00	55	0.00	0.00	0.00	0.00
0	-4105	-3907	1	0.00	55	0.00	0.00	0.00	0.00
0	-7500	-7464	1	0.00	22	0.00	0.00	0.00	0.00
0	-7572	-7500	1	0.00	22	0.00	0.00	0.00	0.00
0	-7662	-7572	1	0.00	22	0.00	0.00	0.00	0.00
0	-3907	-3065	1	0.00	55	0.00	0.00	0.00	0.00
0	-7711	-7662	1	0.00	22	0.00	0.00	0.00	0.00
0	-7806	-7711	1	0.00	22	0.00	0.00	0.00	0.00
0	-3193	-4169	1	0.00	55	0.00	0.00	0.00	0.00
0	-7929	-7806	1	0.00	22	0.00	0.00	0.00	0.00
0	-4169	-4362	1	0.00	55	0.00	0.00	0.00	0.00
0	-4362	-4363	1	0.00	55	0.00	0.00	0.00	0.00
0	-4363	-4170	1	0.00	55	0.00	0.00	0.00	0.00
0	-7975	-7929	1	0.00	22	0.00	0.00	0.00	0.00
0	-8029	-7975	1	0.00	22	0.00	0.00	0.00	0.00
0	-8155	-8029	1	0.00	22	0.00	0.00	0.00	0.00
0	-4170	-3189	1	0.00	55	0.00	0.00	0.00	0.00
0	-8229	-8155	1	0.00	22	0.00	0.00	0.00	0.00
0	-8317	-8229	1	0.00	22	0.00	0.00	0.00	0.00
0	-3309	-4421	1	0.00	55	0.00	0.00	0.00	0.00
0	-8378	-8317	1	0.00	22	0.00	0.00	0.00	0.00
0	-4421	-4815	1	0.00	55	0.00	0.00	0.00	0.00
0	-4815	-4816	1	0.00	55	0.00	0.00	0.00	0.00
0	-4816	-4422	1	0.00	55	0.00	0.00	0.00	0.00
0	-8425	-8378	1	0.00	22	0.00	0.00	0.00	0.00
0	-8480	-8425	1	0.00	22	0.00	0.00	0.00	0.00
0	-8538	-8480	1	0.00	22	0.00	0.00	0.00	0.00
0	-4422	-3317	1	0.00	55	0.00	0.00	0.00	0.00
0	-8621	-8538	1	0.00	22	0.00	0.00	0.00	0.00
0	-8720	-8621	1	0.00	22	0.00	0.00	0.00	0.00
0	-3440	-4888	1	0.00	55	0.00	0.00	0.00	0.00
0	-8825	-8720	1	0.00	22	0.00	0.00	0.00	0.00
0	-4888	-5215	1	0.00	55	0.00	0.00	0.00	0.00
0	-5215	-5216	1	0.00	55	0.00	0.00	0.00	0.00
0	-5216	-4897	1	0.00	55	0.00	0.00	0.00	0.00
0	-8909	-8825	1	0.00	22	0.00	0.00	0.00	0.00
0	-8983	-8909	1	0.00	22	0.00	0.00	0.00	0.00
0	-9095	-8983	1	0.00	22	0.00	0.00	0.00	0.00

0	-4897	-3441		1		0.00	55	0.00	0.00	0.00	0.00	0.00
0	-9150	-9095		1		0.00	22	0.00	0.00	0.00	0.00	0.00
0	-9208	-9150		1		0.00	22	0.00	0.00	0.00	0.00	0.00
0	-3674	-5306		1		0.00	55	0.00	0.00	0.00	0.00	0.00
0	-9284	-9208		1		0.00	22	0.00	0.00	0.00	0.00	0.00
0	-5306	-5605		1		0.00	55	0.00	0.00	0.00	0.00	0.00
0	-5605	-5606		1		0.00	55	0.00	0.00	0.00	0.00	0.00
0	-5606	-5307		1		0.00	55	0.00	0.00	0.00	0.00	0.00
0	-9375	-9284		1		0.00	22	0.00	0.00	0.00	0.00	0.00
0	-9441	-9375		1		0.00	22	0.00	0.00	0.00	0.00	0.00
0	-9485	-9441		1		0.00	22	0.00	0.00	0.00	0.00	0.00
0	-5307	-3675		1		0.00	55	0.00	0.00	0.00	0.00	0.00
0	-9551	-9485		1		0.00	22	0.00	0.00	0.00	0.00	0.00
0	-9599	-9551		1		0.00	22	0.00	0.00	0.00	0.00	0.00
0	-3956	-5691		1		0.00	55	0.00	0.00	0.00	0.00	0.00
0	-9641	-9599		1		0.00	22	0.00	0.00	0.00	0.00	0.00
0	-5691	-6001		1		0.00	55	0.00	0.00	0.00	0.00	0.00
0	-6001	-6002		1		0.00	55	0.00	0.00	0.00	0.00	0.00
0	-6002	-5692		1		0.00	55	0.00	0.00	0.00	0.00	0.00
0	-9728	-9641		1		0.00	22	0.00	0.00	0.00	0.00	0.00
0	-9856	-9728		1		0.00	22	0.00	0.00	0.00	0.00	0.00
0	-9969	-9856		1		0.00	22	0.00	0.00	0.00	0.00	0.00
0	-5692	-3969		1		0.00	55	0.00	0.00	0.00	0.00	0.00
0	-10035	-9969		1		0.00	22	0.00	0.00	0.00	0.00	0.00
0	-10127	-10035		1		0.00	22	0.00	0.00	0.00	0.00	0.00
0	-4235	-5256		1		0.00	55	0.00	0.00	0.00	0.00	0.00
0	-5256	-6106		1		0.00	55	0.00	0.00	0.00	0.00	0.00
0	-10195	-10127		1		0.00	22	0.00	0.00	0.00	0.00	0.00
0	-6106	-6380		1		0.00	55	0.00	0.00	0.00	0.00	0.00
0	-6380	-6381		1		0.00	55	0.00	0.00	0.00	0.00	0.00
0	-6381	-6382		1		0.00	55	0.00	0.00	0.00	0.00	0.00
0	-6382	-6107		1		0.00	55	0.00	0.00	0.00	0.00	0.00
0	-6107	-5257		1		0.00	55	0.00	0.00	0.00	0.00	0.00
0	-10250	-10195		1		0.00	22	0.00	0.00	0.00	0.00	0.00
0	-5257	-4236		1		0.00	55	0.00	0.00	0.00	0.00	0.00
2003	1902	-4691	39	13		0.00	55	0.00	0.00	0.00	0.00	0.00
2004	1901	-4689	39	13		0.00	55	0.00	0.00	0.00	0.00	0.00
2021	1520	1902	58	11		0.00	22	0.00	0.00	0.00	0.00	0.00
2024	1902	-5439	50	13		0.00	55	0.00	0.00	0.00	0.00	0.00
2025	1901	-5437	50	13		0.00	55	0.00	0.00	0.00	0.00	0.00
2040	1901	-5842	50	13		0.00	55	0.00	0.00	0.00	0.00	0.00
2041	1902	-5844	50	13		0.00	55	0.00	0.00	0.00	0.00	0.00
2066	-2477	1901	48	1		0.00	22	0.00	0.00	0.00	0.00	0.00
2066	1901	-2442	48	1		0.00	22	0.00	0.00	0.00	0.00	0.00
2066	-2442	-2426	48	1		0.00	22	0.00	0.00	0.00	0.00	0.00
2066	-2426	-2363	48	1		0.00	22	0.00	0.00	0.00	0.00	0.00
2066	-2363	-2360	31	1		0.00	22	0.00	0.00	0.00	0.00	0.00
2066	-2360	-2356	31	1		0.00	22	0.00	0.00	0.00	0.00	0.00
2066	-2356	-2351	31	1		0.00	22	0.00	0.00	0.00	0.00	0.00
2455	2111	2402	58	11		180.00	77	0.00	0.00	0.00	0.00	0.00
2470	2110	2401	58	11		180.00	99	0.00	0.00	0.00	0.00	0.00
2535	2401	-9374	50	13		0.00	55	0.00	0.00	0.00	0.00	0.00
2536	2402	-9376	50	13		0.00	55	0.00	0.00	0.00	0.00	0.00
2541	2401	-9727	50	13		0.00	55	0.00	0.00	0.00	0.00	0.00
2542	2402	-9740	50	13		0.00	55	0.00	0.00	0.00	0.00	0.00
2590	-2351	-2408	31	1		0.00	22	0.00	0.00	0.00	0.00	0.00
2590	-2408	-2437	31	1		0.00	22	0.00	0.00	0.00	0.00	0.00
2590	-2437	-2463	31	1		0.00	22	0.00	0.00	0.00	0.00	0.00
2590	-2463	-2486	48	1		0.00	22	0.00	0.00	0.00	0.00	0.00
2590	-2486	-2541	48	1		0.00	22	0.00	0.00	0.00	0.00	0.00
2590	-2541	2401	48	1		0.00	22	0.00	0.00	0.00	0.00	0.00
2597	-2352	-2409	31	1		0.00	22	0.00	0.00	0.00	0.00	0.00
2597	-2409	-2438	31	1		0.00	22	0.00	0.00	0.00	0.00	0.00
2597	-2438	-2464	31	1		0.00	22	0.00	0.00	0.00	0.00	0.00
2597	-2464	-2487	48	1		0.00	22	0.00	0.00	0.00	0.00	0.00
2597	-2487	-2539	48	1		0.00	22	0.00	0.00	0.00	0.00	0.00
2597	-2539	2402	48	1		0.00	22	0.00	0.00	0.00	0.00	0.00
2703	-5038	-5037	47	1		180.00	88	0.00	0.00	0.00	0.00	0.00
2703	-5039	-5038	37	1		180.00	88	0.00	0.00	0.00	0.00	0.00
2703	-5040	-5039	37	1		180.00	88	0.00	0.00	0.00	0.00	0.00
2703	-5041	-5040	37	1		180.00	88	0.00	0.00	0.00	0.00	0.00
2703	-5042	-5041	35	1		180.00	88	0.00	0.00	0.00	0.00	0.00
2703	2901	-5042	35	1		180.00	88	0.00	0.00	0.00	0.00	0.00
2703	-5043	2901	35	1		180.00	88	0.00	0.00	0.00	0.00	0.00
2703	-5044	-5043	35	1		180.00	88	0.00	0.00	0.00	0.00	0.00
2703	-5045	-5044	35	1		180.00	88	0.00	0.00	0.00	0.00	0.00
2703	2902	-5045	35	1		180.00	88	0.00	0.00	0.00	0.00	0.00
2703	-5046	2902	35	1		180.00	88	0.00	0.00	0.00	0.00	0.00
2703	-5047	-5046	35	1		180.00	88	0.00	0.00	0.00	0.00	0.00

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2703	-5048	-5047	37	1		180.00	88	0.00	0.00	0.00	0.00
2703	-5049	-5048	37	1		180.00	88	0.00	0.00	0.00	0.00
2703	-5050	-5049	37	1		180.00	88	0.00	0.00	0.00	0.00
2703	-5051	-5050	47	1		180.00	88	0.00	0.00	0.00	0.00
2819	1901	-2497	68	1		0.00	55	0.00	0.00	0.00	0.00
2819	-2497	-2643	68	1		0.00	55	0.00	0.00	0.00	0.00
2819	-2643	-3198	34	1		0.00	55	0.00	0.00	0.00	0.00
2819	-3198	2901	34	1		0.00	55	0.00	0.00	0.00	0.00
2819	-2478	1902	48	1		0.00	22	0.00	0.00	0.00	0.00
2819	1902	-2441	48	1		0.00	22	0.00	0.00	0.00	0.00
2819	-2441	-2427	48	1		0.00	22	0.00	0.00	0.00	0.00
2819	-2427	-2405	48	1		0.00	22	0.00	0.00	0.00	0.00
2819	-2405	-2361	31	1		0.00	22	0.00	0.00	0.00	0.00
2819	-2361	-2357	31	1		0.00	22	0.00	0.00	0.00	0.00
2819	-2357	-2352	31	1		0.00	22	0.00	0.00	0.00	0.00
2820	1902	-2498	68	1		0.00	55	0.00	0.00	0.00	0.00
2820	-2498	-2644	68	1		0.00	55	0.00	0.00	0.00	0.00
2820	-2644	-3199	34	1		0.00	55	0.00	0.00	0.00	0.00
2820	-3199	2902	34	1		0.00	55	0.00	0.00	0.00	0.00
2864	1519	1901	58	11		0.00	22	0.00	0.00	0.00	0.00
3116	-10244	-10243	47	1		180.00	99	0.00	0.00	0.00	0.00
3116	-10245	-10244	37	1		180.00	99	0.00	0.00	0.00	0.00
3116	-10246	-10245	37	1		180.00	99	0.00	0.00	0.00	0.00
3116	-10247	-10246	37	1		180.00	99	0.00	0.00	0.00	0.00
3116	-10248	-10247	35	1		180.00	99	0.00	0.00	0.00	0.00
3116	3301	-10248	35	1		180.00	99	0.00	0.00	0.00	0.00
3116	-10249	3301	35	1		180.00	99	0.00	0.00	0.00	0.00
3116	-10250	-10249	35	1		180.00	99	0.00	0.00	0.00	0.00
3116	-10251	-10250	35	1		180.00	99	0.00	0.00	0.00	0.00
3116	3302	-10251	35	1		180.00	99	0.00	0.00	0.00	0.00
3116	-10252	3302	35	1		180.00	99	0.00	0.00	0.00	0.00
3116	-10253	-10252	35	1		180.00	99	0.00	0.00	0.00	0.00
3116	-10254	-10253	37	1		180.00	99	0.00	0.00	0.00	0.00
3116	-10255	-10254	37	1		180.00	99	0.00	0.00	0.00	0.00
3116	-10256	-10255	37	1		180.00	99	0.00	0.00	0.00	0.00
3116	-10257	-10256	47	1		180.00	99	0.00	0.00	0.00	0.00
3457	2401	-3082	68	1		0.00	55	0.00	0.00	0.00	0.00
3457	-3082	-3442	68	1		0.00	55	0.00	0.00	0.00	0.00
3457	-3442	-4235	68	1		0.00	55	0.00	0.00	0.00	0.00
3457	-4235	-7091	34	1		0.00	55	0.00	0.00	0.00	0.00
3457	-7091	3301	34	1		0.00	55	0.00	0.00	0.00	0.00
3458	2402	-3090	68	1		0.00	55	0.00	0.00	0.00	0.00
3458	-3090	-3448	68	1		0.00	55	0.00	0.00	0.00	0.00
3458	-3448	-4236	68	1		0.00	55	0.00	0.00	0.00	0.00
3458	-4236	-7092	34	1		0.00	55	0.00	0.00	0.00	0.00
3458	-7092	3302	34	1		0.00	55	0.00	0.00	0.00	0.00
3499	-4688	-4747	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-4747	-4804	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-4804	-4859	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-4859	-4925	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-4925	-4977	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-4977	2901	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	2901	-5119	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-5119	-5204	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-5204	-5269	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-5269	-5320	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-5320	-5374	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-5374	-5436	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-5436	-5499	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-5499	-5594	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-5594	-5663	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-5663	-5731	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-5731	-5795	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-5795	-5841	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-5841	-5883	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-5883	-5992	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-5992	-6065	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-6065	-6133	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-6133	-6190	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-6190	-6244	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-6244	-6301	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-6301	-6369	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-6369	-6482	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-6482	-6547	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-6547	-6619	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-6619	-6670	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-6670	-6747	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-6747	-6832	38	1		0.00	11	0.00	0.00	0.00	0.00
3499	-6832	-6914	38	1		0.00	11	0.00	0.00	0.00	0.00

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3499	-6914	-6997	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-6997	-7056	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-7056	-7136	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-7136	-7199	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-7199	-7262	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-7262	-7296	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-7296	-7346	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-7346	-7462	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-7462	-7498	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-7498	-7577	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-7577	-7660	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-7660	-7709	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-7709	-7804	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-7804	-7927	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-7927	-7973	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-7973	-8027	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-8027	-8153	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-8153	-8227	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-8227	-8315	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-8315	-8376	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-8376	-8423	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-8423	-8472	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-8472	-8536	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-8536	-8620	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-8620	-8718	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-8718	-8824	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-8824	-8907	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-8907	-8981	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-8981	-9072	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-9072	-9148	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-9148	-9206	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-9206	-9282	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-9282	-9373	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-9373	-9439	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-9439	-9503	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-9503	-9549	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-9549	-9597	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-9597	-9639	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-9639	-9739	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-9739	-9854	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-9854	-9945	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-9945	-10033	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-10033	-10125	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-10125	-10193	38	1	0.00	11	0.00	0.00	0.00	0.00	
3499	-10193	3301	38	1	0.00	11	0.00	0.00	0.00	0.00	
3501	-4612	-4613	35	1	180.00	88	0.00	0.00	0.00	0.00	
3501	-4613	-4614	35	1	180.00	88	0.00	0.00	0.00	0.00	
3501	-4614	-4615	35	1	180.00	88	0.00	0.00	0.00	0.00	
3501	-4615	-4616	35	1	180.00	88	0.00	0.00	0.00	0.00	
3501	-4616	-4617	35	1	180.00	88	0.00	0.00	0.00	0.00	
3501	-4617	-4618	35	1	180.00	88	0.00	0.00	0.00	0.00	
3501	-4618	-4619	35	1	180.00	88	0.00	0.00	0.00	0.00	
3501	-4619	-4620	35	1	180.00	88	0.00	0.00	0.00	0.00	
3501	-4620	-4621	35	1	180.00	88	0.00	0.00	0.00	0.00	
3501	-4621	-4622	35	1	180.00	88	0.00	0.00	0.00	0.00	
3501	-4622	-4623	35	1	180.00	88	0.00	0.00	0.00	0.00	
3501	-4623	-4624	35	1	180.00	88	0.00	0.00	0.00	0.00	
3501	-4624	-4625	35	1	180.00	88	0.00	0.00	0.00	0.00	
3501	-4625	-4626	35	1	180.00	88	0.00	0.00	0.00	0.00	
3502	-4683	-4682	47	1	180.00	88	0.00	0.00	0.00	0.00	
3502	-4684	-4683	37	1	180.00	88	0.00	0.00	0.00	0.00	
3502	-4685	-4684	37	1	180.00	88	0.00	0.00	0.00	0.00	
3502	-4686	-4685	37	1	180.00	88	0.00	0.00	0.00	0.00	
3502	-4687	-4686	35	1	180.00	88	0.00	0.00	0.00	0.00	
3502	-4688	-4687	35	1	180.00	88	0.00	0.00	0.00	0.00	
3502	-4689	-4688	35	1	180.00	88	0.00	0.00	0.00	0.00	
3502	-4690	-4689	35	1	180.00	88	0.00	0.00	0.00	0.00	
3502	-4691	-4690	35	1	180.00	88	0.00	0.00	0.00	0.00	
3502	-4692	-4691	35	1	180.00	88	0.00	0.00	0.00	0.00	
3502	-4693	-4692	35	1	180.00	88	0.00	0.00	0.00	0.00	
3502	-4694	-4693	35	1	180.00	88	0.00	0.00	0.00	0.00	
3502	-4695	-4694	37	1	180.00	88	0.00	0.00	0.00	0.00	
3502	-4696	-4695	37	1	180.00	88	0.00	0.00	0.00	0.00	
3502	-4697	-4696	37	1	180.00	88	0.00	0.00	0.00	0.00	
3502	-4698	-4697	47	1	180.00	88	0.00	0.00	0.00	0.00	
3505	-5431	-5430	47	1	180.00	88	0.00	0.00	0.00	0.00	
3505	-5432	-5431	37	1	180.00	88	0.00	0.00	0.00	0.00	
3505	-5433	-5432	37	1	180.00	88	0.00	0.00	0.00	0.00	
3505	-5434	-5433	37	1	180.00	88	0.00	0.00	0.00	0.00	

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3505	-5435	-5434	35	1	180.00	88	0.00	0.00	0.00	0.00
3505	-5436	-5435	35	1	180.00	88	0.00	0.00	0.00	0.00
3505	-5437	-5436	35	1	180.00	88	0.00	0.00	0.00	0.00
3505	-5438	-5437	35	1	180.00	88	0.00	0.00	0.00	0.00
3505	-5439	-5438	35	1	180.00	88	0.00	0.00	0.00	0.00
3505	-5440	-5439	35	1	180.00	88	0.00	0.00	0.00	0.00
3505	-5441	-5440	35	1	180.00	88	0.00	0.00	0.00	0.00
3505	-5442	-5441	35	1	180.00	88	0.00	0.00	0.00	0.00
3505	-5443	-5442	37	1	180.00	88	0.00	0.00	0.00	0.00
3505	-5444	-5443	37	1	180.00	88	0.00	0.00	0.00	0.00
3505	-5445	-5444	37	1	180.00	88	0.00	0.00	0.00	0.00
3505	-5446	-5445	47	1	180.00	88	0.00	0.00	0.00	0.00
3506	-5836	-5835	47	1	180.00	88	0.00	0.00	0.00	0.00
3506	-5837	-5836	37	1	180.00	88	0.00	0.00	0.00	0.00
3506	-5838	-5837	37	1	180.00	88	0.00	0.00	0.00	0.00
3506	-5839	-5838	37	1	180.00	88	0.00	0.00	0.00	0.00
3506	-5840	-5839	35	1	180.00	88	0.00	0.00	0.00	0.00
3506	-5841	-5840	35	1	180.00	88	0.00	0.00	0.00	0.00
3506	-5842	-5841	35	1	180.00	88	0.00	0.00	0.00	0.00
3506	-5843	-5842	35	1	180.00	88	0.00	0.00	0.00	0.00
3506	-5844	-5843	35	1	180.00	88	0.00	0.00	0.00	0.00
3506	-5845	-5844	35	1	180.00	88	0.00	0.00	0.00	0.00
3506	-5846	-5845	35	13	180.00	88	0.00	0.00	0.00	0.00
3506	-5847	-5846	35	1	180.00	88	0.00	0.00	0.00	0.00
3506	-5848	-5847	37	1	180.00	88	0.00	0.00	0.00	0.00
3506	-5849	-5848	37	1	180.00	88	0.00	0.00	0.00	0.00
3506	-5850	-5849	37	1	180.00	88	0.00	0.00	0.00	0.00
3506	-5851	-5850	47	1	180.00	88	0.00	0.00	0.00	0.00
3507	-6242	-6234	47	1	180.00	88	0.00	0.00	0.00	0.00
3507	-6235	-6242	37	1	180.00	88	0.00	0.00	0.00	0.00
3507	-6236	-6235	37	1	180.00	88	0.00	0.00	0.00	0.00
3507	-6237	-6236	37	1	180.00	88	0.00	0.00	0.00	0.00
3507	-6243	-6237	35	1	180.00	88	0.00	0.00	0.00	0.00
3507	-6244	-6243	35	1	180.00	88	0.00	0.00	0.00	0.00
3507	-6238	-6244	35	1	180.00	88	0.00	0.00	0.00	0.00
3507	-6245	-6238	35	1	180.00	88	0.00	0.00	0.00	0.00
3507	-6246	-6245	35	1	180.00	88	0.00	0.00	0.00	0.00
3507	-6247	-6246	35	1	180.00	88	0.00	0.00	0.00	0.00
3507	-6248	-6247	35	1	180.00	88	0.00	0.00	0.00	0.00
3507	-6239	-6248	35	1	180.00	88	0.00	0.00	0.00	0.00
3507	-6249	-6239	37	1	180.00	88	0.00	0.00	0.00	0.00
3507	-6250	-6249	37	1	180.00	88	0.00	0.00	0.00	0.00
3507	-6251	-6250	37	1	180.00	88	0.00	0.00	0.00	0.00
3507	-6252	-6251	47	1	180.00	88	0.00	0.00	0.00	0.00
3508	-6687	-6666	47	1	180.00	88	0.00	0.00	0.00	0.00
3508	-6667	-6687	37	1	180.00	88	0.00	0.00	0.00	0.00
3508	-6688	-6667	37	1	180.00	88	0.00	0.00	0.00	0.00
3508	-6668	-6688	37	1	180.00	88	0.00	0.00	0.00	0.00
3508	-6669	-6668	35	1	180.00	88	0.00	0.00	0.00	0.00
3508	-6670	-6669	35	1	180.00	88	0.00	0.00	0.00	0.00
3508	-6689	-6670	35	1	180.00	88	0.00	0.00	0.00	0.00
3508	-6671	-6689	35	1	180.00	88	0.00	0.00	0.00	0.00
3508	-6672	-6671	35	1	180.00	88	0.00	0.00	0.00	0.00
3508	-6673	-6672	35	1	180.00	88	0.00	0.00	0.00	0.00
3508	-6677	-6673	35	1	180.00	88	0.00	0.00	0.00	0.00
3508	-6678	-6677	35	1	180.00	88	0.00	0.00	0.00	0.00
3508	-6690	-6678	37	1	180.00	88	0.00	0.00	0.00	0.00
3508	-6691	-6690	37	1	180.00	88	0.00	0.00	0.00	0.00
3508	-6692	-6691	37	1	180.00	88	0.00	0.00	0.00	0.00
3508	-6693	-6692	47	1	180.00	88	0.00	0.00	0.00	0.00
3509	-7131	-7130	47	1	180.00	88	0.00	0.00	0.00	0.00
3509	-7132	-7131	37	1	180.00	88	0.00	0.00	0.00	0.00
3509	-7133	-7132	37	1	180.00	88	0.00	0.00	0.00	0.00
3509	-7134	-7133	37	1	180.00	88	0.00	0.00	0.00	0.00
3509	-7135	-7134	35	1	180.00	88	0.00	0.00	0.00	0.00
3509	-7136	-7135	35	1	180.00	88	0.00	0.00	0.00	0.00
3509	-7137	-7136	35	1	180.00	88	0.00	0.00	0.00	0.00
3509	-7138	-7137	35	1	180.00	88	0.00	0.00	0.00	0.00
3509	-7139	-7138	35	1	180.00	88	0.00	0.00	0.00	0.00
3509	-7140	-7139	35	1	180.00	88	0.00	0.00	0.00	0.00
3509	-7141	-7140	35	1	180.00	88	0.00	0.00	0.00	0.00
3509	-7142	-7141	35	1	180.00	88	0.00	0.00	0.00	0.00
3509	-7143	-7142	37	1	180.00	88	0.00	0.00	0.00	0.00
3509	-7144	-7143	37	1	180.00	88	0.00	0.00	0.00	0.00
3509	-7145	-7144	37	1	180.00	88	0.00	0.00	0.00	0.00
3509	-7146	-7145	47	1	180.00	88	0.00	0.00	0.00	0.00
3510	-7493	-7492	47	1	180.00	88	0.00	0.00	0.00	0.00
3510	-7494	-7493	37	1	180.00	88	0.00	0.00	0.00	0.00
3510	-7495	-7494	37	1	180.00	88	0.00	0.00	0.00	0.00

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3515	-9736	-9726	37	1	180.00	88	0.00	0.00	0.00	0.00
3515	-9737	-9736	37	1	180.00	88	0.00	0.00	0.00	0.00
3515	-9738	-9737	35	1	180.00	88	0.00	0.00	0.00	0.00
3515	-9739	-9738	35	1	180.00	88	0.00	0.00	0.00	0.00
3515	-9727	-9739	35	1	180.00	88	0.00	0.00	0.00	0.00
3515	-9728	-9727	35	1	180.00	88	0.00	0.00	0.00	0.00
3515	-9740	-9728	35	1	180.00	88	0.00	0.00	0.00	0.00
3515	-9741	-9740	35	1	180.00	88	0.00	0.00	0.00	0.00
3515	-9742	-9741	35	1	180.00	88	0.00	0.00	0.00	0.00
3515	-9743	-9742	35	1	180.00	88	0.00	0.00	0.00	0.00
3515	-9744	-9743	37	1	180.00	88	0.00	0.00	0.00	0.00
3515	-9745	-9744	37	1	180.00	88	0.00	0.00	0.00	0.00
3515	-9746	-9745	37	1	180.00	88	0.00	0.00	0.00	0.00
3515	-9747	-9746	47	1	180.00	88	0.00	0.00	0.00	0.00
3517	-3083	-3082	52	1	0.00	22	0.00	0.00	0.00	0.00
3517	-3084	-3083	52	1	0.00	22	0.00	0.00	0.00	0.00
3517	-3085	-3084	52	1	0.00	22	0.00	0.00	0.00	0.00
3517	-3086	-3085	52	1	0.00	22	0.00	0.00	0.00	0.00
3517	-3087	-3086	52	1	0.00	22	0.00	0.00	0.00	0.00
3517	-3088	-3087	52	1	0.00	22	0.00	0.00	0.00	0.00
3517	-3089	-3088	52	1	0.00	22	0.00	0.00	0.00	0.00
3517	-3090	-3089	52	1	0.00	22	0.00	0.00	0.00	0.00
3556	-4659	-4678	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-4678	-4682	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-4682	-4741	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-4741	-4798	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-4798	-4853	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-4853	-4916	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-4916	-4991	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-4991	-5037	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-5037	-5113	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-5113	-5198	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-5198	-5263	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-5263	-5314	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-5314	-5368	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-5368	-5430	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-5430	-5493	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-5493	-5588	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-5588	-5657	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-5657	-5725	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-5725	-5789	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-5789	-5835	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-5835	-5877	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-5877	-5986	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-5986	-6059	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-6059	-6127	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-6127	-6184	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-6184	-6234	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-6234	-6295	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-6295	-6363	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-6363	-6476	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-6476	-6535	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-6535	-6613	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-6613	-6666	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-6666	-6741	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-6741	-6826	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-6826	-6900	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-6900	-6991	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-6991	-7050	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-7050	-7130	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-7130	-7193	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-7193	-7256	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-7256	-7290	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-7290	-7340	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-7340	-7456	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-7456	-7492	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-7492	-7567	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-7567	-7654	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-7654	-7697	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-7697	-7800	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-7800	-7921	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-7921	-7967	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-7967	-8021	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-8021	-8147	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-8147	-8221	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-8221	-8309	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-8309	-8370	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-8370	-8417	61	1	0.00	33	0.00	0.00	0.00	0.00
3556	-8417	-8468	61	1	0.00	33	0.00	0.00	0.00	0.00

3556	-8468	-8530	61	1	0.00	33	0.00	0.00	0.00	0.00	
3556	-8530	-8615	61	1	0.00	33	0.00	0.00	0.00	0.00	
3556	-8615	-8712	61	1	0.00	33	0.00	0.00	0.00	0.00	
3556	-8712	-8801	61	1	0.00	33	0.00	0.00	0.00	0.00	
3556	-8801	-8901	61	1	0.00	33	0.00	0.00	0.00	0.00	
3556	-8901	-8975	61	1	0.00	33	0.00	0.00	0.00	0.00	
3556	-8975	-9068	61	1	0.00	33	0.00	0.00	0.00	0.00	
3556	-9068	-9142	61	1	0.00	33	0.00	0.00	0.00	0.00	
3556	-9142	-9200	61	1	0.00	33	0.00	0.00	0.00	0.00	
3556	-9200	-9276	61	1	0.00	33	0.00	0.00	0.00	0.00	
3556	-9276	-9367	61	1	0.00	33	0.00	0.00	0.00	0.00	
3556	-9367	-9433	61	1	0.00	33	0.00	0.00	0.00	0.00	
3556	-9433	-9502	61	1	0.00	33	0.00	0.00	0.00	0.00	
3556	-9502	-9543	61	1	0.00	33	0.00	0.00	0.00	0.00	
3556	-9543	-9591	61	1	0.00	33	0.00	0.00	0.00	0.00	
3556	-9591	-9633	61	1	0.00	33	0.00	0.00	0.00	0.00	
3556	-9633	-9734	61	1	0.00	33	0.00	0.00	0.00	0.00	
3556	-9734	-9846	61	1	0.00	33	0.00	0.00	0.00	0.00	
3556	-9846	-9941	61	1	0.00	33	0.00	0.00	0.00	0.00	
3556	-9941	-10027	61	1	0.00	33	0.00	0.00	0.00	0.00	
3556	-10027	-10119	61	1	0.00	33	0.00	0.00	0.00	0.00	
3556	-10119	-10188	61	1	0.00	33	0.00	0.00	0.00	0.00	
3556	-10188	-10243	61	1	0.00	33	0.00	0.00	0.00	0.00	
3557	-4534	-4525	54	1	180.00	22	0.00	0.00	8.00	8.00	
3557	-4547	-4534	54	1	180.00	22	0.00	0.00	8.00	8.00	
3557	-4564	-4547	54	1	180.00	22	0.00	0.00	8.00	8.00	
3557	-4581	-4564	54	1	180.00	22	0.00	0.00	8.00	8.00	
3557	-4600	-4581	54	1	180.00	22	0.00	0.00	8.00	8.00	
3557	-4618	-4600	54	1	180.00	22	0.00	0.00	8.00	8.00	
3557	-4632	-4618	54	1	180.00	22	0.00	0.00	8.00	8.00	
3557	-4649	-4632	54	1	180.00	22	0.00	0.00	8.00	8.00	
3557	-4666	-4649	54	1	180.00	22	0.00	0.00	8.00	8.00	
3557	-4689	-4666	54	1	180.00	22	0.00	0.00	8.00	8.00	
3558	-4748	-4689	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-4805	-4748	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-4860	-4805	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-4926	-4860	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-4969	-4926	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-5043	-4969	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-5120	-5043	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-5205	-5120	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-5270	-5205	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-5321	-5270	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-5375	-5321	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-5437	-5375	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-5500	-5437	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-5595	-5500	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-5664	-5595	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-5740	-5664	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-5796	-5740	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-5842	-5796	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-5884	-5842	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-5993	-5884	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-6066	-5993	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-6134	-6066	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-6191	-6134	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-6238	-6191	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-6302	-6238	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-6370	-6302	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-6483	-6370	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-6548	-6483	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-6620	-6548	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-6689	-6620	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-6748	-6689	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-6833	-6748	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-6915	-6833	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-6998	-6915	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-7057	-6998	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-7137	-7057	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-7200	-7137	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-7263	-7200	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-7297	-7263	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-7347	-7297	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-7463	-7347	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-7499	-7463	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-7578	-7499	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-7661	-7578	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-7710	-7661	54	1	180.00	44	0.80	0.80	0.00	0.00	
3558	-7805	-7710	54	1	180.00	44	0.80	0.80	0.00	0.00	

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3558	-7928	-7805	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-7974	-7928	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-8028	-7974	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-8154	-8028	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-8228	-8154	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-8316	-8228	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-8377	-8316	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-8424	-8377	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-8479	-8424	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-8537	-8479	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-8628	-8537	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-8719	-8628	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-8840	-8719	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-8908	-8840	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-8982	-8908	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-9073	-8982	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-9149	-9073	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-9207	-9149	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-9283	-9207	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-9374	-9283	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-9440	-9374	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-9479	-9440	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-9550	-9479	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-9598	-9550	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-9640	-9598	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-9727	-9640	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-9855	-9727	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-9968	-9855	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-10034	-9968	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-10126	-10034	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-10194	-10126	54	1	180.00	44	0.80	0.80	0.00	0.00
3558	-10249	-10194	54	1	180.00	44	0.80	0.80	0.00	0.00
3560	-4750	-4691	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-4807	-4750	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-4862	-4807	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-4928	-4862	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-4970	-4928	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-5045	-4970	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-5122	-5045	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-5207	-5122	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-5272	-5207	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-5323	-5272	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-5377	-5323	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-5439	-5377	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-5502	-5439	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-5597	-5502	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-5666	-5597	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-5741	-5666	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-5798	-5741	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-5844	-5798	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-5886	-5844	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-6025	-5886	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-6068	-6025	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-6136	-6068	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-6193	-6136	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-6246	-6193	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-6304	-6246	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-6372	-6304	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-6485	-6372	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-6550	-6485	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-6622	-6550	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-6672	-6622	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-6750	-6672	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-6835	-6750	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-6917	-6835	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-7000	-6917	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-7059	-7000	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-7139	-7059	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-7202	-7139	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-7265	-7202	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-7299	-7265	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-7349	-7299	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-7465	-7349	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-7501	-7465	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-7579	-7501	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-7666	-7579	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-7712	-7666	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-7807	-7712	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-7930	-7807	54	1	270.00	44	0.00	0.00	0.80	0.80

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3560	-7976	-7930	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-8030	-7976	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-8156	-8030	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-8230	-8156	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-8318	-8230	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-8379	-8318	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-8426	-8379	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-8481	-8426	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-8539	-8481	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-8629	-8539	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-8721	-8629	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-8841	-8721	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-8910	-8841	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-8984	-8910	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-9074	-8984	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-9151	-9074	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-9209	-9151	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-9285	-9209	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-9376	-9285	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-9442	-9376	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-9486	-9442	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-9552	-9486	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-9600	-9552	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-9642	-9600	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-9740	-9642	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-9847	-9740	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-9970	-9847	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-10036	-9970	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-10128	-10036	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-10196	-10128	54	1	270.00	44	0.00	0.00	0.80	0.80
3560	-10251	-10196	54	1	270.00	44	0.00	0.00	0.80	0.80
3561	-4526	-4535	54	1	180.00	22	0.00	0.00	8.00	8.00
3561	-4535	-4548	54	1	180.00	22	0.00	0.00	8.00	8.00
3561	-4548	-4565	54	1	180.00	22	0.00	0.00	8.00	8.00
3561	-4565	-4582	54	1	180.00	22	0.00	0.00	8.00	8.00
3561	-4582	-4601	54	1	180.00	22	0.00	0.00	8.00	8.00
3561	-4601	-4620	54	1	180.00	22	0.00	0.00	8.00	8.00
3561	-4620	-4634	54	1	180.00	22	0.00	0.00	8.00	8.00
3561	-4634	-4651	54	1	180.00	22	0.00	0.00	8.00	8.00
3561	-4651	-4668	54	1	180.00	22	0.00	0.00	8.00	8.00
3561	-4668	-4691	54	1	180.00	22	0.00	0.00	8.00	8.00
3562	-4660	-4681	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-4681	-4698	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-4698	-4757	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-4757	-4814	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-4814	-4869	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-4869	-4934	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-4934	-4997	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-4997	-5051	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-5051	-5129	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-5129	-5214	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-5214	-5279	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-5279	-5330	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-5330	-5384	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-5384	-5446	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-5446	-5509	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-5509	-5604	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-5604	-5673	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-5673	-5744	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-5744	-5805	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-5805	-5851	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-5851	-5893	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-5893	-5972	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-5972	-6075	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-6075	-6143	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-6143	-6200	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-6200	-6252	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-6252	-6311	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-6311	-6379	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-6379	-6492	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-6492	-6556	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-6556	-6629	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-6629	-6693	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-6693	-6757	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-6757	-6842	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-6842	-6901	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-6901	-7007	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-7007	-7066	61	1	0.00	11	0.00	0.00	0.00	0.00
3562	-7066	-7146	61	1	0.00	11	0.00	0.00	0.00	0.00

3562	-7146	-7209	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-7209	-7272	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-7272	-7306	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-7306	-7356	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-7356	-7472	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-7472	-7508	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-7508	-7586	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-7586	-7671	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-7671	-7723	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-7723	-7813	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-7813	-7937	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-7937	-7983	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-7983	-8037	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-8037	-8163	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-8163	-8237	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-8237	-8325	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-8325	-8386	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-8386	-8433	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-8433	-8486	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-8486	-8546	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-8546	-8635	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-8635	-8728	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-8728	-8809	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-8809	-8917	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-8917	-8991	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-8991	-9100	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-9100	-9158	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-9158	-9216	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-9216	-9292	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-9292	-9383	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-9383	-9449	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-9449	-9507	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-9507	-9559	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-9559	-9607	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-9607	-9649	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-9649	-9747	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-9747	-9863	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-9863	-9974	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-9974	-10043	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-10043	-10135	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-10135	-10201	61	1	0.00	11	0.00	0.00	0.00	0.00	
3562	-10201	-10257	61	1	0.00	11	0.00	0.00	0.00	0.00	
3566	-4526	-4524	61	1	0.00	33	0.00	0.00	0.00	0.00	
3566	-4528	-4526	61	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-4692	-4751	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-4751	-4808	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-4808	-4863	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-4863	-4929	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-4929	-4978	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-4978	2902	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	2902	-5123	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-5123	-5208	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-5208	-5273	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-5273	-5324	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-5324	-5378	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-5378	-5440	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-5440	-5503	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-5503	-5598	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-5598	-5667	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-5667	-5733	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-5733	-5799	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-5799	-5845	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-5845	-5887	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-5887	-5995	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-5995	-6069	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-6069	-6137	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-6137	-6194	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-6194	-6247	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-6247	-6305	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-6305	-6373	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-6373	-6486	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-6486	-6551	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-6551	-6623	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-6623	-6673	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-6673	-6751	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-6751	-6836	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-6836	-6918	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-6918	-7001	38	1	0.00	33	0.00	0.00	0.00	0.00	
3567	-7001	-7060	38	1	0.00	33	0.00	0.00	0.00	0.00	

3567	-7060	-7140	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-7140	-7203	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-7203	-7266	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-7266	-7300	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-7300	-7350	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-7350	-7466	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-7466	-7502	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-7502	-7580	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-7580	-7663	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-7663	-7713	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-7713	-7808	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-7808	-7931	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-7931	-7977	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-7977	-8031	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-8031	-8157	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-8157	-8231	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-8231	-8319	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-8319	-8380	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-8380	-8427	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-8427	-8482	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-8482	-8540	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-8540	-8622	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-8622	-8722	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-8722	-8808	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-8808	-8911	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-8911	-8985	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-8985	-9075	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-9075	-9152	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-9152	-9210	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-9210	-9286	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-9286	-9377	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-9377	-9443	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-9443	-9487	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-9487	-9553	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-9553	-9601	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-9601	-9643	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-9643	-9741	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-9741	-9857	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-9857	-9962	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-9962	-10037	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-10037	-10129	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-10129	-10176	38	1		0.00	33	0.00	0.00	0.00	0.00	
3567	-10176	3302	38	1		0.00	33	0.00	0.00	0.00	0.00	
3568	-4532	-4528	61	1		0.00	33	0.00	0.00	0.00	0.00	
3568	-4539	-4532	61	1		0.00	33	0.00	0.00	0.00	0.00	
3568	-4541	-4539	61	1		0.00	33	0.00	0.00	0.00	0.00	
3570	-4554	-4541	61	1		0.00	33	0.00	0.00	0.00	0.00	
3570	-4569	-4554	61	1		0.00	33	0.00	0.00	0.00	0.00	
3570	-4579	-4569	61	1		0.00	33	0.00	0.00	0.00	0.00	
3571	-4540	-4553	61	1		0.00	33	0.00	0.00	0.00	0.00	
3571	-4553	-4568	61	1		0.00	33	0.00	0.00	0.00	0.00	
3571	-4568	-4578	61	1		0.00	33	0.00	0.00	0.00	0.00	
3574	-4594	-4579	61	1		0.00	33	0.00	0.00	0.00	0.00	
3574	-4611	-4594	61	1		0.00	33	0.00	0.00	0.00	0.00	
3574	-4626	-4611	61	1		0.00	33	0.00	0.00	0.00	0.00	
3575	-4578	-4593	61	1		0.00	33	0.00	0.00	0.00	0.00	
3575	-4593	-4610	61	1		0.00	33	0.00	0.00	0.00	0.00	
3575	-4610	-4612	61	1		0.00	33	0.00	0.00	0.00	0.00	
3577	-2478	-4526	39	13		0.00	11	0.00	0.00	0.00	0.00	
3578	-2477	-4525	39	13		0.00	55	0.00	0.00	0.00	0.00	
3579	-4628	-4626	61	1		0.00	33	0.00	0.00	0.00	0.00	
3579	-4643	-4628	61	1		0.00	33	0.00	0.00	0.00	0.00	
3579	-4660	-4643	61	1		0.00	33	0.00	0.00	0.00	0.00	
3580	-4612	-4627	61	1		0.00	33	0.00	0.00	0.00	0.00	
3580	-4627	-4642	61	1		0.00	33	0.00	0.00	0.00	0.00	
3580	-4642	-4659	61	1		0.00	33	0.00	0.00	0.00	0.00	
3583	-4198	-4683	36	1		0.00	22	0.00	0.00	0.00	0.00	
3584	-4199	-4697	36	1		0.00	22	0.00	0.00	0.00	0.00	
3585	-3733	-4199	36	1		0.00	22	0.00	0.00	0.00	0.00	
3586	-3732	-4198	36	1		0.00	22	0.00	0.00	0.00	0.00	
3587	-3273	-3732	36	1		0.00	22	0.00	0.00	0.00	0.00	
3588	-3268	-3733	36	1		0.00	22	0.00	0.00	0.00	0.00	
3589	-3102	-3268	36	1		0.00	22	0.00	0.00	0.00	0.00	
3590	-3101	-3273	36	1		0.00	22	0.00	0.00	0.00	0.00	
3591	-2878	-3102	36	1		0.00	22	0.00	0.00	0.00	0.00	
3592	-2877	-3101	36	1		0.00	22	0.00	0.00	0.00	0.00	
3593	-2719	-2878	36	1		0.00	22	0.00	0.00	0.00	0.00	
3594	-2718	-2877	36	1		0.00	22	0.00	0.00	0.00	0.00	
3595	-2478	-2546	32	1		0.00	55	0.00	0.00	0.00	0.00	

3595	-2546	-2592	33	1		0.00	55	0.00	0.00	0.00	0.00	
3595	-2592	-3079	34	1		0.00	55	0.00	0.00	0.00	0.00	
3595	-3079	-4692	34	1		0.00	55	0.00	0.00	0.00	0.00	
3596	-2477	-2545	32	1		0.00	55	0.00	0.00	0.00	0.00	
3596	-2545	-2591	33	1		0.00	55	0.00	0.00	0.00	0.00	
3596	-2591	-3078	34	1		0.00	55	0.00	0.00	0.00	0.00	
3596	-3078	-3569	34	1		0.00	55	0.00	0.00	0.00	0.00	
3596	-3569	-4688	34	1		0.00	55	0.00	0.00	0.00	0.00	
3597	-2591	-2718	36	1		0.00	22	0.00	0.00	0.00	0.00	
3598	-2592	-2719	36	1		0.00	22	0.00	0.00	0.00	0.00	
3601	-5043	-4682	53	13		0.00	22	0.00	0.00	0.00	0.00	
3602	-5045	-4698	53	13		0.00	22	0.00	0.00	0.00	0.00	
3605	-4446	-5050	36	1		0.00	22	0.00	0.00	0.00	0.00	
3606	-4445	-5038	36	1		0.00	22	0.00	0.00	0.00	0.00	
3607	-4020	-4446	36	1		0.00	22	0.00	0.00	0.00	0.00	
3608	-4019	-4445	36	1		0.00	22	0.00	0.00	0.00	0.00	
3609	-3396	-4019	36	1		0.00	22	0.00	0.00	0.00	0.00	
3610	-3397	-4020	36	1		0.00	22	0.00	0.00	0.00	0.00	
3611	-3218	-3397	36	1		0.00	22	0.00	0.00	0.00	0.00	
3612	-3217	-3396	36	1		0.00	22	0.00	0.00	0.00	0.00	
3613	-2964	-3218	36	1		0.00	22	0.00	0.00	0.00	0.00	
3614	-2963	-3217	36	1		0.00	22	0.00	0.00	0.00	0.00	
3615	-2779	-2964	36	1		0.00	22	0.00	0.00	0.00	0.00	
3616	-2778	-2963	36	1		0.00	22	0.00	0.00	0.00	0.00	
3617	-2644	-2779	36	1		0.00	22	0.00	0.00	0.00	0.00	
3618	-2643	-2778	36	1		0.00	22	0.00	0.00	0.00	0.00	
3622	-5043	-5430	53	13		0.00	22	0.00	0.00	0.00	0.00	
3623	-5045	-5446	53	13		0.00	22	0.00	0.00	0.00	0.00	
3626	-4936	-5445	36	1		0.00	22	0.00	0.00	0.00	0.00	
3627	-4935	-5431	36	1		0.00	22	0.00	0.00	0.00	0.00	
3628	-4282	-4936	36	1		0.00	22	0.00	0.00	0.00	0.00	
3629	-4281	-4935	36	1		0.00	22	0.00	0.00	0.00	0.00	
3630	-3588	-4281	36	1		0.00	22	0.00	0.00	0.00	0.00	
3631	-3589	-4282	36	1		0.00	22	0.00	0.00	0.00	0.00	
3632	-3349	-3589	36	1		0.00	22	0.00	0.00	0.00	0.00	
3633	-3348	-3588	36	1		0.00	22	0.00	0.00	0.00	0.00	
3634	-3062	-3348	36	1		0.00	22	0.00	0.00	0.00	0.00	
3635	-3063	-3349	36	1		0.00	22	0.00	0.00	0.00	0.00	
3636	-2844	-3063	36	1		0.00	22	0.00	0.00	0.00	0.00	
3637	-2843	-3062	36	1		0.00	22	0.00	0.00	0.00	0.00	
3638	-2698	-2843	36	1		0.00	22	0.00	0.00	0.00	0.00	
3639	-2699	-2844	36	1		0.00	22	0.00	0.00	0.00	0.00	
3642	-2442	-2495	32	1		0.00	55	0.00	0.00	0.00	0.00	
3642	-2495	-2698	33	1		0.00	55	0.00	0.00	0.00	0.00	
3642	-2698	-3322	34	1		0.00	55	0.00	0.00	0.00	0.00	
3642	-3322	-5436	34	1		0.00	55	0.00	0.00	0.00	0.00	
3643	-2441	-2496	32	1		0.00	55	0.00	0.00	0.00	0.00	
3643	-2496	-2699	33	1		0.00	55	0.00	0.00	0.00	0.00	
3643	-2699	-3323	34	1		0.00	55	0.00	0.00	0.00	0.00	
3643	-3323	-5440	34	1		0.00	55	0.00	0.00	0.00	0.00	
3644	-5439	-5851	53	13		0.00	22	0.00	0.00	0.00	0.00	
3645	-5437	-5835	53	13		0.00	22	0.00	0.00	0.00	0.00	
3646	-2442	-6191	50	13		0.00	55	0.00	0.00	0.00	0.00	
3647	-2441	-6193	50	13		0.00	55	0.00	0.00	0.00	0.00	
3648	-5333	-5836	36	1		0.00	22	0.00	0.00	0.00	0.00	
3649	-5334	-5850	36	1		0.00	22	0.00	0.00	0.00	0.00	
3650	-4700	-5334	36	1		0.00	22	0.00	0.00	0.00	0.00	
3651	-4699	-5333	36	1		0.00	22	0.00	0.00	0.00	0.00	
3652	-3885	-4699	36	1		0.00	22	0.00	0.00	0.00	0.00	
3653	-3886	-4700	36	1		0.00	22	0.00	0.00	0.00	0.00	
3654	-3467	-3885	36	1		0.00	22	0.00	0.00	0.00	0.00	
3655	-3468	-3886	36	1		0.00	22	0.00	0.00	0.00	0.00	
3656	-3185	-3467	36	1		0.00	22	0.00	0.00	0.00	0.00	
3657	-3186	-3468	36	1		0.00	22	0.00	0.00	0.00	0.00	
3658	-2905	-3186	36	1		0.00	22	0.00	0.00	0.00	0.00	
3659	-2904	-3185	36	1		0.00	22	0.00	0.00	0.00	0.00	
3660	-2755	-2904	36	1		0.00	22	0.00	0.00	0.00	0.00	
3661	-2756	-2905	36	1		0.00	22	0.00	0.00	0.00	0.00	
3662	-2426	-2520	32	1		0.00	55	0.00	0.00	0.00	0.00	
3662	-2520	-2755	33	1		0.00	55	0.00	0.00	0.00	0.00	
3662	-2755	-3450	34	1		0.00	55	0.00	0.00	0.00	0.00	
3662	-3450	-5841	34	1		0.00	55	0.00	0.00	0.00	0.00	
3663	-2427	-2521	32	1		0.00	55	0.00	0.00	0.00	0.00	
3663	-2521	-2756	33	1		0.00	55	0.00	0.00	0.00	0.00	
3663	-2756	-3451	34	1		0.00	55	0.00	0.00	0.00	0.00	
3663	-3451	-5845	34	1		0.00	55	0.00	0.00	0.00	0.00	
3664	-5842	-6234	53	13		0.00	22	0.00	0.00	0.00	0.00	
3665	-5844	-6252	53	13		0.00	22	0.00	0.00	0.00	0.00	
3667	-2427	-6550	39	13		0.00	55	0.00	0.00	0.00	0.00	

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3668	-2426	-6548	39	13	0.00	55	0.00	0.00	0.00	0.00	
3669	-5746	-6242	36	1	0.00	22	0.00	0.00	0.00	0.00	
3670	-5747	-6251	36	1	0.00	22	0.00	0.00	0.00	0.00	
3671	-5053	-5747	36	1	0.00	22	0.00	0.00	0.00	0.00	
3672	-5052	-5746	36	1	0.00	22	0.00	0.00	0.00	0.00	
3673	-4148	-5052	36	1	0.00	22	0.00	0.00	0.00	0.00	
3674	-4149	-5053	36	1	0.00	22	0.00	0.00	0.00	0.00	
3675	-3748	-4148	36	1	0.00	22	0.00	0.00	0.00	0.00	
3676	-3749	-4149	36	1	0.00	22	0.00	0.00	0.00	0.00	
3677	-3308	-3749	36	1	0.00	22	0.00	0.00	0.00	0.00	
3678	-3307	-3748	36	1	0.00	22	0.00	0.00	0.00	0.00	
3679	-2991	-3307	36	1	0.00	22	0.00	0.00	0.00	0.00	
3680	-2992	-3308	36	1	0.00	22	0.00	0.00	0.00	0.00	
3681	-2811	-2991	36	1	0.00	22	0.00	0.00	0.00	0.00	
3682	-2812	-2992	36	1	0.00	22	0.00	0.00	0.00	0.00	
3683	-2405	-2543	32	1	0.00	55	0.00	0.00	0.00	0.00	
3683	-2543	-2812	33	1	0.00	55	0.00	0.00	0.00	0.00	
3683	-2812	-3697	34	1	0.00	55	0.00	0.00	0.00	0.00	
3683	-3697	-6247	34	1	0.00	55	0.00	0.00	0.00	0.00	
3684	-2363	-2542	32	1	0.00	55	0.00	0.00	0.00	0.00	
3684	-2542	-2811	33	1	0.00	55	0.00	0.00	0.00	0.00	
3684	-2811	-3696	34	1	0.00	55	0.00	0.00	0.00	0.00	
3684	-3696	-6244	34	1	0.00	55	0.00	0.00	0.00	0.00	
3685	-6238	-6666	53	13	0.00	22	0.00	0.00	0.00	0.00	
3686	-6246	-6693	53	13	0.00	22	0.00	0.00	0.00	0.00	
3687	-2405	-6917	39	13	0.00	55	0.00	0.00	0.00	0.00	
3688	-2363	-6915	39	13	0.00	55	0.00	0.00	0.00	0.00	
3689	-6152	-6692	36	1	0.00	22	0.00	0.00	0.00	0.00	
3690	-6151	-6687	36	1	0.00	22	0.00	0.00	0.00	0.00	
3691	-5447	-6151	36	1	0.00	22	0.00	0.00	0.00	0.00	
3692	-5448	-6152	36	1	0.00	22	0.00	0.00	0.00	0.00	
3693	-4403	-5447	36	1	0.00	22	0.00	0.00	0.00	0.00	
3694	-4404	-5448	36	1	0.00	22	0.00	0.00	0.00	0.00	
3695	-4039	-4404	36	1	0.00	22	0.00	0.00	0.00	0.00	
3696	-4038	-4403	36	1	0.00	22	0.00	0.00	0.00	0.00	
3697	-3426	-4038	36	1	0.00	22	0.00	0.00	0.00	0.00	
3698	-3427	-4039	36	1	0.00	22	0.00	0.00	0.00	0.00	
3699	-3120	-3426	36	1	0.00	22	0.00	0.00	0.00	0.00	
3700	-3121	-3427	36	1	0.00	22	0.00	0.00	0.00	0.00	
3701	-2879	-3120	36	1	0.00	22	0.00	0.00	0.00	0.00	
3702	-2880	-3121	36	1	0.00	22	0.00	0.00	0.00	0.00	
3703	-2360	-2554	32	1	0.00	55	0.00	0.00	0.00	0.00	
3703	-2554	-2879	33	1	0.00	55	0.00	0.00	0.00	0.00	
3703	-2879	-3985	34	1	0.00	55	0.00	0.00	0.00	0.00	
3703	-3985	-6670	34	1	0.00	55	0.00	0.00	0.00	0.00	
3704	-2361	-2555	32	1	0.00	55	0.00	0.00	0.00	0.00	
3704	-2555	-2880	33	1	0.00	55	0.00	0.00	0.00	0.00	
3704	-2880	-3986	34	1	0.00	55	0.00	0.00	0.00	0.00	
3704	-3986	-6673	34	1	0.00	55	0.00	0.00	0.00	0.00	
3705	-6672	-7146	53	13	0.00	22	0.00	0.00	0.00	0.00	
3706	-6689	-7130	53	13	0.00	22	0.00	0.00	0.00	0.00	
3707	-2360	-7263	39	13	0.00	55	0.00	0.00	0.00	0.00	
3708	-2361	-7265	39	13	0.00	55	0.00	0.00	0.00	0.00	
3709	-6559	-7145	36	1	0.00	22	0.00	0.00	0.00	0.00	
3710	-6558	-7131	36	1	0.00	22	0.00	0.00	0.00	0.00	
3711	-5853	-6559	36	1	0.00	22	0.00	0.00	0.00	0.00	
3712	-5852	-6558	36	1	0.00	22	0.00	0.00	0.00	0.00	
3713	-4870	-5852	36	1	0.00	22	0.00	0.00	0.00	0.00	
3714	-4871	-5853	36	1	0.00	22	0.00	0.00	0.00	0.00	
3715	-4295	-4870	36	1	0.00	22	0.00	0.00	0.00	0.00	
3716	-4296	-4871	36	1	0.00	22	0.00	0.00	0.00	0.00	
3717	-3663	-4295	36	1	0.00	22	0.00	0.00	0.00	0.00	
3718	-3659	-4296	36	1	0.00	22	0.00	0.00	0.00	0.00	
3719	-3224	-3663	36	1	0.00	22	0.00	0.00	0.00	0.00	
3720	-3225	-3659	36	1	0.00	22	0.00	0.00	0.00	0.00	
3721	-2966	-3225	36	1	0.00	22	0.00	0.00	0.00	0.00	
3722	-2965	-3224	36	1	0.00	22	0.00	0.00	0.00	0.00	
3723	-2356	-2562	32	1	0.00	55	0.00	0.00	0.00	0.00	
3723	-2562	-2965	33	1	0.00	55	0.00	0.00	0.00	0.00	
3723	-2965	-4251	34	1	0.00	55	0.00	0.00	0.00	0.00	
3723	-4251	-7136	34	1	0.00	55	0.00	0.00	0.00	0.00	
3724	-2357	-2563	32	1	0.00	55	0.00	0.00	0.00	0.00	
3724	-2563	-2966	33	1	0.00	55	0.00	0.00	0.00	0.00	
3724	-2966	-4252	34	1	0.00	55	0.00	0.00	0.00	0.00	
3724	-4252	-7140	34	1	0.00	55	0.00	0.00	0.00	0.00	
3725	-7137	-7492	53	13	0.00	22	0.00	0.00	0.00	0.00	
3726	-7139	-7508	53	13	0.00	22	0.00	0.00	0.00	0.00	
3727	-2356	-4104	39	13	0.00	55	0.00	0.00	0.00	8.00	
3728	-2357	-4105	39	13	0.00	55	0.00	0.00	0.00	8.00	

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3729	-7008	-7493	36	1		0.00	22	0.00	0.00	0.00	0.00	
3730	-7009	-7507	36	1		0.00	22	0.00	0.00	0.00	0.00	
3731	-6253	-7009	36	1		0.00	22	0.00	0.00	0.00	0.00	
3732	-6240	-7008	36	1		0.00	22	0.00	0.00	0.00	0.00	
3733	-5284	-6240	36	1		0.00	22	0.00	0.00	0.00	0.00	
3734	-5285	-6253	36	1		0.00	22	0.00	0.00	0.00	0.00	
3735	-4711	-5284	36	1		0.00	22	0.00	0.00	0.00	0.00	
3736	-4712	-5285	36	1		0.00	22	0.00	0.00	0.00	0.00	
3737	-3949	-4712	36	1		0.00	22	0.00	0.00	0.00	0.00	
3738	-3955	-4711	36	1		0.00	22	0.00	0.00	0.00	0.00	
3739	-2352	-2589	32	1		0.00	55	0.00	0.00	0.00	0.00	
3739	-2589	-3065	33	1		0.00	55	0.00	0.00	0.00	0.00	
3739	-3065	-4493	34	1		0.00	55	0.00	0.00	0.00	0.00	
3739	-4493	-7502	34	1		0.00	55	0.00	0.00	0.00	0.00	
3740	-2351	-2588	32	1		0.00	55	0.00	0.00	0.00	0.00	
3740	-2588	-3064	33	1		0.00	55	0.00	0.00	0.00	0.00	
3740	-3064	-4492	34	1		0.00	55	0.00	0.00	0.00	0.00	
3740	-4492	-7498	34	1		0.00	55	0.00	0.00	0.00	0.00	
3741	-7974	-7492	53	13		0.00	22	0.00	0.00	0.00	0.00	
3742	-7976	-7508	53	13		0.00	22	0.00	0.00	0.00	0.00	
3743	-2408	-4104	39	13		0.00	55	0.00	0.00	0.00	8.00	
3744	-2409	-4105	39	13		0.00	55	0.00	0.00	0.00	8.00	
3745	-7358	-7982	36	1		0.00	22	0.00	0.00	0.00	0.00	
3746	-7357	-7968	36	1		0.00	22	0.00	0.00	0.00	0.00	
3747	-6694	-7358	36	1		0.00	22	0.00	0.00	0.00	0.00	
3748	-6674	-7357	36	1		0.00	22	0.00	0.00	0.00	0.00	
3749	-5681	-6694	36	1		0.00	22	0.00	0.00	0.00	0.00	
3750	-5674	-6674	36	1		0.00	22	0.00	0.00	0.00	0.00	
3751	-5065	-5674	36	1		0.00	22	0.00	0.00	0.00	0.00	
3752	-5066	-5681	36	1		0.00	22	0.00	0.00	0.00	0.00	
3753	-4223	-5065	36	1		0.00	22	0.00	0.00	0.00	0.00	
3754	-4224	-5066	36	1		0.00	22	0.00	0.00	0.00	0.00	
3755	-3189	-3474	36	1		0.00	22	0.00	0.00	0.00	0.00	
3756	-2409	-2639	32	1		0.00	55	0.00	0.00	0.00	0.00	
3756	-2639	-3189	33	1		0.00	55	0.00	0.00	0.00	0.00	
3756	-3189	-5014	34	1		0.00	55	0.00	0.00	0.00	0.00	
3756	-5014	-7977	34	1		0.00	55	0.00	0.00	0.00	0.00	
3757	-2408	-2638	32	1		0.00	55	0.00	0.00	0.00	0.00	
3757	-2638	-3193	33	1		0.00	55	0.00	0.00	0.00	0.00	
3757	-3193	-5013	34	1		0.00	55	0.00	0.00	0.00	0.00	
3757	-5013	-7973	34	1		0.00	55	0.00	0.00	0.00	0.00	
3758	-2438	-7807	39	13		0.00	55	0.00	0.00	0.00	0.00	
3759	-2437	-7805	39	13		0.00	55	0.00	0.00	0.00	0.00	
3760	-8426	-7983	53	13		0.00	22	0.00	0.00	0.00	0.00	
3761	-8424	-7967	53	13		0.00	22	0.00	0.00	0.00	0.00	
3762	-7814	-8418	36	1		0.00	22	0.00	0.00	0.00	0.00	
3763	-7815	-8432	36	1		0.00	22	0.00	0.00	0.00	0.00	
3764	-7147	-7814	36	1		0.00	22	0.00	0.00	0.00	0.00	
3765	-7148	-7815	36	1		0.00	22	0.00	0.00	0.00	0.00	
3766	-6100	-7147	36	1		0.00	22	0.00	0.00	0.00	0.00	
3767	-6101	-7148	36	1		0.00	22	0.00	0.00	0.00	0.00	
3768	-5459	-6101	36	1		0.00	22	0.00	0.00	0.00	0.00	
3769	-5458	-6100	36	1		0.00	22	0.00	0.00	0.00	0.00	
3770	-4471	-5458	36	1		0.00	22	0.00	0.00	0.00	0.00	
3771	-3764	-4471	36	1		0.00	22	0.00	0.00	0.00	0.00	
3772	-3767	-4463	36	1		0.00	22	0.00	0.00	0.00	0.00	
3773	-3309	-3764	36	1		0.00	22	0.00	0.00	0.00	0.00	
3774	-3317	-3767	36	1		0.00	22	0.00	0.00	0.00	0.00	
3775	-2437	-2697	32	1		0.00	55	0.00	0.00	0.00	0.00	
3775	-2697	-3309	33	1		0.00	55	0.00	0.00	0.00	0.00	
3775	-3309	-5418	34	1		0.00	55	0.00	0.00	0.00	0.00	
3775	-5418	-8423	34	1		0.00	55	0.00	0.00	0.00	0.00	
3776	-2438	-2692	32	1		0.00	55	0.00	0.00	0.00	0.00	
3776	-2692	-3317	33	1		0.00	55	0.00	0.00	0.00	0.00	
3776	-3317	-5397	34	1		0.00	55	0.00	0.00	0.00	0.00	
3776	-5397	-8427	34	1		0.00	55	0.00	0.00	0.00	0.00	
3777	-2464	-8230	39	13		0.00	55	0.00	0.00	0.00	0.00	
3778	-2463	-8228	39	13		0.00	55	0.00	0.00	0.00	0.00	
3779	-8908	-8417	53	13		0.00	22	0.00	0.00	0.00	0.00	
3780	-8910	-8433	53	13		0.00	22	0.00	0.00	0.00	0.00	
3781	-8327	-8916	36	1		0.00	22	0.00	0.00	0.00	0.00	
3782	-8326	-8902	36	1		0.00	22	0.00	0.00	0.00	0.00	
3783	-7509	-8326	36	1		0.00	22	0.00	0.00	0.00	0.00	
3784	-7510	-8327	36	1		0.00	22	0.00	0.00	0.00	0.00	
3785	-6494	-7510	36	1		0.00	22	0.00	0.00	0.00	0.00	
3786	-6493	-7509	36	1		0.00	22	0.00	0.00	0.00	0.00	
3787	-5854	-6493	36	1		0.00	22	0.00	0.00	0.00	0.00	
3788	-5855	-6494	36	1		0.00	22	0.00	0.00	0.00	0.00	
3789	-4965	-5855	36	1		0.00	22	0.00	0.00	0.00	0.00	

3790	-4964	-5854	36	1	0.00	22	0.00	0.00	0.00	0.00	
3791	-4066	-4965	36	1	0.00	22	0.00	0.00	0.00	0.00	
3792	-4065	-4964	36	1	0.00	22	0.00	0.00	0.00	0.00	
3793	-3440	-4065	36	1	0.00	22	0.00	0.00	0.00	0.00	
3794	-3441	-4066	36	1	0.00	22	0.00	0.00	0.00	0.00	
3795	-2464	-2750	32	1	0.00	55	0.00	0.00	0.00	0.00	
3795	-2750	-3441	33	1	0.00	55	0.00	0.00	0.00	0.00	
3795	-3441	-5817	34	1	0.00	55	0.00	0.00	0.00	0.00	
3795	-5817	-8911	34	1	0.00	55	0.00	0.00	0.00	0.00	
3796	-2463	-2749	32	1	0.00	55	0.00	0.00	0.00	0.00	
3796	-2749	-3440	33	1	0.00	55	0.00	0.00	0.00	0.00	
3796	-3440	-5807	34	1	0.00	55	0.00	0.00	0.00	0.00	
3796	-5807	-8907	34	1	0.00	55	0.00	0.00	0.00	0.00	
3797	-2487	-8539	39	13	0.00	55	0.00	0.00	0.00	0.00	
3798	-2486	-8537	39	13	0.00	55	0.00	0.00	0.00	0.00	
3799	-9376	-8917	53	13	0.00	22	0.00	0.00	0.00	0.00	
3800	-9374	-8901	53	13	0.00	22	0.00	0.00	0.00	0.00	
3801	-8729	-9368	36	1	0.00	22	0.00	0.00	0.00	0.00	
3802	-8730	-9382	36	1	0.00	22	0.00	0.00	0.00	0.00	
3803	-7984	-8729	36	1	0.00	22	0.00	0.00	0.00	0.00	
3804	-7985	-8730	36	1	0.00	22	0.00	0.00	0.00	0.00	
3805	-6926	-7984	36	1	0.00	22	0.00	0.00	0.00	0.00	
3806	-6927	-7985	36	1	0.00	22	0.00	0.00	0.00	0.00	
3807	-6269	-6927	36	1	0.00	22	0.00	0.00	0.00	0.00	
3808	-6259	-6926	36	1	0.00	22	0.00	0.00	0.00	0.00	
3809	-5356	-6259	36	1	0.00	22	0.00	0.00	0.00	0.00	
3810	-5357	-6269	36	1	0.00	22	0.00	0.00	0.00	0.00	
3811	-4322	-5356	36	1	0.00	22	0.00	0.00	0.00	0.00	
3812	-4323	-5357	36	1	0.00	22	0.00	0.00	0.00	0.00	
3813	-3675	-4323	36	1	0.00	22	0.00	0.00	0.00	0.00	
3814	-3674	-4322	36	1	0.00	22	0.00	0.00	0.00	0.00	
3815	-2486	-2806	32	1	0.00	55	0.00	0.00	0.00	0.00	
3815	-2806	-3674	33	1	0.00	55	0.00	0.00	0.00	0.00	
3815	-3674	-6221	34	1	0.00	55	0.00	0.00	0.00	0.00	
3815	-6221	-9373	34	1	0.00	55	0.00	0.00	0.00	0.00	
3816	-2487	-2807	32	1	0.00	55	0.00	0.00	0.00	0.00	
3816	-2807	-3675	33	1	0.00	55	0.00	0.00	0.00	0.00	
3816	-3675	-6230	34	1	0.00	55	0.00	0.00	0.00	0.00	
3816	-6230	-9377	34	1	0.00	55	0.00	0.00	0.00	0.00	
3817	-2541	-8982	50	13	0.00	55	0.00	0.00	0.00	0.00	
3818	-2539	-8984	50	13	0.00	55	0.00	0.00	0.00	0.00	
3819	-9727	-9367	53	13	0.00	22	0.00	0.00	0.00	0.00	
3820	-9740	-9383	53	13	0.00	22	0.00	0.00	0.00	0.00	
3821	-9218	-9746	36	1	0.00	22	0.00	0.00	0.00	0.00	
3822	-9217	-9735	36	1	0.00	22	0.00	0.00	0.00	0.00	
3823	-8434	-9217	36	1	0.00	22	0.00	0.00	0.00	0.00	
3824	-8435	-9218	36	1	0.00	22	0.00	0.00	0.00	0.00	
3825	-7309	-8434	36	1	0.00	22	0.00	0.00	0.00	0.00	
3826	-7310	-8435	36	1	0.00	22	0.00	0.00	0.00	0.00	
3827	-6700	-7310	36	1	0.00	22	0.00	0.00	0.00	0.00	
3828	-6699	-7309	36	1	0.00	22	0.00	0.00	0.00	0.00	
3829	-5766	-6700	36	1	0.00	22	0.00	0.00	0.00	0.00	
3830	-5784	-6699	36	1	0.00	22	0.00	0.00	0.00	0.00	
3831	-4759	-5766	36	1	0.00	22	0.00	0.00	0.00	0.00	
3832	-4758	-5784	36	1	0.00	22	0.00	0.00	0.00	0.00	
3833	-3956	-4758	36	1	0.00	22	0.00	0.00	0.00	0.00	
3834	-3969	-4759	36	1	0.00	22	0.00	0.00	0.00	0.00	
3837	-2541	-2872	32	1	0.00	55	0.00	0.00	0.00	0.00	
3837	-2872	-3956	33	1	0.00	55	0.00	0.00	0.00	0.00	
3837	-3956	-6659	34	1	0.00	55	0.00	0.00	0.00	0.00	
3837	-6659	-9739	34	1	0.00	55	0.00	0.00	0.00	0.00	
3838	-2539	-2873	32	1	0.00	55	0.00	0.00	0.00	0.00	
3838	-2873	-3969	33	1	0.00	55	0.00	0.00	0.00	0.00	
3838	-3969	-6660	34	1	0.00	55	0.00	0.00	0.00	0.00	
3838	-6660	-9741	34	1	0.00	55	0.00	0.00	0.00	0.00	
3839	-10251	-9747	53	13	0.00	22	0.00	0.00	0.00	0.00	
3840	-10249	-9734	53	13	0.00	22	0.00	0.00	0.00	0.00	
3843	-9609	-10256	36	1	0.00	22	0.00	0.00	0.00	0.00	
3844	-9608	-10244	36	1	0.00	22	0.00	0.00	0.00	0.00	
3845	-8919	-9609	36	1	0.00	22	0.00	0.00	0.00	0.00	
3846	-8918	-9608	36	1	0.00	22	0.00	0.00	0.00	0.00	
3847	-7727	-8918	36	1	0.00	22	0.00	0.00	0.00	0.00	
3848	-7728	-8919	36	1	0.00	22	0.00	0.00	0.00	0.00	
3849	-7157	-7728	36	1	0.00	22	0.00	0.00	0.00	0.00	
3850	-7156	-7727	36	1	0.00	22	0.00	0.00	0.00	0.00	
3851	-6174	-7156	36	1	0.00	22	0.00	0.00	0.00	0.00	
3852	-6175	-7157	36	1	0.00	22	0.00	0.00	0.00	0.00	
3853	-5131	-6175	36	1	0.00	22	0.00	0.00	0.00	0.00	
3854	-5130	-6174	36	1	0.00	22	0.00	0.00	0.00	0.00	

3855	-4235	-5130	36	1		0.00	22	0.00	0.00	0.00	0.00	
3856	-4236	-5131	36	1		0.00	22	0.00	0.00	0.00	0.00	
3997	-4538	-4540	61	1		0.00	33	0.00	0.00	0.00	0.00	
3997	-4531	-4538	61	1		0.00	33	0.00	0.00	0.00	0.00	
3997	-4527	-4531	61	1		0.00	33	0.00	0.00	0.00	0.00	
3999	-4525	-4527	61	1		0.00	33	0.00	0.00	0.00	0.00	
3999	-4524	-4525	61	1		0.00	33	0.00	0.00	0.00	0.00	
4553	-3065	-3360	36	1		0.00	22	0.00	0.00	0.00	0.00	
4568	-3473	-4223	36	1		0.00	22	0.00	0.00	0.00	0.00	
5351	-3360	-3949	36	1		0.00	22	0.00	0.00	0.00	0.00	
5366	-3359	-3955	36	1		0.00	22	0.00	0.00	0.00	0.00	
6149	-3474	-4224	36	1		0.00	22	0.00	0.00	0.00	0.00	
6164	-3193	-3473	36	1		0.00	22	0.00	0.00	0.00	0.00	
6947	-4463	-5459	36	1		0.00	22	0.00	0.00	0.00	0.00	
6962	-3064	-3359	36	1		0.00	22	0.00	0.00	0.00	0.00	

Elenco tipi elementi bidimensionali

Simbologia

- Tb = Numero del tipo muro/elemento bidimensionale
 Comm. = Commento
 Tipo = Tipologia
 F = Membranale e Flessionale
 M = Membranale
 W-RC = Winkler resistente solo a compressione
 W-RTC = Winkler resistente a trazione e a compressione
 Uso = Utilizzo
 G = Generico
 P = Parete
 S = Soletta/Platea
 N = Nucleo
 M = Muratura ordinaria
 L = Pilastro
 MA = Muratura armata
 X = Pannello X-LAM
 Spess. = Spessore
 Kt = Coeff. di sottofondo su suolo elastico alla Winkler
 DP = Drucker-Prager
 Ang. att. = Angolo di attrito
 Coes. = Coesione
 Zcv = Quota di riferimento del piano di campagna
 Crit. = Numero del criterio di progetto
 Mat. = Numero del materiale

Tb	Comm.	Tipo	Uso	Spess. <cm>	Kt <daN/cm>	DP	Ang. att. <grad>	Coes. <daN/mq>	Zcv <m>	Crit.	Mat.
25	Lamiera acciaio sp. 6 mm	F	G	0.60		N	0.00	0.00	4.20	3	18
28	Lamiera sp. 4.0 mm + Leca cls1600 sp. 50 mm (t = 0)	F	G	0.81		N	0.00	0.00	4.20	3	18
30	Parete tubo acciaio sp. 7 mm + Leca cls1600 sp.50 mm (t=0)	F	G	1.11		N	0.00	0.00	4.20	1	18
32	Parete tubo campata sud - sp. 6 mm	F	G	0.60		N	0.00	0.00	4.20	1	18
34	Lamiera ali a sbalzo sp. 4 mm	F	G	0.40		N	0.00	0.00	4.20	3	18
38	Parete tubo becco sud - sp. 6 mm	F	G	0.60		N	0.00	0.00	4.20	1	18

Elenco elementi bidimensionali

Simbologia

- Bid. = Numero del muro/elemento bidimensionale
 Tb = Numero del tipo muro/elemento bidimensionale
 FF = Filo fisso
 Dy1 = Scost. filo fisso Y1
 Dy2 = Scost. filo fisso Y2
 Kt = Coeff. di sottofondo su suolo elastico alla Winkler
 NN = Nodi

Bid.	Tb	FF	Dy1 <cm>	Dy2 <cm>	Kt <daN/cm>	NN			
2517	32	22	0.00	0.00		-2574	-2573	-2576	-2577
2517	32	22	0.00	0.00		-2573	-2572	-2575	-2576
2517	32	22	0.00	0.00		-2597	-2596	-2606	-2607
2517	32	22	0.00	0.00		-2567	-2566	-2573	-2574
2517	32	22	0.00	0.00		-2583	-2582	-2593	-2594
2517	32	22	0.00	0.00		-2584	-2583	-2594	-2595
2517	32	22	0.00	0.00		-2576	-2575	-2579	-2580
2517	32	22	0.00	0.00		-2577	-2576	-2580	-2581
2517	32	22	0.00	0.00		-2566	-2565	-2572	-2573
2517	32	22	0.00	0.00		-2598	-2597	-2607	-2608
2517	32	22	0.00	0.00		-2626	-2625	-2635	-2636
2517	32	22	0.00	0.00		-2618	-2617	-2626	-2627
2517	32	22	0.00	0.00		-2627	-2626	-2636	-2637
2517	32	22	0.00	0.00		-2607	-2606	-2616	-2617
2517	32	22	0.00	0.00		-2608	-2607	-2617	-2618
2517	32	22	0.00	0.00		-2594	-2593	-2596	-2597

2517	32	22	0.00	0.00		-2595	-2594	-2597	-2598
2517	32	22	0.00	0.00		-2617	-2616	-2625	-2626
2517	32	22	0.00	0.00		-2581	-2580	-2583	-2584
2517	32	22	0.00	0.00		-2580	-2579	-2582	-2583
2718	32	22	0.00	0.00		-2805	-2804	-2814	-2815
2718	32	22	0.00	0.00		-2823	-2822	-2845	-2846
2718	32	22	0.00	0.00		-3859	-3858	-3909	-3910
2718	32	22	0.00	0.00		-3676	-3664	-3712	-3719
2718	32	22	0.00	0.00		-3665	-3676	-3719	-3720
2718	32	22	0.00	0.00		-2787	-2786	-2796	-2797
2718	32	22	0.00	0.00		-2734	-2733	-2740	-2741
2718	32	22	0.00	0.00		-3572	-3571	-3610	-3611
2718	32	22	0.00	0.00		-2804	-2803	-2813	-2814
2718	32	22	0.00	0.00		-3719	-3712	-3768	-3769
2718	32	22	0.00	0.00		-3720	-3719	-3769	-3765
2718	32	22	0.00	0.00		-3610	-3609	-3664	-3676
2718	32	22	0.00	0.00		-3191	-3187	-3206	-3212
2718	32	22	0.00	0.00		-3115	-3114	-3133	-3134
2718	32	22	0.00	0.00		-3571	-3570	-3609	-3610
2718	32	22	0.00	0.00		-2822	-2821	-2840	-2845
2718	32	22	0.00	0.00		-2931	-2930	-2953	-2954
2718	32	22	0.00	0.00		-2898	-2897	-2909	-2910
2718	32	22	0.00	0.00		-2899	-2898	-2910	-2911
2718	32	22	0.00	0.00		-2882	-2881	-2891	-2892
2718	32	22	0.00	0.00		-2883	-2882	-2892	-2893
2718	32	22	0.00	0.00		-2845	-2840	-2853	-2854
2718	32	22	0.00	0.00		-2893	-2892	-2898	-2899
2718	32	22	0.00	0.00		-2863	-2862	-2870	-2871
2718	32	22	0.00	0.00		-2862	-2859	-2869	-2870
2718	32	22	0.00	0.00		-3206	-3205	-3233	-3226
2718	32	22	0.00	0.00		-2758	-2757	-2763	-2764
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2718	32	22	0.00	0.00		-2653	-2652	-2659	-2660
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2718	32	22	0.00	0.00		-3042	-3041	-3067	-3068
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2718	32	22	0.00	0.00		-2980	-2979	-2986	-2987
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2718	32	22	0.00	0.00		-2968	-2967	-2979	-2980
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2718	32	22	0.00	0.00		-3409	-3408	-3429	-3430
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2718	32	22	0.00	0.00		-3858	-3857	-3908	-3909
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2718	32	22	0.00	0.00		-3187	-3190	-3205	-3206
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2718	32	22	0.00	0.00		-3226	-3233	-3242	-3243
2718	32	22	0.00	0.00		-3261	-3260	-3281	-3282
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2718	32	22	0.00	0.00		-2764	-2763	-2769	-2770
2718	32	22	0.00	0.00		-3134	-3133	-3148	-3149
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2718	32	22	0.00	0.00		-2636	-2635	-2645	-2646
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2719	38	11	0.00	0.00		-3144	-3167	-2669	-2622
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2719	32	22	0.00	0.00		-5321	-3183	-3153	-5375
2719	32	22	0.00	0.00		-3403	-2739	-2746	-3424
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2719	32	22	0.00	0.00		-5500	-3200	-3258	-5595
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2719	32	22	0.00	0.00		-3842	-2853	-2859	-3904
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2720	32	22	0.00	0.00		-4816	-3212	-3227	-5002
2720	38	11	0.00	0.00		-2587	-2913	-3418	-3174
2720	32	22	0.00	0.00		-5045	-3009	-3081	-5122
2720	38	11	0.00	0.00		-3204	-2711	-2671	-3168
2720	32	22	0.00	0.00		-4928	-3061	-3031	-4970
2720	32	22	0.00	0.00		-3252	-2714	-2722	-3325
2720	32	22	0.00	0.00		-5287	-3311	-3345	-5216
2720	32	22	0.00	0.00		-5377	-3159	-3137	-5439
2720	32	22	0.00	0.00		-3061	-2584	-2595	-3031
2720	32	22	0.00	0.00		-5323	-3184	-3159	-5377
2720	38	11	0.00	0.00		-4668	-4651	-3145	-3174
2720	32	22	0.00	0.00		-5355	-3283	-3311	-5287
2720	32	22	0.00	0.00		-3009	-2598	-2608	-3081
2720	32	22	0.00	0.00		-4418	-3068	-3093	-4363
2720	32	22	0.00	0.00		-3269	-2702	-2714	-3252
2720	32	22	0.00	0.00		-3278	-2684	-2691	-3306
2720	32	22	0.00	0.00		-3591	-2815	-2823	-3537
2720	38	11	0.00	0.00		-4651	-4634	-3168	-3145
2720	32	22	0.00	0.00		-4842	-3135	-3150	-4887
2720	32	22	0.00	0.00		-3020	-2577	-2581	-3037
2720	32	22	0.00	0.00		-3425	-2748	-2759	-3399
2720	32	22	0.00	0.00		-3161	-2627	-2637	-3184
2720	32	22	0.00	0.00		-3201	-2661	-2677	-3259
2720	32	22	0.00	0.00		-3888	-2883	-2893	-3826
2720	32	22	0.00	0.00		-4807	-3020	-3037	-4862
2720	32	22	0.00	0.00		-3537	-2823	-2846	-3699
2720	32	22	0.00	0.00		-5207	-3147	-3161	-5272
2720	32	22	0.00	0.00		-5255	-3244	-3262	-5305
2720	32	22	0.00	0.00		-3843	-2855	-2863	-3905
2720	32	22	0.00	0.00		-4970	-3031	-3009	-5045
2720	32	22	0.00	0.00		-3306	-2691	-2702	-3269
2720	32	22	0.00	0.00		-5272	-3161	-3184	-5323
2720	32	22	0.00	0.00		-3184	-2637	-2647	-3159
2720	32	22	0.00	0.00		-5666	-3278	-3306	-5741
2720	32	22	0.00	0.00		-3137	-2654	-2661	-3201
2720	32	22	0.00	0.00		-3964	-2871	-2883	-3888
2720	32	22	0.00	0.00		-3081	-2608	-2618	-3147
2720	32	22	0.00	0.00		-3147	-2618	-2627	-3161
2720	32	22	0.00	0.00		-5002	-3227	-3244	-5255
2720	32	22	0.00	0.00		-4125	-2911	-2931	-4168
2720	38	11	0.00	0.00		-4691	-4668	-3174	-3418

2805	25	22	0.00	0.00		-4236	-3448	-3763	-5257
2805	25	22	0.00	0.00		-3448	-3090	-3089	-3763
2805	25	22	0.00	0.00		-3089	-3088	-4003	-3763
2805	25	22	0.00	0.00		-3088	-3087	-4002	-4003
2805	25	22	0.00	0.00		-3766	-3442	-4235	-5256
2805	25	22	0.00	0.00		-3084	-3083	-3766	-3999
2805	25	22	0.00	0.00		-3086	-3085	-4000	-4001
2805	25	22	0.00	0.00		-3083	-3082	-3442	-3766
2805	25	22	0.00	0.00		-3087	-3086	-4001	-4002
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2812	34	22	0.00	0.00		-4688	-3569	-3550	-4687
2812	34	22	0.00	0.00		-3054	-2877	-3101	
2812	34	22	0.00	0.00		-3078	-2591	-2718	-3054
2812	34	22	0.00	0.00		-2912	-2867	-3370	-3417
2812	34	22	0.00	0.00		-2867	-2591	-3078	
2812	34	22	0.00	0.00		-3054	-2718	-2877	
2812	34	22	0.00	0.00		-3054	-3101	-3273	
2812	34	22	0.00	0.00		-2867	-3078	-3569	-3370
2812	34	22	0.00	0.00		-3417	-3370	-4688	-4689
2812	34	22	0.00	0.00		-3569	-3078	-3054	-3550
2812	34	22	0.00	0.00		-3370	-3569	-4688	
2813	34	22	0.00	0.00		-2950	-3198	2901	
2813	34	22	0.00	0.00		2901	-3198	-3181	-5042
2813	34	22	0.00	0.00		-3181	-2778	-2963	
2813	34	22	0.00	0.00		-3008	-2950	2901	-5043
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2813	34	22	0.00	0.00		-2950	-2643	-3198	
2813	34	22	0.00	0.00		-3198	-2643	-2778	-3181
2813	34	22	0.00	0.00		-3181	-2963	-3217	
2814	34	22	0.00	0.00		-3136	-3038	-5436	-5437
2814	34	22	0.00	0.00		-3303	-3348	-3588	
2814	34	22	0.00	0.00		-3322	-2698	-2843	-3303
2814	34	22	0.00	0.00		-3038	-2698	-3322	
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2814	34	22	0.00	0.00		-3303	-2843	-3062	
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2815	34	22	0.00	0.00		-3450	-2755	-2904	-3422
2815	34	22	0.00	0.00		-3422	-3185	-3467	
2815	34	22	0.00	0.00		-3162	-3450	-5841	
2815	34	22	0.00	0.00		-3162	-2755	-3450	
2815	34	22	0.00	0.00		-3422	-2904	-3185	
2815	34	22	0.00	0.00		-3422	-3467	-3885	
2816	34	22	0.00	0.00		-3655	-3307	-3748	
2816	34	22	0.00	0.00		-3279	-3696	-6244	
2816	34	22	0.00	0.00		-3279	-2811	-3696	
2816	34	22	0.00	0.00		-3696	-2811	-2991	-3655
2816	34	22	0.00	0.00		-3655	-2991	-3307	
2816	34	22	0.00	0.00		-3655	-3748	-4148	
2817	34	22	0.00	0.00		-3947	-4038	-4403	
2817	34	22	0.00	0.00		-3405	-2879	-3985	
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2817	34	22	0.00	0.00		-3985	-2879	-3120	-3947
2820	32	22	0.00	0.00		-5701	-3390	-3407	-5783
2820	32	22	0.00	0.00		-5620	-3376	-3390	-5701
2820	32	22	0.00	0.00		-5605	-3458	-3475	-5808
2820	32	22	0.00	0.00		-5783	-3407	-3428	-5689
2820	32	22	0.00	0.00		-5689	-3428	-3458	-5605
2820	32	22	0.00	0.00		-5387	-3361	-3376	-5620
2821	32	22	0.00	0.00		-5740	-3305	-3274	-5796
2821	32	22	0.00	0.00		-5884	-3324	-3384	-5993
2821	32	22	0.00	0.00		-5796	-3274	-3251	-5842
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2821	32	22	0.00	0.00		-5993	-3384	-3403	-6066
2822	34	22	0.00	0.00		-4219	-3663	-4295	
2822	34	22	0.00	0.00		-4219	-3224	-3663	
2822	34	22	0.00	0.00		-3607	-2965	-4251	
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2823	32	22	0.00	0.00		-5844	-3252	-3325	-5886
2823	32	22	0.00	0.00		-5741	-3306	-3269	-5798
2823	32	22	0.00	0.00		-5886	-3325	-3385	-6025
2823	32	22	0.00	0.00		-5798	-3269	-3252	-5844
2823	32	22	0.00	0.00		-6025	-3385	-3404	-6068
2824	32	22	0.00	0.00		-5774	-3409	-3430	-5690
2824	32	22	0.00	0.00		-5606	-3460	-3477	-5818
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2824	32	22	0.00	0.00		-5398	-3356	-3371	-5621
2824	32	22	0.00	0.00		-5702	-3392	-3409	-5774
2824	32	22	0.00	0.00		-5621	-3371	-3392	-5702

2825	34	22	0.00	0.00		-3906	-3064	-4492
2825	34	22	0.00	0.00		-4459	-3359	-3955
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2826	34	22	0.00	0.00		-5013	-3193	-3473 -4950
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2834	34	22	0.00	0.00		-3055	-2878	-2719
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2834	34	22	0.00	0.00		-3079	-2868	-3375
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2835	34	22	0.00	0.00		-2951	-3009	-5045 2902
2835	34	22	0.00	0.00		-3199	-2951	2902
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2841	34	22	0.00	0.00		-3323	-3039	-5440
2841	34	22	0.00	0.00		-3063	-3349	-3304
2841	34	22	0.00	0.00		-2844	-2699	-3323 -3304
2841	34	22	0.00	0.00		-3589	-3349	-3304
2841	34	22	0.00	0.00		-3039	-3137	-5439 -5440
2841	34	22	0.00	0.00		-2699	-3039	-3323
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2842	34	22	0.00	0.00		-2905	-2756	-3451 -3423
2842	34	22	0.00	0.00		-3423	-3186	-2905
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2843	34	22	0.00	0.00		-2992	-2812	-3697 -3656
2843	34	22	0.00	0.00		-4149	-3749	-3656
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2847	34	22	0.00	0.00		-4404	-4039	-3948
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2847	34	22	0.00	0.00		-2880	-3406	-3986
2848	34	22	0.00	0.00		-2966	-3608	-4252
2848	34	22	0.00	0.00		-4220	-3659	-3225
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2849	34	22	0.00	0.00		-3360	-3065	-4493 -4460
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2849	34	22	0.00	0.00		-3065	-3907	-4493
2850	34	22	0.00	0.00		-4951	-4224	-3474
2850	34	22	0.00	0.00		-3189	-4170	-5014
2850	34	22	0.00	0.00		-3474	-3189	-5014 -4951
2921	34	22	0.00	0.00		-4198	-4683	-4684
2921	34	22	0.00	0.00		-4198	-4684	-4685 -3732
2924	34	22	0.00	0.00		-5436	-3322	-3303 -5435
2925	34	22	0.00	0.00		-3251	-3162	-5841 -5842
2928	34	22	0.00	0.00		-3405	-3985	-6670
2931	32	22	0.00	0.00		-6191	-3398	-3378 -6238
2931	32	22	0.00	0.00		-6238	-3378	-3452 -6302
2931	32	22	0.00	0.00		-6370	-3558	-3605 -6483
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2931	32	22	0.00	0.00		-6066	-3403	-3424 -6134
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2932	38	11	0.00	0.00		-2623	-2622	-2669 -2670
2932	38	11	0.00	0.00		-2670	-2669	-2709 -2710
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2933	32	22	0.00	0.00		-6102	-3664	-3712 -6001
2933	32	22	0.00	0.00		-6036	-3523	-3570 -6104
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2934	34	22	0.00	0.00		-4219	-4295	-4870	
2935	28	22	0.00	0.00		-4670	-4653	-4655	-4672
2935	28	22	0.00	0.00		-4676	-4661	-4663	-4679
2935	28	22	0.00	0.00		-4804	-4747	-4746	-4803
2935	28	22	0.00	0.00		-4746	-4687	-4686	-4745
2935	28	22	0.00	0.00		-4858	-4803	-4802	-4857
2935	28	22	0.00	0.00		-4676	-4674	-4657	-4661
2935	28	22	0.00	0.00		-4864	-4809	-4808	-4863
2935	28	22	0.00	0.00		-4671	-4654	-4652	-4669
2935	28	22	0.00	0.00		-4747	-4688	-4687	-4746
2935	30	22	0.00	0.00		-4690	-4689	-4748	-4749
2935	28	22	0.00	0.00		-4697	-4680	-4677	-4696
2935	28	22	0.00	0.00		-4672	-4655	-4657	-4674
2935	28	22	0.00	0.00		-4855	-4800	-4799	-4854
2935	28	22	0.00	0.00		-4803	-4746	-4745	-4802
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2935	28	22	0.00	0.00		-4754	-4695	-4694	-4753
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2935	28	22	0.00	0.00		-4755	-4696	-4695	-4754
2935	28	22	0.00	0.00		-4813	-4756	-4755	-4812
2935	28	22	0.00	0.00		-4802	-4745	-4744	-4801
2935	28	22	0.00	0.00		-4656	-4673	-4675	-4658
2935	28	22	0.00	0.00		-4812	-4755	-4754	-4811
2935	28	22	0.00	0.00		-4867	-4812	-4811	-4866
2935	28	22	0.00	0.00		-4748	-4689	-4688	-4747
2935	28	22	0.00	0.00		-4666	-4649	-4648	-4665
2935	28	22	0.00	0.00		-4688	-4665	-4670	-4687
2935	28	22	0.00	0.00		-4694	-4695	-4675	-4673
2935	28	22	0.00	0.00		-4698	-4681	-4680	-4697
2935	30	22	0.00	0.00		-4749	-4748	-4805	-4806
2935	28	22	0.00	0.00		-4752	-4693	-4692	-4751
2935	28	22	0.00	0.00		-4809	-4752	-4751	-4808
2935	28	22	0.00	0.00		-4751	-4692	-4691	-4750
2935	30	22	0.00	0.00		-4807	-4806	-4861	-4862
2935	28	22	0.00	0.00		-4745	-4686	-4685	-4744
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2935	28	22	0.00	0.00		-4857	-4802	-4801	-4856
2935	28	22	0.00	0.00		-4667	-4650	-4649	-4666
2935	28	22	0.00	0.00		-4689	-4666	-4665	-4688
2935	28	22	0.00	0.00		-4810	-4753	-4752	-4809
2935	28	22	0.00	0.00		-4686	-4687	-4670	-4672
2935	28	22	0.00	0.00		-4856	-4801	-4800	-4855
2935	28	22	0.00	0.00		-4668	-4651	-4650	-4667
2935	28	22	0.00	0.00		-4669	-4692	-4693	-4671
2935	28	22	0.00	0.00		-4665	-4648	-4653	-4670
2935	28	22	0.00	0.00		-4696	-4677	-4675	-4695
2935	28	22	0.00	0.00		-4744	-4685	-4684	-4743
2935	28	22	0.00	0.00		-4805	-4748	-4747	-4804
2935	28	22	0.00	0.00		-4756	-4697	-4696	-4755
2935	28	22	0.00	0.00		-4677	-4680	-4664	-4662
2935	28	22	0.00	0.00		-4686	-4672	-4674	-4685
2935	28	22	0.00	0.00		-4681	-4660	-4664	-4680
2935	28	22	0.00	0.00		-4753	-4694	-4693	-4752
2935	28	22	0.00	0.00		-4684	-4685	-4674	-4676
2935	28	22	0.00	0.00		-4656	-4654	-4671	-4673
2935	30	22	0.00	0.00		-4750	-4749	-4806	-4807
2935	28	22	0.00	0.00		-4690	-4667	-4666	-4689
2935	28	22	0.00	0.00		-4742	-4683	-4682	-4741
2935	28	22	0.00	0.00		-4868	-4813	-4812	-4867
2935	28	22	0.00	0.00		-4808	-4751	-4750	-4807
2935	28	22	0.00	0.00		-4866	-4811	-4810	-4865
2935	28	22	0.00	0.00		-4691	-4668	-4667	-4690
2935	28	22	0.00	0.00		-4694	-4673	-4671	-4693
2935	30	22	0.00	0.00		-4691	-4690	-4749	-4750
2935	28	22	0.00	0.00		-4801	-4744	-4743	-4800
2935	28	22	0.00	0.00		-4865	-4810	-4809	-4864
2935	28	22	0.00	0.00		-4814	-4757	-4756	-4813
2935	28	22	0.00	0.00		-4659	-4678	-4679	-4663
2935	28	22	0.00	0.00		-4869	-4814	-4813	-4868
2935	28	22	0.00	0.00		-4811	-4754	-4753	-4810
2935	28	22	0.00	0.00		-4799	-4742	-4741	-4798
2935	28	22	0.00	0.00		-4854	-4799	-4798	-4853
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2935	28	22	0.00	0.00		-4757	-4698	-4697	-4756
2935	28	22	0.00	0.00		-4743	-4684	-4683	-4742
2935	28	22	0.00	0.00		-4677	-4662	-4658	-4675
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2935	28	22	0.00	0.00		-4800	-4743	-4742	-4799
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2936	38	11	0.00	0.00		-4620	-4596	-2820	-3204
2936	38	11	0.00	0.00		-4543	-4530	-4018	-3457
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2937	32	22	0.00	0.00		-6246	-3379	-3453	-6304
2937	32	22	0.00	0.00		-6193	-3399	-3379	-6246
2937	32	22	0.00	0.00		-6136	-3425	-3399	-6193
2937	32	22	0.00	0.00		-6372	-3559	-3606	-6485
2937	32	22	0.00	0.00		-6068	-3404	-3425	-6136
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2938	38	11	0.00	0.00		-4559	-4542	-3456	-3203
2938	38	11	0.00	0.00		-4542	-4529	-4017	-3456
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2939	32	22	0.00	0.00		-6173	-3611	-3665	-6103
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2942	38	11	0.00	0.00		-4623	-4622	-3730	-3731
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2943	38	11	0.00	0.00		-3728	-3718	-3211	
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2950	34	22	0.00	0.00		-3304	-3323	-5440	-5441
2951	34	22	0.00	0.00		-3163	-3252	-5844	-5845
2952	34	22	0.00	0.00		-3986	-3406	-6673	
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3131	28	22	0.00	0.00		-5661	-5592	-5591	-5660
3131	28	22	0.00	0.00		-5734	-5669	-5668	-5742
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3131	28	22	0.00	0.00		-5497	-5434	-5433	-5496
3131	28	22	0.00	0.00		-5201	-5116	-5115	-5200
3131	30	22	0.00	0.00		-5206	-5205	-5270	-5271
3131	30	22	0.00	0.00		-5207	-5206	-5271	-5272
3131	28	22	0.00	0.00		-5327	-5276	-5275	-5326
3131	28	22	0.00	0.00		-5436	-5374	-5373	-5435
3131	28	22	0.00	0.00		-5276	-5211	-5210	-5275
3131	28	22	0.00	0.00		-5727	-5659	-5658	-5726
3131	28	22	0.00	0.00		-5590	-5495	-5494	-5589
3131	30	22	0.00	0.00		-5045	-5044	-5121	-5122
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3131	28	22	0.00	0.00		-5275	-5210	-5209	-5274
3131	28	22	0.00	0.00		-5446	-5384	-5383	-5445
3131	28	22	0.00	0.00		-5125	-5047	-5046	-5124
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3131	28	22	0.00	0.00		-5440	-5378	-5377	-5439
3131	28	22	0.00	0.00		-5274	-5209	-5208	-5273
3131	28	22	0.00	0.00		-5499	-5436	-5435	-5498
3131	28	22	0.00	0.00		-5265	-5200	-5199	-5264
3131	28	22	0.00	0.00		-5316	-5265	-5264	-5315
3131	28	22	0.00	0.00		-5794	-5730	-5729	-5793
3131	28	22	0.00	0.00		-5273	-5208	-5207	-5272
3131	28	22	0.00	0.00		-5279	-5214	-5213	-5278
3131	28	22	0.00	0.00		-5670	-5601	-5600	-5669
3131	28	22	0.00	0.00		-5601	-5506	-5505	-5600
3131	28	22	0.00	0.00		-5278	-5213	-5212	-5277
3131	28	22	0.00	0.00		-5369	-5315	-5314	-5368
3131	28	22	0.00	0.00		-5213	-5128	-5127	-5212

3131	28	22	0.00	0.00		-5270	-5205	-5204	-5269
3131	28	22	0.00	0.00		-5264	-5199	-5198	-5263
3131	28	22	0.00	0.00		-5328	-5277	-5276	-5327
3131	28	22	0.00	0.00		-5382	-5328	-5327	-5381
3131	30	22	0.00	0.00		-5377	-5376	-5438	-5439
3131	28	22	0.00	0.00		-5792	-5728	-5727	-5791
3131	28	22	0.00	0.00		-5212	-5127	-5126	-5211
3131	28	22	0.00	0.00		-5127	-5049	-5048	-5126
3131	28	22	0.00	0.00		-5443	-5381	-5380	-5442
3131	28	22	0.00	0.00		-5373	-5319	-5318	-5372
3131	28	22	0.00	0.00		-5791	-5727	-5726	-5790
3131	28	22	0.00	0.00		-5268	-5203	-5202	-5267
3131	30	22	0.00	0.00		-5501	-5500	-5595	-5596
3131	28	22	0.00	0.00		-5380	-5326	-5325	-5379
3131	28	22	0.00	0.00		-5495	-5432	-5431	-5494
3131	28	22	0.00	0.00		-5790	-5726	-5725	-5789
3131	28	22	0.00	0.00		-5796	-5740	-5731	-5795
3131	28	22	0.00	0.00		-5726	-5658	-5657	-5725
3131	28	22	0.00	0.00		-5595	-5500	-5499	-5594
3131	28	22	0.00	0.00		-5371	-5317	-5316	-5370
3131	28	22	0.00	0.00		-5494	-5431	-5430	-5493
3131	28	22	0.00	0.00		-5441	-5379	-5378	-5440
3131	28	22	0.00	0.00		-5266	-5201	-5200	-5265
3131	30	22	0.00	0.00		-5666	-5665	-5732	-5741
3131	30	22	0.00	0.00		-5272	-5271	-5322	-5323
3131	28	22	0.00	0.00		-5324	-5273	-5272	-5323
3131	28	22	0.00	0.00		-5507	-5444	-5443	-5506
3131	28	22	0.00	0.00		-5330	-5279	-5278	-5329
3131	28	22	0.00	0.00		-5124	-5046	2902	-5123
3131	30	22	0.00	0.00		-5502	-5501	-5596	-5597
3131	30	22	0.00	0.00		-5732	-5740	-5796	-5797
3131	28	22	0.00	0.00		-5383	-5329	-5328	-5382
3131	28	22	0.00	0.00		-5329	-5278	-5277	-5328
3131	28	22	0.00	0.00		-5205	-5120	-5119	-5204
3131	28	22	0.00	0.00		-5506	-5443	-5442	-5505
3131	28	22	0.00	0.00		-5321	-5270	-5269	-5320
3131	28	22	0.00	0.00		-5374	-5320	-5319	-5373
3131	28	22	0.00	0.00		-5199	-5114	-5113	-5198
3131	28	22	0.00	0.00		-5669	-5600	-5599	-5668
3131	30	22	0.00	0.00		-5376	-5375	-5437	-5438
3131	28	22	0.00	0.00		-5600	-5505	-5504	-5599
3131	28	22	0.00	0.00		-5326	-5275	-5274	-5325
3131	30	22	0.00	0.00		-5271	-5270	-5321	-5322
3131	28	22	0.00	0.00		-5599	-5504	-5503	-5598
3131	28	22	0.00	0.00		-5381	-5327	-5326	-5380
3131	28	22	0.00	0.00		-5211	-5126	-5125	-5210
3131	28	22	0.00	0.00		-5659	-5590	-5589	-5658
3131	28	22	0.00	0.00		-5673	-5604	-5603	-5672
3131	28	22	0.00	0.00		-5442	-5380	-5379	-5441
3131	28	22	0.00	0.00		-5317	-5266	-5265	-5316
3131	28	22	0.00	0.00		-5503	-5440	-5439	-5502
3131	28	22	0.00	0.00		-5509	-5446	-5445	-5508
3131	28	22	0.00	0.00		-5740	-5664	-5663	-5731
3131	28	22	0.00	0.00		-5202	-5117	-5116	-5201
3131	28	22	0.00	0.00		-5589	-5494	-5493	-5588
3131	28	22	0.00	0.00		-5433	-5371	-5370	-5432
3131	28	22	0.00	0.00		-5603	-5508	-5507	-5602
3131	30	22	0.00	0.00		-5596	-5595	-5664	-5665
3131	28	22	0.00	0.00		-5208	-5123	-5122	-5207
3131	28	22	0.00	0.00		-5602	-5507	-5506	-5601
3131	30	22	0.00	0.00		-5323	-5322	-5376	-5377
3131	28	22	0.00	0.00		-5378	-5324	-5323	-5377
3131	28	22	0.00	0.00		-5319	-5268	-5267	-5318
3131	28	22	0.00	0.00		-5742	-5668	-5667	-5733
3131	28	22	0.00	0.00		-5504	-5441	-5440	-5503
3131	28	22	0.00	0.00		-5114	-5038	-5037	-5113
3131	28	22	0.00	0.00		-5672	-5603	-5602	-5671
3131	28	22	0.00	0.00		-5431	-5369	-5368	-5430
3131	28	22	0.00	0.00		-5729	-5661	-5660	-5728
3131	28	22	0.00	0.00		-5793	-5729	-5728	-5792
3131	30	22	0.00	0.00		-5438	-5437	-5500	-5501
3131	28	22	0.00	0.00		-5267	-5202	-5201	-5266
3131	28	22	0.00	0.00		-5658	-5589	-5588	-5657
3131	28	22	0.00	0.00		-5209	-5124	-5123	-5208
3131	28	22	0.00	0.00		-5126	-5048	-5047	-5125
3131	28	22	0.00	0.00		-5118	-5042	-5041	-5117
3131	28	22	0.00	0.00		-5372	-5318	-5317	-5371
3131	30	22	0.00	0.00		-5122	-5121	-5206	-5207
3131	30	22	0.00	0.00		-5121	-5120	-5205	-5206

3131	28	22	0.00	0.00		-5668	-5599	-5598	-5667
3131	28	22	0.00	0.00		-5604	-5509	-5508	-5603
3131	28	22	0.00	0.00		-5598	-5503	-5502	-5597
3131	30	22	0.00	0.00		-5322	-5321	-5375	-5376
3131	28	22	0.00	0.00		-5117	-5041	-5040	-5116
3131	28	22	0.00	0.00		-5115	-5039	-5038	-5114
3131	28	22	0.00	0.00		-5733	-5667	-5666	-5741
3131	28	22	0.00	0.00		-5804	-5736	-5743	-5803
3131	28	22	0.00	0.00		-5318	-5267	-5266	-5317
3131	30	22	0.00	0.00		-5044	-5043	-5120	-5121
3131	28	22	0.00	0.00		-5667	-5598	-5597	-5666
3131	28	22	0.00	0.00		-5498	-5435	-5434	-5497
3131	28	22	0.00	0.00		-5593	-5498	-5497	-5592
3131	28	22	0.00	0.00		-5736	-5672	-5671	-5743
3131	28	22	0.00	0.00		-5384	-5330	-5329	-5383
3131	28	22	0.00	0.00		-5662	-5593	-5592	-5661
3131	28	22	0.00	0.00		-5444	-5382	-5381	-5443
3131	28	22	0.00	0.00		-5375	-5321	-5320	-5374
3131	28	22	0.00	0.00		-5434	-5372	-5371	-5433
3131	28	22	0.00	0.00		-5800	-5742	-5733	-5799
3131	28	22	0.00	0.00		-5799	-5733	-5741	-5798
3131	28	22	0.00	0.00		-5123	2902	-5045	-5122
3132	32	22	0.00	0.00		-6598	-3910	-3958	-6496
3132	32	22	0.00	0.00		-6496	-3958	-4002	-6382
3132	32	22	0.00	0.00		-6505	-3859	-3910	-6598
3133	32	22	0.00	0.00		-7139	-3826	-3988	-7202
3133	32	22	0.00	0.00		-7465	-4165	-4105	-7501
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3133	32	22	0.00	0.00		-6750	-3699	-3843	-6835
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3152	34	22	0.00	0.00		-3656	-3697	-6247	-6248
3153	34	22	0.00	0.00		-3406	-3537	-6672	-6673
3156	34	22	0.00	0.00		-4066	-3441	-5817	-5773
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3219	34	22	0.00	0.00		-4935	-5431	-5432	
3222	34	22	0.00	0.00		-5333	-5837	-5838	-4699
3222	34	22	0.00	0.00		-5333	-5836	-5837	
3229	34	22	0.00	0.00		-6670	-3985	-3947	-6669
3231	32	22	0.00	0.00		-7710	-4419	-4461	-7805
3231	32	22	0.00	0.00		-7928	-4417	-4362	-7974
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3232	34	22	0.00	0.00		-3825	-3607	-7136	-7137
3233	34	22	0.00	0.00		-7136	-4251	-4219	-7135
3234	28	22	0.00	0.00		-5987	-5878	-5877	-5986
3234	28	22	0.00	0.00		-5888	-5846	-5845	-5887
3234	30	22	0.00	0.00		-6067	-6066	-6134	-6135
3234	28	22	0.00	0.00		-6060	-5987	-5986	-6059
3234	28	22	0.00	0.00		-6070	-5996	-5995	-6069
3234	28	22	0.00	0.00		-6130	-6062	-6061	-6129
3234	28	22	0.00	0.00		-5989	-5880	-5879	-5988
3234	28	22	0.00	0.00		-6249	-6197	-6196	-6239
3234	28	22	0.00	0.00		-6193	-6194	-6137	-6136
3234	28	22	0.00	0.00		-6250	-6198	-6197	-6249
3234	28	22	0.00	0.00		-6142	-6074	-6073	-6141
3234	28	22	0.00	0.00		-6073	-5999	-5998	-6072
3234	28	22	0.00	0.00		-5878	-5836	-5835	-5877
3234	28	22	0.00	0.00		-6185	-6128	-6127	-6184
3234	28	22	0.00	0.00		-5891	-5849	-5848	-5890
3234	28	22	0.00	0.00		-6252	-6200	-6199	-6251

3234	28	22	0.00	0.00		-6000	-5892	-5891	-5999
3234	28	22	0.00	0.00		-5838	-5792	-5791	-5837
3234	28	22	0.00	0.00		-6199	-6142	-6141	-6198
3234	30	22	0.00	0.00		-6068	-6067	-6135	-6136
3234	28	22	0.00	0.00		-5999	-5891	-5890	-5998
3234	28	22	0.00	0.00		-6248	-6195	-6194	-6247
3234	30	22	0.00	0.00		-6136	-6135	-6192	-6193
3234	28	22	0.00	0.00		-6138	-6070	-6069	-6137
3234	28	22	0.00	0.00		-6187	-6130	-6129	-6186
3234	28	22	0.00	0.00		-6236	-6187	-6186	-6235
3234	30	22	0.00	0.00		-5798	-5797	-5843	-5844
3234	28	22	0.00	0.00		-5847	-5801	-5800	-5846
3234	28	22	0.00	0.00		-6198	-6141	-6140	-6197
3234	28	22	0.00	0.00		-6068	-6069	-5995	-6025
3234	28	22	0.00	0.00		-6242	-6185	-6184	-6234
3234	28	22	0.00	0.00		-6246	-6247	-6194	-6193
3234	28	22	0.00	0.00		-5886	-5887	-5845	-5844
3234	28	22	0.00	0.00		-6128	-6060	-6059	-6127
3234	28	22	0.00	0.00		-6238	-6191	-6190	-6244
3234	28	22	0.00	0.00		-6074	-6000	-5999	-6073
3234	28	22	0.00	0.00		-5892	-5850	-5849	-5891
3234	28	22	0.00	0.00		-5884	-5842	-5841	-5883
3234	28	22	0.00	0.00		-5846	-5800	-5799	-5845
3234	28	22	0.00	0.00		-5848	-5802	-5801	-5847
3234	28	22	0.00	0.00		-5837	-5791	-5790	-5836
3234	30	22	0.00	0.00		-5885	-5884	-5993	-5994
3234	28	22	0.00	0.00		-5992	-5883	-5882	-5991
3234	28	22	0.00	0.00		-6140	-6072	-6071	-6139
3234	28	22	0.00	0.00		-5839	-5793	-5792	-5838
3234	28	22	0.00	0.00		-6025	-5995	-5887	-5886
3234	28	22	0.00	0.00		-5882	-5840	-5839	-5881
3234	28	22	0.00	0.00		-5890	-5848	-5847	-5889
3234	28	22	0.00	0.00		-5851	-5805	-5804	-5850
3234	28	22	0.00	0.00		-6244	-6190	-6189	-6243
3234	28	22	0.00	0.00		-6063	-5990	-5989	-6062
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3234	28	22	0.00	0.00		-5881	-5839	-5838	-5880
3234	30	22	0.00	0.00		-5843	-5842	-5884	-5885
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3234	28	22	0.00	0.00		-5840	-5794	-5793	-5839
3234	28	22	0.00	0.00		-5988	-5879	-5878	-5987
3234	28	22	0.00	0.00		-5996	-5888	-5887	-5995
3234	28	22	0.00	0.00		-5998	-5890	-5889	-5997
3234	28	22	0.00	0.00		-6129	-6061	-6060	-6128
3234	28	22	0.00	0.00		-5972	-5893	-5892	-6000
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3234	28	22	0.00	0.00		-6075	-5972	-6000	-6074
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3234	28	22	0.00	0.00		-5883	-5841	-5840	-5882
3234	28	22	0.00	0.00		-6061	-5988	-5987	-6060
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3234	28	22	0.00	0.00		-6066	-5993	-5992	-6065
3234	28	22	0.00	0.00		-5993	-5884	-5883	-5992
3234	28	22	0.00	0.00		-5997	-5889	-5888	-5996
3234	28	22	0.00	0.00		-6141	-6073	-6072	-6140
3234	28	22	0.00	0.00		-6133	-6065	-6064	-6132
3234	28	22	0.00	0.00		-6239	-6196	-6195	-6248
3234	28	22	0.00	0.00		-6188	-6131	-6130	-6187
3234	28	22	0.00	0.00		-6065	-5992	-5991	-6064
3234	28	22	0.00	0.00		-5845	-5799	-5798	-5844
3234	28	22	0.00	0.00		-6064	-5991	-5990	-6063
3234	30	22	0.00	0.00		-5994	-5993	-6066	-6067
3234	28	22	0.00	0.00		-5991	-5882	-5881	-5990
3234	28	22	0.00	0.00		-5841	-5795	-5794	-5840
3234	28	22	0.00	0.00		-6195	-6138	-6137	-6194
3234	30	22	0.00	0.00		-5886	-5885	-5994	-6025
3234	28	22	0.00	0.00		-6131	-6063	-6062	-6130
3234	28	22	0.00	0.00		-6237	-6188	-6187	-6236
3234	30	22	0.00	0.00		-6192	-6191	-6238	-6245
3234	28	22	0.00	0.00		-6071	-5997	-5996	-6070
3234	30	22	0.00	0.00		-6193	-6192	-6245	-6246
3234	28	22	0.00	0.00		-5889	-5847	-5846	-5888
3234	28	22	0.00	0.00		-5836	-5790	-5789	-5835
3234	28	22	0.00	0.00		-6251	-6199	-6198	-6250
3234	28	22	0.00	0.00		-5893	-5851	-5850	-5892
3234	28	22	0.00	0.00		-6200	-6143	-6142	-6199

3234	30	22	0.00	0.00		-5844	-5843	-5885	-5886
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3234	28	22	0.00	0.00		-6136	-6137	-6069	-6068
3234	28	22	0.00	0.00		-6132	-6064	-6063	-6131
3234	28	22	0.00	0.00		-5849	-5803	-5802	-5848
3234	30	22	0.00	0.00		-6025	-5994	-6067	-6068
3234	28	22	0.00	0.00		-6190	-6133	-6132	-6189
3234	28	22	0.00	0.00		-6243	-6189	-6188	-6237
3234	28	22	0.00	0.00		-5850	-5804	-5803	-5849
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3234	28	22	0.00	0.00		-6139	-6071	-6070	-6138
3234	28	22	0.00	0.00		-6189	-6132	-6131	-6188
3234	28	22	0.00	0.00		-6072	-5998	-5997	-6071
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3234	28	22	0.00	0.00		-6197	-6140	-6139	-6196
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3235	32	22	0.00	0.00		-7579	-4254	-4379	-7666
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3235	32	22	0.00	0.00		-7976	-4363	-4503	-8030
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3239	34	22	0.00	0.00		-4950	-5065	-5674	
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3334	32	22	0.00	0.00		-8230	-4887	-4953	-8318
3334	32	22	0.00	0.00		-8481	-5002	-5255	-8539
3334	32	22	0.00	0.00		-8318	-4953	-4885	-8379
3334	32	22	0.00	0.00		-8030	-4503	-4842	-8156
3334	32	22	0.00	0.00		-8721	-5355	-5287	-8841
3334	32	22	0.00	0.00		-8156	-4842	-4887	-8230
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3334	32	22	0.00	0.00		-8841	-5287	-5216	-8910
3334	32	22	0.00	0.00		-8629	-5305	-5355	-8721
3334	32	22	0.00	0.00		-8910	-5216	-5398	-8984
3334	32	22	0.00	0.00		-8539	-5255	-5305	-8629
3335	34	22	0.00	0.00		-7498	-4492	-4459	-7497
3339	34	22	0.00	0.00		-4362	-4169	-7973	-7974
3342	34	22	0.00	0.00		-4421	-5418	-8423	
3345	34	22	0.00	0.00		-5781	-5854	-6493	
3346	34	22	0.00	0.00		-6170	-5356	-6259	
3364	34	22	0.00	0.00		-5747	-5053	-6249	-6250
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3372	34	22	0.00	0.00		-6152	-5448	-6690	-6691
3380	34	22	0.00	0.00		-4460	-4493	-7502	-7503
3384	34	22	0.00	0.00		-4170	-4363	-7976	-7977
3386	34	22	0.00	0.00		-5397	-4422	-8427	
3388	34	22	0.00	0.00		-6494	-5855	-5773	
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3436	32	22	0.00	0.00		-9073	-5620	-5701	-9149
3436	32	22	0.00	0.00		-9440	-5808	-6036	-9479
3436	32	22	0.00	0.00		-9727	-6001	-6206	-9855
3436	32	22	0.00	0.00		-10194	-6495	-6380	-10249
3436	32	22	0.00	0.00		-9968	-6437	-6501	-10034
3436	32	22	0.00	0.00		-9374	-5605	-5808	-9440
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3437	30	22	0.00	0.00		-8229	-8228	-8316	-8317
3437	28	22	0.00	0.00		-10199	-10133	-10132	-10198
3437	28	22	0.00	0.00		-10257	-10201	-10200	-10256
3437	28	22	0.00	0.00		-8427	-8380	-8379	-8426
3437	28	22	0.00	0.00		-10122	-10030	-10029	-10121

3437	28	22	0.00	0.00		-10038	-9946	-9962	-10037
3437	28	22	0.00	0.00		-7974	-7928	-7927	-7973
3437	28	22	0.00	0.00		-7502	-7466	-7465	-7501
3437	28	22	0.00	0.00		-7971	-7925	-7924	-7970
3437	28	22	0.00	0.00		-10129	-10037	-10036	-10128
3437	28	22	0.00	0.00		-8911	-8808	-8841	-8910
3437	28	22	0.00	0.00		-10255	-10199	-10198	-10254
3437	28	22	0.00	0.00		-10041	-9972	-9971	-10040
3437	30	22	0.00	0.00		-10036	-10035	-10127	-10128
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3437	28	22	0.00	0.00		3301	-10193	-10192	-10248
3437	28	22	0.00	0.00		-9446	-9380	-9379	-9445
3437	28	22	0.00	0.00		-10198	-10132	-10131	-10177
3437	28	22	0.00	0.00		-10121	-10029	-10028	-10120
3437	30	22	0.00	0.00		-7666	-7662	-7711	-7712
3437	28	22	0.00	0.00		-10133	-10041	-10040	-10132
3437	28	22	0.00	0.00		3302	-10176	-10196	-10251
3437	28	22	0.00	0.00		-9972	-9849	-9848	-9971
3437	30	22	0.00	0.00		-8984	-8983	-9095	-9074
3437	28	22	0.00	0.00		-10132	-10040	-10039	-10131
3437	28	22	0.00	0.00		-9968	-9855	-9854	-9945
3437	28	22	0.00	0.00		-7269	-7206	-7205	-7268
3437	28	22	0.00	0.00		-10030	-9944	-9943	-10029
3437	28	22	0.00	0.00		-7571	-7497	-7496	-7576
3437	28	22	0.00	0.00		-9557	-9505	-9493	-9556
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3437	30	22	0.00	0.00		-7349	-7348	-7464	-7465
3437	28	22	0.00	0.00		-7257	-7194	-7193	-7256
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3437	28	22	0.00	0.00		-9493	-9446	-9445	-9488
3437	30	22	0.00	0.00		-9600	-9599	-9641	-9642
3437	28	22	0.00	0.00		-9962	-9857	-9847	-9970
3437	28	22	0.00	0.00		-9857	-9741	-9740	-9847
3437	30	22	0.00	0.00		-7348	-7347	-7463	-7464
3437	28	22	0.00	0.00		-9974	-9863	-9840	-9973
3437	30	22	0.00	0.00		-10127	-10126	-10194	-10195
3437	30	22	0.00	0.00		-8983	-8982	-9073	-9095
3437	28	22	0.00	0.00		-9445	-9379	-9378	-9444
3437	28	22	0.00	0.00		-9742	-9644	-9643	-9741
3437	28	22	0.00	0.00		-9644	-9602	-9601	-9643
3437	30	22	0.00	0.00		-10195	-10194	-10249	-10250
3437	28	22	0.00	0.00		-7468	-7352	-7351	-7467
3437	30	22	0.00	0.00		-7265	-7264	-7298	-7299
3437	28	22	0.00	0.00		-9444	-9378	-9377	-9443
3437	28	22	0.00	0.00		-7801	-7705	-7697	-7800
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3437	28	22	0.00	0.00		-7459	-7343	-7342	-7458
3437	30	22	0.00	0.00		-7501	-7500	-7572	-7579
3437	28	22	0.00	0.00		-9727	-9640	-9639	-9739
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3437	28	22	0.00	0.00		-8420	-8373	-8372	-8419
3437	28	22	0.00	0.00		-7472	-7356	-7355	-7471
3437	28	22	0.00	0.00		-8917	-8809	-8827	-8916
3437	28	22	0.00	0.00		-8433	-8386	-8385	-8432
3437	28	22	0.00	0.00		-9373	-9282	-9281	-9372
3437	28	22	0.00	0.00		-10246	-10190	-10175	-10245
3437	28	22	0.00	0.00		-10134	-10042	-10041	-10133
3437	28	22	0.00	0.00		-9747	-9649	-9648	-9746
3437	28	22	0.00	0.00		-8372	-8311	-8310	-8371
3437	30	22	0.00	0.00		-9485	-9479	-9550	-9551
3437	28	22	0.00	0.00		-9744	-9646	-9645	-9743
3437	28	22	0.00	0.00		-9646	-9604	-9603	-9645
3437	28	22	0.00	0.00		-9604	-9556	-9555	-9603
3437	28	22	0.00	0.00		-8423	-8376	-8375	-8422
3437	28	22	0.00	0.00		-8907	-8824	-8807	-8906
3437	30	22	0.00	0.00		-9740	-9728	-9856	-9847
3437	28	22	0.00	0.00		-9743	-9645	-9644	-9742
3437	28	22	0.00	0.00		-9645	-9603	-9602	-9644
3437	28	22	0.00	0.00		-7505	-7469	-7468	-7504
3437	28	22	0.00	0.00		-9555	-9488	-9504	-9554
3437	30	22	0.00	0.00		-8426	-8425	-8480	-8481
3437	30	22	0.00	0.00		-8539	-8538	-8621	-8629
3437	28	22	0.00	0.00		-7813	-7723	-7722	-7812
3437	28	22	0.00	0.00		-7723	-7671	-7670	-7722
3437	30	22	0.00	0.00		-10196	-10195	-10250	-10251
3437	28	22	0.00	0.00		-8424	-8423	-8472	-8479
3437	30	22	0.00	0.00		-8910	-8909	-8983	-8984
3437	30	22	0.00	0.00		-9074	-9095	-9150	-9151

3437	28	22	0.00	0.00		-7812	-7722	-7716	-7811
3437	28	22	0.00	0.00		-7722	-7670	-7669	-7716
3437	28	22	0.00	0.00		-9377	-9286	-9285	-9376
3437	28	22	0.00	0.00		-10254	-10198	-10177	-10253
3437	28	22	0.00	0.00		-7495	-7459	-7458	-7494
3437	30	22	0.00	0.00		-9847	-9856	-9969	-9970
3437	28	22	0.00	0.00		-10040	-9971	-9963	-10039
3437	30	22	0.00	0.00		-7807	-7806	-7929	-7930
3437	30	22	0.00	0.00		-7711	-7710	-7805	-7806
3437	28	22	0.00	0.00		-9506	-9448	-9447	-9505
3437	30	22	0.00	0.00		-7264	-7263	-7297	-7298
3437	30	22	0.00	0.00		-7138	-7137	-7200	-7201
3437	28	22	0.00	0.00		-9739	-9639	-9638	-9738
3437	28	22	0.00	0.00		-7715	-7668	-7643	-7721
3437	28	22	0.00	0.00		-7668	-7583	-7582	-7643
3437	28	22	0.00	0.00		-7583	-7505	-7504	-7582
3437	28	22	0.00	0.00		-10197	-10130	-10129	-10176
3437	28	22	0.00	0.00		-10130	-10038	-10037	-10129
3437	28	22	0.00	0.00		-10200	-10134	-10133	-10199
3437	28	22	0.00	0.00		-7291	-7257	-7256	-7290
3437	28	22	0.00	0.00		-7643	-7582	-7581	-7667
3437	28	22	0.00	0.00		-10176	-10129	-10128	-10196
3437	28	22	0.00	0.00		-10256	-10200	-10199	-10255
3437	28	22	0.00	0.00		-10037	-9962	-9970	-10036
3437	30	22	0.00	0.00		-7299	-7298	-7348	-7349
3437	28	22	0.00	0.00		-7714	-7667	-7663	-7713
3437	28	22	0.00	0.00		-9863	-9747	-9746	-9840
3437	28	22	0.00	0.00		-7581	-7503	-7502	-7580
3437	28	22	0.00	0.00		-7931	-7808	-7807	-7930
3437	28	22	0.00	0.00		-7808	-7713	-7712	-7807
3437	28	22	0.00	0.00		-9855	-9727	-9739	-9854
3437	28	22	0.00	0.00		-7663	-7580	-7579	-7666
3437	28	22	0.00	0.00		-9554	-9504	-9487	-9553
3437	28	22	0.00	0.00		-9504	-9444	-9443	-9487
3437	30	22	0.00	0.00		-8029	-8028	-8154	-8155
3437	28	22	0.00	0.00		-9643	-9601	-9600	-9642
3437	28	22	0.00	0.00		-9849	-9745	-9744	-9848
3437	28	22	0.00	0.00		-7710	-7661	-7660	-7709
3437	28	22	0.00	0.00		-9487	-9443	-9442	-9486
3437	28	22	0.00	0.00		-7935	-7811	-7810	-7934
3437	28	22	0.00	0.00		-9961	-9839	-9853	-9967
3437	30	22	0.00	0.00		-9856	-9855	-9968	-9969
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3437	28	22	0.00	0.00		-7499	-7463	-7462	-7498
3437	28	22	0.00	0.00		-9383	-9292	-9291	-9382
3437	28	22	0.00	0.00		-9853	-9737	-9736	-9838
3437	30	22	0.00	0.00		-9209	-9208	-9284	-9285
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3437	30	22	0.00	0.00		-9095	-9073	-9149	-9150
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3437	28	22	0.00	0.00		-7658	-7576	-7570	-7657
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3437	28	22	0.00	0.00		-9943	-9852	-9837	-9942
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3437	30	22	0.00	0.00		-8909	-8908	-8982	-8983
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3437	28	22	0.00	0.00		-9374	-9283	-9282	-9373

3437	28	22	0.00	0.00		-10042	-9973	-9972	-10041
3437	28	22	0.00	0.00		-7356	-7306	-7305	-7355
3437	28	22	0.00	0.00		-7306	-7272	-7271	-7305
3437	28	22	0.00	0.00		-7272	-7209	-7208	-7271
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3437	28	22	0.00	0.00		-10043	-9974	-9973	-10042
3437	28	22	0.00	0.00		-10135	-10043	-10042	-10134
3437	28	22	0.00	0.00		-10201	-10135	-10134	-10200
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3437	28	22	0.00	0.00		-7271	-7208	-7207	-7270
3437	28	22	0.00	0.00		-7208	-7145	-7144	-7207
3437	28	22	0.00	0.00		-9556	-9493	-9488	-9555
3437	28	22	0.00	0.00		-7470	-7354	-7353	-7469
3437	28	22	0.00	0.00		-8977	-8903	-8902	-8976
3437	30	22	0.00	0.00		-9970	-9969	-10035	-10036
3437	30	22	0.00	0.00		-10128	-10127	-10195	-10196
3437	28	22	0.00	0.00		-9603	-9555	-9554	-9602
3437	28	22	0.00	0.00		-9143	-9093	-9068	-9142
3437	28	22	0.00	0.00		-9488	-9445	-9444	-9504
3437	28	22	0.00	0.00		-8976	-8902	-8901	-8975
3437	28	22	0.00	0.00		-7303	-7269	-7268	-7302
3437	30	22	0.00	0.00		-9284	-9283	-9374	-9375
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3437	28	22	0.00	0.00		-8728	-8635	-8634	-8727
3437	28	22	0.00	0.00		-7805	-7710	-7709	-7804
3437	28	22	0.00	0.00		-9601	-9553	-9552	-9600
3437	28	22	0.00	0.00		-9553	-9487	-9486	-9552
3437	28	22	0.00	0.00		-9443	-9377	-9376	-9442
3437	28	22	0.00	0.00		-7467	-7351	-7350	-7466
3437	28	22	0.00	0.00		-7351	-7301	-7300	-7350
3437	28	22	0.00	0.00		-7301	-7267	-7266	-7300
3437	28	22	0.00	0.00		-7267	-7204	-7203	-7266
3437	28	22	0.00	0.00		-8485	-8432	-8431	-8484
3437	28	22	0.00	0.00		-8915	-8826	-8843	-8914
3437	28	22	0.00	0.00		-9479	-9440	-9439	-9503
3437	28	22	0.00	0.00		-9440	-9374	-9373	-9439
3437	28	22	0.00	0.00		-9639	-9597	-9596	-9638
3437	28	22	0.00	0.00		-9597	-9549	-9548	-9596
3437	28	22	0.00	0.00		-9549	-9503	-9484	-9548
3437	28	22	0.00	0.00		-8311	-8223	-8222	-8310
3437	28	22	0.00	0.00		-7508	-7472	-7471	-7507
3437	28	22	0.00	0.00		-7973	-7927	-7926	-7972
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3437	30	22	0.00	0.00		-7975	-7974	-8028	-8029
3437	28	22	0.00	0.00		-7296	-7262	-7261	-7295
3437	28	22	0.00	0.00		-7262	-7199	-7198	-7261
3437	30	22	0.00	0.00		-8379	-8378	-8425	-8426
3437	28	22	0.00	0.00		-7497	-7461	-7460	-7496
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3437	28	22	0.00	0.00		-7496	-7460	-7459	-7495
3437	28	22	0.00	0.00		-7460	-7344	-7343	-7459
3437	28	22	0.00	0.00		-7344	-7294	-7293	-7343
3437	28	22	0.00	0.00		-7294	-7260	-7259	-7293
3437	28	22	0.00	0.00		-7260	-7197	-7196	-7259
3437	28	22	0.00	0.00		-7197	-7134	-7133	-7196
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3437	28	22	0.00	0.00		-7494	-7458	-7457	-7493
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3437	28	22	0.00	0.00		-7493	-7457	-7456	-7492
3437	28	22	0.00	0.00		-7457	-7341	-7340	-7456
3437	28	22	0.00	0.00		-7341	-7291	-7290	-7340

3437	28	22	0.00	0.00		-8534	-8471	-8470	-8533
3437	28	22	0.00	0.00		-8471	-8421	-8420	-8470
3437	28	22	0.00	0.00		-7194	-7131	-7130	-7193
3437	30	22	0.00	0.00		-7465	-7464	-7500	-7501
3437	30	22	0.00	0.00		-7464	-7463	-7499	-7500
3437	28	22	0.00	0.00		-8617	-8533	-8532	-8616
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3437	28	22	0.00	0.00		-8714	-8616	-8627	-8713
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3437	28	22	0.00	0.00		-8532	-8469	-8477	-8531
3437	28	22	0.00	0.00		-7580	-7502	-7501	-7579
3437	30	22	0.00	0.00		-8030	-8029	-8155	-8156
3437	28	22	0.00	0.00		-8802	-8713	-8712	-8801
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3437	30	22	0.00	0.00		-9969	-9968	-10034	-10035
3437	30	22	0.00	0.00		-9728	-9727	-9855	-9856
3437	28	22	0.00	0.00		-7503	-7467	-7466	-7502
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3437	28	22	0.00	0.00		-9839	-9738	-9737	-9853
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3437	28	22	0.00	0.00		-10191	-10123	-10122	-10190
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3437	28	22	0.00	0.00		-8037	-7983	-7982	-8036
3437	28	22	0.00	0.00		-8432	-8385	-8384	-8431
3437	28	22	0.00	0.00		-10190	-10122	-10121	-10175
3437	30	22	0.00	0.00		-9599	-9598	-9640	-9641
3437	28	22	0.00	0.00		-8236	-8162	-8161	-8235
3437	28	22	0.00	0.00		-9944	-9838	-9852	-9943
3437	28	22	0.00	0.00		-9838	-9736	-9726	-9852
3437	28	22	0.00	0.00		-8431	-8384	-8383	-8430
3437	28	22	0.00	0.00		-8384	-8323	-8322	-8383
3437	28	22	0.00	0.00		-8323	-8235	-8234	-8322
3437	28	22	0.00	0.00		-8235	-8161	-8160	-8234
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3437	28	22	0.00	0.00		-10189	-10120	-10119	-10188
3437	28	22	0.00	0.00		-10120	-10028	-10027	-10119
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3437	28	22	0.00	0.00		-9942	-9837	-9846	-9941
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3437	30	22	0.00	0.00		-7202	-7201	-7264	-7265
3437	30	22	0.00	0.00		-7201	-7200	-7263	-7264
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3437	28	22	0.00	0.00		-9649	-9607	-9606	-9648
3437	28	22	0.00	0.00		-9607	-9559	-9558	-9606
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3437	28	22	0.00	0.00		-9449	-9383	-9382	-9448
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3437	28	22	0.00	0.00		-9606	-9558	-9557	-9605
3437	28	22	0.00	0.00		-9558	-9506	-9505	-9557
3437	30	22	0.00	0.00		-9486	-9485	-9551	-9552
3437	28	22	0.00	0.00		-9448	-9382	-9381	-9447
3437	28	22	0.00	0.00		-9745	-9647	-9646	-9744
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3437	28	22	0.00	0.00		-9605	-9557	-9556	-9604
3437	28	22	0.00	0.00		-7498	-7462	-7461	-7497
3437	28	22	0.00	0.00		-9505	-9447	-9446	-9493
3437	30	22	0.00	0.00		-7976	-7975	-8029	-8030
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3437	30	22	0.00	0.00		-8317	-8316	-8377	-8378
3437	30	22	0.00	0.00		-8155	-8154	-8228	-8229
3437	28	22	0.00	0.00		-8537	-8536	-8620	-8628
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3437	28	22	0.00	0.00		-8719	-8718	-8824	-8840
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3437	28	22	0.00	0.00		-8376	-8315	-8314	-8375
3437	28	22	0.00	0.00		-8315	-8227	-8226	-8314
3437	28	22	0.00	0.00		-8227	-8153	-8152	-8226

3437	28	22	0.00	0.00		-8153	-8027	-8026	-8152
3437	28	22	0.00	0.00		-8027	-7973	-7972	-8026
3437	28	22	0.00	0.00		-8422	-8375	-8374	-8421
3437	28	22	0.00	0.00		-8375	-8314	-8313	-8374
3437	28	22	0.00	0.00		-8314	-8226	-8225	-8313
3437	28	22	0.00	0.00		-8226	-8152	-8151	-8225
3437	28	22	0.00	0.00		-8152	-8026	-8025	-8151
3437	28	22	0.00	0.00		-8026	-7972	-7971	-8025
3437	28	22	0.00	0.00		-8421	-8374	-8373	-8420
3437	28	22	0.00	0.00		-8374	-8313	-8312	-8373
3437	28	22	0.00	0.00		-8313	-8225	-8224	-8312
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3437	28	22	0.00	0.00		-8025	-7971	-7970	-8024
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3437	28	22	0.00	0.00		-8373	-8312	-8311	-8372
3437	28	22	0.00	0.00		-8312	-8224	-8223	-8311
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3437	28	22	0.00	0.00		-8150	-8024	-8023	-8149
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3437	28	22	0.00	0.00		-8419	-8372	-8371	-8418
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3437	28	22	0.00	0.00		-9503	-9439	-9438	-9484
3437	28	22	0.00	0.00		-8223	-8149	-8148	-8222
3437	28	22	0.00	0.00		-8149	-8023	-8022	-8148
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3437	28	22	0.00	0.00		-8418	-8371	-8370	-8417
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3437	28	22	0.00	0.00		-8310	-8222	-8221	-8309
3437	28	22	0.00	0.00		-8222	-8148	-8147	-8221
3437	28	22	0.00	0.00		-8148	-8022	-8021	-8147
3437	28	22	0.00	0.00		-8022	-7968	-7967	-8021
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3437	28	22	0.00	0.00		-9736	-9636	-9635	-9726
3437	28	22	0.00	0.00		-9636	-9594	-9593	-9635
3437	28	22	0.00	0.00		-7586	-7508	-7507	-7585
3437	28	22	0.00	0.00		-7982	-7936	-7935	-7981
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3437	28	22	0.00	0.00		-9726	-9635	-9634	-9735
3437	28	22	0.00	0.00		-7670	-7585	-7584	-7669
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3437	28	22	0.00	0.00		-7981	-7935	-7934	-7980
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3437	30	22	0.00	0.00		-9641	-9640	-9727	-9728
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3437	28	22	0.00	0.00		-7933	-7809	-7781	-7932
3437	28	22	0.00	0.00		-7809	-7721	-7714	-7781
3437	28	22	0.00	0.00		-7721	-7643	-7667	-7714
3437	28	22	0.00	0.00		-9100	-8991	-8990	-9099
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3437	28	22	0.00	0.00		-9157	-9099	-9098	-9156
3437	28	22	0.00	0.00		-7667	-7581	-7580	-7663
3437	28	22	0.00	0.00		-8990	-8916	-8915	-8989
3437	28	22	0.00	0.00		-9381	-9290	-9289	-9380
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3437	28	22	0.00	0.00		-7713	-7663	-7666	-7712
3437	28	22	0.00	0.00		-9156	-9098	-9097	-9155
3437	28	22	0.00	0.00		-9098	-8989	-8988	-9097
3437	30	22	0.00	0.00		-7500	-7499	-7578	-7572
3437	28	22	0.00	0.00		-9380	-9289	-9288	-9379
3437	28	22	0.00	0.00		-7928	-7805	-7804	-7927
3437	28	22	0.00	0.00		-9213	-9155	-9154	-9212
3437	28	22	0.00	0.00		-9155	-9097	-9096	-9154

3437	28	22	0.00	0.00		-7661	-7578	-7577	-7660
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3437	28	22	0.00	0.00		-7660	-7577	-7571	-7659
3437	28	22	0.00	0.00		-7577	-7498	-7497	-7571
3437	28	22	0.00	0.00		-7972	-7926	-7925	-7971
3437	28	22	0.00	0.00		-7926	-7780	-7803	-7925
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3437	28	22	0.00	0.00		-7659	-7571	-7576	-7658
3437	28	22	0.00	0.00		-9076	-8986	-8985	-9075
3437	28	22	0.00	0.00		-8986	-8912	-8911	-8985
3437	28	22	0.00	0.00		-7925	-7803	-7802	-7924
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3437	28	22	0.00	0.00		-7707	-7658	-7657	-7698
3437	28	22	0.00	0.00		-9075	-8985	-8984	-9074
3437	28	22	0.00	0.00		-8985	-8911	-8910	-8984
3437	28	22	0.00	0.00		-7970	-7924	-7923	-7969
3437	30	22	0.00	0.00		-9441	-9440	-9479	-9485
3437	28	22	0.00	0.00		-9283	-9207	-9206	-9282
3437	28	22	0.00	0.00		-9207	-9149	-9148	-9206
3437	28	22	0.00	0.00		-9149	-9073	-9072	-9148
3437	28	22	0.00	0.00		-9073	-8982	-8981	-9072
3437	28	22	0.00	0.00		-8982	-8908	-8907	-8981
3437	28	22	0.00	0.00		-9282	-9206	-9205	-9281
3437	28	22	0.00	0.00		-7779	-7706	-7705	-7801
3437	28	22	0.00	0.00		-9148	-9072	-9071	-9147
3437	28	22	0.00	0.00		-7656	-7569	-7568	-7655
3437	28	22	0.00	0.00		-7569	-7494	-7493	-7568
3437	28	22	0.00	0.00		-9372	-9281	-9280	-9371
3437	28	22	0.00	0.00		-9281	-9205	-9204	-9280
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3437	28	22	0.00	0.00		-9147	-9071	-9094	-9146
3437	28	22	0.00	0.00		-7655	-7568	-7567	-7654
3437	28	22	0.00	0.00		-7568	-7493	-7492	-7567
3437	28	22	0.00	0.00		-9371	-9280	-9279	-9370
3437	30	22	0.00	0.00		-7929	-7928	-7974	-7975
3437	28	22	0.00	0.00		-9204	-9146	-9145	-9203
3437	28	22	0.00	0.00		-9146	-9094	-9070	-9145
3437	28	22	0.00	0.00		-9094	-8979	-8978	-9070
3437	28	22	0.00	0.00		-8979	-8905	-8904	-8978
3437	28	22	0.00	0.00		-9370	-9279	-9278	-9369
3437	28	22	0.00	0.00		-9279	-9203	-9202	-9278
3437	28	22	0.00	0.00		-7209	-7146	-7145	-7208
3437	28	22	0.00	0.00		-7507	-7471	-7470	-7506
3437	28	22	0.00	0.00		-7471	-7355	-7354	-7470
3437	28	22	0.00	0.00		-7355	-7305	-7304	-7354
3437	28	22	0.00	0.00		-9369	-9278	-9277	-9368
3437	28	22	0.00	0.00		-9278	-9202	-9201	-9277
3437	28	22	0.00	0.00		-9202	-9144	-9143	-9201
3437	28	22	0.00	0.00		-7506	-7470	-7469	-7505
3437	28	22	0.00	0.00		-9069	-8977	-8976	-9093
3437	28	22	0.00	0.00		-7354	-7304	-7303	-7353
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3437	28	22	0.00	0.00		-7270	-7207	-7206	-7269
3437	28	22	0.00	0.00		-7207	-7144	-7143	-7206
3437	28	22	0.00	0.00		-8470	-8420	-8419	-8469
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3437	28	22	0.00	0.00		-7353	-7303	-7302	-7352
3437	30	22	0.00	0.00		-9285	-9284	-9375	-9376
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3437	28	22	0.00	0.00		-7206	-7143	-7142	-7205
3437	30	22	0.00	0.00		-9150	-9149	-9207	-9208
3437	28	22	0.00	0.00		-10033	-9945	-9961	-10032
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3437	28	22	0.00	0.00		-8635	-8546	-8545	-8634
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3437	28	22	0.00	0.00		-8916	-8827	-8826	-8915
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3437	28	22	0.00	0.00		-8727	-8634	-8633	-8726
3437	28	22	0.00	0.00		-8634	-8545	-8544	-8633
3437	30	22	0.00	0.00		-8621	-8628	-8719	-8720
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3437	28	22	0.00	0.00		-7466	-7350	-7349	-7465
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3437	28	22	0.00	0.00		-7300	-7266	-7265	-7299

3437	28	22	0.00	0.00		-7266	-7203	-7202	-7265
3437	28	22	0.00	0.00		-7203	-7140	-7139	-7202
3437	28	22	0.00	0.00		-8484	-8431	-8430	-8483
3437	30	22	0.00	0.00		-7572	-7578	-7661	-7662
3437	28	22	0.00	0.00		-7463	-7347	-7346	-7462
3437	28	22	0.00	0.00		-7347	-7297	-7296	-7346
3437	28	22	0.00	0.00		-7297	-7263	-7262	-7296
3437	28	22	0.00	0.00		-8543	-8483	-8474	-8542
3437	28	22	0.00	0.00		-8483	-8430	-8429	-8474
3437	28	22	0.00	0.00		-7462	-7346	-7345	-7461
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3437	28	22	0.00	0.00		-8724	-8631	-8630	-8723
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3437	28	22	0.00	0.00		-8912	-8787	-8808	-8911
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3437	28	22	0.00	0.00		-9973	-9840	-9849	-9972
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3437	28	22	0.00	0.00		-8808	-8722	-8721	-8841
3437	28	22	0.00	0.00		-8722	-8622	-8629	-8721
3437	28	22	0.00	0.00		-8622	-8540	-8539	-8629
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3437	28	22	0.00	0.00		-8824	-8718	-8717	-8807
3437	28	22	0.00	0.00		-8718	-8620	-8619	-8717
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3437	28	22	0.00	0.00		-9971	-9848	-9862	-9963
3437	28	22	0.00	0.00		-9848	-9744	-9743	-9862
3437	28	22	0.00	0.00		-10253	-10177	-10197	-10252
3437	28	22	0.00	0.00		-10177	-10131	-10130	-10197
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3437	28	22	0.00	0.00		-10252	-10197	-10176	3302
3437	28	22	0.00	0.00		-8806	-8716	-8715	-8839
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3437	28	22	0.00	0.00		-8533	-8470	-8469	-8532
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3437	28	22	0.00	0.00		-8234	-8160	-8159	-8233
3437	28	22	0.00	0.00		-8160	-8034	-8033	-8159
3437	28	22	0.00	0.00		-10193	-10125	-10124	-10192
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3437	28	22	0.00	0.00		-8469	-8419	-8418	-8477
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3437	30	22	0.00	0.00		-8629	-8621	-8720	-8721
3437	28	22	0.00	0.00		-9288	-9212	-9211	-9287
3437	28	22	0.00	0.00		-8386	-8325	-8324	-8385
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3437	28	22	0.00	0.00		-10031	-9967	-9944	-10030
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3437	28	22	0.00	0.00		-8914	-8843	-8842	-8913
3437	28	22	0.00	0.00		-8162	-8036	-8035	-8161
3437	28	22	0.00	0.00		-8036	-7982	-7981	-8035
3437	28	22	0.00	0.00		-9152	-9075	-9074	-9151
3437	28	22	0.00	0.00		-9596	-9548	-9547	-9595
3437	28	22	0.00	0.00		-9548	-9484	-9483	-9547

3437	30	22	0.00	0.00		-9442	-9441	-9485	-9486
3437	28	22	0.00	0.00		-9438	-9372	-9371	-9437
3437	28	22	0.00	0.00		-8035	-7981	-7980	-8034
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3437	28	22	0.00	0.00		-9093	-8976	-8975	-9068
3437	28	22	0.00	0.00		-9483	-9437	-9436	-9478
3437	28	22	0.00	0.00		-8034	-7980	-7979	-8033
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3437	28	22	0.00	0.00		-8159	-8033	-8032	-8158
3437	28	22	0.00	0.00		-9289	-9213	-9212	-9288
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3437	28	22	0.00	0.00		-8381	-8320	-8319	-8380
3437	28	22	0.00	0.00		-8320	-8232	-8231	-8319
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3437	28	22	0.00	0.00		-8228	-8154	-8153	-8227
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3437	28	22	0.00	0.00		-8479	-8472	-8536	-8537
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3437	28	22	0.00	0.00		-9637	-9595	-9594	-9636
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3437	28	22	0.00	0.00		-8723	-8630	-8622	-8722
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3437	28	22	0.00	0.00		-8902	-8802	-8801	-8901
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3437	28	22	0.00	0.00		-8546	-8486	-8485	-8545
3437	28	22	0.00	0.00		-8486	-8433	-8432	-8485
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3437	28	22	0.00	0.00		-8980	-8906	-8905	-8979
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3437	28	22	0.00	0.00		-9544	-9476	-9502	-9543
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3437	28	22	0.00	0.00		-8632	-8543	-8542	-8631
3437	28	22	0.00	0.00		-8725	-8632	-8631	-8724
3437	28	22	0.00	0.00		-9484	-9438	-9437	-9483
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3437	28	22	0.00	0.00		-9206	-9148	-9147	-9205
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3437	28	22	0.00	0.00		-9292	-9216	-9215	-9291
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3437	28	22	0.00	0.00		-9545	-9477	-9476	-9544
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3437	28	22	0.00	0.00		-8536	-8472	-8478	-8535
3437	28	22	0.00	0.00		-9286	-9210	-9209	-9285
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3437	28	22	0.00	0.00		-9378	-9287	-9286	-9377
3437	28	22	0.00	0.00		-8535	-8478	-8471	-8534
3437	28	22	0.00	0.00		-8478	-8422	-8421	-8471
3437	28	22	0.00	0.00		-9203	-9145	-9144	-9202
3437	30	22	0.00	0.00		-9551	-9550	-9598	-9599
3437	28	22	0.00	0.00		-9070	-8978	-8977	-9069
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3437	28	22	0.00	0.00		-9158	-9100	-9099	-9157
3437	28	22	0.00	0.00		-8531	-8477	-8468	-8530
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3437	28	22	0.00	0.00		-9071	-8980	-8979	-9094
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3437	28	22	0.00	0.00		-8627	-8531	-8530	-8615
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3437	28	22	0.00	0.00		-8843	-8725	-8724	-8842
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3437	28	22	0.00	0.00		-8717	-8619	-8618	-8716
3437	28	22	0.00	0.00		-9072	-8981	-8980	-9071
3437	28	22	0.00	0.00		-8713	-8627	-8615	-8712
3437	28	22	0.00	0.00		-9210	-9152	-9151	-9209
3438	32	22	0.00	0.00		-10036	-6505	-6598	-10128
3438	32	22	0.00	0.00		-9376	-5606	-5818	-9442
3438	32	22	0.00	0.00		-9642	-6103	-6002	-9740
3438	32	22	0.00	0.00		-8984	-5398	-5621	-9074
3438	32	22	0.00	0.00		-9847	-6222	-6438	-9970
3438	32	22	0.00	0.00		-9486	-6037	-6105	-9552
3438	32	22	0.00	0.00		-9552	-6105	-6173	-9600
3438	32	22	0.00	0.00		-10196	-6496	-6382	-10251
3438	32	22	0.00	0.00		-9209	-5774	-5690	-9285
3438	32	22	0.00	0.00		-9285	-5690	-5606	-9376
3438	32	22	0.00	0.00		-9151	-5702	-5774	-9209
3438	32	22	0.00	0.00		-9740	-6002	-6222	-9847
3438	32	22	0.00	0.00		-9074	-5621	-5702	-9151
3438	32	22	0.00	0.00		-9970	-6438	-6505	-10036
3438	32	22	0.00	0.00		-10128	-6598	-6496	-10196
3438	32	22	0.00	0.00		-9442	-5818	-6037	-9486
3438	32	22	0.00	0.00		-9600	-6173	-6103	-9642
3440	34	22	0.00	0.00		-7008	-7494	-7495	-6240
3443	34	22	0.00	0.00		-7973	-5013	-4950	-7972
3447	34	22	0.00	0.00		-4815	-4421	-8423	-8424
3448	34	22	0.00	0.00		-8423	-5418	-5352	-8422
3451	34	22	0.00	0.00		-5215	-4888	-8907	-8908
3451	34	22	0.00	0.00		-4888	-5807	-8907	
3452	34	22	0.00	0.00		-6170	-6259	-6926	
3453	34	22	0.00	0.00		-5306	-6221	-9373	
3471	34	22	0.00	0.00		-6692	-6152	-6691	
3474	34	22	0.00	0.00		-7145	-6559	-7144	
3474	34	22	0.00	0.00		-6559	-5853	-7143	-7144
3478	34	22	0.00	0.00		-7009	-6253	-7505	-7506
3482	34	22	0.00	0.00		-4951	-5014	-7977	-7978
3484	34	22	0.00	0.00		-5353	-5397	-8427	-8428
3485	34	22	0.00	0.00		-4422	-4816	-8426	-8427
3487	34	22	0.00	0.00		-5817	-4897	-8911	
3487	34	22	0.00	0.00		-4897	-5216	-8910	-8911
3490	34	22	0.00	0.00		-6927	-6269	-6171	
3491	34	22	0.00	0.00		-6230	-5307	-9377	
3494	34	22	0.00	0.00		-6578	-5784	-6699	
3494	34	22	0.00	0.00		-6578	-6699	-7309	
3495	34	22	0.00	0.00		-5766	-6700	-6579	
3495	34	22	0.00	0.00		-7310	-6700	-6579	
3553	34	22	0.00	0.00		-7021	-7156	-7727	
3554	25	22	0.00	0.00		-6107	-6382	-10251	3302

3554	34	22	0.00	0.00		-7022	-7092	3302	-10252
3554	25	22	0.00	0.00		-7092	-6107	3302	
3555	34	22	0.00	0.00		3301	-7091	-7021	-10248
3555	25	22	0.00	0.00		-6380	-6106	3301	-10249
3555	25	22	0.00	0.00		-6106	-7091	3301	
3556	34	22	0.00	0.00		-7728	-7157	-7022	
3569	34	22	0.00	0.00		-7008	-7493	-7494	
3572	34	22	0.00	0.00		-7357	-7968	-7969	
3572	34	22	0.00	0.00		-7357	-7969	-7970	-6674
3577	34	22	0.00	0.00		-7814	-8419	-8420	-7147
3577	34	22	0.00	0.00		-7814	-8418	-8419	
3579	34	22	0.00	0.00		-8907	-5807	-5781	-8906
3581	34	22	0.00	0.00		-9373	-6221	-6170	-9372
3582	34	22	0.00	0.00		-5605	-5306	-9373	-9374
3583	34	22	0.00	0.00		-8326	-8902	-8903	
3583	34	22	0.00	0.00		-8326	-8903	-8904	-7509
3599	34	22	0.00	0.00		-7507	-7009	-7506	
3601	34	22	0.00	0.00		-7358	-6694	-7980	-7981
3601	34	22	0.00	0.00		-7982	-7358	-7981	
3605	34	22	0.00	0.00		-8432	-7815	-8431	
3605	34	22	0.00	0.00		-7815	-7148	-8430	-8431
3607	34	22	0.00	0.00		-5773	-5817	-8911	-8912
3609	34	22	0.00	0.00		-8916	-8327	-8915	
3609	34	22	0.00	0.00		-8327	-7510	-8914	-8915
3611	34	22	0.00	0.00		-6171	-6230	-9377	-9378
3612	34	22	0.00	0.00		-5307	-5606	-9376	-9377
3614	34	22	0.00	0.00		-9382	-8730	-9381	
3614	34	22	0.00	0.00		-8730	-7985	-9380	-9381
3616	34	22	0.00	0.00		-8729	-9368	-9369	
3616	34	22	0.00	0.00		-8729	-9369	-9370	-7984
3618	34	22	0.00	0.00		-5691	-6659	-9739	
3618	34	22	0.00	0.00		-6001	-5691	-9739	-9727
3618	34	22	0.00	0.00		-9739	-6659	-6578	-9738
3620	34	22	0.00	0.00		-5692	-6002	-9740	-9741
3620	34	22	0.00	0.00		-6579	-6660	-9741	-9742
3620	34	22	0.00	0.00		-6660	-5692	-9741	
3622	34	22	0.00	0.00		-9746	-9218	-9745	
3622	34	22	0.00	0.00		-9218	-8435	-9744	-9745
3624	34	22	0.00	0.00		-9217	-9735	-9726	
3624	34	22	0.00	0.00		-9217	-9726	-9736	-8434
3627	34	22	0.00	0.00		-9608	-10244	-10245	
3627	34	22	0.00	0.00		-9608	-10245	-10246	-8918
3629	34	22	0.00	0.00		-10256	-9609	-10255	
3629	34	22	0.00	0.00		-9609	-8919	-10254	-10255
3824	28	22	0.00	0.00		-4583	-4588	-4572	-4571
3824	28	22	0.00	0.00		-4611	-4594	-4597	-4625
3824	28	22	0.00	0.00		-4626	-4611	-4625	
3824	28	22	0.00	0.00		-4621	-4603	-4601	-4620
3824	28	22	0.00	0.00		-4652	-4635	-4634	-4651
3824	28	22	0.00	0.00		-4589	-4598	-4608	-4592
3824	28	22	0.00	0.00		-4607	-4583	-4592	-4608
3824	28	22	0.00	0.00		-4573	-4570	-4558	-4555
3824	28	22	0.00	0.00		-4651	-4634	-4633	-4650
3824	28	22	0.00	0.00		-4536	-4527	-4531	
3824	28	22	0.00	0.00		-4594	-4579	-4590	-4597
3824	28	22	0.00	0.00		-4579	-4569	-4574	-4590
3824	28	22	0.00	0.00		-4569	-4554	-4562	-4574
3824	28	22	0.00	0.00		-4554	-4541	-4551	-4562
3824	28	22	0.00	0.00		-4541	-4539	-4545	-4551
3824	28	22	0.00	0.00		-4583	-4607	-4604	-4588
3824	28	22	0.00	0.00		-4649	-4632	-4631	-4648
3824	28	22	0.00	0.00		-4634	-4620	-4619	-4633
3824	28	22	0.00	0.00		-4648	-4631	-4636	-4653
3824	28	22	0.00	0.00		-4631	-4617	-4616	-4636
3824	28	22	0.00	0.00		-4636	-4616	-4615	-4638
3824	28	22	0.00	0.00		-4615	-4614	-4640	-4638
3824	28	22	0.00	0.00		-4614	-4613	-4629	-4640
3824	28	22	0.00	0.00		-4613	-4612	-4627	-4629
3824	28	22	0.00	0.00		-4627	-4642	-4644	-4629
3824	28	22	0.00	0.00		-4642	-4659	-4663	-4644
3824	28	22	0.00	0.00		-4562	-4551	-4558	-4570
3824	28	22	0.00	0.00		-4545	-4555	-4558	-4551
3824	28	22	0.00	0.00		-4570	-4573	-4587	-4586
3824	28	22	0.00	0.00		-4650	-4633	-4632	-4649
3824	28	22	0.00	0.00		-4633	-4619	-4618	-4632
3824	28	22	0.00	0.00		-4597	-4590	-4591	-4609
3824	28	22	0.00	0.00		-4591	-4590	-4574	-4586
3824	28	22	0.00	0.00		-4586	-4587	-4605	-4606
3824	28	22	0.00	0.00		-4632	-4618	-4617	-4631

3824	28	22	0.00	0.00		-4629	-4644	-4646	-4640
3824	28	22	0.00	0.00		-4644	-4663	-4661	-4646
3824	28	22	0.00	0.00		-4646	-4661	-4657	-4640
3824	28	22	0.00	0.00		-4532	-4528	-4537	
3824	28	22	0.00	0.00		-4635	-4621	-4620	-4634
3824	28	22	0.00	0.00		-4653	-4636	-4638	-4655
3824	28	22	0.00	0.00		-4655	-4638	-4640	-4657
3824	28	22	0.00	0.00		-4660	-4643	-4645	-4664
3824	28	22	0.00	0.00		-4643	-4628	-4630	-4645
3824	28	22	0.00	0.00		-4628	-4626	-4625	-4630
3824	28	22	0.00	0.00		-4625	-4624	-4641	-4630
3824	28	22	0.00	0.00		-4624	-4623	-4639	-4641
3824	28	22	0.00	0.00		-4623	-4622	-4637	-4639
3824	28	22	0.00	0.00		-4637	-4622	-4621	-4635
3824	28	22	0.00	0.00		-4654	-4637	-4635	-4652
3824	28	22	0.00	0.00		-4539	-4532	-4537	-4545
3824	28	22	0.00	0.00		-4537	-4550	-4555	-4545
3824	28	22	0.00	0.00		-4550	-4567	-4573	-4555
3824	28	22	0.00	0.00		-4567	-4585	-4587	-4573
3824	28	22	0.00	0.00		-4585	-4603	-4605	-4587
3824	28	22	0.00	0.00		-4603	-4621	-4622	-4605
3824	28	22	0.00	0.00		-4622	-4623	-4606	-4605
3824	28	22	0.00	0.00		-4623	-4624	-4609	-4606
3824	28	22	0.00	0.00		-4624	-4625	-4597	-4609
3824	28	22	0.00	0.00		-4658	-4662	-4647	-4641
3824	28	22	0.00	0.00		-4662	-4664	-4645	-4647
3824	28	22	0.00	0.00		-4647	-4645	-4630	-4641
3824	28	22	0.00	0.00		-4639	-4637	-4654	-4656
3824	28	22	0.00	0.00		-4639	-4656	-4658	-4641
3824	28	22	0.00	0.00		-4570	-4586	-4574	-4562
3824	28	22	0.00	0.00		-4606	-4609	-4591	-4586
3824	28	22	0.00	0.00		-4603	-4585	-4582	-4601
3824	28	22	0.00	0.00		-4585	-4567	-4565	-4582
3824	28	22	0.00	0.00		-4567	-4550	-4548	-4565
3824	28	22	0.00	0.00		-4550	-4537	-4535	-4548
3824	28	22	0.00	0.00		-4537	-4528	-4526	-4535
3824	28	22	0.00	0.00		-4620	-4601	-4599	-4619
3824	28	22	0.00	0.00		-4601	-4582	-4580	-4599
3824	28	22	0.00	0.00		-4582	-4565	-4563	-4580
3824	28	22	0.00	0.00		-4565	-4548	-4546	-4563
3824	28	22	0.00	0.00		-4548	-4535	-4533	-4546
3824	28	22	0.00	0.00		-4535	-4526	-4524	-4533
3824	28	22	0.00	0.00		-4619	-4599	-4600	-4618
3824	28	22	0.00	0.00		-4599	-4580	-4581	-4600
3824	28	22	0.00	0.00		-4580	-4563	-4564	-4581
3824	28	22	0.00	0.00		-4563	-4546	-4547	-4564
3824	28	22	0.00	0.00		-4546	-4533	-4534	-4547
3824	28	22	0.00	0.00		-4533	-4524	-4525	-4534
3824	28	22	0.00	0.00		-4618	-4600	-4602	-4617
3824	28	22	0.00	0.00		-4600	-4581	-4584	-4602
3824	28	22	0.00	0.00		-4581	-4564	-4566	-4584
3824	28	22	0.00	0.00		-4564	-4547	-4549	-4566
3824	28	22	0.00	0.00		-4547	-4534	-4536	-4549
3824	28	22	0.00	0.00		-4534	-4525	-4527	-4536
3824	28	22	0.00	0.00		-4610	-4612	-4613	
3824	28	22	0.00	0.00		-4602	-4584	-4588	-4604
3824	28	22	0.00	0.00		-4584	-4566	-4572	-4588
3824	28	22	0.00	0.00		-4566	-4549	-4556	-4572
3824	28	22	0.00	0.00		-4549	-4536	-4544	-4556
3824	28	22	0.00	0.00		-4536	-4531	-4538	-4544
3824	28	22	0.00	0.00		-4538	-4540	-4552	-4544
3824	28	22	0.00	0.00		-4540	-4553	-4561	-4552
3824	28	22	0.00	0.00		-4553	-4568	-4575	-4561
3824	28	22	0.00	0.00		-4568	-4578	-4589	-4575
3824	28	22	0.00	0.00		-4578	-4593	-4598	-4589
3824	28	22	0.00	0.00		-4593	-4610	-4613	-4598
3824	28	22	0.00	0.00		-4613	-4614	-4608	-4598
3824	28	22	0.00	0.00		-4614	-4615	-4607	-4608
3824	28	22	0.00	0.00		-4615	-4616	-4604	-4607
3824	28	22	0.00	0.00		-4617	-4602	-4604	-4616
3824	28	22	0.00	0.00		-4544	-4552	-4557	-4556
3824	28	22	0.00	0.00		-4561	-4571	-4557	-4552
3824	28	22	0.00	0.00		-4572	-4556	-4557	-4571
3824	28	22	0.00	0.00		-4575	-4583	-4571	-4561
3824	28	22	0.00	0.00		-4575	-4589	-4592	-4583

Carichi

Condizioni di carico elementari

Simbologia

CCE = Numero della condizione di carico elementare
 Comm. = Commento
 Tipo CCE = Tipo di CCE per calcolo agli stati limite
 Sic. = Contributo alla sicurezza
 F = a favore
 S = a sfavore
 A = ambigua
 Var. = Tipo di variabilità
 B = di base
 I = indipendente
 A = ambigua
 Dir. = Direzione del vento
 Tipo = Tipologia di pressione vento
 M = Massimizzata
 E = Esterna
 I = Interna
 Mx = Moltiplicatore della massa in dir. X
 My = Moltiplicatore della massa in dir. Y
 Mz = Moltiplicatore della massa in dir. Z
 Jpx = Moltiplicatore del momento d'inerzia intorno all'asse X
 Jpy = Moltiplicatore del momento d'inerzia intorno all'asse Y
 Jpz = Moltiplicatore del momento d'inerzia intorno all'asse Z

CCE	Comm.	Tipo CCE	Sic.	Var.	Dir. <grad>	Tipo	Mx	My	Mz	Jpx	Jpy	Jpz
1	Peso proprio	1 D.M. 18 Permanenti strutturali	S	--	--	--	1.00	1.00	1.00	0.00	0.00	1.00
2	Permanenti G1	1 D.M. 18 Permanenti strutturali	S	--	--	--	1.00	1.00	1.00	0.00	0.00	1.00
3	Permanenti NS G2	2 D.M. 18 Permanenti non strutturali	S	--	--	--	1.00	1.00	1.00	0.00	0.00	1.00
4	Variabili impalc. (pieno)	5 D.M. 18 Variabili Categoria C - Ambienti suscettibili di affollamento	S	B	--	--	1.00	1.00	1.00	0.00	0.00	1.00
5	Variabili impalc. (caso 1)	5 D.M. 18 Variabili Categoria C - Ambienti suscettibili di affollamento	S	B	--	--	1.00	1.00	1.00	0.00	0.00	1.00
6	Variabili impalc. (caso 2)	5 D.M. 18 Variabili Categoria C - Ambienti suscettibili di affollamento	S	B	--	--	1.00	1.00	1.00	0.00	0.00	1.00
7	Variabili impalc. (caso 3)	5 D.M. 18 Variabili Categoria C - Ambienti suscettibili di affollamento	S	B	--	--	1.00	1.00	1.00	0.00	0.00	1.00
8	Variabili impalc. (caso 4) tors	5 D.M. 18 Variabili Categoria C - Ambienti suscettibili di affollamento	S	B	--	--	1.00	1.00	1.00	0.00	0.00	1.00
9	Var. termiche	10 D.M. 18 Variabili Variazioni termiche	S	B	--	--	1.00	1.00	0.00	0.00	0.00	1.00
10	Vento +X	11 D.M. 18 Variabili Vento	S	A	0.00	M	0.00	0.00	0.00	0.00	0.00	0.00
11	Vento +Z vertic.	11 D.M. 18 Variabili Vento	S	A	0.00	M	0.00	0.00	0.00	0.00	0.00	0.00
12	Vento mz tors.	11 D.M. 18 Variabili Vento	S	A	0.00	M	0.00	0.00	0.00	0.00	0.00	0.00

Elenco carichi nodi

Condizione di carico n. 6: Variabili impalc. (caso 2)

Carichi concentrati

Simbologia

Nodo = Numero del nodo
 Fx = Componente X della forza applicata
 Fy = Componente Y della forza applicata
 Fz = Componente Z della forza applicata
 Mx = Momento intorno all'asse X
 My = Momento intorno all'asse Y
 Mz = Momento intorno all'asse Z

Nodo	Fx <daN>	Fy <daN>	Fz <daN>	Mx <daNm>	My <daNm>	Mz <daNm>
-10251	0.00	0.00	1.00	0.00	0.00	0.00

Elenco carichi aste

Condizione di carico n. 1: Peso proprio

Elenco peso proprio aste

Simbologia

Sez. = Numero della sezione
 Comm. = Commento
 A = Area
 Mat. = Materiale
 P = Peso specifico
 PL = Peso specifico a metro lineare

Sez.	Comm.	A <cmq>	Mat.	P <daN/mc>	PL <daN/m>
31	Tubo circolare d=114.3x6 mm - S355	20.414100	Acciaio	7850.00	16.03
32	Tubo 60x80x5 mm - S355	13.000000	Acciaio	7850.00	10.21
33	Tubo 60x100x5 mm - S355	15.000000	Acciaio	7850.00	11.78
34	Tubo 80x120x5 mm - S355	19.000000	Acciaio	7850.00	14.91
35	2 L80x60x8 - dist 6 mm - S275	21.465700	Acciaio	7850.00	16.85
36	Nervatura 50x6 mm - S275	5.640000	Acciaio	7850.00	4.43
37	2 L80x60x8 - dist 6 mm - S275	21.465700	Acciaio	7850.00	16.85
38	Tubo 80x80x4 mm - S235	12.160000	Acciaio	7850.00	9.55

39	Tubo circolare d=70x4 mm - S355	8.293810	Acciaio	7850.00	6.51
47	2 L80x60x8 - dist 6 mm - S275	21.465700	Acciaio	7850.00	16.85
48	Tubo circolare d=101.6x6 mm - S355	18.020200	Acciaio	7850.00	14.15
50	Tubo circolare d=90x4 mm - S355	10.807100	Acciaio	7850.00	8.48
52	T 80x80x6 mm - S275	9.240000	Acciaio	7850.00	7.25
53	Tubo 60x60x4 mm - S235	8.960000	Acciaio	7850.00	7.03
54	L80x8 mm - S275	12.267400	Acciaio	7850.00	9.63
58	Appoggio travi - 200x200	400.000000	Acciaio	7850.00	314.00
61	Tubo 60x120x4 mm - S235	13.760000	Acciaio	7850.00	10.80
68	Tubo 80x100x(2x5+6) mm - S355 (32)	26.240000	Acciaio	7850.00	20.60

Elenco carichi aste

Condizione di carico n. 3: Permanenti NS G2

Carichi distribuiti

Simbologia

- Asta = Numero dell'asta
- N1 = Nodo iniziale
- N2 = Nodo finale
- E = Elemento provenienza del carico
- S = Solaio
- T = Tamponatura
- NE = Numero elemento di provenienza del carico
- T = Tipo di carico
- QA = Primo carico accidentale
- QA2 = Secondo carico accidentale
- QA3 = Terzo carico accidentale
- QPS = Carico permanente strutturale
- QPN = Carico permanente non strutturale
- VE = Vento
- M = Manuale
- DC = Direzione del carico
- XG, YG, ZG = secondo gli assi globali
- XL, YL, ZL = secondo gli assi locali
- Xi = Distanza iniziale
- Qi = Carico iniziale
- Xf = Distanza finale
- Qf = Carico finale

Asta	N1	N2	E	N	T	DC	Xi	Qi	Xf	Qf	Asta	N1	N2	E	N	T	DC	Xi	Qi	Xf	Qf
							<m>	<daN/m>	<m>	<daN/m>								<m>	<daN/m>	<m>	<daN/m>
3556	-5430	-5493	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-5493	-5588	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-5588	-5657	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-5657	-5725	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-5725	-5789	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-5789	-5835	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-5835	-5877	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-5877	-5986	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-5986	-6059	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-6059	-6127	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-6127	-6184	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-6184	-6234	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-6234	-6295	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-6295	-6363	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-6363	-6476	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-6476	-6535	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-6535	-6613	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-6613	-6666	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-6666	-6741	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-6741	-6826	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-6826	-6900	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-6900	-6991	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-6991	-7050	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-7050	-7130	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-7130	-7193	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-7193	-7256	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-7256	-7290	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-7290	-7340	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-7340	-7456	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-7456	-7492	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-7492	-7567	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-7567	-7654	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-7654	-7697	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-7697	-7800	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-7800	-7921	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-7921	-7967	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-7967	-8021	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-8021	-8147	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-8147	-8221	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-8221	-8309	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-8309	-8370	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-8370	-8417	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-8417	-8468	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-8468	-8530	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-8530	-8615	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-8615	-8712	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-8712	-8801	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-8801	-8901	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-8901	-8975	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-8975	-9068	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-9068	-9142	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-9142	-9200	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-9200	-9276	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-9276	-9367	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-9367	-9433	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-9433	-9502	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-9502	-9543	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-9543	-9591	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-9591	-9633	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-9633	-9734	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-9734	-9846	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-9846	-9941	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-9941	-10027	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-10027	-10119	S	--	M	ZG	0.00	30.00	0.17	30.00
3556	-10119	-10188	S	--	M	ZG	0.00	30.00	0.17	30.00	3556	-10188	-10243	S	--	M	ZG	0.00	30.00	0.17	30.00
3562	-4660	-4681	S	--	M	ZG	0.00	30.00	0.16	30.00	3562	-4681	-4698	S	--	M	ZG	0.00	30.00	0.16	30.00
3562	-4698	-4757	S	--	M	ZG	0.00	30.00	0.17	30.00	3562	-4757	-4814	S	--	M	ZG	0.00	30.00	0.17	30.00
3562	-4814	-4869	S	--	M	ZG	0.00	30.00	0.17	30.00	3562	-4869	-4934	S	--	M	ZG	0.00	30.00	0.17	30.00
3562	-4934	-4997	S	--	M	ZG	0.00	30.00	0.17	30.00	3562	-4997	-5051	S	--	M	ZG	0.00	30.00	0.17	30.00
3562	-5051	-5129	S	--	M	ZG	0.00	30.00	0.17	30.00	3562	-5129	-5214	S	--	M	ZG	0.00	30.00	0.17	30.00

3562	-5214	-5279	S--	MZG	0.00	30.00	0.17	30.00	3562	-5279	-5330	S--	MZG	0.00	30.00	0.17	30.00
3562	-5330	-5384	S--	MZG	0.00	30.00	0.17	30.00	3562	-5384	-5446	S--	MZG	0.00	30.00	0.17	30.00
3562	-5446	-5509	S--	MZG	0.00	30.00	0.17	30.00	3562	-5509	-5604	S--	MZG	0.00	30.00	0.17	30.00
3562	-5604	-5673	S--	MZG	0.00	30.00	0.17	30.00	3562	-5673	-5744	S--	MZG	0.00	30.00	0.17	30.00
3562	-5744	-5805	S--	MZG	0.00	30.00	0.17	30.00	3562	-5805	-5851	S--	MZG	0.00	30.00	0.17	30.00
3562	-5851	-5893	S--	MZG	0.00	30.00	0.17	30.00	3562	-5893	-5972	S--	MZG	0.00	30.00	0.17	30.00
3562	-5972	-6075	S--	MZG	0.00	30.00	0.17	30.00	3562	-6075	-6143	S--	MZG	0.00	30.00	0.17	30.00
3562	-6143	-6200	S--	MZG	0.00	30.00	0.17	30.00	3562	-6200	-6252	S--	MZG	0.00	30.00	0.17	30.00
3562	-6252	-6311	S--	MZG	0.00	30.00	0.17	30.00	3562	-6311	-6379	S--	MZG	0.00	30.00	0.17	30.00
3562	-6379	-6492	S--	MZG	0.00	30.00	0.17	30.00	3562	-6492	-6556	S--	MZG	0.00	30.00	0.17	30.00
3562	-6556	-6629	S--	MZG	0.00	30.00	0.17	30.00	3562	-6629	-6693	S--	MZG	0.00	30.00	0.17	30.00
3562	-6693	-6757	S--	MZG	0.00	30.00	0.17	30.00	3562	-6757	-6842	S--	MZG	0.00	30.00	0.17	30.00
3562	-6842	-6901	S--	MZG	0.00	30.00	0.17	30.00	3562	-6901	-7007	S--	MZG	0.00	30.00	0.17	30.00
3562	-7007	-7066	S--	MZG	0.00	30.00	0.17	30.00	3562	-7066	-7146	S--	MZG	0.00	30.00	0.17	30.00
3562	-7146	-7209	S--	MZG	0.00	30.00	0.17	30.00	3562	-7209	-7272	S--	MZG	0.00	30.00	0.17	30.00
3562	-7272	-7306	S--	MZG	0.00	30.00	0.17	30.00	3562	-7306	-7356	S--	MZG	0.00	30.00	0.17	30.00
3562	-7356	-7472	S--	MZG	0.00	30.00	0.17	30.00	3562	-7472	-7508	S--	MZG	0.00	30.00	0.17	30.00
3562	-7508	-7586	S--	MZG	0.00	30.00	0.17	30.00	3562	-7586	-7671	S--	MZG	0.00	30.00	0.17	30.00
3562	-7671	-7723	S--	MZG	0.00	30.00	0.17	30.00	3562	-7723	-7813	S--	MZG	0.00	30.00	0.17	30.00
3562	-7813	-7937	S--	MZG	0.00	30.00	0.17	30.00	3562	-7937	-7983	S--	MZG	0.00	30.00	0.17	30.00
3562	-7983	-8037	S--	MZG	0.00	30.00	0.17	30.00	3562	-8037	-8163	S--	MZG	0.00	30.00	0.17	30.00
3562	-8163	-8237	S--	MZG	0.00	30.00	0.17	30.00	3562	-8237	-8325	S--	MZG	0.00	30.00	0.17	30.00
3562	-8325	-8386	S--	MZG	0.00	30.00	0.17	30.00	3562	-8386	-8433	S--	MZG	0.00	30.00	0.17	30.00
3562	-8433	-8486	S--	MZG	0.00	30.00	0.17	30.00	3562	-8486	-8546	S--	MZG	0.00	30.00	0.17	30.00
3562	-8546	-8635	S--	MZG	0.00	30.00	0.17	30.00	3562	-8635	-8728	S--	MZG	0.00	30.00	0.17	30.00
3562	-8728	-8809	S--	MZG	0.00	30.00	0.17	30.00	3562	-8809	-8917	S--	MZG	0.00	30.00	0.17	30.00
3562	-8917	-8991	S--	MZG	0.00	30.00	0.17	30.00	3562	-8991	-9100	S--	MZG	0.00	30.00	0.17	30.00
3562	-9100	-9158	S--	MZG	0.00	30.00	0.17	30.00	3562	-9158	-9216	S--	MZG	0.00	30.00	0.17	30.00
3562	-9216	-9292	S--	MZG	0.00	30.00	0.17	30.00	3562	-9292	-9383	S--	MZG	0.00	30.00	0.17	30.00
3562	-9383	-9449	S--	MZG	0.00	30.00	0.17	30.00	3562	-9449	-9507	S--	MZG	0.00	30.00	0.17	30.00
3562	-9507	-9559	S--	MZG	0.00	30.00	0.17	30.00	3562	-9559	-9607	S--	MZG	0.00	30.00	0.17	30.00
3562	-9607	-9649	S--	MZG	0.00	30.00	0.17	30.00	3562	-9649	-9747	S--	MZG	0.00	30.00	0.17	30.00
3562	-9747	-9863	S--	MZG	0.00	30.00	0.17	30.00	3562	-9863	-9974	S--	MZG	0.00	30.00	0.17	30.00
3562	-9974	-10043	S--	MZG	0.00	30.00	0.17	30.00	3562	-10043	-10135	S--	MZG	0.00	30.00	0.17	30.00
3562	-10135	-10201	S--	MZG	0.00	30.00	0.17	30.00	3562	-10201	-10257	S--	MZG	0.00	30.00	0.17	30.00
3566	-4526	-4524	S--	MZG	0.00	30.00	0.14	30.00	3566	-4528	-4526	S--	MZG	0.00	30.00	0.14	30.00
3568	-4532	-4528	S--	MZG	0.00	30.00	0.14	30.00	3568	-4539	-4532	S--	MZG	0.00	30.00	0.14	30.00
3568	-4541	-4539	S--	MZG	0.00	30.00	0.14	30.00	3570	-4554	-4541	S--	MZG	0.00	30.00	0.17	30.00
3570	-4569	-4554	S--	MZG	0.00	30.00	0.17	30.00	3570	-4579	-4569	S--	MZG	0.00	30.00	0.17	30.00
3571	-4540	-4553	S--	MZG	0.00	30.00	0.17	30.00	3571	-4553	-4568	S--	MZG	0.00	30.00	0.17	30.00
3571	-4568	-4578	S--	MZG	0.00	30.00	0.17	30.00	3574	-4594	-4579	S--	MZG	0.00	30.00	0.14	30.00
3574	-4611	-4594	S--	MZG	0.00	30.00	0.14	30.00	3574	-4626	-4611	S--	MZG	0.00	30.00	0.14	30.00
3575	-4578	-4593	S--	MZG	0.00	30.00	0.14	30.00	3575	-4593	-4610	S--	MZG	0.00	30.00	0.14	30.00
3575	-4610	-4612	S--	MZG	0.00	30.00	0.14	30.00	3579	-4628	-4626	S--	MZG	0.00	30.00	0.16	30.00
3579	-4643	-4628	S--	MZG	0.00	30.00	0.16	30.00	3579	-4660	-4643	S--	MZG	0.00	30.00	0.16	30.00
3580	-4612	-4627	S--	MZG	0.00	30.00	0.16	30.00	3580	-4627	-4642	S--	MZG	0.00	30.00	0.16	30.00
3580	-4642	-4659	S--	MZG	0.00	30.00	0.16	30.00	3997	-4538	-4540	S--	MZG	0.00	30.00	0.14	30.00
3997	-4531	-4538	S--	MZG	0.00	30.00	0.14	30.00	3997	-4527	-4531	S--	MZG	0.00	30.00	0.14	30.00
3999	-4525	-4527	S--	MZG	0.00	30.00	0.14	30.00	3999	-4524	-4525	S--	MZG	0.00	30.00	0.14	30.00

Elenco carichi aste

Condizione di carico n. 9: Var. termiche

Carichi distribuiti

Simbologia

Asta = Numero dell'asta

N1 = Nodo iniziale

N2 = Nodo finale

DT = Incremento di temperatura

Gy = Gradiente termico in dir. Y

Gz = Gradiente termico in dir. Z

Asta	N1	N2	DT <°C>	Gy <°C/m>	Gz <°C/m>
2003	1902	-4691	25.00		
2024	1902	-5439	25.00		
2040	1901	-5842	25.00		
2066	-2477	1901	25.00		
2066	-2442	-2426	25.00		
2066	-2363	-2360	25.00		
2066	-2356	-2351	25.00		
2536	2402	-9376	25.00		
2542	2402	-9740	25.00		
2590	-2408	-2437	25.00		
2590	-2463	-2486	25.00		
2590	-2541	2401	25.00		
2597	-2409	-2438	25.00		
2597	-2464	-2487	25.00		
2004	1901	-4689	25.00		
2025	1901	-5437	25.00		
2041	1902	-5844	25.00		
2066	1901	-2442	25.00		
2066	-2426	-2363	25.00		
2066	-2360	-2356	25.00		
2535	2401	-9374	25.00		
2541	2401	-9727	25.00		
2590	-2351	-2408	25.00		
2590	-2437	-2463	25.00		
2590	-2486	-2541	25.00		
2597	-2352	-2409	25.00		
2597	-2438	-2464	25.00		
2597	-2487	-2539	25.00		

2597	-2539	2402	25.00			2703	-5038	-5037	25.00		
2703	-5039	-5038	25.00			2703	-5040	-5039	25.00		
2703	-5041	-5040	25.00			2703	-5042	-5041	25.00		
2703	2901	-5042	25.00			2703	-5043	2901	25.00		
2703	-5044	-5043	25.00			2703	-5045	-5044	25.00		
2703	2902	-5045	25.00			2703	-5046	2902	25.00		
2703	-5047	-5046	25.00			2703	-5048	-5047	25.00		
2703	-5049	-5048	25.00			2703	-5050	-5049	25.00		
2703	-5051	-5050	25.00			2819	1901	-2497	25.00		
2819	-2497	-2643	25.00			2819	-2643	-3198	25.00		
2819	-3198	2901	25.00			2819	-2478	1902	25.00		
2819	1902	-2441	25.00			2819	-2441	-2427	25.00		
2819	-2427	-2405	25.00			2819	-2405	-2361	25.00		
2819	-2361	-2357	25.00			2819	-2357	-2352	25.00		
2820	1902	-2498	25.00			2820	-2498	-2644	25.00		
2820	-2644	-3199	25.00			2820	-3199	2902	25.00		
3116	-10244	-10243	25.00			3116	-10245	-10244	25.00		
3116	-10246	-10245	25.00			3116	-10247	-10246	25.00		
3116	-10248	-10247	25.00			3116	3301	-10248	25.00		
3116	-10249	3301	25.00			3116	-10250	-10249	25.00		
3116	-10251	-10250	25.00			3116	3302	-10251	25.00		
3116	-10252	3302	25.00			3116	-10253	-10252	25.00		
3116	-10254	-10253	25.00			3116	-10255	-10254	25.00		
3116	-10256	-10255	25.00			3116	-10257	-10256	25.00		
3457	2401	-3082	25.00			3457	-3082	-3442	25.00		
3457	-3442	-4235	25.00			3457	-4235	-7091	25.00		
3457	-7091	3301	25.00			3458	2402	-3090	25.00		
3458	-3090	-3448	25.00			3458	-3448	-4236	25.00		
3458	-4236	-7092	25.00			3458	-7092	3302	25.00		
3501	-4612	-4613	25.00			3501	-4613	-4614	25.00		
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3562	-7508	-7586	25.00			3562	-7586	-7671	25.00		
3562	-7671	-7723	25.00			3562	-7723	-7813	25.00		
3562	-7813	-7937	25.00			3562	-7937	-7983	25.00		
3562	-7983	-8037	25.00			3562	-8037	-8163	25.00		
3562	-8163	-8237	25.00			3562	-8237	-8325	25.00		
3562	-8325	-8386	25.00			3562	-8386	-8433	25.00		
3562	-8433	-8486	25.00			3562	-8486	-8546	25.00		
3562	-8546	-8635	25.00			3562	-8635	-8728	25.00		
3562	-8728	-8809	25.00			3562	-8809	-8917	25.00		
3562	-8917	-8991	25.00			3562	-8991	-9100	25.00		
3562	-9100	-9158	25.00			3562	-9158	-9216	25.00		
3562	-9216	-9292	25.00			3562	-9292	-9383	25.00		
3562	-9383	-9449	25.00			3562	-9449	-9507	25.00		
3562	-9507	-9559	25.00			3562	-9559	-9607	25.00		
3562	-9607	-9649	25.00			3562	-9649	-9747	25.00		
3562	-9747	-9863	25.00			3562	-9863	-9974	25.00		
3562	-9974	-10043	25.00			3562	-10043	-10135	25.00		
3562	-10135	-10201	25.00			3562	-10201	-10257	25.00		
3566	-4526	-4524	25.00			3566	-4526	-4526	25.00		
3568	-4532	-4528	25.00			3568	-4539	-4532	25.00		
3568	-4541	-4539	25.00			3570	-4554	-4541	25.00		
3570	-4569	-4554	25.00			3570	-4579	-4569	25.00		
3571	-4540	-4553	25.00			3571	-4553	-4568	25.00		
3571	-4568	-4578	25.00			3574	-4594	-4579	25.00		
3574	-4611	-4594	25.00			3574	-4626	-4611	25.00		
3575	-4578	-4593	25.00			3575	-4593	-4610	25.00		
3575	-4610	-4612	25.00			3579	-4628	-4626	25.00		
3579	-4643	-4628	25.00			3579	-4660	-4643	25.00		
3580	-4612	-4627	25.00			3580	-4627	-4642	25.00		
3580	-4642	-4659	25.00			3583	-4198	-4683	25.00		
3584	-4199	-4697	25.00			3585	-3733	-4199	25.00		
3586	-3732	-4198	25.00			3587	-3273	-3732	25.00		
3588	-3268	-3733	25.00			3589	-3102	-3268	25.00		
3590	-3101	-3273	25.00			3591	-2878	-3102	25.00		
3592	-2877	-3101	25.00			3593	-2719	-2878	25.00		
3594	-2718	-2877	25.00			3595	-2478	-2546	25.00		
3595	-2546	-2592	25.00			3595	-2592	-3079	25.00		
3595	-3079	-4692	25.00			3596	-2477	-2545	25.00		
3596	-2545	-2591	25.00			3596	-2591	-3078	25.00		
3596	-3078	-3569	25.00			3596	-3569	-4688	25.00		

3597	-2591	-2718	25.00			3598	-2592	-2719	25.00		
3601	-5043	-4682	25.00			3602	-5045	-4698	25.00		
3605	-4446	-5050	25.00			3606	-4445	-5038	25.00		
3607	-4020	-4446	25.00			3608	-4019	-4445	25.00		
3609	-3396	-4019	25.00			3610	-3397	-4020	25.00		
3611	-3218	-3397	25.00			3612	-3217	-3396	25.00		
3613	-2964	-3218	25.00			3614	-2963	-3217	25.00		
3615	-2779	-2964	25.00			3616	-2778	-2963	25.00		
3617	-2644	-2779	25.00			3618	-2643	-2778	25.00		
3622	-5043	-5430	25.00			3623	-5045	-5446	25.00		
3626	-4936	-5445	25.00			3627	-4935	-5431	25.00		
3628	-4282	-4936	25.00			3629	-4281	-4935	25.00		
3630	-3588	-4281	25.00			3631	-3589	-4282	25.00		
3632	-3349	-3589	25.00			3633	-3348	-3588	25.00		
3634	-3062	-3348	25.00			3635	-3063	-3349	25.00		
3636	-2844	-3063	25.00			3637	-2843	-3062	25.00		
3638	-2698	-2843	25.00			3639	-2699	-2844	25.00		
3642	-2442	-2495	25.00			3642	-2495	-2698	25.00		
3642	-2698	-3322	25.00			3642	-3322	-5436	25.00		
3643	-2441	-2496	25.00			3643	-2496	-2699	25.00		
3643	-2699	-3323	25.00			3643	-3323	-5440	25.00		
3644	-5439	-5851	25.00			3645	-5437	-5835	25.00		
3646	-2442	-6191	25.00			3647	-2441	-6193	25.00		
3648	-5333	-5836	25.00			3649	-5334	-5850	25.00		
3650	-4700	-5334	25.00			3651	-4699	-5333	25.00		
3652	-3885	-4699	25.00			3653	-3886	-4700	25.00		
3654	-3467	-3885	25.00			3655	-3468	-3886	25.00		
3656	-3185	-3467	25.00			3657	-3186	-3468	25.00		
3658	-2905	-3186	25.00			3659	-2904	-3185	25.00		
3660	-2755	-2904	25.00			3661	-2756	-2905	25.00		
3662	-2426	-2520	25.00			3662	-2520	-2755	25.00		
3662	-2755	-3450	25.00			3662	-3450	-5841	25.00		
3663	-2427	-2521	25.00			3663	-2521	-2756	25.00		
3663	-2756	-3451	25.00			3663	-3451	-5845	25.00		
3664	-5842	-6234	25.00			3665	-5844	-6252	25.00		
3667	-2427	-6550	25.00			3668	-2426	-6548	25.00		
3669	-5746	-6242	25.00			3670	-5747	-6251	25.00		
3671	-5053	-5747	25.00			3672	-5052	-5746	25.00		
3673	-4148	-5052	25.00			3674	-4149	-5053	25.00		
3675	-3748	-4148	25.00			3676	-3749	-4149	25.00		
3677	-3308	-3749	25.00			3678	-3307	-3748	25.00		
3679	-2991	-3307	25.00			3680	-2992	-3308	25.00		
3681	-2811	-2991	25.00			3682	-2812	-2992	25.00		
3683	-2405	-2543	25.00			3683	-2543	-2812	25.00		
3683	-2812	-3697	25.00			3683	-3697	-6247	25.00		
3684	-2363	-2542	25.00			3684	-2542	-2811	25.00		
3684	-2811	-3696	25.00			3684	-3696	-6244	25.00		
3685	-6238	-6666	25.00			3686	-6246	-6693	25.00		
3687	-2405	-6917	25.00			3688	-2363	-6915	25.00		
3689	-6152	-6692	25.00			3690	-6151	-6687	25.00		
3691	-5447	-6151	25.00			3692	-5448	-6152	25.00		
3693	-4403	-5447	25.00			3694	-4404	-5448	25.00		
3695	-4039	-4404	25.00			3696	-4038	-4403	25.00		
3697	-3426	-4038	25.00			3698	-3427	-4039	25.00		
3699	-3120	-3426	25.00			3700	-3121	-3427	25.00		
3701	-2879	-3120	25.00			3702	-2880	-3121	25.00		
3703	-2360	-2554	25.00			3703	-2554	-2879	25.00		
3703	-2879	-3985	25.00			3703	-3985	-6670	25.00		
3704	-2361	-2555	25.00			3704	-2555	-2880	25.00		
3704	-2880	-3986	25.00			3704	-3986	-6673	25.00		
3705	-6672	-7146	25.00			3706	-6689	-7130	25.00		
3707	-2360	-7263	25.00			3708	-2361	-7265	25.00		
3709	-6559	-7145	25.00			3710	-6558	-7131	25.00		
3711	-5853	-6559	25.00			3712	-5852	-6558	25.00		
3713	-4870	-5852	25.00			3714	-4871	-5853	25.00		
3715	-4295	-4870	25.00			3716	-4296	-4871	25.00		
3717	-3663	-4295	25.00			3718	-3659	-4296	25.00		
3719	-3224	-3663	25.00			3720	-3225	-3659	25.00		
3721	-2966	-3225	25.00			3722	-2965	-3224	25.00		
3723	-2356	-2562	25.00			3723	-2562	-2965	25.00		
3723	-2965	-4251	25.00			3723	-4251	-7136	25.00		
3724	-2357	-2563	25.00			3724	-2563	-2966	25.00		
3724	-2966	-4252	25.00			3724	-4252	-7140	25.00		
3725	-7137	-7492	25.00			3726	-7139	-7508	25.00		
3727	-2356	-4104	25.00			3728	-2357	-4105	25.00		
3729	-7008	-7493	25.00			3730	-7009	-7507	25.00		
3731	-6253	-7009	25.00			3732	-6240	-7008	25.00		
3733	-5284	-6240	25.00			3734	-5285	-6253	25.00		
3735	-4711	-5284	25.00			3736	-4712	-5285	25.00		

3737	-3949	-4712	25.00			3738	-3955	-4711	25.00		
3739	-2352	-2589	25.00			3739	-2589	-3065	25.00		
3739	-3065	-4493	25.00			3739	-4493	-7502	25.00		
3740	-2351	-2588	25.00			3740	-2588	-3064	25.00		
3740	-3064	-4492	25.00			3740	-4492	-7498	25.00		
3741	-7974	-7492	25.00			3742	-7976	-7508	25.00		
3743	-2408	-4104	25.00			3744	-2409	-4105	25.00		
3745	-7358	-7982	25.00			3746	-7357	-7968	25.00		
3747	-6694	-7358	25.00			3748	-6674	-7357	25.00		
3749	-5681	-6694	25.00			3750	-5674	-6674	25.00		
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3753	-4223	-5065	25.00			3754	-4224	-5066	25.00		
3755	-3189	-3474	25.00			3756	-2409	-2639	25.00		
3756	-2639	-3189	25.00			3756	-3189	-5014	25.00		
3756	-5014	-7977	25.00			3757	-2408	-2638	25.00		
3757	-2638	-3193	25.00			3757	-3193	-5013	25.00		
3757	-5013	-7973	25.00			3758	-2438	-7807	25.00		
3759	-2437	-7805	25.00			3760	-8426	-7983	25.00		
3761	-8424	-7967	25.00			3762	-7814	-8418	25.00		
3763	-7815	-8432	25.00			3764	-7147	-7814	25.00		
3765	-7148	-7815	25.00			3766	-6100	-7147	25.00		
3767	-6101	-7148	25.00			3768	-5459	-6101	25.00		
3769	-5458	-6100	25.00			3770	-4471	-5458	25.00		
3771	-3764	-4471	25.00			3772	-3767	-4463	25.00		
3773	-3309	-3764	25.00			3774	-3317	-3767	25.00		
3775	-2437	-2697	25.00			3775	-2697	-3309	25.00		
3775	-3309	-5418	25.00			3775	-5418	-8423	25.00		
3776	-2438	-2692	25.00			3776	-2692	-3317	25.00		
3776	-3317	-5397	25.00			3776	-5397	-8427	25.00		
3777	-2464	-8230	25.00			3778	-2463	-8228	25.00		
3779	-8908	-8417	25.00			3780	-8910	-8433	25.00		
3781	-8327	-8916	25.00			3782	-8326	-8902	25.00		
3783	-7509	-8326	25.00			3784	-7510	-8327	25.00		
3785	-6494	-7510	25.00			3786	-6493	-7509	25.00		
3787	-5854	-6493	25.00			3788	-5855	-6494	25.00		
3789	-4965	-5855	25.00			3790	-4964	-5854	25.00		
3791	-4066	-4965	25.00			3792	-4065	-4964	25.00		
3793	-3440	-4065	25.00			3794	-3441	-4066	25.00		
3795	-2464	-2750	25.00			3795	-2750	-3441	25.00		
3795	-3441	-5817	25.00			3795	-5817	-8911	25.00		
3796	-2463	-2749	25.00			3796	-2749	-3440	25.00		
3796	-3440	-5807	25.00			3796	-5807	-8907	25.00		
3797	-2487	-8539	25.00			3798	-2486	-8537	25.00		
3799	-9376	-8917	25.00			3800	-9374	-8901	25.00		
3801	-8729	-9368	25.00			3802	-8730	-9382	25.00		
3803	-7984	-8729	25.00			3804	-7985	-8730	25.00		
3805	-6926	-7984	25.00			3806	-6927	-7985	25.00		
3807	-6269	-6927	25.00			3808	-6259	-6926	25.00		
3809	-5356	-6259	25.00			3810	-5357	-6269	25.00		
3811	-4322	-5356	25.00			3812	-4323	-5357	25.00		
3813	-3675	-4323	25.00			3814	-3674	-4322	25.00		
3815	-2486	-2806	25.00			3815	-2806	-3674	25.00		
3815	-3674	-6221	25.00			3815	-6221	-9373	25.00		
3816	-2487	-2807	25.00			3816	-2807	-3675	25.00		
3816	-3675	-6230	25.00			3816	-6230	-9377	25.00		
3817	-2541	-8982	25.00			3818	-2539	-8984	25.00		
3819	-9727	-9367	25.00			3820	-9740	-9383	25.00		
3821	-9218	-9746	25.00			3822	-9217	-9735	25.00		
3823	-8434	-9217	25.00			3824	-8435	-9218	25.00		
3825	-7309	-8434	25.00			3826	-7310	-8435	25.00		
3827	-6700	-7310	25.00			3828	-6699	-7309	25.00		
3829	-5766	-6700	25.00			3830	-5784	-6699	25.00		
3831	-4759	-5766	25.00			3832	-4758	-5784	25.00		
3833	-3956	-4758	25.00			3834	-3969	-4759	25.00		
3837	-2541	-2872	25.00			3837	-2872	-3956	25.00		
3837	-3956	-6659	25.00			3837	-6659	-9739	25.00		
3838	-2539	-2873	25.00			3838	-2873	-3969	25.00		
3838	-3969	-6660	25.00			3838	-6660	-9741	25.00		
3839	-10251	-9747	25.00			3840	-10249	-9734	25.00		
3843	-9609	-10256	25.00			3844	-9608	-10244	25.00		
3845	-8919	-9609	25.00			3846	-8918	-9608	25.00		
3847	-7727	-8918	25.00			3848	-7728	-8919	25.00		
3849	-7157	-7728	25.00			3850	-7156	-7727	25.00		
3851	-6174	-7156	25.00			3852	-6175	-7157	25.00		
3853	-5131	-6175	25.00			3854	-5130	-6174	25.00		
3855	-4235	-5130	25.00			3856	-4236	-5131	25.00		
3997	-4538	-4540	25.00			3997	-4531	-4538	25.00		
3997	-4527	-4531	25.00			3999	-4525	-4527	25.00		
3999	-4524	-4525	25.00			4553	-3065	-3360	25.00		

3556	-8417	-8468	S--	MZG	0.00	18.64	0.17	18.64	3556	-8468	-8530	S--	MZG	0.00	18.64	0.17	18.64
3556	-8530	-8615	S--	MZG	0.00	18.64	0.17	18.64	3556	-8615	-8712	S--	MZG	0.00	18.64	0.17	18.64
3556	-8712	-8801	S--	MZG	0.00	18.64	0.17	18.64	3556	-8801	-8901	S--	MZG	0.00	18.64	0.17	18.64
3556	-8901	-8975	S--	MZG	0.00	18.64	0.17	18.64	3556	-8975	-9068	S--	MZG	0.00	18.64	0.17	18.64
3556	-9068	-9142	S--	MZG	0.00	18.64	0.17	18.64	3556	-9142	-9200	S--	MZG	0.00	18.64	0.17	18.64
3556	-9200	-9276	S--	MZG	0.00	18.64	0.17	18.64	3556	-9276	-9367	S--	MZG	0.00	18.64	0.17	18.64
3556	-9367	-9433	S--	MZG	0.00	18.64	0.17	18.64	3556	-9433	-9502	S--	MZG	0.00	18.64	0.17	18.64
3556	-9502	-9543	S--	MZG	0.00	18.64	0.17	18.64	3556	-9543	-9591	S--	MZG	0.00	18.64	0.17	18.64
3556	-9591	-9633	S--	MZG	0.00	18.64	0.17	18.64	3556	-9633	-9734	S--	MZG	0.00	18.64	0.17	18.64
3556	-9734	-9846	S--	MZG	0.00	18.64	0.17	18.64	3556	-9846	-9941	S--	MZG	0.00	18.64	0.17	18.64
3556	-9941	-10027	S--	MZG	0.00	18.64	0.17	18.64	3556	-10027	-10119	S--	MZG	0.00	18.64	0.17	18.64
3556	-10119	-10188	S--	MZG	0.00	18.64	0.17	18.64	3556	-10188	-10243	S--	MZG	0.00	18.64	0.17	18.64
3562	-4660	-4681	S--	MZG	0.00	-18.64	0.16	-18.64	3562	-4681	-4698	S--	MZG	0.00	-18.64	0.16	-18.64
3562	-4698	-4757	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-4757	-4814	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-4814	-4869	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-4869	-4934	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-4934	-4997	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-4997	-5051	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-5051	-5129	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-5129	-5214	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-5214	-5279	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-5279	-5330	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-5330	-5384	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-5384	-5446	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-5446	-5509	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-5509	-5604	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-5604	-5673	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-5673	-5744	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-5744	-5805	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-5805	-5851	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-5851	-5893	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-5893	-5972	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-5972	-6075	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-6075	-6143	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-6143	-6200	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-6200	-6252	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-6252	-6311	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-6311	-6379	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-6379	-6492	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-6492	-6556	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-6556	-6629	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-6629	-6693	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-6693	-6757	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-6757	-6842	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-6842	-6901	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-6901	-7007	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-7007	-7066	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-7066	-7146	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-7146	-7209	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-7209	-7272	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-7272	-7306	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-7306	-7356	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-7356	-7472	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-7472	-7508	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-7508	-7586	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-7586	-7671	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-7671	-7723	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-7723	-7813	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-7813	-7937	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-7937	-7983	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-7983	-8037	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-8037	-8163	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-8163	-8237	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-8237	-8325	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-8325	-8386	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-8386	-8433	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-8433	-8486	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-8486	-8546	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-8546	-8635	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-8635	-8728	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-8728	-8809	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-8809	-8917	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-8917	-8991	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-8991	-9100	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-9100	-9158	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-9158	-9216	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-9216	-9292	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-9292	-9383	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-9383	-9449	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-9449	-9507	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-9507	-9559	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-9559	-9607	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-9607	-9649	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-9649	-9747	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-9747	-9863	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-9863	-9974	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-9974	-10043	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-10043	-10135	S--	MZG	0.00	-18.64	0.17	-18.64
3562	-10135	-10201	S--	MZG	0.00	-18.64	0.17	-18.64	3562	-10201	-10257	S--	MZG	0.00	-18.64	0.17	-18.64

Elenco peso proprio elementi bidimensionali

Simbologia

- Tb = Numero del tipo muro/elemento bidimensionale
- Comm. = Commento
- Spess. = Spessore
- Mat. = Materiale
- P = Peso specifico
- PQ = Peso specifico per unità di superficie

Tb	Comm.	Spess. <cm>	Mat.	P <daN/mc>	PQ <daN/mq>
25	Lamiera acciaio sp. 6 mm	0.60	Acciaio	7850.00	47.10
28	Lamiera sp. 4.0 mm + Leca cls1600 sp. 50 mm (t = 0)	0.81	Acciaio	7850.00	63.90
30	Parete tubo acciaio sp. 7 mm + Leca cls1600 sp.50 mm (t=0)	1.11	Acciaio	7850.00	87.45
32	Parete tubo campata sud - sp. 6 mm	0.60	Acciaio	7850.00	47.10
34	Lamiera ali a sbalzo sp. 4 mm	0.40	Acciaio	7850.00	31.40
38	Parete tubo becco sud - sp. 6 mm	0.60	Acciaio	7850.00	47.10

Elenco carichi elementi bidimensionali

Condizione di carico n. 2: Permanenti G1

Carichi uniformi

Simbologia

Bid. = Numero del muro/elemento bidimensionale

N1 = Nodo1

N2 = Nodo2

N3 = Nodo3

N4 = Nodo4

T = Tipo di carico

PP = Peso proprio

VE = Vento

M = Manuale

DC = Direzione del carico

G = secondo gli assi globali

L = secondo gli assi locali

Qx = Carico in dir. X

Qy = Carico in dir. Y

Qz = Carico in dir. Z

Bid.	N1	N2	N3	N4	T	DC	Qx <daN/mq>	Qy <daN/mq>	Qz <daN/mq>
2718	-3859	-3858	-3909	-3910	M	G	0.00	0.00	110.00
2718	-3676	-3664	-3712	-3719	M	G	0.00	0.00	110.00
2718	-3665	-3676	-3719	-3720	M	G	0.00	0.00	110.00
2718	-3572	-3571	-3610	-3611	M	G	0.00	0.00	110.00
2718	-3719	-3712	-3768	-3769	M	G	0.00	0.00	110.00
2718	-3720	-3719	-3769	-3765	M	G	0.00	0.00	110.00
2718	-3610	-3609	-3664	-3676	M	G	0.00	0.00	110.00
2718	-3571	-3570	-3609	-3610	M	G	0.00	0.00	110.00
2718	-3769	-3768	-3810	-3811	M	G	0.00	0.00	110.00
2718	-3765	-3769	-3811	-3812	M	G	0.00	0.00	110.00
2718	-3858	-3857	-3908	-3909	M	G	0.00	0.00	110.00
2718	-3957	-3950	-4000	-4001	M	G	0.00	0.00	110.00
2718	-3812	-3811	-3858	-3859	M	G	0.00	0.00	110.00
2718	-3909	-3908	-3950	-3957	M	G	0.00	0.00	110.00
2718	-3958	-3957	-4001	-4002	M	G	0.00	0.00	110.00
2718	-3811	-3810	-3857	-3858	M	G	0.00	0.00	110.00
2718	-3525	-3524	-3571	-3572	M	G	0.00	0.00	110.00
2718	-3910	-3909	-3957	-3958	M	G	0.00	0.00	110.00
2718	-3524	-3523	-3570	-3571	M	G	0.00	0.00	110.00
2718	-3611	-3610	-3676	-3665	M	G	0.00	0.00	110.00
2816	-3655	-3748	-4148	-4148	M	G	0.00	0.00	110.00
2817	-3947	-4038	-4403	-4403	M	G	0.00	0.00	110.00
2822	-4219	-3663	-4295	-4295	M	G	0.00	0.00	110.00
2843	-4149	-3749	-3656	-3656	M	G	0.00	0.00	110.00
2847	-4404	-4039	-3948	-3948	M	G	0.00	0.00	110.00
2848	-3659	-4296	-4220	-4220	M	G	0.00	0.00	110.00
2921	-4198	-4683	-4684	-4684	M	G	0.00	0.00	110.00
2921	-4198	-4684	-4685	-3732	M	G	0.00	0.00	110.00
2931	-6370	-3558	-3605	-6483	M	G	0.00	0.00	110.00
2933	-6102	-3664	-3712	-6001	M	G	0.00	0.00	110.00
2933	-6036	-3523	-3570	-6104	M	G	0.00	0.00	110.00
2933	-6104	-3570	-3609	-6172	M	G	0.00	0.00	110.00
2933	-6172	-3609	-3664	-6102	M	G	0.00	0.00	110.00
2933	-6001	-3712	-3768	-6206	M	G	0.00	0.00	110.00
2934	-4219	-4295	-4870	-4870	M	G	0.00	0.00	110.00
2935	-4670	-4653	-4655	-4672	M	G	0.00	0.00	110.00
2935	-4676	-4661	-4663	-4679	M	G	0.00	0.00	110.00
2935	-4804	-4747	-4746	-4803	M	G	0.00	0.00	110.00
2935	-4746	-4687	-4686	-4745	M	G	0.00	0.00	110.00
2935	-4858	-4803	-4802	-4857	M	G	0.00	0.00	110.00
2935	-4676	-4674	-4657	-4661	M	G	0.00	0.00	110.00
2935	-4864	-4809	-4808	-4863	M	G	0.00	0.00	110.00
2935	-4671	-4654	-4652	-4669	M	G	0.00	0.00	110.00
2935	-4747	-4688	-4687	-4746	M	G	0.00	0.00	110.00
2935	-4690	-4689	-4748	-4749	M	G	0.00	0.00	110.00
2935	-4697	-4680	-4677	-4696	M	G	0.00	0.00	110.00
2935	-4672	-4655	-4657	-4674	M	G	0.00	0.00	110.00
2935	-4855	-4800	-4799	-4854	M	G	0.00	0.00	110.00
2935	-4803	-4746	-4745	-4802	M	G	0.00	0.00	110.00
2935	-4669	-4652	-4651	-4668	M	G	0.00	0.00	110.00
2935	-4754	-4695	-4694	-4753	M	G	0.00	0.00	110.00
2935	-4859	-4804	-4803	-4858	M	G	0.00	0.00	110.00
2935	-4755	-4696	-4695	-4754	M	G	0.00	0.00	110.00
2935	-4813	-4756	-4755	-4812	M	G	0.00	0.00	110.00
2935	-4802	-4745	-4744	-4801	M	G	0.00	0.00	110.00
2935	-4656	-4673	-4675	-4658	M	G	0.00	0.00	110.00
2935	-4812	-4755	-4754	-4811	M	G	0.00	0.00	110.00
2935	-4867	-4812	-4811	-4866	M	G	0.00	0.00	110.00
2935	-4748	-4689	-4688	-4747	M	G	0.00	0.00	110.00
2935	-4666	-4649	-4648	-4665	M	G	0.00	0.00	110.00
2935	-4688	-4665	-4670	-4687	M	G	0.00	0.00	110.00
2935	-4694	-4695	-4675	-4673	M	G	0.00	0.00	110.00

2935	-4698	-4681	-4680	-4697	MG	0.00	0.00	110.00
2935	-4749	-4748	-4805	-4806	MG	0.00	0.00	110.00
2935	-4752	-4693	-4692	-4751	MG	0.00	0.00	110.00
2935	-4809	-4752	-4751	-4808	MG	0.00	0.00	110.00
2935	-4751	-4692	-4691	-4750	MG	0.00	0.00	110.00
2935	-4807	-4806	-4861	-4862	MG	0.00	0.00	110.00
2935	-4745	-4686	-4685	-4744	MG	0.00	0.00	110.00
2935	-4692	-4669	-4668	-4691	MG	0.00	0.00	110.00
2935	-4857	-4802	-4801	-4856	MG	0.00	0.00	110.00
2935	-4667	-4650	-4649	-4666	MG	0.00	0.00	110.00
2935	-4689	-4666	-4665	-4688	MG	0.00	0.00	110.00
2935	-4810	-4753	-4752	-4809	MG	0.00	0.00	110.00
2935	-4686	-4687	-4670	-4672	MG	0.00	0.00	110.00
2935	-4856	-4801	-4800	-4855	MG	0.00	0.00	110.00
2935	-4668	-4651	-4650	-4667	MG	0.00	0.00	110.00
2935	-4669	-4692	-4693	-4671	MG	0.00	0.00	110.00
2935	-4665	-4648	-4653	-4670	MG	0.00	0.00	110.00
2935	-4696	-4677	-4675	-4695	MG	0.00	0.00	110.00
2935	-4744	-4685	-4684	-4743	MG	0.00	0.00	110.00
2935	-4805	-4748	-4747	-4804	MG	0.00	0.00	110.00
2935	-4756	-4697	-4696	-4755	MG	0.00	0.00	110.00
2935	-4677	-4680	-4664	-4662	MG	0.00	0.00	110.00
2935	-4686	-4672	-4674	-4685	MG	0.00	0.00	110.00
2935	-4681	-4660	-4664	-4680	MG	0.00	0.00	110.00
2935	-4753	-4694	-4693	-4752	MG	0.00	0.00	110.00
2935	-4684	-4685	-4674	-4676	MG	0.00	0.00	110.00
2935	-4656	-4654	-4671	-4673	MG	0.00	0.00	110.00
2935	-4750	-4749	-4806	-4807	MG	0.00	0.00	110.00
2935	-4690	-4667	-4666	-4689	MG	0.00	0.00	110.00
2935	-4742	-4683	-4682	-4741	MG	0.00	0.00	110.00
2935	-4868	-4813	-4812	-4867	MG	0.00	0.00	110.00
2935	-4808	-4751	-4750	-4807	MG	0.00	0.00	110.00
2935	-4866	-4811	-4810	-4865	MG	0.00	0.00	110.00
2935	-4691	-4668	-4667	-4690	MG	0.00	0.00	110.00
2935	-4694	-4673	-4671	-4693	MG	0.00	0.00	110.00
2935	-4691	-4690	-4749	-4750	MG	0.00	0.00	110.00
2935	-4801	-4744	-4743	-4800	MG	0.00	0.00	110.00
2935	-4865	-4810	-4809	-4864	MG	0.00	0.00	110.00
2935	-4814	-4757	-4756	-4813	MG	0.00	0.00	110.00
2935	-4659	-4678	-4679	-4663	MG	0.00	0.00	110.00
2935	-4869	-4814	-4813	-4868	MG	0.00	0.00	110.00
2935	-4811	-4754	-4753	-4810	MG	0.00	0.00	110.00
2935	-4799	-4742	-4741	-4798	MG	0.00	0.00	110.00
2935	-4854	-4799	-4798	-4853	MG	0.00	0.00	110.00
2935	-4684	-4676	-4679	-4683	MG	0.00	0.00	110.00
2935	-4683	-4679	-4678	-4682	MG	0.00	0.00	110.00
2935	-4757	-4698	-4697	-4756	MG	0.00	0.00	110.00
2935	-4743	-4684	-4683	-4742	MG	0.00	0.00	110.00
2935	-4677	-4662	-4658	-4675	MG	0.00	0.00	110.00
2935	-4860	-4805	-4804	-4859	MG	0.00	0.00	110.00
2935	-4806	-4805	-4860	-4861	MG	0.00	0.00	110.00
2935	-4800	-4743	-4742	-4799	MG	0.00	0.00	110.00
2935	-4863	-4808	-4807	-4862	MG	0.00	0.00	110.00
2937	-6372	-3559	-3606	-6485	MG	0.00	0.00	110.00
2939	-6105	-3572	-3611	-6173	MG	0.00	0.00	110.00
2939	-6037	-3525	-3572	-6105	MG	0.00	0.00	110.00
2939	-6002	-3720	-3765	-6222	MG	0.00	0.00	110.00
2939	-6173	-3611	-3665	-6103	MG	0.00	0.00	110.00
2939	-6103	-3665	-3720	-6002	MG	0.00	0.00	110.00
2940	-4459	-3955	-4711	-4711	MG	0.00	0.00	110.00
2944	-5352	-3764	-4471	-4471	MG	0.00	0.00	110.00
2945	-4697	-4199	-4696	-4696	MG	0.00	0.00	110.00
2945	-4199	-3733	-4695	-4696	MG	0.00	0.00	110.00
2953	-4871	-4296	-4220	-4220	MG	0.00	0.00	110.00
2954	-3949	-4712	-4460	-4460	MG	0.00	0.00	110.00
2955	-5353	-4463	-3767	-3767	MG	0.00	0.00	110.00
3007	-3763	-4003	-6107	-5257	MG	0.00	0.00	110.00
3008	-3999	-3766	-5256	-6106	MG	0.00	0.00	110.00
3022	-4445	-5039	-5040	-4019	MG	0.00	0.00	110.00
3031	-6689	-3536	-3698	-6748	MG	0.00	0.00	110.00
3031	-6620	-3590	-3536	-6689	MG	0.00	0.00	110.00
3031	-6483	-3605	-3657	-6548	MG	0.00	0.00	110.00
3031	-6548	-3657	-3590	-6620	MG	0.00	0.00	110.00
3032	-6206	-3768	-3810	-6437	MG	0.00	0.00	110.00
3032	-6437	-3810	-3857	-6501	MG	0.00	0.00	110.00
3033	-3607	-4251	-7136	-7136	MG	0.00	0.00	110.00
3034	-5041	-4976	-4992	-5040	MG	0.00	0.00	110.00
3034	-4918	-4855	-4854	-4917	MG	0.00	0.00	110.00
3034	-5042	-4968	-4976	-5041	MG	0.00	0.00	110.00

3034	-4932	-4866	-4865	-4931	MG	0.00	0.00	110.00
3034	-4967	-4918	-4917	-4966	MG	0.00	0.00	110.00
3034	-5048	-4995	-4979	-5047	MG	0.00	0.00	110.00
3034	-4926	-4860	-4859	-4925	MG	0.00	0.00	110.00
3034	-4861	-4860	-4926	-4927	MG	0.00	0.00	110.00
3034	-4994	-4930	-4929	-4978	MG	0.00	0.00	110.00
3034	-4929	-4863	-4862	-4928	MG	0.00	0.00	110.00
3034	-4924	-4858	-4857	-4919	MG	0.00	0.00	110.00
3034	-4978	-4929	-4928	-4970	MG	0.00	0.00	110.00
3034	-4927	-4926	-4969	-4993	MG	0.00	0.00	110.00
3034	-4925	-4859	-4858	-4924	MG	0.00	0.00	110.00
3034	-4976	-4919	-4923	-4992	MG	0.00	0.00	110.00
3034	-4995	-4932	-4931	-4979	MG	0.00	0.00	110.00
3034	-5046	-4994	-4978	2902	MG	0.00	0.00	110.00
3034	-4969	-4926	-4925	-4977	MG	0.00	0.00	110.00
3034	-4919	-4857	-4856	-4923	MG	0.00	0.00	110.00
3034	-5051	-4997	-4980	-5050	MG	0.00	0.00	110.00
3034	2902	-4978	-4970	-5045	MG	0.00	0.00	110.00
3034	-5043	-4969	-4977	2901	MG	0.00	0.00	110.00
3034	-4920	-4867	-4866	-4932	MG	0.00	0.00	110.00
3034	-4992	-4923	-4918	-4967	MG	0.00	0.00	110.00
3034	-4996	-4920	-4932	-4995	MG	0.00	0.00	110.00
3034	-4923	-4856	-4855	-4918	MG	0.00	0.00	110.00
3034	-4930	-4864	-4863	-4929	MG	0.00	0.00	110.00
3034	-4997	-4934	-4933	-4980	MG	0.00	0.00	110.00
3034	-5039	-4967	-4966	-5038	MG	0.00	0.00	110.00
3034	2901	-4977	-4968	-5042	MG	0.00	0.00	110.00
3034	-4993	-4969	-5043	-5044	MG	0.00	0.00	110.00
3034	-4931	-4865	-4864	-4930	MG	0.00	0.00	110.00
3034	-4862	-4861	-4927	-4928	MG	0.00	0.00	110.00
3034	-5040	-4992	-4967	-5039	MG	0.00	0.00	110.00
3034	-4970	-4993	-5044	-5045	MG	0.00	0.00	110.00
3034	-4934	-4869	-4868	-4933	MG	0.00	0.00	110.00
3034	-4968	-4924	-4919	-4976	MG	0.00	0.00	110.00
3034	-4917	-4854	-4853	-4916	MG	0.00	0.00	110.00
3034	-5050	-4980	-4996	-5049	MG	0.00	0.00	110.00
3034	-5047	-4979	-4994	-5046	MG	0.00	0.00	110.00
3034	-4928	-4927	-4993	-4970	MG	0.00	0.00	110.00
3034	-4979	-4931	-4930	-4994	MG	0.00	0.00	110.00
3034	-5049	-4996	-4995	-5048	MG	0.00	0.00	110.00
3034	-4977	-4925	-4924	-4968	MG	0.00	0.00	110.00
3034	-4933	-4868	-4867	-4920	MG	0.00	0.00	110.00
3034	-5038	-4966	-4991	-5037	MG	0.00	0.00	110.00
3034	-4966	-4917	-4916	-4991	MG	0.00	0.00	110.00
3034	-4980	-4933	-4920	-4996	MG	0.00	0.00	110.00
3036	-6485	-3606	-3658	-6550	MG	0.00	0.00	110.00
3036	-6550	-3658	-3591	-6622	MG	0.00	0.00	110.00
3036	-6672	-3537	-3699	-6750	MG	0.00	0.00	110.00
3036	-6622	-3591	-3537	-6672	MG	0.00	0.00	110.00
3038	-4459	-4711	-5284	-5284	MG	0.00	0.00	110.00
3039	-6438	-3812	-3859	-6505	MG	0.00	0.00	110.00
3039	-6222	-3765	-3812	-6438	MG	0.00	0.00	110.00
3041	-4950	-4223	-5065	-5065	MG	0.00	0.00	110.00
3052	-4446	-4020	-5048	-5049	MG	0.00	0.00	110.00
3060	-4252	-3608	-7140	-7140	MG	0.00	0.00	110.00
3061	-5285	-4712	-4460	-4460	MG	0.00	0.00	110.00
3062	-4224	-5066	-4951	-4951	MG	0.00	0.00	110.00
3106	-4000	-3999	-6106	-6380	MG	0.00	0.00	110.00
3107	-4003	-4002	-6382	-6107	MG	0.00	0.00	110.00
3119	-4445	-5038	-5039	-5039	MG	0.00	0.00	110.00
3120	-4935	-5432	-5433	-4281	MG	0.00	0.00	110.00
3121	-6244	-3696	-3655	-6243	MG	0.00	0.00	110.00
3129	-7297	-4167	-4221	-7347	MG	0.00	0.00	110.00
3129	-6915	-3904	-3963	-6998	MG	0.00	0.00	110.00
3129	-6833	-3842	-3904	-6915	MG	0.00	0.00	110.00
3129	-7463	-4164	-4104	-7499	MG	0.00	0.00	110.00
3129	-7200	-3987	-4124	-7263	MG	0.00	0.00	110.00
3129	-6998	-3963	-3887	-7057	MG	0.00	0.00	110.00
3129	-7499	-4104	-4253	-7578	MG	0.00	0.00	110.00
3129	-7263	-4124	-4167	-7297	MG	0.00	0.00	110.00
3129	-7347	-4221	-4164	-7463	MG	0.00	0.00	110.00
3129	-6748	-3698	-3842	-6833	MG	0.00	0.00	110.00
3129	-7057	-3887	-3825	-7137	MG	0.00	0.00	110.00
3129	-7137	-3825	-3987	-7200	MG	0.00	0.00	110.00
3130	-6501	-3857	-3908	-6597	MG	0.00	0.00	110.00
3130	-6495	-3950	-4000	-6380	MG	0.00	0.00	110.00
3130	-6597	-3908	-3950	-6495	MG	0.00	0.00	110.00
3131	-5116	-5040	-5039	-5115	MG	0.00	0.00	110.00
3131	-5671	-5602	-5601	-5670	MG	0.00	0.00	110.00

3131	-5663	-5594	-5593	-5662	MG	0.00	0.00	110.00
3131	-5435	-5373	-5372	-5434	MG	0.00	0.00	110.00
3131	-5741	-5732	-5797	-5798	MG	0.00	0.00	110.00
3131	-5119	2901	-5042	-5118	MG	0.00	0.00	110.00
3131	-5129	-5051	-5050	-5128	MG	0.00	0.00	110.00
3131	-5200	-5115	-5114	-5199	MG	0.00	0.00	110.00
3131	-5325	-5274	-5273	-5324	MG	0.00	0.00	110.00
3131	-5795	-5731	-5730	-5794	MG	0.00	0.00	110.00
3131	-5594	-5499	-5498	-5593	MG	0.00	0.00	110.00
3131	-5592	-5497	-5496	-5591	MG	0.00	0.00	110.00
3131	-5204	-5119	-5118	-5203	MG	0.00	0.00	110.00
3131	-5277	-5212	-5211	-5276	MG	0.00	0.00	110.00
3131	-5591	-5496	-5495	-5590	MG	0.00	0.00	110.00
3131	-5203	-5118	-5117	-5202	MG	0.00	0.00	110.00
3131	-5805	-5744	-5736	-5804	MG	0.00	0.00	110.00
3131	-5735	-5670	-5669	-5734	MG	0.00	0.00	110.00
3131	-5505	-5442	-5441	-5504	MG	0.00	0.00	110.00
3131	-5432	-5370	-5369	-5431	MG	0.00	0.00	110.00
3131	-5445	-5383	-5382	-5444	MG	0.00	0.00	110.00
3131	-5744	-5673	-5672	-5736	MG	0.00	0.00	110.00
3131	-5120	-5043	2901	-5119	MG	0.00	0.00	110.00
3131	-5379	-5325	-5324	-5378	MG	0.00	0.00	110.00
3131	-5439	-5438	-5501	-5502	MG	0.00	0.00	110.00
3131	-5731	-5663	-5662	-5730	MG	0.00	0.00	110.00
3131	-5508	-5445	-5444	-5507	MG	0.00	0.00	110.00
3131	-5728	-5660	-5659	-5727	MG	0.00	0.00	110.00
3131	-5660	-5591	-5590	-5659	MG	0.00	0.00	110.00
3131	-5496	-5433	-5432	-5495	MG	0.00	0.00	110.00
3131	-5665	-5664	-5740	-5732	MG	0.00	0.00	110.00
3131	-5802	-5735	-5734	-5801	MG	0.00	0.00	110.00
3131	-5730	-5662	-5661	-5729	MG	0.00	0.00	110.00
3131	-5370	-5316	-5315	-5369	MG	0.00	0.00	110.00
3131	-5214	-5129	-5128	-5213	MG	0.00	0.00	110.00
3131	-5803	-5743	-5735	-5802	MG	0.00	0.00	110.00
3131	-5743	-5671	-5670	-5735	MG	0.00	0.00	110.00
3131	-5210	-5125	-5124	-5209	MG	0.00	0.00	110.00
3131	-5128	-5050	-5049	-5127	MG	0.00	0.00	110.00
3131	-5801	-5734	-5742	-5800	MG	0.00	0.00	110.00
3131	-5661	-5592	-5591	-5660	MG	0.00	0.00	110.00
3131	-5734	-5669	-5668	-5742	MG	0.00	0.00	110.00
3131	-5320	-5269	-5268	-5319	MG	0.00	0.00	110.00
3131	-5269	-5204	-5203	-5268	MG	0.00	0.00	110.00
3131	-5497	-5434	-5433	-5496	MG	0.00	0.00	110.00
3131	-5201	-5116	-5115	-5200	MG	0.00	0.00	110.00
3131	-5206	-5205	-5270	-5271	MG	0.00	0.00	110.00
3131	-5207	-5206	-5271	-5272	MG	0.00	0.00	110.00
3131	-5327	-5276	-5275	-5326	MG	0.00	0.00	110.00
3131	-5436	-5374	-5373	-5435	MG	0.00	0.00	110.00
3131	-5276	-5211	-5210	-5275	MG	0.00	0.00	110.00
3131	-5727	-5659	-5658	-5726	MG	0.00	0.00	110.00
3131	-5590	-5495	-5494	-5589	MG	0.00	0.00	110.00
3131	-5045	-5044	-5121	-5122	MG	0.00	0.00	110.00
3131	-5315	-5264	-5263	-5314	MG	0.00	0.00	110.00
3131	-5275	-5210	-5209	-5274	MG	0.00	0.00	110.00
3131	-5446	-5384	-5383	-5445	MG	0.00	0.00	110.00
3131	-5125	-5047	-5046	-5124	MG	0.00	0.00	110.00
3131	-5664	-5595	-5594	-5663	MG	0.00	0.00	110.00
3131	-5437	-5375	-5374	-5436	MG	0.00	0.00	110.00
3131	-5500	-5437	-5436	-5499	MG	0.00	0.00	110.00
3131	-5597	-5596	-5665	-5666	MG	0.00	0.00	110.00
3131	-5440	-5378	-5377	-5439	MG	0.00	0.00	110.00
3131	-5274	-5209	-5208	-5273	MG	0.00	0.00	110.00
3131	-5499	-5436	-5435	-5498	MG	0.00	0.00	110.00
3131	-5265	-5200	-5199	-5264	MG	0.00	0.00	110.00
3131	-5316	-5265	-5264	-5315	MG	0.00	0.00	110.00
3131	-5794	-5730	-5729	-5793	MG	0.00	0.00	110.00
3131	-5273	-5208	-5207	-5272	MG	0.00	0.00	110.00
3131	-5279	-5214	-5213	-5278	MG	0.00	0.00	110.00
3131	-5670	-5601	-5600	-5669	MG	0.00	0.00	110.00
3131	-5601	-5506	-5505	-5600	MG	0.00	0.00	110.00
3131	-5278	-5213	-5212	-5277	MG	0.00	0.00	110.00
3131	-5369	-5315	-5314	-5368	MG	0.00	0.00	110.00
3131	-5213	-5128	-5127	-5212	MG	0.00	0.00	110.00
3131	-5270	-5205	-5204	-5269	MG	0.00	0.00	110.00
3131	-5264	-5199	-5198	-5263	MG	0.00	0.00	110.00
3131	-5328	-5277	-5276	-5327	MG	0.00	0.00	110.00
3131	-5382	-5328	-5327	-5381	MG	0.00	0.00	110.00
3131	-5377	-5376	-5438	-5439	MG	0.00	0.00	110.00
3131	-5792	-5728	-5727	-5791	MG	0.00	0.00	110.00

3131	-5212	-5127	-5126	-5211	MG	0.00	0.00	110.00
3131	-5127	-5049	-5048	-5126	MG	0.00	0.00	110.00
3131	-5443	-5381	-5380	-5442	MG	0.00	0.00	110.00
3131	-5373	-5319	-5318	-5372	MG	0.00	0.00	110.00
3131	-5791	-5727	-5726	-5790	MG	0.00	0.00	110.00
3131	-5268	-5203	-5202	-5267	MG	0.00	0.00	110.00
3131	-5501	-5500	-5595	-5596	MG	0.00	0.00	110.00
3131	-5380	-5326	-5325	-5379	MG	0.00	0.00	110.00
3131	-5495	-5432	-5431	-5494	MG	0.00	0.00	110.00
3131	-5790	-5726	-5725	-5789	MG	0.00	0.00	110.00
3131	-5796	-5740	-5731	-5795	MG	0.00	0.00	110.00
3131	-5726	-5658	-5657	-5725	MG	0.00	0.00	110.00
3131	-5595	-5500	-5499	-5594	MG	0.00	0.00	110.00
3131	-5371	-5317	-5316	-5370	MG	0.00	0.00	110.00
3131	-5494	-5431	-5430	-5493	MG	0.00	0.00	110.00
3131	-5441	-5379	-5378	-5440	MG	0.00	0.00	110.00
3131	-5266	-5201	-5200	-5265	MG	0.00	0.00	110.00
3131	-5666	-5665	-5732	-5741	MG	0.00	0.00	110.00
3131	-5272	-5271	-5322	-5323	MG	0.00	0.00	110.00
3131	-5324	-5273	-5272	-5323	MG	0.00	0.00	110.00
3131	-5507	-5444	-5443	-5506	MG	0.00	0.00	110.00
3131	-5330	-5279	-5278	-5329	MG	0.00	0.00	110.00
3131	-5124	-5046	2902	-5123	MG	0.00	0.00	110.00
3131	-5502	-5501	-5596	-5597	MG	0.00	0.00	110.00
3131	-5732	-5740	-5796	-5797	MG	0.00	0.00	110.00
3131	-5383	-5329	-5328	-5382	MG	0.00	0.00	110.00
3131	-5329	-5278	-5277	-5328	MG	0.00	0.00	110.00
3131	-5205	-5120	-5119	-5204	MG	0.00	0.00	110.00
3131	-5506	-5443	-5442	-5505	MG	0.00	0.00	110.00
3131	-5321	-5270	-5269	-5320	MG	0.00	0.00	110.00
3131	-5374	-5320	-5319	-5373	MG	0.00	0.00	110.00
3131	-5199	-5114	-5113	-5198	MG	0.00	0.00	110.00
3131	-5669	-5600	-5599	-5668	MG	0.00	0.00	110.00
3131	-5376	-5375	-5437	-5438	MG	0.00	0.00	110.00
3131	-5600	-5505	-5504	-5599	MG	0.00	0.00	110.00
3131	-5326	-5275	-5274	-5325	MG	0.00	0.00	110.00
3131	-5271	-5270	-5321	-5322	MG	0.00	0.00	110.00
3131	-5599	-5504	-5503	-5598	MG	0.00	0.00	110.00
3131	-5381	-5327	-5326	-5380	MG	0.00	0.00	110.00
3131	-5211	-5126	-5125	-5210	MG	0.00	0.00	110.00
3131	-5659	-5590	-5589	-5658	MG	0.00	0.00	110.00
3131	-5673	-5604	-5603	-5672	MG	0.00	0.00	110.00
3131	-5442	-5380	-5379	-5441	MG	0.00	0.00	110.00
3131	-5317	-5266	-5265	-5316	MG	0.00	0.00	110.00
3131	-5503	-5440	-5439	-5502	MG	0.00	0.00	110.00
3131	-5509	-5446	-5445	-5508	MG	0.00	0.00	110.00
3131	-5740	-5664	-5663	-5731	MG	0.00	0.00	110.00
3131	-5202	-5117	-5116	-5201	MG	0.00	0.00	110.00
3131	-5589	-5494	-5493	-5588	MG	0.00	0.00	110.00
3131	-5433	-5371	-5370	-5432	MG	0.00	0.00	110.00
3131	-5603	-5508	-5507	-5602	MG	0.00	0.00	110.00
3131	-5596	-5595	-5664	-5665	MG	0.00	0.00	110.00
3131	-5208	-5123	-5122	-5207	MG	0.00	0.00	110.00
3131	-5602	-5507	-5506	-5601	MG	0.00	0.00	110.00
3131	-5323	-5322	-5376	-5377	MG	0.00	0.00	110.00
3131	-5378	-5324	-5323	-5377	MG	0.00	0.00	110.00
3131	-5319	-5268	-5267	-5318	MG	0.00	0.00	110.00
3131	-5742	-5668	-5667	-5733	MG	0.00	0.00	110.00
3131	-5504	-5441	-5440	-5503	MG	0.00	0.00	110.00
3131	-5114	-5038	-5037	-5113	MG	0.00	0.00	110.00
3131	-5672	-5603	-5602	-5671	MG	0.00	0.00	110.00
3131	-5431	-5369	-5368	-5430	MG	0.00	0.00	110.00
3131	-5729	-5661	-5660	-5728	MG	0.00	0.00	110.00
3131	-5793	-5729	-5728	-5792	MG	0.00	0.00	110.00
3131	-5438	-5437	-5500	-5501	MG	0.00	0.00	110.00
3131	-5267	-5202	-5201	-5266	MG	0.00	0.00	110.00
3131	-5658	-5589	-5588	-5657	MG	0.00	0.00	110.00
3131	-5209	-5124	-5123	-5208	MG	0.00	0.00	110.00
3131	-5126	-5048	-5047	-5125	MG	0.00	0.00	110.00
3131	-5118	-5042	-5041	-5117	MG	0.00	0.00	110.00
3131	-5372	-5318	-5317	-5371	MG	0.00	0.00	110.00
3131	-5122	-5121	-5206	-5207	MG	0.00	0.00	110.00
3131	-5121	-5120	-5205	-5206	MG	0.00	0.00	110.00
3131	-5668	-5599	-5598	-5667	MG	0.00	0.00	110.00
3131	-5604	-5509	-5508	-5603	MG	0.00	0.00	110.00
3131	-5598	-5503	-5502	-5597	MG	0.00	0.00	110.00
3131	-5322	-5321	-5375	-5376	MG	0.00	0.00	110.00
3131	-5117	-5041	-5040	-5116	MG	0.00	0.00	110.00
3131	-5115	-5039	-5038	-5114	MG	0.00	0.00	110.00

3131	-5733	-5667	-5666	-5741	MG	0.00	0.00	110.00
3131	-5804	-5736	-5743	-5803	MG	0.00	0.00	110.00
3131	-5318	-5267	-5266	-5317	MG	0.00	0.00	110.00
3131	-5044	-5043	-5120	-5121	MG	0.00	0.00	110.00
3131	-5667	-5598	-5597	-5666	MG	0.00	0.00	110.00
3131	-5498	-5435	-5434	-5497	MG	0.00	0.00	110.00
3131	-5593	-5498	-5497	-5592	MG	0.00	0.00	110.00
3131	-5736	-5672	-5671	-5743	MG	0.00	0.00	110.00
3131	-5384	-5330	-5329	-5383	MG	0.00	0.00	110.00
3131	-5662	-5593	-5592	-5661	MG	0.00	0.00	110.00
3131	-5444	-5382	-5381	-5443	MG	0.00	0.00	110.00
3131	-5375	-5321	-5320	-5374	MG	0.00	0.00	110.00
3131	-5434	-5372	-5371	-5433	MG	0.00	0.00	110.00
3131	-5800	-5742	-5733	-5799	MG	0.00	0.00	110.00
3131	-5799	-5733	-5741	-5798	MG	0.00	0.00	110.00
3131	-5123	2902	-5045	-5122	MG	0.00	0.00	110.00
3132	-6598	-3910	-3958	-6496	MG	0.00	0.00	110.00
3132	-6496	-3958	-4002	-6382	MG	0.00	0.00	110.00
3132	-6505	-3859	-3910	-6598	MG	0.00	0.00	110.00
3133	-7139	-3826	-3988	-7202	MG	0.00	0.00	110.00
3133	-7465	-4165	-4105	-7501	MG	0.00	0.00	110.00
3133	-6835	-3843	-3905	-6917	MG	0.00	0.00	110.00
3133	-6917	-3905	-3964	-7000	MG	0.00	0.00	110.00
3133	-7202	-3988	-4125	-7265	MG	0.00	0.00	110.00
3133	-6750	-3699	-3843	-6835	MG	0.00	0.00	110.00
3133	-7059	-3888	-3826	-7139	MG	0.00	0.00	110.00
3133	-7299	-4168	-4222	-7349	MG	0.00	0.00	110.00
3133	-7349	-4222	-4165	-7465	MG	0.00	0.00	110.00
3133	-7000	-3964	-3888	-7059	MG	0.00	0.00	110.00
3133	-7501	-4105	-4254	-7579	MG	0.00	0.00	110.00
3133	-7265	-4125	-4168	-7299	MG	0.00	0.00	110.00
3138	-5781	-4065	-4964	-4964	MG	0.00	0.00	110.00
3139	-5306	-3674	-6221	-6221	MG	0.00	0.00	110.00
3147	-5050	-4446	-5049	-5049	MG	0.00	0.00	110.00
3150	-4936	-4282	-5443	-5444	MG	0.00	0.00	110.00
3152	-3656	-3697	-6247	-6248	MG	0.00	0.00	110.00
3156	-5773	-4965	-4066	-4066	MG	0.00	0.00	110.00
3157	-3675	-5307	-6230	-6230	MG	0.00	0.00	110.00
3205	-5256	-4235	-7091	-7091	MG	0.00	0.00	110.00
3206	-4236	-5257	-7092	-7092	MG	0.00	0.00	110.00
3207	-4001	-4000	-6380	-6381	MG	0.00	0.00	110.00
3207	-4002	-4001	-6381	-6382	MG	0.00	0.00	110.00
3219	-4935	-5431	-5432	-5432	MG	0.00	0.00	110.00
3222	-5333	-5837	-5838	-4699	MG	0.00	0.00	110.00
3222	-5333	-5836	-5837	-5837	MG	0.00	0.00	110.00
3229	-6670	-3985	-3947	-6669	MG	0.00	0.00	110.00
3231	-7710	-4419	-4461	-7805	MG	0.00	0.00	110.00
3231	-7928	-4417	-4362	-7974	MG	0.00	0.00	110.00
3231	-7974	-4362	-4494	-8028	MG	0.00	0.00	110.00
3231	-7805	-4461	-4417	-7928	MG	0.00	0.00	110.00
3231	-7661	-4378	-4419	-7710	MG	0.00	0.00	110.00
3231	-7578	-4253	-4378	-7661	MG	0.00	0.00	110.00
3232	-3825	-3607	-7136	-7137	MG	0.00	0.00	110.00
3233	-7136	-4251	-4219	-7135	MG	0.00	0.00	110.00
3234	-5987	-5878	-5877	-5986	MG	0.00	0.00	110.00
3234	-5888	-5846	-5845	-5887	MG	0.00	0.00	110.00
3234	-6067	-6066	-6134	-6135	MG	0.00	0.00	110.00
3234	-6060	-5987	-5986	-6059	MG	0.00	0.00	110.00
3234	-6070	-5996	-5995	-6069	MG	0.00	0.00	110.00
3234	-6130	-6062	-6061	-6129	MG	0.00	0.00	110.00
3234	-5989	-5880	-5879	-5988	MG	0.00	0.00	110.00
3234	-6249	-6197	-6196	-6239	MG	0.00	0.00	110.00
3234	-6193	-6194	-6137	-6136	MG	0.00	0.00	110.00
3234	-6250	-6198	-6197	-6249	MG	0.00	0.00	110.00
3234	-6142	-6074	-6073	-6141	MG	0.00	0.00	110.00
3234	-6073	-5999	-5998	-6072	MG	0.00	0.00	110.00
3234	-5878	-5836	-5835	-5877	MG	0.00	0.00	110.00
3234	-6185	-6128	-6127	-6184	MG	0.00	0.00	110.00
3234	-5891	-5849	-5848	-5890	MG	0.00	0.00	110.00
3234	-6252	-6200	-6199	-6251	MG	0.00	0.00	110.00
3234	-6000	-5892	-5891	-5999	MG	0.00	0.00	110.00
3234	-5838	-5792	-5791	-5837	MG	0.00	0.00	110.00
3234	-6199	-6142	-6141	-6198	MG	0.00	0.00	110.00
3234	-6068	-6067	-6135	-6136	MG	0.00	0.00	110.00
3234	-5999	-5891	-5890	-5998	MG	0.00	0.00	110.00
3234	-6248	-6195	-6194	-6247	MG	0.00	0.00	110.00
3234	-6136	-6135	-6192	-6193	MG	0.00	0.00	110.00
3234	-6138	-6070	-6069	-6137	MG	0.00	0.00	110.00
3234	-6187	-6130	-6129	-6186	MG	0.00	0.00	110.00

3234	-6236	-6187	-6186	-6235	MG	0.00	0.00	110.00
3234	-5798	-5797	-5843	-5844	MG	0.00	0.00	110.00
3234	-5847	-5801	-5800	-5846	MG	0.00	0.00	110.00
3234	-6198	-6141	-6140	-6197	MG	0.00	0.00	110.00
3234	-6068	-6069	-5995	-6025	MG	0.00	0.00	110.00
3234	-6242	-6185	-6184	-6234	MG	0.00	0.00	110.00
3234	-6246	-6247	-6194	-6193	MG	0.00	0.00	110.00
3234	-5886	-5887	-5845	-5844	MG	0.00	0.00	110.00
3234	-6128	-6060	-6059	-6127	MG	0.00	0.00	110.00
3234	-6238	-6191	-6190	-6244	MG	0.00	0.00	110.00
3234	-6074	-6000	-5999	-6073	MG	0.00	0.00	110.00
3234	-5892	-5850	-5849	-5891	MG	0.00	0.00	110.00
3234	-5884	-5842	-5841	-5883	MG	0.00	0.00	110.00
3234	-5846	-5800	-5799	-5845	MG	0.00	0.00	110.00
3234	-5848	-5802	-5801	-5847	MG	0.00	0.00	110.00
3234	-5837	-5791	-5790	-5836	MG	0.00	0.00	110.00
3234	-5885	-5884	-5993	-5994	MG	0.00	0.00	110.00
3234	-5992	-5883	-5882	-5991	MG	0.00	0.00	110.00
3234	-6140	-6072	-6071	-6139	MG	0.00	0.00	110.00
3234	-5839	-5793	-5792	-5838	MG	0.00	0.00	110.00
3234	-6025	-5995	-5887	-5886	MG	0.00	0.00	110.00
3234	-5882	-5840	-5839	-5881	MG	0.00	0.00	110.00
3234	-5890	-5848	-5847	-5889	MG	0.00	0.00	110.00
3234	-5851	-5805	-5804	-5850	MG	0.00	0.00	110.00
3234	-6244	-6190	-6189	-6243	MG	0.00	0.00	110.00
3234	-6063	-5990	-5989	-6062	MG	0.00	0.00	110.00
3234	-5990	-5881	-5880	-5989	MG	0.00	0.00	110.00
3234	-6196	-6139	-6138	-6195	MG	0.00	0.00	110.00
3234	-5881	-5839	-5838	-5880	MG	0.00	0.00	110.00
3234	-5843	-5842	-5884	-5885	MG	0.00	0.00	110.00
3234	-5797	-5796	-5842	-5843	MG	0.00	0.00	110.00
3234	-5842	-5796	-5795	-5841	MG	0.00	0.00	110.00
3234	-6062	-5989	-5988	-6061	MG	0.00	0.00	110.00
3234	-5840	-5794	-5793	-5839	MG	0.00	0.00	110.00
3234	-5988	-5879	-5878	-5987	MG	0.00	0.00	110.00
3234	-5996	-5888	-5887	-5995	MG	0.00	0.00	110.00
3234	-5998	-5890	-5889	-5997	MG	0.00	0.00	110.00
3234	-6129	-6061	-6060	-6128	MG	0.00	0.00	110.00
3234	-5972	-5893	-5892	-6000	MG	0.00	0.00	110.00
3234	-5880	-5838	-5837	-5879	MG	0.00	0.00	110.00
3234	-6075	-5972	-6000	-6074	MG	0.00	0.00	110.00
3234	-5879	-5837	-5836	-5878	MG	0.00	0.00	110.00
3234	-5883	-5841	-5840	-5882	MG	0.00	0.00	110.00
3234	-6061	-5988	-5987	-6060	MG	0.00	0.00	110.00
3234	-6134	-6066	-6065	-6133	MG	0.00	0.00	110.00
3234	-6066	-5993	-5992	-6065	MG	0.00	0.00	110.00
3234	-5993	-5884	-5883	-5992	MG	0.00	0.00	110.00
3234	-5997	-5889	-5888	-5996	MG	0.00	0.00	110.00
3234	-6141	-6073	-6072	-6140	MG	0.00	0.00	110.00
3234	-6133	-6065	-6064	-6132	MG	0.00	0.00	110.00
3234	-6239	-6196	-6195	-6248	MG	0.00	0.00	110.00
3234	-6188	-6131	-6130	-6187	MG	0.00	0.00	110.00
3234	-6065	-5992	-5991	-6064	MG	0.00	0.00	110.00
3234	-5845	-5799	-5798	-5844	MG	0.00	0.00	110.00
3234	-6064	-5991	-5990	-6063	MG	0.00	0.00	110.00
3234	-5994	-5993	-6066	-6067	MG	0.00	0.00	110.00
3234	-5991	-5882	-5881	-5990	MG	0.00	0.00	110.00
3234	-5841	-5795	-5794	-5840	MG	0.00	0.00	110.00
3234	-6195	-6138	-6137	-6194	MG	0.00	0.00	110.00
3234	-5886	-5885	-5994	-6025	MG	0.00	0.00	110.00
3234	-6131	-6063	-6062	-6130	MG	0.00	0.00	110.00
3234	-6237	-6188	-6187	-6236	MG	0.00	0.00	110.00
3234	-6192	-6191	-6238	-6245	MG	0.00	0.00	110.00
3234	-6071	-5997	-5996	-6070	MG	0.00	0.00	110.00
3234	-6193	-6192	-6245	-6246	MG	0.00	0.00	110.00
3234	-5889	-5847	-5846	-5888	MG	0.00	0.00	110.00
3234	-5836	-5790	-5789	-5835	MG	0.00	0.00	110.00
3234	-6251	-6199	-6198	-6250	MG	0.00	0.00	110.00
3234	-5893	-5851	-5850	-5892	MG	0.00	0.00	110.00
3234	-6200	-6143	-6142	-6199	MG	0.00	0.00	110.00
3234	-5844	-5843	-5885	-5886	MG	0.00	0.00	110.00
3234	-6186	-6129	-6128	-6185	MG	0.00	0.00	110.00
3234	-6136	-6137	-6069	-6068	MG	0.00	0.00	110.00
3234	-6132	-6064	-6063	-6131	MG	0.00	0.00	110.00
3234	-5849	-5803	-5802	-5848	MG	0.00	0.00	110.00
3234	-6025	-5994	-6067	-6068	MG	0.00	0.00	110.00
3234	-6190	-6133	-6132	-6189	MG	0.00	0.00	110.00
3234	-6243	-6189	-6188	-6237	MG	0.00	0.00	110.00
3234	-5850	-5804	-5803	-5849	MG	0.00	0.00	110.00

3234	-6191	-6134	-6133	-6190	MG	0.00	0.00	110.00
3234	-6139	-6071	-6070	-6138	MG	0.00	0.00	110.00
3234	-6189	-6132	-6131	-6188	MG	0.00	0.00	110.00
3234	-6072	-5998	-5997	-6071	MG	0.00	0.00	110.00
3234	-6135	-6134	-6191	-6192	MG	0.00	0.00	110.00
3234	-6143	-6075	-6074	-6142	MG	0.00	0.00	110.00
3234	-6197	-6140	-6139	-6196	MG	0.00	0.00	110.00
3234	-6235	-6186	-6185	-6242	MG	0.00	0.00	110.00
3235	-7579	-4254	-4379	-7666	MG	0.00	0.00	110.00
3235	-7666	-4379	-4420	-7712	MG	0.00	0.00	110.00
3235	-7976	-4363	-4503	-8030	MG	0.00	0.00	110.00
3235	-7930	-4418	-4363	-7976	MG	0.00	0.00	110.00
3235	-7807	-4462	-4418	-7930	MG	0.00	0.00	110.00
3235	-7712	-4420	-4462	-7807	MG	0.00	0.00	110.00
3236	-4104	-3906	-7498	-7499	MG	0.00	0.00	110.00
3236	-3906	-4492	-7498	-7498	MG	0.00	0.00	110.00
3239	-4950	-5065	-5674	-5674	MG	0.00	0.00	110.00
3240	-4169	-5013	-7973	-7973	MG	0.00	0.00	110.00
3242	-5352	-4471	-5458	-5458	MG	0.00	0.00	110.00
3242	-5352	-5458	-6100	-6100	MG	0.00	0.00	110.00
3245	-5781	-4964	-5854	-5854	MG	0.00	0.00	110.00
3246	-6170	-4322	-5356	-5356	MG	0.00	0.00	110.00
3246	-6221	-3674	-4322	-6170	MG	0.00	0.00	110.00
3255	-5445	-4936	-5444	-5444	MG	0.00	0.00	110.00
3257	-5334	-4700	-5848	-5849	MG	0.00	0.00	110.00
3257	-5850	-5334	-5849	-5849	MG	0.00	0.00	110.00
3259	-3948	-3986	-6673	-6677	MG	0.00	0.00	110.00
3264	-4220	-4252	-7140	-7141	MG	0.00	0.00	110.00
3266	-3608	-3826	-7139	-7140	MG	0.00	0.00	110.00
3267	-4493	-3907	-7502	-7502	MG	0.00	0.00	110.00
3267	-3907	-4105	-7501	-7502	MG	0.00	0.00	110.00
3268	-5681	-5066	-4951	-4951	MG	0.00	0.00	110.00
3269	-5014	-4170	-7977	-7977	MG	0.00	0.00	110.00
3270	-4463	-5459	-5353	-5353	MG	0.00	0.00	110.00
3270	-6101	-5459	-5353	-5353	MG	0.00	0.00	110.00
3271	-4965	-5855	-5773	-5773	MG	0.00	0.00	110.00
3272	-4323	-3675	-6230	-6171	MG	0.00	0.00	110.00
3272	-6171	-5357	-4323	-4323	MG	0.00	0.00	110.00
3273	-6578	-4758	-5784	-5784	MG	0.00	0.00	110.00
3273	-5691	-3956	-6659	-6659	MG	0.00	0.00	110.00
3273	-6659	-3956	-4758	-6578	MG	0.00	0.00	110.00
3274	-4759	-3969	-6660	-6579	MG	0.00	0.00	110.00
3274	-6579	-5766	-4759	-4759	MG	0.00	0.00	110.00
3274	-3969	-5692	-6660	-6660	MG	0.00	0.00	110.00
3305	-5257	-6107	-7092	-7092	MG	0.00	0.00	110.00
3307	-6106	-5256	-7091	-7091	MG	0.00	0.00	110.00
3308	-7022	-6175	-5131	-5131	MG	0.00	0.00	110.00
3308	-5131	-4236	-7092	-7022	MG	0.00	0.00	110.00
3309	-7091	-4235	-5130	-7021	MG	0.00	0.00	110.00
3309	-7021	-5130	-6174	-6174	MG	0.00	0.00	110.00
3325	-5746	-6242	-6235	-6235	MG	0.00	0.00	110.00
3325	-5746	-6235	-6236	-5052	MG	0.00	0.00	110.00
3331	-6151	-6667	-6688	-5447	MG	0.00	0.00	110.00
3332	-8719	-5354	-5286	-8840	MG	0.00	0.00	110.00
3332	-8840	-5286	-5215	-8908	MG	0.00	0.00	110.00
3332	-8908	-5215	-5387	-8982	MG	0.00	0.00	110.00
3332	-8479	-5001	-5254	-8537	MG	0.00	0.00	110.00
3332	-8377	-4884	-4815	-8424	MG	0.00	0.00	110.00
3332	-8228	-4886	-4952	-8316	MG	0.00	0.00	110.00
3332	-8537	-5254	-5304	-8628	MG	0.00	0.00	110.00
3332	-8028	-4494	-4841	-8154	MG	0.00	0.00	110.00
3332	-8316	-4952	-4884	-8377	MG	0.00	0.00	110.00
3332	-8154	-4841	-4886	-8228	MG	0.00	0.00	110.00
3332	-8424	-4815	-5001	-8479	MG	0.00	0.00	110.00
3332	-8628	-5304	-5354	-8719	MG	0.00	0.00	110.00
3333	-6304	-6303	-6371	-6372	MG	0.00	0.00	110.00
3333	-6999	-6998	-7057	-7058	MG	0.00	0.00	110.00
3333	-6917	-6916	-6999	-7000	MG	0.00	0.00	110.00
3333	-6378	-6310	-6309	-6377	MG	0.00	0.00	110.00
3333	-6828	-6743	-6742	-6827	MG	0.00	0.00	110.00
3333	-6301	-6244	-6243	-6300	MG	0.00	0.00	110.00
3333	-6303	-6302	-6370	-6371	MG	0.00	0.00	110.00
3333	-6916	-6915	-6998	-6999	MG	0.00	0.00	110.00
3333	-7061	-7002	-7001	-7060	MG	0.00	0.00	110.00
3333	-6833	-6748	-6747	-6832	MG	0.00	0.00	110.00
3333	-7141	-7061	-7060	-7140	MG	0.00	0.00	110.00
3333	-6834	-6833	-6915	-6916	MG	0.00	0.00	110.00
3333	-6374	-6306	-6305	-6373	MG	0.00	0.00	110.00
3333	-6624	-6539	-6551	-6623	MG	0.00	0.00	110.00

3333	-6994	-6911	-6910	-6993	MG	0.00	0.00	110.00
3333	-7140	-7060	-7059	-7139	MG	0.00	0.00	110.00
3333	-6993	-6910	-6909	-6992	MG	0.00	0.00	110.00
3333	-6379	-6311	-6310	-6378	MG	0.00	0.00	110.00
3333	-6842	-6757	-6756	-6841	MG	0.00	0.00	110.00
3333	-6364	-6296	-6295	-6363	MG	0.00	0.00	110.00
3333	-7062	-7003	-7002	-7061	MG	0.00	0.00	110.00
3333	-7003	-6920	-6919	-7002	MG	0.00	0.00	110.00
3333	-6536	-6477	-6476	-6535	MG	0.00	0.00	110.00
3333	-6484	-6483	-6548	-6549	MG	0.00	0.00	110.00
3333	-7057	-6998	-6997	-7056	MG	0.00	0.00	110.00
3333	-6302	-6238	-6244	-6301	MG	0.00	0.00	110.00
3333	-6547	-6482	-6481	-6538	MG	0.00	0.00	110.00
3333	-6369	-6301	-6300	-6368	MG	0.00	0.00	110.00
3333	-6371	-6370	-6483	-6484	MG	0.00	0.00	110.00
3333	-6485	-6484	-6549	-6550	MG	0.00	0.00	110.00
3333	-7133	-7053	-7052	-7132	MG	0.00	0.00	110.00
3333	-7000	-6999	-7058	-7059	MG	0.00	0.00	110.00
3333	-6492	-6379	-6378	-6491	MG	0.00	0.00	110.00
3333	-6368	-6300	-6299	-6367	MG	0.00	0.00	110.00
3333	-7132	-7052	-7051	-7131	MG	0.00	0.00	110.00
3333	-7136	-7056	-7055	-7135	MG	0.00	0.00	110.00
3333	-6308	-6249	-6239	-6307	MG	0.00	0.00	110.00
3333	-6678	-6625	-6624	-6677	MG	0.00	0.00	110.00
3333	-6625	-6552	-6539	-6624	MG	0.00	0.00	110.00
3333	-6671	-6689	-6748	-6749	MG	0.00	0.00	110.00
3333	-6677	-6624	-6623	-6673	MG	0.00	0.00	110.00
3333	-7146	-7066	-7065	-7145	MG	0.00	0.00	110.00
3333	-7051	-6992	-6991	-7050	MG	0.00	0.00	110.00
3333	-6299	-6237	-6236	-6298	MG	0.00	0.00	110.00
3333	-6306	-6248	-6247	-6305	MG	0.00	0.00	110.00
3333	-6748	-6689	-6670	-6747	MG	0.00	0.00	110.00
3333	-6487	-6374	-6373	-6486	MG	0.00	0.00	110.00
3333	-7056	-6997	-6996	-7055	MG	0.00	0.00	110.00
3333	-6629	-6556	-6555	-6628	MG	0.00	0.00	110.00
3333	-6832	-6747	-6746	-6831	MG	0.00	0.00	110.00
3333	-7143	-7063	-7062	-7142	MG	0.00	0.00	110.00
3333	-7055	-6996	-6995	-7054	MG	0.00	0.00	110.00
3333	-6901	-6842	-6841	-6923	MG	0.00	0.00	110.00
3333	-6297	-6235	-6242	-6296	MG	0.00	0.00	110.00
3333	-6614	-6536	-6535	-6613	MG	0.00	0.00	110.00
3333	-6754	-6690	-6678	-6753	MG	0.00	0.00	110.00
3333	-6477	-6364	-6363	-6476	MG	0.00	0.00	110.00
3333	-6375	-6307	-6306	-6374	MG	0.00	0.00	110.00
3333	-6998	-6915	-6914	-6997	MG	0.00	0.00	110.00
3333	-6619	-6547	-6538	-6618	MG	0.00	0.00	110.00
3333	-6995	-6912	-6911	-6994	MG	0.00	0.00	110.00
3333	-6246	-6245	-6303	-6304	MG	0.00	0.00	110.00
3333	-6830	-6745	-6744	-6829	MG	0.00	0.00	110.00
3333	-6482	-6369	-6368	-6481	MG	0.00	0.00	110.00
3333	-7053	-6994	-6993	-7052	MG	0.00	0.00	110.00
3333	-6377	-6309	-6308	-6376	MG	0.00	0.00	110.00
3333	-6538	-6481	-6480	-6546	MG	0.00	0.00	110.00
3333	-6835	-6834	-6916	-6917	MG	0.00	0.00	110.00
3333	-6829	-6744	-6743	-6828	MG	0.00	0.00	110.00
3333	-6481	-6368	-6367	-6480	MG	0.00	0.00	110.00
3333	-7007	-6901	-6923	-7006	MG	0.00	0.00	110.00
3333	-6300	-6243	-6237	-6299	MG	0.00	0.00	110.00
3333	-6668	-6617	-6616	-6688	MG	0.00	0.00	110.00
3333	-6757	-6693	-6692	-6756	MG	0.00	0.00	110.00
3333	-6546	-6480	-6479	-6537	MG	0.00	0.00	110.00
3333	-6307	-6239	-6248	-6306	MG	0.00	0.00	110.00
3333	-6751	-6673	-6672	-6750	MG	0.00	0.00	110.00
3333	-7131	-7051	-7050	-7130	MG	0.00	0.00	110.00
3333	-6915	-6833	-6832	-6914	MG	0.00	0.00	110.00
3333	-6537	-6479	-6478	-6545	MG	0.00	0.00	110.00
3333	-7059	-7058	-7138	-7139	MG	0.00	0.00	110.00
3333	-6742	-6687	-6666	-6741	MG	0.00	0.00	110.00
3333	-6997	-6914	-6913	-6996	MG	0.00	0.00	110.00
3333	-6922	-6840	-6839	-6921	MG	0.00	0.00	110.00
3333	-6556	-6492	-6491	-6555	MG	0.00	0.00	110.00
3333	-6840	-6755	-6754	-6839	MG	0.00	0.00	110.00
3333	-6545	-6478	-6477	-6536	MG	0.00	0.00	110.00
3333	-6311	-6252	-6251	-6310	MG	0.00	0.00	110.00
3333	-6365	-6297	-6296	-6364	MG	0.00	0.00	110.00
3333	-6921	-6839	-6838	-6920	MG	0.00	0.00	110.00
3333	-6839	-6754	-6753	-6838	MG	0.00	0.00	110.00
3333	-6491	-6378	-6377	-6490	MG	0.00	0.00	110.00
3333	-7142	-7062	-7061	-7141	MG	0.00	0.00	110.00

3333	-7134	-7054	-7053	-7133	MG	0.00	0.00	110.00
3333	-6310	-6251	-6250	-6309	MG	0.00	0.00	110.00
3333	-6912	-6830	-6829	-6911	MG	0.00	0.00	110.00
3333	-6490	-6377	-6376	-6489	MG	0.00	0.00	110.00
3333	-6753	-6678	-6677	-6752	MG	0.00	0.00	110.00
3333	-6621	-6620	-6689	-6671	MG	0.00	0.00	110.00
3333	-6549	-6548	-6620	-6621	MG	0.00	0.00	110.00
3333	-6673	-6623	-6622	-6672	MG	0.00	0.00	110.00
3333	-6618	-6538	-6546	-6617	MG	0.00	0.00	110.00
3333	-6670	-6619	-6618	-6669	MG	0.00	0.00	110.00
3333	-6752	-6677	-6673	-6751	MG	0.00	0.00	110.00
3333	-7001	-6918	-6917	-7000	MG	0.00	0.00	110.00
3333	-6376	-6308	-6307	-6375	MG	0.00	0.00	110.00
3333	-6372	-6371	-6484	-6485	MG	0.00	0.00	110.00
3333	-6550	-6549	-6621	-6622	MG	0.00	0.00	110.00
3333	-6552	-6488	-6487	-6539	MG	0.00	0.00	110.00
3333	-6488	-6375	-6374	-6487	MG	0.00	0.00	110.00
3333	-6480	-6367	-6366	-6479	MG	0.00	0.00	110.00
3333	-7145	-7065	-7064	-7144	MG	0.00	0.00	110.00
3333	-6367	-6299	-6298	-6366	MG	0.00	0.00	110.00
3333	-6992	-6909	-6900	-6991	MG	0.00	0.00	110.00
3333	-6616	-6537	-6545	-6615	MG	0.00	0.00	110.00
3333	-6539	-6487	-6486	-6551	MG	0.00	0.00	110.00
3333	-6827	-6742	-6741	-6826	MG	0.00	0.00	110.00
3333	-7058	-7057	-7137	-7138	MG	0.00	0.00	110.00
3333	-6914	-6832	-6831	-6913	MG	0.00	0.00	110.00
3333	-6623	-6551	-6550	-6622	MG	0.00	0.00	110.00
3333	-7135	-7055	-7054	-7134	MG	0.00	0.00	110.00
3333	-6551	-6486	-6485	-6550	MG	0.00	0.00	110.00
3333	-6373	-6305	-6304	-6372	MG	0.00	0.00	110.00
3333	-6996	-6913	-6912	-6995	MG	0.00	0.00	110.00
3333	-6913	-6831	-6830	-6912	MG	0.00	0.00	110.00
3333	-7137	-7057	-7056	-7136	MG	0.00	0.00	110.00
3333	-6548	-6483	-6482	-6547	MG	0.00	0.00	110.00
3333	-6620	-6548	-6547	-6619	MG	0.00	0.00	110.00
3333	-6370	-6302	-6301	-6369	MG	0.00	0.00	110.00
3333	-7054	-6995	-6994	-7053	MG	0.00	0.00	110.00
3333	-6296	-6242	-6234	-6295	MG	0.00	0.00	110.00
3333	-6622	-6621	-6671	-6672	MG	0.00	0.00	110.00
3333	-6745	-6668	-6688	-6744	MG	0.00	0.00	110.00
3333	-6838	-6753	-6752	-6837	MG	0.00	0.00	110.00
3333	-6627	-6554	-6553	-6626	MG	0.00	0.00	110.00
3333	-6690	-6626	-6625	-6678	MG	0.00	0.00	110.00
3333	-6911	-6829	-6828	-6910	MG	0.00	0.00	110.00
3333	-6626	-6553	-6552	-6625	MG	0.00	0.00	110.00
3333	-6672	-6671	-6749	-6750	MG	0.00	0.00	110.00
3333	-7066	-7007	-7006	-7065	MG	0.00	0.00	110.00
3333	-7052	-6993	-6992	-7051	MG	0.00	0.00	110.00
3333	-6489	-6376	-6375	-6488	MG	0.00	0.00	110.00
3333	-6910	-6828	-6827	-6909	MG	0.00	0.00	110.00
3333	-6617	-6546	-6537	-6616	MG	0.00	0.00	110.00
3333	-6687	-6614	-6613	-6666	MG	0.00	0.00	110.00
3333	-6746	-6669	-6668	-6745	MG	0.00	0.00	110.00
3333	-7065	-7006	-7005	-7064	MG	0.00	0.00	110.00
3333	-6743	-6667	-6687	-6742	MG	0.00	0.00	110.00
3333	-6923	-6841	-6840	-6922	MG	0.00	0.00	110.00
3333	-7144	-7064	-7063	-7143	MG	0.00	0.00	110.00
3333	-6756	-6692	-6691	-6755	MG	0.00	0.00	110.00
3333	-6841	-6756	-6755	-6840	MG	0.00	0.00	110.00
3333	-7005	-6922	-6921	-7004	MG	0.00	0.00	110.00
3333	-6298	-6236	-6235	-6297	MG	0.00	0.00	110.00
3333	-6366	-6298	-6297	-6365	MG	0.00	0.00	110.00
3333	-6755	-6691	-6690	-6754	MG	0.00	0.00	110.00
3333	-6615	-6545	-6536	-6614	MG	0.00	0.00	110.00
3333	-7063	-7004	-7003	-7062	MG	0.00	0.00	110.00
3333	-6692	-6628	-6627	-6691	MG	0.00	0.00	110.00
3333	-6628	-6555	-6554	-6627	MG	0.00	0.00	110.00
3333	-6555	-6491	-6490	-6554	MG	0.00	0.00	110.00
3333	-6750	-6749	-6834	-6835	MG	0.00	0.00	110.00
3333	-6831	-6746	-6745	-6830	MG	0.00	0.00	110.00
3333	-6483	-6370	-6369	-6482	MG	0.00	0.00	110.00
3333	-6245	-6238	-6302	-6303	MG	0.00	0.00	110.00
3333	-6693	-6629	-6628	-6692	MG	0.00	0.00	110.00
3333	-6554	-6490	-6489	-6553	MG	0.00	0.00	110.00
3333	-6691	-6627	-6626	-6690	MG	0.00	0.00	110.00
3333	-6688	-6616	-6615	-6667	MG	0.00	0.00	110.00
3333	-6836	-6751	-6750	-6835	MG	0.00	0.00	110.00
3333	-6919	-6837	-6836	-6918	MG	0.00	0.00	110.00
3333	-6669	-6618	-6617	-6668	MG	0.00	0.00	110.00

3333	-6749	-6748	-6833	-6834	MG	0.00	0.00	110.00
3333	-6747	-6670	-6669	-6746	MG	0.00	0.00	110.00
3333	-7060	-7001	-7000	-7059	MG	0.00	0.00	110.00
3333	-6305	-6247	-6246	-6304	MG	0.00	0.00	110.00
3333	-6918	-6836	-6835	-6917	MG	0.00	0.00	110.00
3333	-6689	-6620	-6619	-6670	MG	0.00	0.00	110.00
3333	-6478	-6365	-6364	-6477	MG	0.00	0.00	110.00
3333	-6479	-6366	-6365	-6478	MG	0.00	0.00	110.00
3333	-7002	-6919	-6918	-7001	MG	0.00	0.00	110.00
3333	-7006	-6923	-6922	-7005	MG	0.00	0.00	110.00
3333	-6667	-6615	-6614	-6687	MG	0.00	0.00	110.00
3333	-6909	-6827	-6826	-6900	MG	0.00	0.00	110.00
3333	-6920	-6838	-6837	-6919	MG	0.00	0.00	110.00
3333	-6553	-6489	-6488	-6552	MG	0.00	0.00	110.00
3333	-7004	-6921	-6920	-7003	MG	0.00	0.00	110.00
3333	-6486	-6373	-6372	-6485	MG	0.00	0.00	110.00
3333	-6744	-6688	-6667	-6743	MG	0.00	0.00	110.00
3333	-6837	-6752	-6751	-6836	MG	0.00	0.00	110.00
3333	-6309	-6250	-6249	-6308	MG	0.00	0.00	110.00
3333	-7064	-7005	-7004	-7063	MG	0.00	0.00	110.00
3334	-8230	-4887	-4953	-8318	MG	0.00	0.00	110.00
3334	-8481	-5002	-5255	-8539	MG	0.00	0.00	110.00
3334	-8318	-4953	-4885	-8379	MG	0.00	0.00	110.00
3334	-8030	-4503	-4842	-8156	MG	0.00	0.00	110.00
3334	-8721	-5355	-5287	-8841	MG	0.00	0.00	110.00
3334	-8156	-4842	-4887	-8230	MG	0.00	0.00	110.00
3334	-8379	-4885	-4816	-8426	MG	0.00	0.00	110.00
3334	-8426	-4816	-5002	-8481	MG	0.00	0.00	110.00
3334	-8841	-5287	-5216	-8910	MG	0.00	0.00	110.00
3334	-8629	-5305	-5355	-8721	MG	0.00	0.00	110.00
3334	-8910	-5216	-5398	-8984	MG	0.00	0.00	110.00
3334	-8539	-5255	-5305	-8629	MG	0.00	0.00	110.00
3335	-7498	-4492	-4459	-7497	MG	0.00	0.00	110.00
3339	-4362	-4169	-7973	-7974	MG	0.00	0.00	110.00
3342	-4421	-5418	-8423	-8423	MG	0.00	0.00	110.00
3345	-5781	-5854	-6493	-6493	MG	0.00	0.00	110.00
3346	-6170	-5356	-6259	-6259	MG	0.00	0.00	110.00
3364	-5747	-5053	-6249	-6250	MG	0.00	0.00	110.00
3364	-6251	-5747	-6250	-6250	MG	0.00	0.00	110.00
3372	-6152	-5448	-6690	-6691	MG	0.00	0.00	110.00
3380	-4460	-4493	-7502	-7503	MG	0.00	0.00	110.00
3384	-4170	-4363	-7976	-7977	MG	0.00	0.00	110.00
3386	-5397	-4422	-8427	-8427	MG	0.00	0.00	110.00
3388	-6494	-5855	-5773	-5773	MG	0.00	0.00	110.00
3390	-5357	-6269	-6171	-6171	MG	0.00	0.00	110.00
3424	-7021	-6174	-7156	-7156	MG	0.00	0.00	110.00
3426	-6175	-7157	-7022	-7022	MG	0.00	0.00	110.00
3435	-6151	-6687	-6667	-6667	MG	0.00	0.00	110.00
3436	-9550	-6104	-6172	-9598	MG	0.00	0.00	110.00
3436	-9073	-5620	-5701	-9149	MG	0.00	0.00	110.00
3436	-9440	-5808	-6036	-9479	MG	0.00	0.00	110.00
3436	-9727	-6001	-6206	-9855	MG	0.00	0.00	110.00
3436	-10194	-6495	-6380	-10249	MG	0.00	0.00	110.00
3436	-9968	-6437	-6501	-10034	MG	0.00	0.00	110.00
3436	-9374	-5605	-5808	-9440	MG	0.00	0.00	110.00
3436	-9207	-5783	-5689	-9283	MG	0.00	0.00	110.00
3436	-9283	-5689	-5605	-9374	MG	0.00	0.00	110.00
3436	-9479	-6036	-6104	-9550	MG	0.00	0.00	110.00
3436	-9149	-5701	-5783	-9207	MG	0.00	0.00	110.00
3436	-9598	-6172	-6102	-9640	MG	0.00	0.00	110.00
3436	-9640	-6102	-6001	-9727	MG	0.00	0.00	110.00
3436	-9855	-6206	-6437	-9968	MG	0.00	0.00	110.00
3436	-8982	-5387	-5620	-9073	MG	0.00	0.00	110.00
3436	-10034	-6501	-6597	-10126	MG	0.00	0.00	110.00
3436	-10126	-6597	-6495	-10194	MG	0.00	0.00	110.00
3437	-8229	-8228	-8316	-8317	MG	0.00	0.00	110.00
3437	-10199	-10133	-10132	-10198	MG	0.00	0.00	110.00
3437	-10257	-10201	-10200	-10256	MG	0.00	0.00	110.00
3437	-8427	-8380	-8379	-8426	MG	0.00	0.00	110.00
3437	-10122	-10030	-10029	-10121	MG	0.00	0.00	110.00
3437	-10038	-9946	-9962	-10037	MG	0.00	0.00	110.00
3437	-7974	-7928	-7927	-7973	MG	0.00	0.00	110.00
3437	-7502	-7466	-7465	-7501	MG	0.00	0.00	110.00
3437	-7971	-7925	-7924	-7970	MG	0.00	0.00	110.00
3437	-10129	-10037	-10036	-10128	MG	0.00	0.00	110.00
3437	-8911	-8808	-8841	-8910	MG	0.00	0.00	110.00
3437	-10255	-10199	-10198	-10254	MG	0.00	0.00	110.00
3437	-10041	-9972	-9971	-10040	MG	0.00	0.00	110.00
3437	-10036	-10035	-10127	-10128	MG	0.00	0.00	110.00

3437	-8424	-8377	-8376	-8423	MG	0.00	0.00	110.00
3437	3301	-10193	-10192	-10248	MG	0.00	0.00	110.00
3437	-9446	-9380	-9379	-9445	MG	0.00	0.00	110.00
3437	-10198	-10132	-10131	-10177	MG	0.00	0.00	110.00
3437	-10121	-10029	-10028	-10120	MG	0.00	0.00	110.00
3437	-7666	-7662	-7711	-7712	MG	0.00	0.00	110.00
3437	-10133	-10041	-10040	-10132	MG	0.00	0.00	110.00
3437	3302	-10176	-10196	-10251	MG	0.00	0.00	110.00
3437	-9972	-9849	-9848	-9971	MG	0.00	0.00	110.00
3437	-8984	-8983	-9095	-9074	MG	0.00	0.00	110.00
3437	-10132	-10040	-10039	-10131	MG	0.00	0.00	110.00
3437	-9968	-9855	-9854	-9945	MG	0.00	0.00	110.00
3437	-7269	-7206	-7205	-7268	MG	0.00	0.00	110.00
3437	-10030	-9944	-9943	-10029	MG	0.00	0.00	110.00
3437	-7571	-7497	-7496	-7576	MG	0.00	0.00	110.00
3437	-9557	-9505	-9493	-9556	MG	0.00	0.00	110.00
3437	-8230	-8229	-8317	-8318	MG	0.00	0.00	110.00
3437	-9447	-9381	-9380	-9446	MG	0.00	0.00	110.00
3437	-7349	-7348	-7464	-7465	MG	0.00	0.00	110.00
3437	-7257	-7194	-7193	-7256	MG	0.00	0.00	110.00
3437	-10175	-10121	-10120	-10189	MG	0.00	0.00	110.00
3437	-9493	-9446	-9445	-9488	MG	0.00	0.00	110.00
3437	-9600	-9599	-9641	-9642	MG	0.00	0.00	110.00
3437	-9962	-9857	-9847	-9970	MG	0.00	0.00	110.00
3437	-9857	-9741	-9740	-9847	MG	0.00	0.00	110.00
3437	-7348	-7347	-7463	-7464	MG	0.00	0.00	110.00
3437	-9974	-9863	-9840	-9973	MG	0.00	0.00	110.00
3437	-10127	-10126	-10194	-10195	MG	0.00	0.00	110.00
3437	-8983	-8982	-9073	-9095	MG	0.00	0.00	110.00
3437	-9445	-9379	-9378	-9444	MG	0.00	0.00	110.00
3437	-9742	-9644	-9643	-9741	MG	0.00	0.00	110.00
3437	-9644	-9602	-9601	-9643	MG	0.00	0.00	110.00
3437	-10195	-10194	-10249	-10250	MG	0.00	0.00	110.00
3437	-7468	-7352	-7351	-7467	MG	0.00	0.00	110.00
3437	-7265	-7264	-7298	-7299	MG	0.00	0.00	110.00
3437	-9444	-9378	-9377	-9443	MG	0.00	0.00	110.00
3437	-7801	-7705	-7697	-7800	MG	0.00	0.00	110.00
3437	-7705	-7655	-7654	-7697	MG	0.00	0.00	110.00
3437	-7459	-7343	-7342	-7458	MG	0.00	0.00	110.00
3437	-7501	-7500	-7572	-7579	MG	0.00	0.00	110.00
3437	-9727	-9640	-9639	-9739	MG	0.00	0.00	110.00
3437	-9648	-9606	-9605	-9647	MG	0.00	0.00	110.00
3437	-8420	-8373	-8372	-8419	MG	0.00	0.00	110.00
3437	-7472	-7356	-7355	-7471	MG	0.00	0.00	110.00
3437	-8917	-8809	-8827	-8916	MG	0.00	0.00	110.00
3437	-8433	-8386	-8385	-8432	MG	0.00	0.00	110.00
3437	-9373	-9282	-9281	-9372	MG	0.00	0.00	110.00
3437	-10246	-10190	-10175	-10245	MG	0.00	0.00	110.00
3437	-10134	-10042	-10041	-10133	MG	0.00	0.00	110.00
3437	-9747	-9649	-9648	-9746	MG	0.00	0.00	110.00
3437	-8372	-8311	-8310	-8371	MG	0.00	0.00	110.00
3437	-9485	-9479	-9550	-9551	MG	0.00	0.00	110.00
3437	-9744	-9646	-9645	-9743	MG	0.00	0.00	110.00
3437	-9646	-9604	-9603	-9645	MG	0.00	0.00	110.00
3437	-9604	-9556	-9555	-9603	MG	0.00	0.00	110.00
3437	-8423	-8376	-8375	-8422	MG	0.00	0.00	110.00
3437	-8907	-8824	-8807	-8906	MG	0.00	0.00	110.00
3437	-9740	-9728	-9856	-9847	MG	0.00	0.00	110.00
3437	-9743	-9645	-9644	-9742	MG	0.00	0.00	110.00
3437	-9645	-9603	-9602	-9644	MG	0.00	0.00	110.00
3437	-7505	-7469	-7468	-7504	MG	0.00	0.00	110.00
3437	-9555	-9488	-9504	-9554	MG	0.00	0.00	110.00
3437	-8426	-8425	-8480	-8481	MG	0.00	0.00	110.00
3437	-8539	-8538	-8621	-8629	MG	0.00	0.00	110.00
3437	-7813	-7723	-7722	-7812	MG	0.00	0.00	110.00
3437	-7723	-7671	-7670	-7722	MG	0.00	0.00	110.00
3437	-10196	-10195	-10250	-10251	MG	0.00	0.00	110.00
3437	-8424	-8423	-8472	-8479	MG	0.00	0.00	110.00
3437	-8910	-8909	-8983	-8984	MG	0.00	0.00	110.00
3437	-9074	-9095	-9150	-9151	MG	0.00	0.00	110.00
3437	-7812	-7722	-7716	-7811	MG	0.00	0.00	110.00
3437	-7722	-7670	-7669	-7716	MG	0.00	0.00	110.00
3437	-9377	-9286	-9285	-9376	MG	0.00	0.00	110.00
3437	-10254	-10198	-10177	-10253	MG	0.00	0.00	110.00
3437	-7495	-7459	-7458	-7494	MG	0.00	0.00	110.00
3437	-9847	-9856	-9969	-9970	MG	0.00	0.00	110.00
3437	-10040	-9971	-9963	-10039	MG	0.00	0.00	110.00
3437	-7807	-7806	-7929	-7930	MG	0.00	0.00	110.00
3437	-7711	-7710	-7805	-7806	MG	0.00	0.00	110.00

3437	-9506	-9448	-9447	-9505	MG	0.00	0.00	110.00
3437	-7264	-7263	-7297	-7298	MG	0.00	0.00	110.00
3437	-7138	-7137	-7200	-7201	MG	0.00	0.00	110.00
3437	-9739	-9639	-9638	-9738	MG	0.00	0.00	110.00
3437	-7715	-7668	-7643	-7721	MG	0.00	0.00	110.00
3437	-7668	-7583	-7582	-7643	MG	0.00	0.00	110.00
3437	-7583	-7505	-7504	-7582	MG	0.00	0.00	110.00
3437	-10197	-10130	-10129	-10176	MG	0.00	0.00	110.00
3437	-10130	-10038	-10037	-10129	MG	0.00	0.00	110.00
3437	-10200	-10134	-10133	-10199	MG	0.00	0.00	110.00
3437	-7291	-7257	-7256	-7290	MG	0.00	0.00	110.00
3437	-7643	-7582	-7581	-7667	MG	0.00	0.00	110.00
3437	-10176	-10129	-10128	-10196	MG	0.00	0.00	110.00
3437	-10256	-10200	-10199	-10255	MG	0.00	0.00	110.00
3437	-10037	-9962	-9970	-10036	MG	0.00	0.00	110.00
3437	-7299	-7298	-7348	-7349	MG	0.00	0.00	110.00
3437	-7714	-7667	-7663	-7713	MG	0.00	0.00	110.00
3437	-9863	-9747	-9746	-9840	MG	0.00	0.00	110.00
3437	-7581	-7503	-7502	-7580	MG	0.00	0.00	110.00
3437	-7931	-7808	-7807	-7930	MG	0.00	0.00	110.00
3437	-7808	-7713	-7712	-7807	MG	0.00	0.00	110.00
3437	-9855	-9727	-9739	-9854	MG	0.00	0.00	110.00
3437	-7663	-7580	-7579	-7666	MG	0.00	0.00	110.00
3437	-9554	-9504	-9487	-9553	MG	0.00	0.00	110.00
3437	-9504	-9444	-9443	-9487	MG	0.00	0.00	110.00
3437	-8029	-8028	-8154	-8155	MG	0.00	0.00	110.00
3437	-9643	-9601	-9600	-9642	MG	0.00	0.00	110.00
3437	-9849	-9745	-9744	-9848	MG	0.00	0.00	110.00
3437	-7710	-7661	-7660	-7709	MG	0.00	0.00	110.00
3437	-9487	-9443	-9442	-9486	MG	0.00	0.00	110.00
3437	-7935	-7811	-7810	-7934	MG	0.00	0.00	110.00
3437	-9961	-9839	-9853	-9967	MG	0.00	0.00	110.00
3437	-9856	-9855	-9968	-9969	MG	0.00	0.00	110.00
3437	-9640	-9598	-9597	-9639	MG	0.00	0.00	110.00
3437	-9598	-9550	-9549	-9597	MG	0.00	0.00	110.00
3437	-9550	-9479	-9503	-9549	MG	0.00	0.00	110.00
3437	-7499	-7463	-7462	-7498	MG	0.00	0.00	110.00
3437	-9383	-9292	-9291	-9382	MG	0.00	0.00	110.00
3437	-9853	-9737	-9736	-9838	MG	0.00	0.00	110.00
3437	-9209	-9208	-9284	-9285	MG	0.00	0.00	110.00
3437	-9208	-9207	-9283	-9284	MG	0.00	0.00	110.00
3437	-9095	-9073	-9149	-9150	MG	0.00	0.00	110.00
3437	-8721	-8720	-8825	-8841	MG	0.00	0.00	110.00
3437	-8720	-8719	-8840	-8825	MG	0.00	0.00	110.00
3437	-8538	-8537	-8628	-8621	MG	0.00	0.00	110.00
3437	-10245	-10175	-10189	-10244	MG	0.00	0.00	110.00
3437	-7658	-7576	-7570	-7657	MG	0.00	0.00	110.00
3437	-7576	-7496	-7495	-7570	MG	0.00	0.00	110.00
3437	-9943	-9852	-9837	-9942	MG	0.00	0.00	110.00
3437	-7924	-7802	-7779	-7923	MG	0.00	0.00	110.00
3437	-7802	-7698	-7706	-7779	MG	0.00	0.00	110.00
3437	-7698	-7657	-7656	-7706	MG	0.00	0.00	110.00
3437	-7657	-7570	-7569	-7656	MG	0.00	0.00	110.00
3437	-7570	-7495	-7494	-7569	MG	0.00	0.00	110.00
3437	-7969	-7923	-7922	-7968	MG	0.00	0.00	110.00
3437	-7923	-7779	-7801	-7922	MG	0.00	0.00	110.00
3437	-7671	-7586	-7585	-7670	MG	0.00	0.00	110.00
3437	-7706	-7656	-7655	-7705	MG	0.00	0.00	110.00
3437	-10249	-10194	-10193	3301	MG	0.00	0.00	110.00
3437	-7139	-7138	-7201	-7202	MG	0.00	0.00	110.00
3437	-7968	-7922	-7921	-7967	MG	0.00	0.00	110.00
3437	-7922	-7801	-7800	-7921	MG	0.00	0.00	110.00
3437	-9205	-9147	-9146	-9204	MG	0.00	0.00	110.00
3437	-8909	-8908	-8982	-8983	MG	0.00	0.00	110.00
3437	-7806	-7805	-7928	-7929	MG	0.00	0.00	110.00
3437	-7662	-7661	-7710	-7711	MG	0.00	0.00	110.00
3437	-7930	-7929	-7975	-7976	MG	0.00	0.00	110.00
3437	-8425	-8424	-8479	-8480	MG	0.00	0.00	110.00
3437	-7712	-7711	-7806	-7807	MG	0.00	0.00	110.00
3437	-9374	-9283	-9282	-9373	MG	0.00	0.00	110.00
3437	-10042	-9973	-9972	-10041	MG	0.00	0.00	110.00
3437	-7356	-7306	-7305	-7355	MG	0.00	0.00	110.00
3437	-7306	-7272	-7271	-7305	MG	0.00	0.00	110.00
3437	-7272	-7209	-7208	-7271	MG	0.00	0.00	110.00
3437	-9741	-9643	-9642	-9740	MG	0.00	0.00	110.00
3437	-10043	-9974	-9973	-10042	MG	0.00	0.00	110.00
3437	-10135	-10043	-10042	-10134	MG	0.00	0.00	110.00
3437	-10201	-10135	-10134	-10200	MG	0.00	0.00	110.00
3437	-7305	-7271	-7270	-7304	MG	0.00	0.00	110.00

3437	-7271	-7208	-7207	-7270	MG	0.00	0.00	110.00
3437	-7208	-7145	-7144	-7207	MG	0.00	0.00	110.00
3437	-9556	-9493	-9488	-9555	MG	0.00	0.00	110.00
3437	-7470	-7354	-7353	-7469	MG	0.00	0.00	110.00
3437	-8977	-8903	-8902	-8976	MG	0.00	0.00	110.00
3437	-9970	-9969	-10035	-10036	MG	0.00	0.00	110.00
3437	-10128	-10127	-10195	-10196	MG	0.00	0.00	110.00
3437	-9603	-9555	-9554	-9602	MG	0.00	0.00	110.00
3437	-9143	-9093	-9068	-9142	MG	0.00	0.00	110.00
3437	-9488	-9445	-9444	-9504	MG	0.00	0.00	110.00
3437	-8976	-8902	-8901	-8975	MG	0.00	0.00	110.00
3437	-7303	-7269	-7268	-7302	MG	0.00	0.00	110.00
3437	-9284	-9283	-9374	-9375	MG	0.00	0.00	110.00
3437	-9602	-9554	-9553	-9601	MG	0.00	0.00	110.00
3437	-7504	-7468	-7467	-7503	MG	0.00	0.00	110.00
3437	-8809	-8728	-8727	-8827	MG	0.00	0.00	110.00
3437	-8728	-8635	-8634	-8727	MG	0.00	0.00	110.00
3437	-7805	-7710	-7709	-7804	MG	0.00	0.00	110.00
3437	-9601	-9553	-9552	-9600	MG	0.00	0.00	110.00
3437	-9553	-9487	-9486	-9552	MG	0.00	0.00	110.00
3437	-9443	-9377	-9376	-9442	MG	0.00	0.00	110.00
3437	-7467	-7351	-7350	-7466	MG	0.00	0.00	110.00
3437	-7351	-7301	-7300	-7350	MG	0.00	0.00	110.00
3437	-7301	-7267	-7266	-7300	MG	0.00	0.00	110.00
3437	-7267	-7204	-7203	-7266	MG	0.00	0.00	110.00
3437	-8485	-8432	-8431	-8484	MG	0.00	0.00	110.00
3437	-8915	-8826	-8843	-8914	MG	0.00	0.00	110.00
3437	-9479	-9440	-9439	-9503	MG	0.00	0.00	110.00
3437	-9440	-9374	-9373	-9439	MG	0.00	0.00	110.00
3437	-9639	-9597	-9596	-9638	MG	0.00	0.00	110.00
3437	-9597	-9549	-9548	-9596	MG	0.00	0.00	110.00
3437	-9549	-9503	-9484	-9548	MG	0.00	0.00	110.00
3437	-8311	-8223	-8222	-8310	MG	0.00	0.00	110.00
3437	-7508	-7472	-7471	-7507	MG	0.00	0.00	110.00
3437	-7973	-7927	-7926	-7972	MG	0.00	0.00	110.00
3437	-7983	-7937	-7936	-7982	MG	0.00	0.00	110.00
3437	-7263	-7200	-7199	-7262	MG	0.00	0.00	110.00
3437	-7200	-7137	-7136	-7199	MG	0.00	0.00	110.00
3437	-10029	-9943	-9942	-10028	MG	0.00	0.00	110.00
3437	-7975	-7974	-8028	-8029	MG	0.00	0.00	110.00
3437	-7296	-7262	-7261	-7295	MG	0.00	0.00	110.00
3437	-7262	-7199	-7198	-7261	MG	0.00	0.00	110.00
3437	-8379	-8378	-8425	-8426	MG	0.00	0.00	110.00
3437	-7497	-7461	-7460	-7496	MG	0.00	0.00	110.00
3437	-7461	-7345	-7344	-7460	MG	0.00	0.00	110.00
3437	-7345	-7295	-7294	-7344	MG	0.00	0.00	110.00
3437	-7295	-7261	-7260	-7294	MG	0.00	0.00	110.00
3437	-7261	-7198	-7197	-7260	MG	0.00	0.00	110.00
3437	-7198	-7135	-7134	-7197	MG	0.00	0.00	110.00
3437	-7496	-7460	-7459	-7495	MG	0.00	0.00	110.00
3437	-7460	-7344	-7343	-7459	MG	0.00	0.00	110.00
3437	-7344	-7294	-7293	-7343	MG	0.00	0.00	110.00
3437	-7294	-7260	-7259	-7293	MG	0.00	0.00	110.00
3437	-7260	-7197	-7196	-7259	MG	0.00	0.00	110.00
3437	-7197	-7134	-7133	-7196	MG	0.00	0.00	110.00
3437	-6558	-7131	-7132	-7132	MG	0.00	0.00	110.00
3437	-6558	-7132	-7133	-5852	MG	0.00	0.00	110.00
3437	-7343	-7293	-7292	-7342	MG	0.00	0.00	110.00
3437	-7293	-7259	-7258	-7292	MG	0.00	0.00	110.00
3437	-7259	-7196	-7195	-7258	MG	0.00	0.00	110.00
3437	-7196	-7133	-7132	-7195	MG	0.00	0.00	110.00
3437	-7494	-7458	-7457	-7493	MG	0.00	0.00	110.00
3437	-7458	-7342	-7341	-7457	MG	0.00	0.00	110.00
3437	-7342	-7292	-7291	-7341	MG	0.00	0.00	110.00
3437	-7292	-7258	-7257	-7291	MG	0.00	0.00	110.00
3437	-7258	-7195	-7194	-7257	MG	0.00	0.00	110.00
3437	-7195	-7132	-7131	-7194	MG	0.00	0.00	110.00
3437	-7493	-7457	-7456	-7492	MG	0.00	0.00	110.00
3437	-7457	-7341	-7340	-7456	MG	0.00	0.00	110.00
3437	-7341	-7291	-7290	-7340	MG	0.00	0.00	110.00
3437	-8534	-8471	-8470	-8533	MG	0.00	0.00	110.00
3437	-8471	-8421	-8420	-8470	MG	0.00	0.00	110.00
3437	-7194	-7131	-7130	-7193	MG	0.00	0.00	110.00
3437	-7465	-7464	-7500	-7501	MG	0.00	0.00	110.00
3437	-7464	-7463	-7499	-7500	MG	0.00	0.00	110.00
3437	-8617	-8533	-8532	-8616	MG	0.00	0.00	110.00
3437	-7298	-7297	-7347	-7348	MG	0.00	0.00	110.00
3437	-10194	-10126	-10125	-10193	MG	0.00	0.00	110.00
3437	-10126	-10034	-10033	-10125	MG	0.00	0.00	110.00

3437	-10034	-9968	-9945	-10033	MG	0.00	0.00	110.00
3437	-8714	-8616	-8627	-8713	MG	0.00	0.00	110.00
3437	-8616	-8532	-8531	-8627	MG	0.00	0.00	110.00
3437	-8532	-8469	-8477	-8531	MG	0.00	0.00	110.00
3437	-7580	-7502	-7501	-7579	MG	0.00	0.00	110.00
3437	-8030	-8029	-8155	-8156	MG	0.00	0.00	110.00
3437	-8802	-8713	-8712	-8801	MG	0.00	0.00	110.00
3437	-7302	-7268	-7267	-7301	MG	0.00	0.00	110.00
3437	-9969	-9968	-10034	-10035	MG	0.00	0.00	110.00
3437	-9728	-9727	-9855	-9856	MG	0.00	0.00	110.00
3437	-7503	-7467	-7466	-7502	MG	0.00	0.00	110.00
3437	-8841	-8825	-8909	-8910	MG	0.00	0.00	110.00
3437	-8825	-8840	-8908	-8909	MG	0.00	0.00	110.00
3437	-9839	-9738	-9737	-9853	MG	0.00	0.00	110.00
3437	-10247	-10191	-10190	-10246	MG	0.00	0.00	110.00
3437	-10191	-10123	-10122	-10190	MG	0.00	0.00	110.00
3437	-10123	-10031	-10030	-10122	MG	0.00	0.00	110.00
3437	-8237	-8163	-8162	-8236	MG	0.00	0.00	110.00
3437	-7977	-7931	-7930	-7976	MG	0.00	0.00	110.00
3437	-8037	-7983	-7982	-8036	MG	0.00	0.00	110.00
3437	-8432	-8385	-8384	-8431	MG	0.00	0.00	110.00
3437	-10190	-10122	-10121	-10175	MG	0.00	0.00	110.00
3437	-9599	-9598	-9640	-9641	MG	0.00	0.00	110.00
3437	-8236	-8162	-8161	-8235	MG	0.00	0.00	110.00
3437	-9944	-9838	-9852	-9943	MG	0.00	0.00	110.00
3437	-9838	-9736	-9726	-9852	MG	0.00	0.00	110.00
3437	-8431	-8384	-8383	-8430	MG	0.00	0.00	110.00
3437	-8384	-8323	-8322	-8383	MG	0.00	0.00	110.00
3437	-8323	-8235	-8234	-8322	MG	0.00	0.00	110.00
3437	-8235	-8161	-8160	-8234	MG	0.00	0.00	110.00
3437	-8161	-8035	-8034	-8160	MG	0.00	0.00	110.00
3437	-9852	-9726	-9735	-9837	MG	0.00	0.00	110.00
3437	-10244	-10189	-10188	-10243	MG	0.00	0.00	110.00
3437	-10189	-10120	-10119	-10188	MG	0.00	0.00	110.00
3437	-10120	-10028	-10027	-10119	MG	0.00	0.00	110.00
3437	-10028	-9942	-9941	-10027	MG	0.00	0.00	110.00
3437	-9942	-9837	-9846	-9941	MG	0.00	0.00	110.00
3437	-9837	-9735	-9734	-9846	MG	0.00	0.00	110.00
3437	-7202	-7201	-7264	-7265	MG	0.00	0.00	110.00
3437	-7201	-7200	-7263	-7264	MG	0.00	0.00	110.00
3437	-9375	-9374	-9440	-9441	MG	0.00	0.00	110.00
3437	-10035	-10034	-10126	-10127	MG	0.00	0.00	110.00
3437	-9649	-9607	-9606	-9648	MG	0.00	0.00	110.00
3437	-9607	-9559	-9558	-9606	MG	0.00	0.00	110.00
3437	-9559	-9507	-9506	-9558	MG	0.00	0.00	110.00
3437	-9507	-9449	-9448	-9506	MG	0.00	0.00	110.00
3437	-9449	-9383	-9382	-9448	MG	0.00	0.00	110.00
3437	-9746	-9648	-9647	-9745	MG	0.00	0.00	110.00
3437	-9376	-9375	-9441	-9442	MG	0.00	0.00	110.00
3437	-9606	-9558	-9557	-9605	MG	0.00	0.00	110.00
3437	-9558	-9506	-9505	-9557	MG	0.00	0.00	110.00
3437	-9486	-9485	-9551	-9552	MG	0.00	0.00	110.00
3437	-9448	-9382	-9381	-9447	MG	0.00	0.00	110.00
3437	-9745	-9647	-9646	-9744	MG	0.00	0.00	110.00
3437	-9647	-9605	-9604	-9646	MG	0.00	0.00	110.00
3437	-9605	-9557	-9556	-9604	MG	0.00	0.00	110.00
3437	-7498	-7462	-7461	-7497	MG	0.00	0.00	110.00
3437	-9505	-9447	-9446	-9493	MG	0.00	0.00	110.00
3437	-7976	-7975	-8029	-8030	MG	0.00	0.00	110.00
3437	-8156	-8155	-8229	-8230	MG	0.00	0.00	110.00
3437	-8318	-8317	-8378	-8379	MG	0.00	0.00	110.00
3437	-8317	-8316	-8377	-8378	MG	0.00	0.00	110.00
3437	-8155	-8154	-8228	-8229	MG	0.00	0.00	110.00
3437	-8537	-8536	-8620	-8628	MG	0.00	0.00	110.00
3437	-8628	-8620	-8718	-8719	MG	0.00	0.00	110.00
3437	-8719	-8718	-8824	-8840	MG	0.00	0.00	110.00
3437	-8840	-8824	-8907	-8908	MG	0.00	0.00	110.00
3437	-8376	-8315	-8314	-8375	MG	0.00	0.00	110.00
3437	-8315	-8227	-8226	-8314	MG	0.00	0.00	110.00
3437	-8227	-8153	-8152	-8226	MG	0.00	0.00	110.00
3437	-8153	-8027	-8026	-8152	MG	0.00	0.00	110.00
3437	-8027	-7973	-7972	-8026	MG	0.00	0.00	110.00
3437	-8422	-8375	-8374	-8421	MG	0.00	0.00	110.00
3437	-8375	-8314	-8313	-8374	MG	0.00	0.00	110.00
3437	-8314	-8226	-8225	-8313	MG	0.00	0.00	110.00
3437	-8226	-8152	-8151	-8225	MG	0.00	0.00	110.00
3437	-8152	-8026	-8025	-8151	MG	0.00	0.00	110.00
3437	-8026	-7972	-7971	-8025	MG	0.00	0.00	110.00
3437	-8421	-8374	-8373	-8420	MG	0.00	0.00	110.00

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3437	-8374	-8313	-8312	-8373	MG	0.00	0.00	110.00
3437	-8313	-8225	-8224	-8312	MG	0.00	0.00	110.00
3437	-8225	-8151	-8150	-8224	MG	0.00	0.00	110.00
3437	-8151	-8025	-8024	-8150	MG	0.00	0.00	110.00
3437	-8025	-7971	-7970	-8024	MG	0.00	0.00	110.00
3437	-8545	-8485	-8484	-8544	MG	0.00	0.00	110.00
3437	-8373	-8312	-8311	-8372	MG	0.00	0.00	110.00
3437	-8312	-8224	-8223	-8311	MG	0.00	0.00	110.00
3437	-8224	-8150	-8149	-8223	MG	0.00	0.00	110.00
3437	-8150	-8024	-8023	-8149	MG	0.00	0.00	110.00
3437	-8024	-7970	-7969	-8023	MG	0.00	0.00	110.00
3437	-8419	-8372	-8371	-8418	MG	0.00	0.00	110.00
3437	-7579	-7572	-7662	-7666	MG	0.00	0.00	110.00
3437	-9503	-9439	-9438	-9484	MG	0.00	0.00	110.00
3437	-8223	-8149	-8148	-8222	MG	0.00	0.00	110.00
3437	-8149	-8023	-8022	-8148	MG	0.00	0.00	110.00
3437	-8023	-7969	-7968	-8022	MG	0.00	0.00	110.00
3437	-8418	-8371	-8370	-8417	MG	0.00	0.00	110.00
3437	-8371	-8310	-8309	-8370	MG	0.00	0.00	110.00
3437	-8310	-8222	-8221	-8309	MG	0.00	0.00	110.00
3437	-8222	-8148	-8147	-8221	MG	0.00	0.00	110.00
3437	-8148	-8022	-8021	-8147	MG	0.00	0.00	110.00
3437	-8022	-7968	-7967	-8021	MG	0.00	0.00	110.00
3437	-9595	-9547	-9546	-9594	MG	0.00	0.00	110.00
3437	-8378	-8377	-8424	-8425	MG	0.00	0.00	110.00
3437	-7937	-7813	-7812	-7936	MG	0.00	0.00	110.00
3437	-9437	-9371	-9370	-9436	MG	0.00	0.00	110.00
3437	-9736	-9636	-9635	-9726	MG	0.00	0.00	110.00
3437	-9636	-9594	-9593	-9635	MG	0.00	0.00	110.00
3437	-7586	-7508	-7507	-7585	MG	0.00	0.00	110.00
3437	-7982	-7936	-7935	-7981	MG	0.00	0.00	110.00
3437	-7936	-7812	-7811	-7935	MG	0.00	0.00	110.00
3437	-9436	-9370	-9369	-9435	MG	0.00	0.00	110.00
3437	-9726	-9635	-9634	-9735	MG	0.00	0.00	110.00
3437	-7670	-7585	-7584	-7669	MG	0.00	0.00	110.00
3437	-7585	-7507	-7506	-7584	MG	0.00	0.00	110.00
3437	-7981	-7935	-7934	-7980	MG	0.00	0.00	110.00
3437	-9477	-9435	-9434	-9476	MG	0.00	0.00	110.00
3437	-7811	-7716	-7715	-7810	MG	0.00	0.00	110.00
3437	-7716	-7669	-7668	-7715	MG	0.00	0.00	110.00
3437	-7669	-7584	-7583	-7668	MG	0.00	0.00	110.00
3437	-7584	-7506	-7505	-7583	MG	0.00	0.00	110.00
3437	-7980	-7934	-7933	-7979	MG	0.00	0.00	110.00
3437	-7934	-7810	-7809	-7933	MG	0.00	0.00	110.00
3437	-7810	-7715	-7721	-7809	MG	0.00	0.00	110.00
3437	-9642	-9641	-9728	-9740	MG	0.00	0.00	110.00
3437	-9641	-9640	-9727	-9728	MG	0.00	0.00	110.00
3437	-9552	-9551	-9599	-9600	MG	0.00	0.00	110.00
3437	-7979	-7933	-7932	-7978	MG	0.00	0.00	110.00
3437	-7933	-7809	-7781	-7932	MG	0.00	0.00	110.00
3437	-7809	-7721	-7714	-7781	MG	0.00	0.00	110.00
3437	-7721	-7643	-7667	-7714	MG	0.00	0.00	110.00
3437	-9100	-8991	-8990	-9099	MG	0.00	0.00	110.00
3437	-7582	-7504	-7503	-7581	MG	0.00	0.00	110.00
3437	-7978	-7932	-7931	-7977	MG	0.00	0.00	110.00
3437	-7932	-7781	-7808	-7931	MG	0.00	0.00	110.00
3437	-7781	-7714	-7713	-7808	MG	0.00	0.00	110.00
3437	-9157	-9099	-9098	-9156	MG	0.00	0.00	110.00
3437	-7667	-7581	-7580	-7663	MG	0.00	0.00	110.00
3437	-8990	-8916	-8915	-8989	MG	0.00	0.00	110.00
3437	-9381	-9290	-9289	-9380	MG	0.00	0.00	110.00
3437	-9290	-9214	-9213	-9289	MG	0.00	0.00	110.00
3437	-7713	-7663	-7666	-7712	MG	0.00	0.00	110.00
3437	-9156	-9098	-9097	-9155	MG	0.00	0.00	110.00
3437	-9098	-8989	-8988	-9097	MG	0.00	0.00	110.00
3437	-7500	-7499	-7578	-7572	MG	0.00	0.00	110.00
3437	-9380	-9289	-9288	-9379	MG	0.00	0.00	110.00
3437	-7928	-7805	-7804	-7927	MG	0.00	0.00	110.00
3437	-9213	-9155	-9154	-9212	MG	0.00	0.00	110.00
3437	-9155	-9097	-9096	-9154	MG	0.00	0.00	110.00
3437	-7661	-7578	-7577	-7660	MG	0.00	0.00	110.00
3437	-7578	-7499	-7498	-7577	MG	0.00	0.00	110.00
3437	-7927	-7804	-7780	-7926	MG	0.00	0.00	110.00
3437	-7804	-7709	-7708	-7780	MG	0.00	0.00	110.00
3437	-7709	-7660	-7659	-7708	MG	0.00	0.00	110.00
3437	-7660	-7577	-7571	-7659	MG	0.00	0.00	110.00
3437	-7577	-7498	-7497	-7571	MG	0.00	0.00	110.00
3437	-7972	-7926	-7925	-7971	MG	0.00	0.00	110.00
3437	-7926	-7780	-7803	-7925	MG	0.00	0.00	110.00

3437	-7780	-7708	-7707	-7803	MG	0.00	0.00	110.00
3437	-7708	-7659	-7658	-7707	MG	0.00	0.00	110.00
3437	-7659	-7571	-7576	-7658	MG	0.00	0.00	110.00
3437	-9076	-8986	-8985	-9075	MG	0.00	0.00	110.00
3437	-8986	-8912	-8911	-8985	MG	0.00	0.00	110.00
3437	-7925	-7803	-7802	-7924	MG	0.00	0.00	110.00
3437	-7803	-7707	-7698	-7802	MG	0.00	0.00	110.00
3437	-7707	-7658	-7657	-7698	MG	0.00	0.00	110.00
3437	-9075	-8985	-8984	-9074	MG	0.00	0.00	110.00
3437	-8985	-8911	-8910	-8984	MG	0.00	0.00	110.00
3437	-7970	-7924	-7923	-7969	MG	0.00	0.00	110.00
3437	-9441	-9440	-9479	-9485	MG	0.00	0.00	110.00
3437	-9283	-9207	-9206	-9282	MG	0.00	0.00	110.00
3437	-9207	-9149	-9148	-9206	MG	0.00	0.00	110.00
3437	-9149	-9073	-9072	-9148	MG	0.00	0.00	110.00
3437	-9073	-8982	-8981	-9072	MG	0.00	0.00	110.00
3437	-8982	-8908	-8907	-8981	MG	0.00	0.00	110.00
3437	-9282	-9206	-9205	-9281	MG	0.00	0.00	110.00
3437	-7779	-7706	-7705	-7801	MG	0.00	0.00	110.00
3437	-9148	-9072	-9071	-9147	MG	0.00	0.00	110.00
3437	-7656	-7569	-7568	-7655	MG	0.00	0.00	110.00
3437	-7569	-7494	-7493	-7568	MG	0.00	0.00	110.00
3437	-9372	-9281	-9280	-9371	MG	0.00	0.00	110.00
3437	-9281	-9205	-9204	-9280	MG	0.00	0.00	110.00
3437	-8033	-7979	-7978	-8032	MG	0.00	0.00	110.00
3437	-9147	-9071	-9094	-9146	MG	0.00	0.00	110.00
3437	-7655	-7568	-7567	-7654	MG	0.00	0.00	110.00
3437	-7568	-7493	-7492	-7567	MG	0.00	0.00	110.00
3437	-9371	-9280	-9279	-9370	MG	0.00	0.00	110.00
3437	-7929	-7928	-7974	-7975	MG	0.00	0.00	110.00
3437	-9204	-9146	-9145	-9203	MG	0.00	0.00	110.00
3437	-9146	-9094	-9070	-9145	MG	0.00	0.00	110.00
3437	-9094	-8979	-8978	-9070	MG	0.00	0.00	110.00
3437	-8979	-8905	-8904	-8978	MG	0.00	0.00	110.00
3437	-9370	-9279	-9278	-9369	MG	0.00	0.00	110.00
3437	-9279	-9203	-9202	-9278	MG	0.00	0.00	110.00
3437	-7209	-7146	-7145	-7208	MG	0.00	0.00	110.00
3437	-7507	-7471	-7470	-7506	MG	0.00	0.00	110.00
3437	-7471	-7355	-7354	-7470	MG	0.00	0.00	110.00
3437	-7355	-7305	-7304	-7354	MG	0.00	0.00	110.00
3437	-9369	-9278	-9277	-9368	MG	0.00	0.00	110.00
3437	-9278	-9202	-9201	-9277	MG	0.00	0.00	110.00
3437	-9202	-9144	-9143	-9201	MG	0.00	0.00	110.00
3437	-7506	-7470	-7469	-7505	MG	0.00	0.00	110.00
3437	-9069	-8977	-8976	-9093	MG	0.00	0.00	110.00
3437	-7354	-7304	-7303	-7353	MG	0.00	0.00	110.00
3437	-7304	-7270	-7269	-7303	MG	0.00	0.00	110.00
3437	-7270	-7207	-7206	-7269	MG	0.00	0.00	110.00
3437	-7207	-7144	-7143	-7206	MG	0.00	0.00	110.00
3437	-8470	-8420	-8419	-8469	MG	0.00	0.00	110.00
3437	-7469	-7353	-7352	-7468	MG	0.00	0.00	110.00
3437	-7353	-7303	-7302	-7352	MG	0.00	0.00	110.00
3437	-9285	-9284	-9375	-9376	MG	0.00	0.00	110.00
3437	-9214	-9156	-9155	-9213	MG	0.00	0.00	110.00
3437	-7206	-7143	-7142	-7205	MG	0.00	0.00	110.00
3437	-9150	-9149	-9207	-9208	MG	0.00	0.00	110.00
3437	-10033	-9945	-9961	-10032	MG	0.00	0.00	110.00
3437	-7352	-7302	-7301	-7351	MG	0.00	0.00	110.00
3437	-8635	-8546	-8545	-8634	MG	0.00	0.00	110.00
3437	-7268	-7205	-7204	-7267	MG	0.00	0.00	110.00
3437	-7205	-7142	-7141	-7204	MG	0.00	0.00	110.00
3437	-8916	-8827	-8826	-8915	MG	0.00	0.00	110.00
3437	-8827	-8727	-8726	-8826	MG	0.00	0.00	110.00
3437	-8727	-8634	-8633	-8726	MG	0.00	0.00	110.00
3437	-8634	-8545	-8544	-8633	MG	0.00	0.00	110.00
3437	-8621	-8628	-8719	-8720	MG	0.00	0.00	110.00
3437	-7204	-7141	-7140	-7203	MG	0.00	0.00	110.00
3437	-7466	-7350	-7349	-7465	MG	0.00	0.00	110.00
3437	-7350	-7300	-7299	-7349	MG	0.00	0.00	110.00
3437	-7300	-7266	-7265	-7299	MG	0.00	0.00	110.00
3437	-7266	-7203	-7202	-7265	MG	0.00	0.00	110.00
3437	-7203	-7140	-7139	-7202	MG	0.00	0.00	110.00
3437	-8484	-8431	-8430	-8483	MG	0.00	0.00	110.00
3437	-7572	-7578	-7661	-7662	MG	0.00	0.00	110.00
3437	-7463	-7347	-7346	-7462	MG	0.00	0.00	110.00
3437	-7347	-7297	-7296	-7346	MG	0.00	0.00	110.00
3437	-7297	-7263	-7262	-7296	MG	0.00	0.00	110.00
3437	-8543	-8483	-8474	-8542	MG	0.00	0.00	110.00
3437	-8483	-8430	-8429	-8474	MG	0.00	0.00	110.00

3437	-7462	-7346	-7345	-7461	MG	0.00	0.00	110.00
3437	-7346	-7296	-7295	-7345	MG	0.00	0.00	110.00
3437	-8724	-8631	-8630	-8723	MG	0.00	0.00	110.00
3437	-8631	-8542	-8541	-8630	MG	0.00	0.00	110.00
3437	-7199	-7136	-7135	-7198	MG	0.00	0.00	110.00
3437	-8474	-8429	-8428	-8473	MG	0.00	0.00	110.00
3437	-8912	-8787	-8808	-8911	MG	0.00	0.00	110.00
3437	-8787	-8723	-8722	-8808	MG	0.00	0.00	110.00
3437	-9973	-9840	-9849	-9972	MG	0.00	0.00	110.00
3437	-9840	-9746	-9745	-9849	MG	0.00	0.00	110.00
3437	-8541	-8473	-8482	-8540	MG	0.00	0.00	110.00
3437	-8473	-8428	-8427	-8482	MG	0.00	0.00	110.00
3437	-8808	-8722	-8721	-8841	MG	0.00	0.00	110.00
3437	-8722	-8622	-8629	-8721	MG	0.00	0.00	110.00
3437	-8622	-8540	-8539	-8629	MG	0.00	0.00	110.00
3437	-8540	-8482	-8481	-8539	MG	0.00	0.00	110.00
3437	-8482	-8427	-8426	-8481	MG	0.00	0.00	110.00
3437	-8824	-8718	-8717	-8807	MG	0.00	0.00	110.00
3437	-8718	-8620	-8619	-8717	MG	0.00	0.00	110.00
3437	-8620	-8536	-8535	-8619	MG	0.00	0.00	110.00
3437	-9971	-9848	-9862	-9963	MG	0.00	0.00	110.00
3437	-9848	-9744	-9743	-9862	MG	0.00	0.00	110.00
3437	-10253	-10177	-10197	-10252	MG	0.00	0.00	110.00
3437	-10177	-10131	-10130	-10197	MG	0.00	0.00	110.00
3437	-10131	-10039	-10038	-10130	MG	0.00	0.00	110.00
3437	-10039	-9963	-9946	-10038	MG	0.00	0.00	110.00
3437	-9963	-9862	-9858	-9946	MG	0.00	0.00	110.00
3437	-9862	-9743	-9742	-9858	MG	0.00	0.00	110.00
3437	-10252	-10197	-10176	3302	MG	0.00	0.00	110.00
3437	-8806	-8716	-8715	-8839	MG	0.00	0.00	110.00
3437	-8716	-8618	-8617	-8715	MG	0.00	0.00	110.00
3437	-8618	-8534	-8533	-8617	MG	0.00	0.00	110.00
3437	-9946	-9858	-9857	-9962	MG	0.00	0.00	110.00
3437	-9858	-9742	-9741	-9857	MG	0.00	0.00	110.00
3437	-8904	-8839	-8803	-8903	MG	0.00	0.00	110.00
3437	-8839	-8715	-8714	-8803	MG	0.00	0.00	110.00
3437	-8715	-8617	-8616	-8714	MG	0.00	0.00	110.00
3437	-9215	-9157	-9156	-9214	MG	0.00	0.00	110.00
3437	-8533	-8470	-8469	-8532	MG	0.00	0.00	110.00
3437	-9201	-9143	-9142	-9200	MG	0.00	0.00	110.00
3437	-8903	-8803	-8802	-8902	MG	0.00	0.00	110.00
3437	-8803	-8714	-8713	-8802	MG	0.00	0.00	110.00
3437	-8234	-8160	-8159	-8233	MG	0.00	0.00	110.00
3437	-8160	-8034	-8033	-8159	MG	0.00	0.00	110.00
3437	-10193	-10125	-10124	-10192	MG	0.00	0.00	110.00
3437	-10125	-10033	-10032	-10124	MG	0.00	0.00	110.00
3437	-8469	-8419	-8418	-8477	MG	0.00	0.00	110.00
3437	-9945	-9854	-9839	-9961	MG	0.00	0.00	110.00
3437	-9854	-9739	-9738	-9839	MG	0.00	0.00	110.00
3437	-10248	-10192	-10191	-10247	MG	0.00	0.00	110.00
3437	-10192	-10124	-10123	-10191	MG	0.00	0.00	110.00
3437	-10124	-10032	-10031	-10123	MG	0.00	0.00	110.00
3437	-10032	-9961	-9967	-10031	MG	0.00	0.00	110.00
3437	-9379	-9288	-9287	-9378	MG	0.00	0.00	110.00
3437	-8629	-8621	-8720	-8721	MG	0.00	0.00	110.00
3437	-9288	-9212	-9211	-9287	MG	0.00	0.00	110.00
3437	-8386	-8325	-8324	-8385	MG	0.00	0.00	110.00
3437	-8325	-8237	-8236	-8324	MG	0.00	0.00	110.00
3437	-10031	-9967	-9944	-10030	MG	0.00	0.00	110.00
3437	-9967	-9853	-9838	-9944	MG	0.00	0.00	110.00
3437	-9287	-9211	-9210	-9286	MG	0.00	0.00	110.00
3437	-9211	-9153	-9152	-9210	MG	0.00	0.00	110.00
3437	-8385	-8324	-8323	-8384	MG	0.00	0.00	110.00
3437	-8324	-8236	-8235	-8323	MG	0.00	0.00	110.00
3437	-8914	-8843	-8842	-8913	MG	0.00	0.00	110.00
3437	-8162	-8036	-8035	-8161	MG	0.00	0.00	110.00
3437	-8036	-7982	-7981	-8035	MG	0.00	0.00	110.00
3437	-9152	-9075	-9074	-9151	MG	0.00	0.00	110.00
3437	-9596	-9548	-9547	-9595	MG	0.00	0.00	110.00
3437	-9548	-9484	-9483	-9547	MG	0.00	0.00	110.00
3437	-9442	-9441	-9485	-9486	MG	0.00	0.00	110.00
3437	-9438	-9372	-9371	-9437	MG	0.00	0.00	110.00
3437	-8035	-7981	-7980	-8034	MG	0.00	0.00	110.00
3437	-8430	-8383	-8382	-8429	MG	0.00	0.00	110.00
3437	-8383	-8322	-8321	-8382	MG	0.00	0.00	110.00
3437	-8322	-8234	-8233	-8321	MG	0.00	0.00	110.00
3437	-9093	-8976	-8975	-9068	MG	0.00	0.00	110.00
3437	-9483	-9437	-9436	-9478	MG	0.00	0.00	110.00
3437	-8034	-7980	-7979	-8033	MG	0.00	0.00	110.00

3437	-8429	-8382	-8381	-8428	MG	0.00	0.00	110.00
3437	-8382	-8321	-8320	-8381	MG	0.00	0.00	110.00
3437	-8321	-8233	-8232	-8320	MG	0.00	0.00	110.00
3437	-8233	-8159	-8158	-8232	MG	0.00	0.00	110.00
3437	-8159	-8033	-8032	-8158	MG	0.00	0.00	110.00
3437	-9289	-9213	-9212	-9288	MG	0.00	0.00	110.00
3437	-8428	-8381	-8380	-8427	MG	0.00	0.00	110.00
3437	-8381	-8320	-8319	-8380	MG	0.00	0.00	110.00
3437	-8320	-8232	-8231	-8319	MG	0.00	0.00	110.00
3437	-8232	-8158	-8157	-8231	MG	0.00	0.00	110.00
3437	-8158	-8032	-8031	-8157	MG	0.00	0.00	110.00
3437	-8032	-7978	-7977	-8031	MG	0.00	0.00	110.00
3437	-8380	-8319	-8318	-8379	MG	0.00	0.00	110.00
3437	-8319	-8231	-8230	-8318	MG	0.00	0.00	110.00
3437	-8231	-8157	-8156	-8230	MG	0.00	0.00	110.00
3437	-8157	-8031	-8030	-8156	MG	0.00	0.00	110.00
3437	-8031	-7977	-7976	-8030	MG	0.00	0.00	110.00
3437	-8481	-8480	-8538	-8539	MG	0.00	0.00	110.00
3437	-8480	-8479	-8537	-8538	MG	0.00	0.00	110.00
3437	-8377	-8316	-8315	-8376	MG	0.00	0.00	110.00
3437	-8316	-8228	-8227	-8315	MG	0.00	0.00	110.00
3437	-8228	-8154	-8153	-8227	MG	0.00	0.00	110.00
3437	-8154	-8028	-8027	-8153	MG	0.00	0.00	110.00
3437	-8028	-7974	-7973	-8027	MG	0.00	0.00	110.00
3437	-8479	-8472	-8536	-8537	MG	0.00	0.00	110.00
3437	-8991	-8917	-8916	-8990	MG	0.00	0.00	110.00
3437	-9382	-9291	-9290	-9381	MG	0.00	0.00	110.00
3437	-9368	-9277	-9276	-9367	MG	0.00	0.00	110.00
3437	-9277	-9201	-9200	-9276	MG	0.00	0.00	110.00
3437	-9637	-9595	-9594	-9636	MG	0.00	0.00	110.00
3437	-9099	-8990	-8989	-9098	MG	0.00	0.00	110.00
3437	-9547	-9483	-9478	-9546	MG	0.00	0.00	110.00
3437	-8826	-8726	-8725	-8843	MG	0.00	0.00	110.00
3437	-8726	-8633	-8632	-8725	MG	0.00	0.00	110.00
3437	-8723	-8630	-8622	-8722	MG	0.00	0.00	110.00
3437	-9151	-9150	-9208	-9209	MG	0.00	0.00	110.00
3437	-9594	-9546	-9545	-9593	MG	0.00	0.00	110.00
3437	-8989	-8915	-8914	-8988	MG	0.00	0.00	110.00
3437	-8902	-8802	-8801	-8901	MG	0.00	0.00	110.00
3437	-8981	-8907	-8906	-8980	MG	0.00	0.00	110.00
3437	-8546	-8486	-8485	-8545	MG	0.00	0.00	110.00
3437	-8486	-8433	-8432	-8485	MG	0.00	0.00	110.00
3437	-9097	-8988	-8987	-9096	MG	0.00	0.00	110.00
3437	-8988	-8914	-8913	-8987	MG	0.00	0.00	110.00
3437	-8980	-8906	-8905	-8979	MG	0.00	0.00	110.00
3437	-9435	-9369	-9368	-9434	MG	0.00	0.00	110.00
3437	-9212	-9154	-9153	-9211	MG	0.00	0.00	110.00
3437	-9154	-9096	-9076	-9153	MG	0.00	0.00	110.00
3437	-9096	-8987	-8986	-9076	MG	0.00	0.00	110.00
3437	-9544	-9476	-9502	-9543	MG	0.00	0.00	110.00
3437	-9476	-9434	-9433	-9502	MG	0.00	0.00	110.00
3437	-8633	-8544	-8543	-8632	MG	0.00	0.00	110.00
3437	-8544	-8484	-8483	-8543	MG	0.00	0.00	110.00
3437	-9153	-9076	-9075	-9152	MG	0.00	0.00	110.00
3437	-8905	-8806	-8839	-8904	MG	0.00	0.00	110.00
3437	-9439	-9373	-9372	-9438	MG	0.00	0.00	110.00
3437	-9738	-9638	-9637	-9737	MG	0.00	0.00	110.00
3437	-9638	-9596	-9595	-9637	MG	0.00	0.00	110.00
3437	-8632	-8543	-8542	-8631	MG	0.00	0.00	110.00
3437	-8725	-8632	-8631	-8724	MG	0.00	0.00	110.00
3437	-9484	-9438	-9437	-9483	MG	0.00	0.00	110.00
3437	-8913	-8842	-8787	-8912	MG	0.00	0.00	110.00
3437	-9737	-9637	-9636	-9736	MG	0.00	0.00	110.00
3437	-8842	-8724	-8723	-8787	MG	0.00	0.00	110.00
3437	-8542	-8474	-8473	-8541	MG	0.00	0.00	110.00
3437	-9592	-9544	-9543	-9591	MG	0.00	0.00	110.00
3437	-8472	-8423	-8422	-8478	MG	0.00	0.00	110.00
3437	-8987	-8913	-8912	-8986	MG	0.00	0.00	110.00
3437	-9434	-9368	-9367	-9433	MG	0.00	0.00	110.00
3437	-8630	-8541	-8540	-8622	MG	0.00	0.00	110.00
3437	-9206	-9148	-9147	-9205	MG	0.00	0.00	110.00
3437	-9546	-9478	-9477	-9545	MG	0.00	0.00	110.00
3437	-9478	-9436	-9435	-9477	MG	0.00	0.00	110.00
3437	-9292	-9216	-9215	-9291	MG	0.00	0.00	110.00
3437	-9216	-9158	-9157	-9215	MG	0.00	0.00	110.00
3437	-9635	-9593	-9592	-9634	MG	0.00	0.00	110.00
3437	-9593	-9545	-9544	-9592	MG	0.00	0.00	110.00
3437	-9545	-9477	-9476	-9544	MG	0.00	0.00	110.00
3437	-8477	-8418	-8417	-8468	MG	0.00	0.00	110.00

3437	-9291	-9215	-9214	-9290	MG	0.00	0.00	110.00
3437	-9735	-9634	-9633	-9734	MG	0.00	0.00	110.00
3437	-9634	-9592	-9591	-9633	MG	0.00	0.00	110.00
3437	-8536	-8472	-8478	-8535	MG	0.00	0.00	110.00
3437	-9286	-9210	-9209	-9285	MG	0.00	0.00	110.00
3437	-8906	-8807	-8806	-8905	MG	0.00	0.00	110.00
3437	-9378	-9287	-9286	-9377	MG	0.00	0.00	110.00
3437	-8535	-8478	-8471	-8534	MG	0.00	0.00	110.00
3437	-8478	-8422	-8421	-8471	MG	0.00	0.00	110.00
3437	-9203	-9145	-9144	-9202	MG	0.00	0.00	110.00
3437	-9551	-9550	-9598	-9599	MG	0.00	0.00	110.00
3437	-9070	-8978	-8977	-9069	MG	0.00	0.00	110.00
3437	-9145	-9070	-9069	-9144	MG	0.00	0.00	110.00
3437	-9158	-9100	-9099	-9157	MG	0.00	0.00	110.00
3437	-8531	-8477	-8468	-8530	MG	0.00	0.00	110.00
3437	-9144	-9069	-9093	-9143	MG	0.00	0.00	110.00
3437	-9071	-8980	-8979	-9094	MG	0.00	0.00	110.00
3437	-8619	-8535	-8534	-8618	MG	0.00	0.00	110.00
3437	-8627	-8531	-8530	-8615	MG	0.00	0.00	110.00
3437	-9280	-9204	-9203	-9279	MG	0.00	0.00	110.00
3437	-8163	-8037	-8036	-8162	MG	0.00	0.00	110.00
3437	-8978	-8904	-8903	-8977	MG	0.00	0.00	110.00
3437	-8843	-8725	-8724	-8842	MG	0.00	0.00	110.00
3437	-8807	-8717	-8716	-8806	MG	0.00	0.00	110.00
3437	-8717	-8619	-8618	-8716	MG	0.00	0.00	110.00
3437	-9072	-8981	-8980	-9071	MG	0.00	0.00	110.00
3437	-8713	-8627	-8615	-8712	MG	0.00	0.00	110.00
3437	-9210	-9152	-9151	-9209	MG	0.00	0.00	110.00
3438	-10036	-6505	-6598	-10128	MG	0.00	0.00	110.00
3438	-9376	-5606	-5818	-9442	MG	0.00	0.00	110.00
3438	-9642	-6103	-6002	-9740	MG	0.00	0.00	110.00
3438	-8984	-5398	-5621	-9074	MG	0.00	0.00	110.00
3438	-9847	-6222	-6438	-9970	MG	0.00	0.00	110.00
3438	-9486	-6037	-6105	-9552	MG	0.00	0.00	110.00
3438	-9552	-6105	-6173	-9600	MG	0.00	0.00	110.00
3438	-10196	-6496	-6382	-10251	MG	0.00	0.00	110.00
3438	-9209	-5774	-5690	-9285	MG	0.00	0.00	110.00
3438	-9285	-5690	-5606	-9376	MG	0.00	0.00	110.00
3438	-9151	-5702	-5774	-9209	MG	0.00	0.00	110.00
3438	-9740	-6002	-6222	-9847	MG	0.00	0.00	110.00
3438	-9074	-5621	-5702	-9151	MG	0.00	0.00	110.00
3438	-9970	-6438	-6505	-10036	MG	0.00	0.00	110.00
3438	-10128	-6598	-6496	-10196	MG	0.00	0.00	110.00
3438	-9442	-5818	-6037	-9486	MG	0.00	0.00	110.00
3438	-9600	-6173	-6103	-9642	MG	0.00	0.00	110.00
3440	-7008	-7494	-7495	-6240	MG	0.00	0.00	110.00
3443	-7973	-5013	-4950	-7972	MG	0.00	0.00	110.00
3447	-4815	-4421	-8423	-8424	MG	0.00	0.00	110.00
3448	-8423	-5418	-5352	-8422	MG	0.00	0.00	110.00
3451	-5215	-4888	-8907	-8908	MG	0.00	0.00	110.00
3451	-4888	-5807	-8907	-8907	MG	0.00	0.00	110.00
3452	-6170	-6259	-6926	-6926	MG	0.00	0.00	110.00
3453	-5306	-6221	-9373	-9373	MG	0.00	0.00	110.00
3471	-6692	-6152	-6691	-6691	MG	0.00	0.00	110.00
3474	-7145	-6559	-7144	-7144	MG	0.00	0.00	110.00
3474	-6559	-5853	-7143	-7144	MG	0.00	0.00	110.00
3478	-7009	-6253	-7505	-7506	MG	0.00	0.00	110.00
3482	-4951	-5014	-7977	-7978	MG	0.00	0.00	110.00
3484	-5353	-5397	-8427	-8428	MG	0.00	0.00	110.00
3485	-4422	-4816	-8426	-8427	MG	0.00	0.00	110.00
3487	-5817	-4897	-8911	-8911	MG	0.00	0.00	110.00
3487	-4897	-5216	-8910	-8911	MG	0.00	0.00	110.00
3490	-6927	-6269	-6171	-6171	MG	0.00	0.00	110.00
3491	-6230	-5307	-9377	-9377	MG	0.00	0.00	110.00
3494	-6578	-5784	-6699	-6699	MG	0.00	0.00	110.00
3494	-6578	-6699	-7309	-7309	MG	0.00	0.00	110.00
3495	-5766	-6700	-6579	-6579	MG	0.00	0.00	110.00
3495	-7310	-6700	-6579	-6579	MG	0.00	0.00	110.00
3553	-7021	-7156	-7727	-7727	MG	0.00	0.00	110.00
3554	-6107	-6382	-10251	3302	MG	0.00	0.00	110.00
3554	-7022	-7092	3302	-10252	MG	0.00	0.00	110.00
3554	-7092	-6107	3302	3302	MG	0.00	0.00	110.00
3555	3301	-7091	-7021	-10248	MG	0.00	0.00	110.00
3555	-6380	-6106	3301	-10249	MG	0.00	0.00	110.00
3555	-6106	-7091	3301	3301	MG	0.00	0.00	110.00
3556	-7728	-7157	-7022	-7022	MG	0.00	0.00	110.00
3569	-7008	-7493	-7494	-7494	MG	0.00	0.00	110.00
3572	-7357	-7968	-7969	-7969	MG	0.00	0.00	110.00
3572	-7357	-7969	-7970	-6674	MG	0.00	0.00	110.00

3577	-7814	-8419	-8420	-7147	MG	0.00	0.00	110.00
3577	-7814	-8418	-8419	-8419	MG	0.00	0.00	110.00
3579	-8907	-5807	-5781	-8906	MG	0.00	0.00	110.00
3581	-9373	-6221	-6170	-9372	MG	0.00	0.00	110.00
3582	-5605	-5306	-9373	-9374	MG	0.00	0.00	110.00
3583	-8326	-8902	-8903	-8903	MG	0.00	0.00	110.00
3583	-8326	-8903	-8904	-7509	MG	0.00	0.00	110.00
3599	-7507	-7009	-7506	-7506	MG	0.00	0.00	110.00
3601	-7358	-6694	-7980	-7981	MG	0.00	0.00	110.00
3601	-7982	-7358	-7981	-7981	MG	0.00	0.00	110.00
3605	-8432	-7815	-8431	-8431	MG	0.00	0.00	110.00
3605	-7815	-7148	-8430	-8431	MG	0.00	0.00	110.00
3607	-5773	-5817	-8911	-8912	MG	0.00	0.00	110.00
3609	-8916	-8327	-8915	-8915	MG	0.00	0.00	110.00
3609	-8327	-7510	-8914	-8915	MG	0.00	0.00	110.00
3611	-6171	-6230	-9377	-9378	MG	0.00	0.00	110.00
3612	-5307	-5606	-9376	-9377	MG	0.00	0.00	110.00
3614	-9382	-8730	-9381	-9381	MG	0.00	0.00	110.00
3614	-8730	-7985	-9380	-9381	MG	0.00	0.00	110.00
3616	-8729	-9368	-9369	-9369	MG	0.00	0.00	110.00
3616	-8729	-9369	-9370	-7984	MG	0.00	0.00	110.00
3618	-5691	-6659	-9739	-9739	MG	0.00	0.00	110.00
3618	-6001	-5691	-9739	-9727	MG	0.00	0.00	110.00
3618	-9739	-6659	-6578	-9738	MG	0.00	0.00	110.00
3620	-5692	-6002	-9740	-9741	MG	0.00	0.00	110.00
3620	-6579	-6660	-9741	-9742	MG	0.00	0.00	110.00
3620	-6660	-5692	-9741	-9741	MG	0.00	0.00	110.00
3622	-9746	-9218	-9745	-9745	MG	0.00	0.00	110.00
3622	-9218	-8435	-9744	-9745	MG	0.00	0.00	110.00
3624	-9217	-9735	-9726	-9726	MG	0.00	0.00	110.00
3624	-9217	-9726	-9736	-8434	MG	0.00	0.00	110.00
3627	-9608	-10244	-10245	-10245	MG	0.00	0.00	110.00
3627	-9608	-10245	-10246	-8918	MG	0.00	0.00	110.00
3629	-10256	-9609	-10255	-10255	MG	0.00	0.00	110.00
3629	-9609	-8919	-10254	-10255	MG	0.00	0.00	110.00
3824	-4583	-4588	-4572	-4571	MG	0.00	0.00	110.00
3824	-4611	-4594	-4597	-4625	MG	0.00	0.00	110.00
3824	-4626	-4611	-4625	-4625	MG	0.00	0.00	110.00
3824	-4621	-4603	-4601	-4620	MG	0.00	0.00	110.00
3824	-4652	-4635	-4634	-4651	MG	0.00	0.00	110.00
3824	-4589	-4598	-4608	-4592	MG	0.00	0.00	110.00
3824	-4607	-4583	-4592	-4608	MG	0.00	0.00	110.00
3824	-4573	-4570	-4558	-4555	MG	0.00	0.00	110.00
3824	-4651	-4634	-4633	-4650	MG	0.00	0.00	110.00
3824	-4536	-4527	-4531	-4531	MG	0.00	0.00	110.00
3824	-4594	-4579	-4590	-4597	MG	0.00	0.00	110.00
3824	-4579	-4569	-4574	-4590	MG	0.00	0.00	110.00
3824	-4569	-4554	-4562	-4574	MG	0.00	0.00	110.00
3824	-4554	-4541	-4551	-4562	MG	0.00	0.00	110.00
3824	-4541	-4539	-4545	-4551	MG	0.00	0.00	110.00
3824	-4583	-4607	-4604	-4588	MG	0.00	0.00	110.00
3824	-4649	-4632	-4631	-4648	MG	0.00	0.00	110.00
3824	-4634	-4620	-4619	-4633	MG	0.00	0.00	110.00
3824	-4648	-4631	-4636	-4653	MG	0.00	0.00	110.00
3824	-4631	-4617	-4616	-4636	MG	0.00	0.00	110.00
3824	-4636	-4616	-4615	-4638	MG	0.00	0.00	110.00
3824	-4615	-4614	-4640	-4638	MG	0.00	0.00	110.00
3824	-4614	-4613	-4629	-4640	MG	0.00	0.00	110.00
3824	-4613	-4612	-4627	-4629	MG	0.00	0.00	110.00
3824	-4627	-4642	-4644	-4629	MG	0.00	0.00	110.00
3824	-4642	-4659	-4663	-4644	MG	0.00	0.00	110.00
3824	-4562	-4551	-4558	-4570	MG	0.00	0.00	110.00
3824	-4545	-4555	-4558	-4551	MG	0.00	0.00	110.00
3824	-4570	-4573	-4587	-4586	MG	0.00	0.00	110.00
3824	-4650	-4633	-4632	-4649	MG	0.00	0.00	110.00
3824	-4633	-4619	-4618	-4632	MG	0.00	0.00	110.00
3824	-4597	-4590	-4591	-4609	MG	0.00	0.00	110.00
3824	-4591	-4590	-4574	-4586	MG	0.00	0.00	110.00
3824	-4586	-4587	-4605	-4606	MG	0.00	0.00	110.00
3824	-4632	-4618	-4617	-4631	MG	0.00	0.00	110.00
3824	-4629	-4644	-4646	-4640	MG	0.00	0.00	110.00
3824	-4644	-4663	-4661	-4646	MG	0.00	0.00	110.00
3824	-4646	-4661	-4657	-4640	MG	0.00	0.00	110.00
3824	-4532	-4528	-4537	-4537	MG	0.00	0.00	110.00
3824	-4635	-4621	-4620	-4634	MG	0.00	0.00	110.00
3824	-4653	-4636	-4638	-4655	MG	0.00	0.00	110.00
3824	-4655	-4638	-4640	-4657	MG	0.00	0.00	110.00
3824	-4660	-4643	-4645	-4664	MG	0.00	0.00	110.00
3824	-4643	-4628	-4630	-4645	MG	0.00	0.00	110.00

3824	-4628	-4626	-4625	-4630	MG	0.00	0.00	110.00
3824	-4625	-4624	-4641	-4630	MG	0.00	0.00	110.00
3824	-4624	-4623	-4639	-4641	MG	0.00	0.00	110.00
3824	-4623	-4622	-4637	-4639	MG	0.00	0.00	110.00
3824	-4637	-4622	-4621	-4635	MG	0.00	0.00	110.00
3824	-4654	-4637	-4635	-4652	MG	0.00	0.00	110.00
3824	-4539	-4532	-4537	-4545	MG	0.00	0.00	110.00
3824	-4537	-4550	-4555	-4545	MG	0.00	0.00	110.00
3824	-4550	-4567	-4573	-4555	MG	0.00	0.00	110.00
3824	-4567	-4585	-4587	-4573	MG	0.00	0.00	110.00
3824	-4585	-4603	-4605	-4587	MG	0.00	0.00	110.00
3824	-4603	-4621	-4622	-4605	MG	0.00	0.00	110.00
3824	-4622	-4623	-4606	-4605	MG	0.00	0.00	110.00
3824	-4623	-4624	-4609	-4606	MG	0.00	0.00	110.00
3824	-4624	-4625	-4597	-4609	MG	0.00	0.00	110.00
3824	-4658	-4662	-4647	-4641	MG	0.00	0.00	110.00
3824	-4662	-4664	-4645	-4647	MG	0.00	0.00	110.00
3824	-4647	-4645	-4630	-4641	MG	0.00	0.00	110.00
3824	-4639	-4637	-4654	-4656	MG	0.00	0.00	110.00
3824	-4639	-4656	-4658	-4641	MG	0.00	0.00	110.00
3824	-4570	-4586	-4574	-4562	MG	0.00	0.00	110.00
3824	-4606	-4609	-4591	-4586	MG	0.00	0.00	110.00
3824	-4603	-4585	-4582	-4601	MG	0.00	0.00	110.00
3824	-4585	-4567	-4565	-4582	MG	0.00	0.00	110.00
3824	-4567	-4550	-4548	-4565	MG	0.00	0.00	110.00
3824	-4550	-4537	-4535	-4548	MG	0.00	0.00	110.00
3824	-4537	-4528	-4526	-4535	MG	0.00	0.00	110.00
3824	-4620	-4601	-4599	-4619	MG	0.00	0.00	110.00
3824	-4601	-4582	-4580	-4599	MG	0.00	0.00	110.00
3824	-4582	-4565	-4563	-4580	MG	0.00	0.00	110.00
3824	-4565	-4548	-4546	-4563	MG	0.00	0.00	110.00
3824	-4548	-4535	-4533	-4546	MG	0.00	0.00	110.00
3824	-4535	-4526	-4524	-4533	MG	0.00	0.00	110.00
3824	-4619	-4599	-4600	-4618	MG	0.00	0.00	110.00
3824	-4599	-4580	-4581	-4600	MG	0.00	0.00	110.00
3824	-4580	-4563	-4564	-4581	MG	0.00	0.00	110.00
3824	-4563	-4546	-4547	-4564	MG	0.00	0.00	110.00
3824	-4546	-4533	-4534	-4547	MG	0.00	0.00	110.00
3824	-4533	-4524	-4525	-4534	MG	0.00	0.00	110.00
3824	-4618	-4600	-4602	-4617	MG	0.00	0.00	110.00
3824	-4600	-4581	-4584	-4602	MG	0.00	0.00	110.00
3824	-4581	-4564	-4566	-4584	MG	0.00	0.00	110.00
3824	-4564	-4547	-4549	-4566	MG	0.00	0.00	110.00
3824	-4547	-4534	-4536	-4549	MG	0.00	0.00	110.00
3824	-4534	-4525	-4527	-4536	MG	0.00	0.00	110.00
3824	-4610	-4612	-4613	-4613	MG	0.00	0.00	110.00
3824	-4602	-4584	-4588	-4604	MG	0.00	0.00	110.00
3824	-4584	-4566	-4572	-4588	MG	0.00	0.00	110.00
3824	-4566	-4549	-4556	-4572	MG	0.00	0.00	110.00
3824	-4549	-4536	-4544	-4556	MG	0.00	0.00	110.00
3824	-4536	-4531	-4538	-4544	MG	0.00	0.00	110.00
3824	-4538	-4540	-4552	-4544	MG	0.00	0.00	110.00
3824	-4540	-4553	-4561	-4552	MG	0.00	0.00	110.00
3824	-4553	-4568	-4575	-4561	MG	0.00	0.00	110.00
3824	-4568	-4578	-4589	-4575	MG	0.00	0.00	110.00
3824	-4578	-4593	-4598	-4589	MG	0.00	0.00	110.00
3824	-4593	-4610	-4613	-4598	MG	0.00	0.00	110.00
3824	-4613	-4614	-4608	-4598	MG	0.00	0.00	110.00
3824	-4614	-4615	-4607	-4608	MG	0.00	0.00	110.00
3824	-4615	-4616	-4604	-4607	MG	0.00	0.00	110.00
3824	-4617	-4602	-4604	-4616	MG	0.00	0.00	110.00
3824	-4544	-4552	-4557	-4556	MG	0.00	0.00	110.00
3824	-4561	-4571	-4557	-4552	MG	0.00	0.00	110.00
3824	-4572	-4556	-4557	-4571	MG	0.00	0.00	110.00
3824	-4575	-4583	-4571	-4561	MG	0.00	0.00	110.00
3824	-4575	-4589	-4592	-4583	MG	0.00	0.00	110.00

Elenco carichi elementi bidimensionali
Condizione di carico n. 3: Permanenti NS G2
Carichi uniformi

Bid.	N1	N2	N3	N4	TDC	Qx <daN/mq>	Qy <daN/mq>	Qz <daN/mq>
2718	-3859	-3858	-3909	-3910	MG	0.00	0.00	100.00
2718	-3676	-3664	-3712	-3719	MG	0.00	0.00	100.00
2718	-3665	-3676	-3719	-3720	MG	0.00	0.00	100.00
2718	-3572	-3571	-3610	-3611	MG	0.00	0.00	100.00
2718	-3719	-3712	-3768	-3769	MG	0.00	0.00	100.00
2718	-3720	-3719	-3769	-3765	MG	0.00	0.00	100.00

2718	-3610	-3609	-3664	-3676	MG	0.00	0.00	100.00
2718	-3571	-3570	-3609	-3610	MG	0.00	0.00	100.00
2718	-3769	-3768	-3810	-3811	MG	0.00	0.00	100.00
2718	-3765	-3769	-3811	-3812	MG	0.00	0.00	100.00
2718	-3858	-3857	-3908	-3909	MG	0.00	0.00	100.00
2718	-3957	-3950	-4000	-4001	MG	0.00	0.00	100.00
2718	-3812	-3811	-3858	-3859	MG	0.00	0.00	100.00
2718	-3909	-3908	-3950	-3957	MG	0.00	0.00	100.00
2718	-3958	-3957	-4001	-4002	MG	0.00	0.00	100.00
2718	-3811	-3810	-3857	-3858	MG	0.00	0.00	100.00
2718	-3525	-3524	-3571	-3572	MG	0.00	0.00	100.00
2718	-3910	-3909	-3957	-3958	MG	0.00	0.00	100.00
2718	-3524	-3523	-3570	-3571	MG	0.00	0.00	100.00
2718	-3611	-3610	-3676	-3665	MG	0.00	0.00	100.00
2816	-3655	-3748	-4148	-4148	MG	0.00	0.00	100.00
2817	-3947	-4038	-4403	-4403	MG	0.00	0.00	100.00
2822	-4219	-3663	-4295	-4295	MG	0.00	0.00	100.00
2843	-4149	-3749	-3656	-3656	MG	0.00	0.00	100.00
2847	-4404	-4039	-3948	-3948	MG	0.00	0.00	100.00
2848	-3659	-4296	-4220	-4220	MG	0.00	0.00	100.00
2921	-4198	-4683	-4684	-4684	MG	0.00	0.00	100.00
2921	-4198	-4684	-4685	-3732	MG	0.00	0.00	100.00
2931	-6370	-3558	-3605	-6483	MG	0.00	0.00	100.00
2933	-6102	-3664	-3712	-6001	MG	0.00	0.00	100.00
2933	-6036	-3523	-3570	-6104	MG	0.00	0.00	100.00
2933	-6104	-3570	-3609	-6172	MG	0.00	0.00	100.00
2933	-6172	-3609	-3664	-6102	MG	0.00	0.00	100.00
2933	-6001	-3712	-3768	-6206	MG	0.00	0.00	100.00
2934	-4219	-4295	-4870	-4870	MG	0.00	0.00	100.00
2935	-4670	-4653	-4655	-4672	MG	0.00	0.00	100.00
2935	-4676	-4661	-4663	-4679	MG	0.00	0.00	100.00
2935	-4804	-4747	-4746	-4803	MG	0.00	0.00	100.00
2935	-4746	-4687	-4686	-4745	MG	0.00	0.00	100.00
2935	-4858	-4803	-4802	-4857	MG	0.00	0.00	100.00
2935	-4676	-4674	-4657	-4661	MG	0.00	0.00	100.00
2935	-4864	-4809	-4808	-4863	MG	0.00	0.00	100.00
2935	-4671	-4654	-4652	-4669	MG	0.00	0.00	100.00
2935	-4747	-4688	-4687	-4746	MG	0.00	0.00	100.00
2935	-4690	-4689	-4748	-4749	MG	0.00	0.00	100.00
2935	-4697	-4680	-4677	-4696	MG	0.00	0.00	100.00
2935	-4672	-4655	-4657	-4674	MG	0.00	0.00	100.00
2935	-4855	-4800	-4799	-4854	MG	0.00	0.00	100.00
2935	-4803	-4746	-4745	-4802	MG	0.00	0.00	100.00
2935	-4669	-4652	-4651	-4668	MG	0.00	0.00	100.00
2935	-4754	-4695	-4694	-4753	MG	0.00	0.00	100.00
2935	-4859	-4804	-4803	-4858	MG	0.00	0.00	100.00
2935	-4755	-4696	-4695	-4754	MG	0.00	0.00	100.00
2935	-4813	-4756	-4755	-4812	MG	0.00	0.00	100.00
2935	-4802	-4745	-4744	-4801	MG	0.00	0.00	100.00
2935	-4656	-4673	-4675	-4658	MG	0.00	0.00	100.00
2935	-4812	-4755	-4754	-4811	MG	0.00	0.00	100.00
2935	-4867	-4812	-4811	-4866	MG	0.00	0.00	100.00
2935	-4748	-4689	-4688	-4747	MG	0.00	0.00	100.00
2935	-4666	-4649	-4648	-4665	MG	0.00	0.00	100.00
2935	-4688	-4665	-4670	-4687	MG	0.00	0.00	100.00
2935	-4694	-4695	-4675	-4673	MG	0.00	0.00	100.00
2935	-4698	-4681	-4680	-4697	MG	0.00	0.00	100.00
2935	-4749	-4748	-4805	-4806	MG	0.00	0.00	100.00
2935	-4752	-4693	-4692	-4751	MG	0.00	0.00	100.00
2935	-4809	-4752	-4751	-4808	MG	0.00	0.00	100.00
2935	-4751	-4692	-4691	-4750	MG	0.00	0.00	100.00
2935	-4807	-4806	-4861	-4862	MG	0.00	0.00	100.00
2935	-4745	-4686	-4685	-4744	MG	0.00	0.00	100.00
2935	-4692	-4669	-4668	-4691	MG	0.00	0.00	100.00
2935	-4857	-4802	-4801	-4856	MG	0.00	0.00	100.00
2935	-4667	-4650	-4649	-4666	MG	0.00	0.00	100.00
2935	-4689	-4666	-4665	-4688	MG	0.00	0.00	100.00
2935	-4810	-4753	-4752	-4809	MG	0.00	0.00	100.00
2935	-4686	-4687	-4670	-4672	MG	0.00	0.00	100.00
2935	-4856	-4801	-4800	-4855	MG	0.00	0.00	100.00
2935	-4668	-4651	-4650	-4667	MG	0.00	0.00	100.00
2935	-4669	-4692	-4693	-4671	MG	0.00	0.00	100.00
2935	-4665	-4648	-4653	-4670	MG	0.00	0.00	100.00
2935	-4696	-4677	-4675	-4695	MG	0.00	0.00	100.00
2935	-4744	-4685	-4684	-4743	MG	0.00	0.00	100.00
2935	-4805	-4748	-4747	-4804	MG	0.00	0.00	100.00
2935	-4756	-4697	-4696	-4755	MG	0.00	0.00	100.00
2935	-4677	-4680	-4664	-4662	MG	0.00	0.00	100.00
2935	-4686	-4672	-4674	-4685	MG	0.00	0.00	100.00

2935	-4681	-4660	-4664	-4680	MG	0.00	0.00	100.00
2935	-4753	-4694	-4693	-4752	MG	0.00	0.00	100.00
2935	-4684	-4685	-4674	-4676	MG	0.00	0.00	100.00
2935	-4656	-4654	-4671	-4673	MG	0.00	0.00	100.00
2935	-4750	-4749	-4806	-4807	MG	0.00	0.00	100.00
2935	-4690	-4667	-4666	-4689	MG	0.00	0.00	100.00
2935	-4742	-4683	-4682	-4741	MG	0.00	0.00	100.00
2935	-4868	-4813	-4812	-4867	MG	0.00	0.00	100.00
2935	-4808	-4751	-4750	-4807	MG	0.00	0.00	100.00
2935	-4866	-4811	-4810	-4865	MG	0.00	0.00	100.00
2935	-4691	-4668	-4667	-4690	MG	0.00	0.00	100.00
2935	-4694	-4673	-4671	-4693	MG	0.00	0.00	100.00
2935	-4691	-4690	-4749	-4750	MG	0.00	0.00	100.00
2935	-4801	-4744	-4743	-4800	MG	0.00	0.00	100.00
2935	-4865	-4810	-4809	-4864	MG	0.00	0.00	100.00
2935	-4814	-4757	-4756	-4813	MG	0.00	0.00	100.00
2935	-4659	-4678	-4679	-4663	MG	0.00	0.00	100.00
2935	-4869	-4814	-4813	-4868	MG	0.00	0.00	100.00
2935	-4811	-4754	-4753	-4810	MG	0.00	0.00	100.00
2935	-4799	-4742	-4741	-4798	MG	0.00	0.00	100.00
2935	-4854	-4799	-4798	-4853	MG	0.00	0.00	100.00
2935	-4684	-4676	-4679	-4683	MG	0.00	0.00	100.00
2935	-4683	-4679	-4678	-4682	MG	0.00	0.00	100.00
2935	-4757	-4698	-4697	-4756	MG	0.00	0.00	100.00
2935	-4743	-4684	-4683	-4742	MG	0.00	0.00	100.00
2935	-4677	-4662	-4658	-4675	MG	0.00	0.00	100.00
2935	-4860	-4805	-4804	-4859	MG	0.00	0.00	100.00
2935	-4806	-4805	-4860	-4861	MG	0.00	0.00	100.00
2935	-4800	-4743	-4742	-4799	MG	0.00	0.00	100.00
2935	-4863	-4808	-4807	-4862	MG	0.00	0.00	100.00
2937	-6372	-3559	-3606	-6485	MG	0.00	0.00	100.00
2939	-6105	-3572	-3611	-6173	MG	0.00	0.00	100.00
2939	-6037	-3525	-3572	-6105	MG	0.00	0.00	100.00
2939	-6002	-3720	-3765	-6222	MG	0.00	0.00	100.00
2939	-6173	-3611	-3665	-6103	MG	0.00	0.00	100.00
2939	-6103	-3665	-3720	-6002	MG	0.00	0.00	100.00
2940	-4459	-3955	-4711	-4711	MG	0.00	0.00	100.00
2944	-5352	-3764	-4471	-4471	MG	0.00	0.00	100.00
2945	-4697	-4199	-4696	-4696	MG	0.00	0.00	100.00
2945	-4199	-3733	-4695	-4696	MG	0.00	0.00	100.00
2953	-4871	-4296	-4220	-4220	MG	0.00	0.00	100.00
2954	-3949	-4712	-4460	-4460	MG	0.00	0.00	100.00
2955	-5353	-4463	-3767	-3767	MG	0.00	0.00	100.00
3007	-3763	-4003	-6107	-5257	MG	0.00	0.00	100.00
3008	-3999	-3766	-5256	-6106	MG	0.00	0.00	100.00
3022	-4445	-5039	-5040	-4019	MG	0.00	0.00	100.00
3031	-6689	-3536	-3698	-6748	MG	0.00	0.00	100.00
3031	-6620	-3590	-3536	-6689	MG	0.00	0.00	100.00
3031	-6483	-3605	-3657	-6548	MG	0.00	0.00	100.00
3031	-6548	-3657	-3590	-6620	MG	0.00	0.00	100.00
3032	-6206	-3768	-3810	-6437	MG	0.00	0.00	100.00
3032	-6437	-3810	-3857	-6501	MG	0.00	0.00	100.00
3033	-3607	-4251	-7136	-7136	MG	0.00	0.00	100.00
3034	-5041	-4976	-4992	-5040	MG	0.00	0.00	100.00
3034	-4918	-4855	-4854	-4917	MG	0.00	0.00	100.00
3034	-5042	-4968	-4976	-5041	MG	0.00	0.00	100.00
3034	-4932	-4866	-4865	-4931	MG	0.00	0.00	100.00
3034	-4967	-4918	-4917	-4966	MG	0.00	0.00	100.00
3034	-5048	-4995	-4979	-5047	MG	0.00	0.00	100.00
3034	-4926	-4860	-4859	-4925	MG	0.00	0.00	100.00
3034	-4861	-4860	-4926	-4927	MG	0.00	0.00	100.00
3034	-4994	-4930	-4929	-4978	MG	0.00	0.00	100.00
3034	-4929	-4863	-4862	-4928	MG	0.00	0.00	100.00
3034	-4924	-4858	-4857	-4919	MG	0.00	0.00	100.00
3034	-4978	-4929	-4928	-4970	MG	0.00	0.00	100.00
3034	-4927	-4926	-4969	-4993	MG	0.00	0.00	100.00
3034	-4925	-4859	-4858	-4924	MG	0.00	0.00	100.00
3034	-4976	-4919	-4923	-4992	MG	0.00	0.00	100.00
3034	-4995	-4932	-4931	-4979	MG	0.00	0.00	100.00
3034	-5046	-4994	-4978	2902	MG	0.00	0.00	100.00
3034	-4969	-4926	-4925	-4977	MG	0.00	0.00	100.00
3034	-4919	-4857	-4856	-4923	MG	0.00	0.00	100.00
3034	-5051	-4997	-4980	-5050	MG	0.00	0.00	100.00
3034	2902	-4978	-4970	-5045	MG	0.00	0.00	100.00
3034	-5043	-4969	-4977	2901	MG	0.00	0.00	100.00
3034	-4920	-4867	-4866	-4932	MG	0.00	0.00	100.00
3034	-4992	-4923	-4918	-4967	MG	0.00	0.00	100.00
3034	-4996	-4920	-4932	-4995	MG	0.00	0.00	100.00
3034	-4923	-4856	-4855	-4918	MG	0.00	0.00	100.00

3034	-4930	-4864	-4863	-4929	MG	0.00	0.00	100.00
3034	-4997	-4934	-4933	-4980	MG	0.00	0.00	100.00
3034	-5039	-4967	-4966	-5038	MG	0.00	0.00	100.00
3034	2901	-4977	-4968	-5042	MG	0.00	0.00	100.00
3034	-4993	-4969	-5043	-5044	MG	0.00	0.00	100.00
3034	-4931	-4865	-4864	-4930	MG	0.00	0.00	100.00
3034	-4862	-4861	-4927	-4928	MG	0.00	0.00	100.00
3034	-5040	-4992	-4967	-5039	MG	0.00	0.00	100.00
3034	-4970	-4993	-5044	-5045	MG	0.00	0.00	100.00
3034	-4934	-4869	-4868	-4933	MG	0.00	0.00	100.00
3034	-4968	-4924	-4919	-4976	MG	0.00	0.00	100.00
3034	-4917	-4854	-4853	-4916	MG	0.00	0.00	100.00
3034	-5050	-4980	-4996	-5049	MG	0.00	0.00	100.00
3034	-5047	-4979	-4994	-5046	MG	0.00	0.00	100.00
3034	-4928	-4927	-4993	-4970	MG	0.00	0.00	100.00
3034	-4979	-4931	-4930	-4994	MG	0.00	0.00	100.00
3034	-5049	-4996	-4995	-5048	MG	0.00	0.00	100.00
3034	-4977	-4925	-4924	-4968	MG	0.00	0.00	100.00
3034	-4933	-4868	-4867	-4920	MG	0.00	0.00	100.00
3034	-5038	-4966	-4991	-5037	MG	0.00	0.00	100.00
3034	-4966	-4917	-4916	-4991	MG	0.00	0.00	100.00
3034	-4980	-4933	-4920	-4996	MG	0.00	0.00	100.00
3036	-6485	-3606	-3658	-6550	MG	0.00	0.00	100.00
3036	-6550	-3658	-3591	-6622	MG	0.00	0.00	100.00
3036	-6672	-3537	-3699	-6750	MG	0.00	0.00	100.00
3036	-6622	-3591	-3537	-6672	MG	0.00	0.00	100.00
3038	-4459	-4711	-5284	-5284	MG	0.00	0.00	100.00
3039	-6438	-3812	-3859	-6505	MG	0.00	0.00	100.00
3039	-6222	-3765	-3812	-6438	MG	0.00	0.00	100.00
3041	-4950	-4223	-5065	-5065	MG	0.00	0.00	100.00
3052	-4446	-4020	-5048	-5049	MG	0.00	0.00	100.00
3060	-4252	-3608	-7140	-7140	MG	0.00	0.00	100.00
3061	-5285	-4712	-4460	-4460	MG	0.00	0.00	100.00
3062	-4224	-5066	-4951	-4951	MG	0.00	0.00	100.00
3106	-4000	-3999	-6106	-6380	MG	0.00	0.00	100.00
3107	-4003	-4002	-6382	-6107	MG	0.00	0.00	100.00
3119	-4445	-5038	-5039	-5039	MG	0.00	0.00	100.00
3120	-4935	-5432	-5433	-4281	MG	0.00	0.00	100.00
3121	-6244	-3696	-3655	-6243	MG	0.00	0.00	100.00
3129	-7297	-4167	-4221	-7347	MG	0.00	0.00	100.00
3129	-6915	-3904	-3963	-6998	MG	0.00	0.00	100.00
3129	-6833	-3842	-3904	-6915	MG	0.00	0.00	100.00
3129	-7463	-4164	-4104	-7499	MG	0.00	0.00	100.00
3129	-7200	-3987	-4124	-7263	MG	0.00	0.00	100.00
3129	-6998	-3963	-3887	-7057	MG	0.00	0.00	100.00
3129	-7499	-4104	-4253	-7578	MG	0.00	0.00	100.00
3129	-7263	-4124	-4167	-7297	MG	0.00	0.00	100.00
3129	-7347	-4221	-4164	-7463	MG	0.00	0.00	100.00
3129	-6748	-3698	-3842	-6833	MG	0.00	0.00	100.00
3129	-7057	-3887	-3825	-7137	MG	0.00	0.00	100.00
3129	-7137	-3825	-3987	-7200	MG	0.00	0.00	100.00
3130	-6501	-3857	-3908	-6597	MG	0.00	0.00	100.00
3130	-6495	-3950	-4000	-6380	MG	0.00	0.00	100.00
3130	-6597	-3908	-3950	-6495	MG	0.00	0.00	100.00
3131	-5116	-5040	-5039	-5115	MG	0.00	0.00	100.00
3131	-5671	-5602	-5601	-5670	MG	0.00	0.00	100.00
3131	-5663	-5594	-5593	-5662	MG	0.00	0.00	100.00
3131	-5435	-5373	-5372	-5434	MG	0.00	0.00	100.00
3131	-5741	-5732	-5797	-5798	MG	0.00	0.00	100.00
3131	-5119	2901	-5042	-5118	MG	0.00	0.00	100.00
3131	-5129	-5051	-5050	-5128	MG	0.00	0.00	100.00
3131	-5200	-5115	-5114	-5199	MG	0.00	0.00	100.00
3131	-5325	-5274	-5273	-5324	MG	0.00	0.00	100.00
3131	-5795	-5731	-5730	-5794	MG	0.00	0.00	100.00
3131	-5594	-5499	-5498	-5593	MG	0.00	0.00	100.00
3131	-5592	-5497	-5496	-5591	MG	0.00	0.00	100.00
3131	-5204	-5119	-5118	-5203	MG	0.00	0.00	100.00
3131	-5277	-5212	-5211	-5276	MG	0.00	0.00	100.00
3131	-5591	-5496	-5495	-5590	MG	0.00	0.00	100.00
3131	-5203	-5118	-5117	-5202	MG	0.00	0.00	100.00
3131	-5805	-5744	-5736	-5804	MG	0.00	0.00	100.00
3131	-5735	-5670	-5669	-5734	MG	0.00	0.00	100.00
3131	-5505	-5442	-5441	-5504	MG	0.00	0.00	100.00
3131	-5432	-5370	-5369	-5431	MG	0.00	0.00	100.00
3131	-5445	-5383	-5382	-5444	MG	0.00	0.00	100.00
3131	-5744	-5673	-5672	-5736	MG	0.00	0.00	100.00
3131	-5120	-5043	2901	-5119	MG	0.00	0.00	100.00
3131	-5379	-5325	-5324	-5378	MG	0.00	0.00	100.00
3131	-5439	-5438	-5501	-5502	MG	0.00	0.00	100.00

3131	-5731	-5663	-5662	-5730	MG	0.00	0.00	100.00
3131	-5508	-5445	-5444	-5507	MG	0.00	0.00	100.00
3131	-5728	-5660	-5659	-5727	MG	0.00	0.00	100.00
3131	-5660	-5591	-5590	-5659	MG	0.00	0.00	100.00
3131	-5496	-5433	-5432	-5495	MG	0.00	0.00	100.00
3131	-5665	-5664	-5740	-5732	MG	0.00	0.00	100.00
3131	-5802	-5735	-5734	-5801	MG	0.00	0.00	100.00
3131	-5730	-5662	-5661	-5729	MG	0.00	0.00	100.00
3131	-5370	-5316	-5315	-5369	MG	0.00	0.00	100.00
3131	-5214	-5129	-5128	-5213	MG	0.00	0.00	100.00
3131	-5803	-5743	-5735	-5802	MG	0.00	0.00	100.00
3131	-5743	-5671	-5670	-5735	MG	0.00	0.00	100.00
3131	-5210	-5125	-5124	-5209	MG	0.00	0.00	100.00
3131	-5128	-5050	-5049	-5127	MG	0.00	0.00	100.00
3131	-5801	-5734	-5742	-5800	MG	0.00	0.00	100.00
3131	-5661	-5592	-5591	-5660	MG	0.00	0.00	100.00
3131	-5734	-5669	-5668	-5742	MG	0.00	0.00	100.00
3131	-5320	-5269	-5268	-5319	MG	0.00	0.00	100.00
3131	-5269	-5204	-5203	-5268	MG	0.00	0.00	100.00
3131	-5497	-5434	-5433	-5496	MG	0.00	0.00	100.00
3131	-5201	-5116	-5115	-5200	MG	0.00	0.00	100.00
3131	-5206	-5205	-5270	-5271	MG	0.00	0.00	100.00
3131	-5207	-5206	-5271	-5272	MG	0.00	0.00	100.00
3131	-5327	-5276	-5275	-5326	MG	0.00	0.00	100.00
3131	-5436	-5374	-5373	-5435	MG	0.00	0.00	100.00
3131	-5276	-5211	-5210	-5275	MG	0.00	0.00	100.00
3131	-5727	-5659	-5658	-5726	MG	0.00	0.00	100.00
3131	-5590	-5495	-5494	-5589	MG	0.00	0.00	100.00
3131	-5045	-5044	-5121	-5122	MG	0.00	0.00	100.00
3131	-5315	-5264	-5263	-5314	MG	0.00	0.00	100.00
3131	-5275	-5210	-5209	-5274	MG	0.00	0.00	100.00
3131	-5446	-5384	-5383	-5445	MG	0.00	0.00	100.00
3131	-5125	-5047	-5046	-5124	MG	0.00	0.00	100.00
3131	-5664	-5595	-5594	-5663	MG	0.00	0.00	100.00
3131	-5437	-5375	-5374	-5436	MG	0.00	0.00	100.00
3131	-5500	-5437	-5436	-5499	MG	0.00	0.00	100.00
3131	-5597	-5596	-5665	-5666	MG	0.00	0.00	100.00
3131	-5440	-5378	-5377	-5439	MG	0.00	0.00	100.00
3131	-5274	-5209	-5208	-5273	MG	0.00	0.00	100.00
3131	-5499	-5436	-5435	-5498	MG	0.00	0.00	100.00
3131	-5265	-5200	-5199	-5264	MG	0.00	0.00	100.00
3131	-5316	-5265	-5264	-5315	MG	0.00	0.00	100.00
3131	-5794	-5730	-5729	-5793	MG	0.00	0.00	100.00
3131	-5273	-5208	-5207	-5272	MG	0.00	0.00	100.00
3131	-5279	-5214	-5213	-5278	MG	0.00	0.00	100.00
3131	-5670	-5601	-5600	-5669	MG	0.00	0.00	100.00
3131	-5601	-5506	-5505	-5600	MG	0.00	0.00	100.00
3131	-5278	-5213	-5212	-5277	MG	0.00	0.00	100.00
3131	-5369	-5315	-5314	-5368	MG	0.00	0.00	100.00
3131	-5213	-5128	-5127	-5212	MG	0.00	0.00	100.00
3131	-5270	-5205	-5204	-5269	MG	0.00	0.00	100.00
3131	-5264	-5199	-5198	-5263	MG	0.00	0.00	100.00
3131	-5328	-5277	-5276	-5327	MG	0.00	0.00	100.00
3131	-5382	-5328	-5327	-5381	MG	0.00	0.00	100.00
3131	-5377	-5376	-5438	-5439	MG	0.00	0.00	100.00
3131	-5792	-5728	-5727	-5791	MG	0.00	0.00	100.00
3131	-5212	-5127	-5126	-5211	MG	0.00	0.00	100.00
3131	-5127	-5049	-5048	-5126	MG	0.00	0.00	100.00
3131	-5443	-5381	-5380	-5442	MG	0.00	0.00	100.00
3131	-5373	-5319	-5318	-5372	MG	0.00	0.00	100.00
3131	-5791	-5727	-5726	-5790	MG	0.00	0.00	100.00
3131	-5268	-5203	-5202	-5267	MG	0.00	0.00	100.00
3131	-5501	-5500	-5595	-5596	MG	0.00	0.00	100.00
3131	-5380	-5326	-5325	-5379	MG	0.00	0.00	100.00
3131	-5495	-5432	-5431	-5494	MG	0.00	0.00	100.00
3131	-5790	-5726	-5725	-5789	MG	0.00	0.00	100.00
3131	-5796	-5740	-5731	-5795	MG	0.00	0.00	100.00
3131	-5726	-5658	-5657	-5725	MG	0.00	0.00	100.00
3131	-5595	-5500	-5499	-5594	MG	0.00	0.00	100.00
3131	-5371	-5317	-5316	-5370	MG	0.00	0.00	100.00
3131	-5494	-5431	-5430	-5493	MG	0.00	0.00	100.00
3131	-5441	-5379	-5378	-5440	MG	0.00	0.00	100.00
3131	-5266	-5201	-5200	-5265	MG	0.00	0.00	100.00
3131	-5666	-5665	-5732	-5741	MG	0.00	0.00	100.00
3131	-5272	-5271	-5322	-5323	MG	0.00	0.00	100.00
3131	-5324	-5273	-5272	-5323	MG	0.00	0.00	100.00
3131	-5507	-5444	-5443	-5506	MG	0.00	0.00	100.00
3131	-5330	-5279	-5278	-5329	MG	0.00	0.00	100.00
3131	-5124	-5046	2902	-5123	MG	0.00	0.00	100.00

3131	-5502	-5501	-5596	-5597	MG	0.00	0.00	100.00
3131	-5732	-5740	-5796	-5797	MG	0.00	0.00	100.00
3131	-5383	-5329	-5328	-5382	MG	0.00	0.00	100.00
3131	-5329	-5278	-5277	-5328	MG	0.00	0.00	100.00
3131	-5205	-5120	-5119	-5204	MG	0.00	0.00	100.00
3131	-5506	-5443	-5442	-5505	MG	0.00	0.00	100.00
3131	-5321	-5270	-5269	-5320	MG	0.00	0.00	100.00
3131	-5374	-5320	-5319	-5373	MG	0.00	0.00	100.00
3131	-5199	-5114	-5113	-5198	MG	0.00	0.00	100.00
3131	-5669	-5600	-5599	-5668	MG	0.00	0.00	100.00
3131	-5376	-5375	-5437	-5438	MG	0.00	0.00	100.00
3131	-5600	-5505	-5504	-5599	MG	0.00	0.00	100.00
3131	-5326	-5275	-5274	-5325	MG	0.00	0.00	100.00
3131	-5271	-5270	-5321	-5322	MG	0.00	0.00	100.00
3131	-5599	-5504	-5503	-5598	MG	0.00	0.00	100.00
3131	-5381	-5327	-5326	-5380	MG	0.00	0.00	100.00
3131	-5211	-5126	-5125	-5210	MG	0.00	0.00	100.00
3131	-5659	-5590	-5589	-5658	MG	0.00	0.00	100.00
3131	-5673	-5604	-5603	-5672	MG	0.00	0.00	100.00
3131	-5442	-5380	-5379	-5441	MG	0.00	0.00	100.00
3131	-5317	-5266	-5265	-5316	MG	0.00	0.00	100.00
3131	-5503	-5440	-5439	-5502	MG	0.00	0.00	100.00
3131	-5509	-5446	-5445	-5508	MG	0.00	0.00	100.00
3131	-5740	-5664	-5663	-5731	MG	0.00	0.00	100.00
3131	-5202	-5117	-5116	-5201	MG	0.00	0.00	100.00
3131	-5589	-5494	-5493	-5588	MG	0.00	0.00	100.00
3131	-5433	-5371	-5370	-5432	MG	0.00	0.00	100.00
3131	-5603	-5508	-5507	-5602	MG	0.00	0.00	100.00
3131	-5596	-5595	-5664	-5665	MG	0.00	0.00	100.00
3131	-5208	-5123	-5122	-5207	MG	0.00	0.00	100.00
3131	-5602	-5507	-5506	-5601	MG	0.00	0.00	100.00
3131	-5323	-5322	-5376	-5377	MG	0.00	0.00	100.00
3131	-5378	-5324	-5323	-5377	MG	0.00	0.00	100.00
3131	-5319	-5268	-5267	-5318	MG	0.00	0.00	100.00
3131	-5742	-5668	-5667	-5733	MG	0.00	0.00	100.00
3131	-5504	-5441	-5440	-5503	MG	0.00	0.00	100.00
3131	-5114	-5038	-5037	-5113	MG	0.00	0.00	100.00
3131	-5672	-5603	-5602	-5671	MG	0.00	0.00	100.00
3131	-5431	-5369	-5368	-5430	MG	0.00	0.00	100.00
3131	-5729	-5661	-5660	-5728	MG	0.00	0.00	100.00
3131	-5793	-5729	-5728	-5792	MG	0.00	0.00	100.00
3131	-5438	-5437	-5500	-5501	MG	0.00	0.00	100.00
3131	-5267	-5202	-5201	-5266	MG	0.00	0.00	100.00
3131	-5658	-5589	-5588	-5657	MG	0.00	0.00	100.00
3131	-5209	-5124	-5123	-5208	MG	0.00	0.00	100.00
3131	-5126	-5048	-5047	-5125	MG	0.00	0.00	100.00
3131	-5118	-5042	-5041	-5117	MG	0.00	0.00	100.00
3131	-5372	-5318	-5317	-5371	MG	0.00	0.00	100.00
3131	-5122	-5121	-5206	-5207	MG	0.00	0.00	100.00
3131	-5121	-5120	-5205	-5206	MG	0.00	0.00	100.00
3131	-5668	-5599	-5598	-5667	MG	0.00	0.00	100.00
3131	-5604	-5509	-5508	-5603	MG	0.00	0.00	100.00
3131	-5598	-5503	-5502	-5597	MG	0.00	0.00	100.00
3131	-5322	-5321	-5375	-5376	MG	0.00	0.00	100.00
3131	-5117	-5041	-5040	-5116	MG	0.00	0.00	100.00
3131	-5115	-5039	-5038	-5114	MG	0.00	0.00	100.00
3131	-5733	-5667	-5666	-5741	MG	0.00	0.00	100.00
3131	-5804	-5736	-5743	-5803	MG	0.00	0.00	100.00
3131	-5318	-5267	-5266	-5317	MG	0.00	0.00	100.00
3131	-5044	-5043	-5120	-5121	MG	0.00	0.00	100.00
3131	-5667	-5598	-5597	-5666	MG	0.00	0.00	100.00
3131	-5498	-5435	-5434	-5497	MG	0.00	0.00	100.00
3131	-5593	-5498	-5497	-5592	MG	0.00	0.00	100.00
3131	-5736	-5672	-5671	-5743	MG	0.00	0.00	100.00
3131	-5384	-5330	-5329	-5383	MG	0.00	0.00	100.00
3131	-5662	-5593	-5592	-5661	MG	0.00	0.00	100.00
3131	-5444	-5382	-5381	-5443	MG	0.00	0.00	100.00
3131	-5375	-5321	-5320	-5374	MG	0.00	0.00	100.00
3131	-5434	-5372	-5371	-5433	MG	0.00	0.00	100.00
3131	-5800	-5742	-5733	-5799	MG	0.00	0.00	100.00
3131	-5799	-5733	-5741	-5798	MG	0.00	0.00	100.00
3131	-5123	2902	-5045	-5122	MG	0.00	0.00	100.00
3132	-6598	-3910	-3958	-6496	MG	0.00	0.00	100.00
3132	-6496	-3958	-4002	-6382	MG	0.00	0.00	100.00
3132	-6505	-3859	-3910	-6598	MG	0.00	0.00	100.00
3133	-7139	-3826	-3988	-7202	MG	0.00	0.00	100.00
3133	-7465	-4165	-4105	-7501	MG	0.00	0.00	100.00
3133	-6835	-3843	-3905	-6917	MG	0.00	0.00	100.00
3133	-6917	-3905	-3964	-7000	MG	0.00	0.00	100.00

3133	-7202	-3988	-4125	-7265	MG	0.00	0.00	100.00
3133	-6750	-3699	-3843	-6835	MG	0.00	0.00	100.00
3133	-7059	-3888	-3826	-7139	MG	0.00	0.00	100.00
3133	-7299	-4168	-4222	-7349	MG	0.00	0.00	100.00
3133	-7349	-4222	-4165	-7465	MG	0.00	0.00	100.00
3133	-7000	-3964	-3888	-7059	MG	0.00	0.00	100.00
3133	-7501	-4105	-4254	-7579	MG	0.00	0.00	100.00
3133	-7265	-4125	-4168	-7299	MG	0.00	0.00	100.00
3138	-5781	-4065	-4964	-4964	MG	0.00	0.00	100.00
3139	-5306	-3674	-6221	-6221	MG	0.00	0.00	100.00
3147	-5050	-4446	-5049	-5049	MG	0.00	0.00	100.00
3150	-4936	-4282	-5443	-5444	MG	0.00	0.00	100.00
3152	-3656	-3697	-6247	-6248	MG	0.00	0.00	100.00
3156	-5773	-4965	-4066	-4066	MG	0.00	0.00	100.00
3157	-3675	-5307	-6230	-6230	MG	0.00	0.00	100.00
3205	-5256	-4235	-7091	-7091	MG	0.00	0.00	100.00
3206	-4236	-5257	-7092	-7092	MG	0.00	0.00	100.00
3207	-4001	-4000	-6380	-6381	MG	0.00	0.00	100.00
3207	-4002	-4001	-6381	-6382	MG	0.00	0.00	100.00
3219	-4935	-5431	-5432	-5432	MG	0.00	0.00	100.00
3222	-5333	-5837	-5838	-4699	MG	0.00	0.00	100.00
3222	-5333	-5836	-5837	-5837	MG	0.00	0.00	100.00
3229	-6670	-3985	-3947	-6669	MG	0.00	0.00	100.00
3231	-7710	-4419	-4461	-7805	MG	0.00	0.00	100.00
3231	-7928	-4417	-4362	-7974	MG	0.00	0.00	100.00
3231	-7974	-4362	-4494	-8028	MG	0.00	0.00	100.00
3231	-7805	-4461	-4417	-7928	MG	0.00	0.00	100.00
3231	-7661	-4378	-4419	-7710	MG	0.00	0.00	100.00
3231	-7578	-4253	-4378	-7661	MG	0.00	0.00	100.00
3232	-3825	-3607	-7136	-7137	MG	0.00	0.00	100.00
3233	-7136	-4251	-4219	-7135	MG	0.00	0.00	100.00
3234	-5987	-5878	-5877	-5986	MG	0.00	0.00	100.00
3234	-5888	-5846	-5845	-5887	MG	0.00	0.00	100.00
3234	-6067	-6066	-6134	-6135	MG	0.00	0.00	100.00
3234	-6060	-5987	-5986	-6059	MG	0.00	0.00	100.00
3234	-6070	-5996	-5995	-6069	MG	0.00	0.00	100.00
3234	-6130	-6062	-6061	-6129	MG	0.00	0.00	100.00
3234	-5989	-5880	-5879	-5988	MG	0.00	0.00	100.00
3234	-6249	-6197	-6196	-6239	MG	0.00	0.00	100.00
3234	-6193	-6194	-6137	-6136	MG	0.00	0.00	100.00
3234	-6250	-6198	-6197	-6249	MG	0.00	0.00	100.00
3234	-6142	-6074	-6073	-6141	MG	0.00	0.00	100.00
3234	-6073	-5999	-5998	-6072	MG	0.00	0.00	100.00
3234	-5878	-5836	-5835	-5877	MG	0.00	0.00	100.00
3234	-6185	-6128	-6127	-6184	MG	0.00	0.00	100.00
3234	-5891	-5849	-5848	-5890	MG	0.00	0.00	100.00
3234	-6252	-6200	-6199	-6251	MG	0.00	0.00	100.00
3234	-6000	-5892	-5891	-5999	MG	0.00	0.00	100.00
3234	-5838	-5792	-5791	-5837	MG	0.00	0.00	100.00
3234	-6199	-6142	-6141	-6198	MG	0.00	0.00	100.00
3234	-6068	-6067	-6135	-6136	MG	0.00	0.00	100.00
3234	-5999	-5891	-5890	-5998	MG	0.00	0.00	100.00
3234	-6248	-6195	-6194	-6247	MG	0.00	0.00	100.00
3234	-6136	-6135	-6192	-6193	MG	0.00	0.00	100.00
3234	-6138	-6070	-6069	-6137	MG	0.00	0.00	100.00
3234	-6187	-6130	-6129	-6186	MG	0.00	0.00	100.00
3234	-6236	-6187	-6186	-6235	MG	0.00	0.00	100.00
3234	-5798	-5797	-5843	-5844	MG	0.00	0.00	100.00
3234	-5847	-5801	-5800	-5846	MG	0.00	0.00	100.00
3234	-6198	-6141	-6140	-6197	MG	0.00	0.00	100.00
3234	-6068	-6069	-5995	-6025	MG	0.00	0.00	100.00
3234	-6242	-6185	-6184	-6234	MG	0.00	0.00	100.00
3234	-6246	-6247	-6194	-6193	MG	0.00	0.00	100.00
3234	-5886	-5887	-5845	-5844	MG	0.00	0.00	100.00
3234	-6128	-6060	-6059	-6127	MG	0.00	0.00	100.00
3234	-6238	-6191	-6190	-6244	MG	0.00	0.00	100.00
3234	-6074	-6000	-5999	-6073	MG	0.00	0.00	100.00
3234	-5892	-5850	-5849	-5891	MG	0.00	0.00	100.00
3234	-5884	-5842	-5841	-5883	MG	0.00	0.00	100.00
3234	-5846	-5800	-5799	-5845	MG	0.00	0.00	100.00
3234	-5848	-5802	-5801	-5847	MG	0.00	0.00	100.00
3234	-5837	-5791	-5790	-5836	MG	0.00	0.00	100.00
3234	-5885	-5884	-5993	-5994	MG	0.00	0.00	100.00
3234	-5992	-5883	-5882	-5991	MG	0.00	0.00	100.00
3234	-6140	-6072	-6071	-6139	MG	0.00	0.00	100.00
3234	-5839	-5793	-5792	-5838	MG	0.00	0.00	100.00
3234	-6025	-5995	-5887	-5886	MG	0.00	0.00	100.00
3234	-5882	-5840	-5839	-5881	MG	0.00	0.00	100.00
3234	-5890	-5848	-5847	-5889	MG	0.00	0.00	100.00

3234	-5851	-5805	-5804	-5850	MG	0.00	0.00	100.00
3234	-6244	-6190	-6189	-6243	MG	0.00	0.00	100.00
3234	-6063	-5990	-5989	-6062	MG	0.00	0.00	100.00
3234	-5990	-5881	-5880	-5989	MG	0.00	0.00	100.00
3234	-6196	-6139	-6138	-6195	MG	0.00	0.00	100.00
3234	-5881	-5839	-5838	-5880	MG	0.00	0.00	100.00
3234	-5843	-5842	-5884	-5885	MG	0.00	0.00	100.00
3234	-5797	-5796	-5842	-5843	MG	0.00	0.00	100.00
3234	-5842	-5796	-5795	-5841	MG	0.00	0.00	100.00
3234	-6062	-5989	-5988	-6061	MG	0.00	0.00	100.00
3234	-5840	-5794	-5793	-5839	MG	0.00	0.00	100.00
3234	-5988	-5879	-5878	-5987	MG	0.00	0.00	100.00
3234	-5996	-5888	-5887	-5995	MG	0.00	0.00	100.00
3234	-5998	-5890	-5889	-5997	MG	0.00	0.00	100.00
3234	-6129	-6061	-6060	-6128	MG	0.00	0.00	100.00
3234	-5972	-5893	-5892	-6000	MG	0.00	0.00	100.00
3234	-5880	-5838	-5837	-5879	MG	0.00	0.00	100.00
3234	-6075	-5972	-6000	-6074	MG	0.00	0.00	100.00
3234	-5879	-5837	-5836	-5878	MG	0.00	0.00	100.00
3234	-5883	-5841	-5840	-5882	MG	0.00	0.00	100.00
3234	-6061	-5988	-5987	-6060	MG	0.00	0.00	100.00
3234	-6134	-6066	-6065	-6133	MG	0.00	0.00	100.00
3234	-6066	-5993	-5992	-6065	MG	0.00	0.00	100.00
3234	-5993	-5884	-5883	-5992	MG	0.00	0.00	100.00
3234	-5997	-5889	-5888	-5996	MG	0.00	0.00	100.00
3234	-6141	-6073	-6072	-6140	MG	0.00	0.00	100.00
3234	-6133	-6065	-6064	-6132	MG	0.00	0.00	100.00
3234	-6239	-6196	-6195	-6248	MG	0.00	0.00	100.00
3234	-6188	-6131	-6130	-6187	MG	0.00	0.00	100.00
3234	-6065	-5992	-5991	-6064	MG	0.00	0.00	100.00
3234	-5845	-5799	-5798	-5844	MG	0.00	0.00	100.00
3234	-6064	-5991	-5990	-6063	MG	0.00	0.00	100.00
3234	-5994	-5993	-6066	-6067	MG	0.00	0.00	100.00
3234	-5991	-5882	-5881	-5990	MG	0.00	0.00	100.00
3234	-5841	-5795	-5794	-5840	MG	0.00	0.00	100.00
3234	-6195	-6138	-6137	-6194	MG	0.00	0.00	100.00
3234	-5886	-5885	-5994	-6025	MG	0.00	0.00	100.00
3234	-6131	-6063	-6062	-6130	MG	0.00	0.00	100.00
3234	-6237	-6188	-6187	-6236	MG	0.00	0.00	100.00
3234	-6192	-6191	-6238	-6245	MG	0.00	0.00	100.00
3234	-6071	-5997	-5996	-6070	MG	0.00	0.00	100.00
3234	-6193	-6192	-6245	-6246	MG	0.00	0.00	100.00
3234	-5889	-5847	-5846	-5888	MG	0.00	0.00	100.00
3234	-5836	-5790	-5789	-5835	MG	0.00	0.00	100.00
3234	-6251	-6199	-6198	-6250	MG	0.00	0.00	100.00
3234	-5893	-5851	-5850	-5892	MG	0.00	0.00	100.00
3234	-6200	-6143	-6142	-6199	MG	0.00	0.00	100.00
3234	-5844	-5843	-5885	-5886	MG	0.00	0.00	100.00
3234	-6186	-6129	-6128	-6185	MG	0.00	0.00	100.00
3234	-6136	-6137	-6069	-6068	MG	0.00	0.00	100.00
3234	-6132	-6064	-6063	-6131	MG	0.00	0.00	100.00
3234	-5849	-5803	-5802	-5848	MG	0.00	0.00	100.00
3234	-6025	-5994	-6067	-6068	MG	0.00	0.00	100.00
3234	-6190	-6133	-6132	-6189	MG	0.00	0.00	100.00
3234	-6243	-6189	-6188	-6237	MG	0.00	0.00	100.00
3234	-5850	-5804	-5803	-5849	MG	0.00	0.00	100.00
3234	-6191	-6134	-6133	-6190	MG	0.00	0.00	100.00
3234	-6139	-6071	-6070	-6138	MG	0.00	0.00	100.00
3234	-6189	-6132	-6131	-6188	MG	0.00	0.00	100.00
3234	-6072	-5998	-5997	-6071	MG	0.00	0.00	100.00
3234	-6135	-6134	-6191	-6192	MG	0.00	0.00	100.00
3234	-6143	-6075	-6074	-6142	MG	0.00	0.00	100.00
3234	-6197	-6140	-6139	-6196	MG	0.00	0.00	100.00
3234	-6235	-6186	-6185	-6242	MG	0.00	0.00	100.00
3235	-7579	-4254	-4379	-7666	MG	0.00	0.00	100.00
3235	-7666	-4379	-4420	-7712	MG	0.00	0.00	100.00
3235	-7976	-4363	-4503	-8030	MG	0.00	0.00	100.00
3235	-7930	-4418	-4363	-7976	MG	0.00	0.00	100.00
3235	-7807	-4462	-4418	-7930	MG	0.00	0.00	100.00
3235	-7712	-4420	-4462	-7807	MG	0.00	0.00	100.00
3236	-4104	-3906	-7498	-7499	MG	0.00	0.00	100.00
3236	-3906	-4492	-7498	-7498	MG	0.00	0.00	100.00
3239	-4950	-5065	-5674	-5674	MG	0.00	0.00	100.00
3240	-4169	-5013	-7973	-7973	MG	0.00	0.00	100.00
3242	-5352	-4471	-5458	-5458	MG	0.00	0.00	100.00
3242	-5352	-5458	-6100	-6100	MG	0.00	0.00	100.00
3245	-5781	-4964	-5854	-5854	MG	0.00	0.00	100.00
3246	-6170	-4322	-5356	-5356	MG	0.00	0.00	100.00
3246	-6221	-3674	-4322	-6170	MG	0.00	0.00	100.00

3255	-5445	-4936	-5444	-5444	MG	0.00	0.00	100.00
3257	-5334	-4700	-5848	-5849	MG	0.00	0.00	100.00
3257	-5850	-5334	-5849	-5849	MG	0.00	0.00	100.00
3259	-3948	-3986	-6673	-6677	MG	0.00	0.00	100.00
3264	-4220	-4252	-7140	-7141	MG	0.00	0.00	100.00
3266	-3608	-3826	-7139	-7140	MG	0.00	0.00	100.00
3267	-4493	-3907	-7502	-7502	MG	0.00	0.00	100.00
3267	-3907	-4105	-7501	-7502	MG	0.00	0.00	100.00
3268	-5681	-5066	-4951	-4951	MG	0.00	0.00	100.00
3269	-5014	-4170	-7977	-7977	MG	0.00	0.00	100.00
3270	-4463	-5459	-5353	-5353	MG	0.00	0.00	100.00
3270	-6101	-5459	-5353	-5353	MG	0.00	0.00	100.00
3271	-4965	-5855	-5773	-5773	MG	0.00	0.00	100.00
3272	-4323	-3675	-6230	-6171	MG	0.00	0.00	100.00
3272	-6171	-5357	-4323	-4323	MG	0.00	0.00	100.00
3273	-6578	-4758	-5784	-5784	MG	0.00	0.00	100.00
3273	-5691	-3956	-6659	-6659	MG	0.00	0.00	100.00
3273	-6659	-3956	-4758	-6578	MG	0.00	0.00	100.00
3274	-4759	-3969	-6660	-6579	MG	0.00	0.00	100.00
3274	-6579	-5766	-4759	-4759	MG	0.00	0.00	100.00
3274	-3969	-5692	-6660	-6660	MG	0.00	0.00	100.00
3305	-5257	-6107	-7092	-7092	MG	0.00	0.00	100.00
3307	-6106	-5256	-7091	-7091	MG	0.00	0.00	100.00
3308	-7022	-6175	-5131	-5131	MG	0.00	0.00	100.00
3308	-5131	-4236	-7092	-7022	MG	0.00	0.00	100.00
3309	-7091	-4235	-5130	-7021	MG	0.00	0.00	100.00
3309	-7021	-5130	-6174	-6174	MG	0.00	0.00	100.00
3325	-5746	-6242	-6235	-6235	MG	0.00	0.00	100.00
3325	-5746	-6235	-6236	-5052	MG	0.00	0.00	100.00
3331	-6151	-6667	-6688	-5447	MG	0.00	0.00	100.00
3332	-8719	-5354	-5286	-8840	MG	0.00	0.00	100.00
3332	-8840	-5286	-5215	-8908	MG	0.00	0.00	100.00
3332	-8908	-5215	-5387	-8982	MG	0.00	0.00	100.00
3332	-8479	-5001	-5254	-8537	MG	0.00	0.00	100.00
3332	-8377	-4884	-4815	-8424	MG	0.00	0.00	100.00
3332	-8228	-4886	-4952	-8316	MG	0.00	0.00	100.00
3332	-8537	-5254	-5304	-8628	MG	0.00	0.00	100.00
3332	-8028	-4494	-4841	-8154	MG	0.00	0.00	100.00
3332	-8316	-4952	-4884	-8377	MG	0.00	0.00	100.00
3332	-8154	-4841	-4886	-8228	MG	0.00	0.00	100.00
3332	-8424	-4815	-5001	-8479	MG	0.00	0.00	100.00
3332	-8628	-5304	-5354	-8719	MG	0.00	0.00	100.00
3333	-6304	-6303	-6371	-6372	MG	0.00	0.00	100.00
3333	-6999	-6998	-7057	-7058	MG	0.00	0.00	100.00
3333	-6917	-6916	-6999	-7000	MG	0.00	0.00	100.00
3333	-6378	-6310	-6309	-6377	MG	0.00	0.00	100.00
3333	-6828	-6743	-6742	-6827	MG	0.00	0.00	100.00
3333	-6301	-6244	-6243	-6300	MG	0.00	0.00	100.00
3333	-6303	-6302	-6370	-6371	MG	0.00	0.00	100.00
3333	-6916	-6915	-6998	-6999	MG	0.00	0.00	100.00
3333	-7061	-7002	-7001	-7060	MG	0.00	0.00	100.00
3333	-6833	-6748	-6747	-6832	MG	0.00	0.00	100.00
3333	-7141	-7061	-7060	-7140	MG	0.00	0.00	100.00
3333	-6834	-6833	-6915	-6916	MG	0.00	0.00	100.00
3333	-6374	-6306	-6305	-6373	MG	0.00	0.00	100.00
3333	-6624	-6539	-6551	-6623	MG	0.00	0.00	100.00
3333	-6994	-6911	-6910	-6993	MG	0.00	0.00	100.00
3333	-7140	-7060	-7059	-7139	MG	0.00	0.00	100.00
3333	-6993	-6910	-6909	-6992	MG	0.00	0.00	100.00
3333	-6379	-6311	-6310	-6378	MG	0.00	0.00	100.00
3333	-6842	-6757	-6756	-6841	MG	0.00	0.00	100.00
3333	-6364	-6296	-6295	-6363	MG	0.00	0.00	100.00
3333	-7062	-7003	-7002	-7061	MG	0.00	0.00	100.00
3333	-7003	-6920	-6919	-7002	MG	0.00	0.00	100.00
3333	-6536	-6477	-6476	-6535	MG	0.00	0.00	100.00
3333	-6484	-6483	-6548	-6549	MG	0.00	0.00	100.00
3333	-7057	-6998	-6997	-7056	MG	0.00	0.00	100.00
3333	-6302	-6238	-6244	-6301	MG	0.00	0.00	100.00
3333	-6547	-6482	-6481	-6538	MG	0.00	0.00	100.00
3333	-6369	-6301	-6300	-6368	MG	0.00	0.00	100.00
3333	-6371	-6370	-6483	-6484	MG	0.00	0.00	100.00
3333	-6485	-6484	-6549	-6550	MG	0.00	0.00	100.00
3333	-7133	-7053	-7052	-7132	MG	0.00	0.00	100.00
3333	-7000	-6999	-7058	-7059	MG	0.00	0.00	100.00
3333	-6492	-6379	-6378	-6491	MG	0.00	0.00	100.00
3333	-6368	-6300	-6299	-6367	MG	0.00	0.00	100.00
3333	-7132	-7052	-7051	-7131	MG	0.00	0.00	100.00
3333	-7136	-7056	-7055	-7135	MG	0.00	0.00	100.00
3333	-6308	-6249	-6239	-6307	MG	0.00	0.00	100.00

3333	-6678	-6625	-6624	-6677	MG	0.00	0.00	100.00
3333	-6625	-6552	-6539	-6624	MG	0.00	0.00	100.00
3333	-6671	-6689	-6748	-6749	MG	0.00	0.00	100.00
3333	-6677	-6624	-6623	-6673	MG	0.00	0.00	100.00
3333	-7146	-7066	-7065	-7145	MG	0.00	0.00	100.00
3333	-7051	-6992	-6991	-7050	MG	0.00	0.00	100.00
3333	-6299	-6237	-6236	-6298	MG	0.00	0.00	100.00
3333	-6306	-6248	-6247	-6305	MG	0.00	0.00	100.00
3333	-6748	-6689	-6670	-6747	MG	0.00	0.00	100.00
3333	-6487	-6374	-6373	-6486	MG	0.00	0.00	100.00
3333	-7056	-6997	-6996	-7055	MG	0.00	0.00	100.00
3333	-6629	-6556	-6555	-6628	MG	0.00	0.00	100.00
3333	-6832	-6747	-6746	-6831	MG	0.00	0.00	100.00
3333	-7143	-7063	-7062	-7142	MG	0.00	0.00	100.00
3333	-7055	-6996	-6995	-7054	MG	0.00	0.00	100.00
3333	-6901	-6842	-6841	-6923	MG	0.00	0.00	100.00
3333	-6297	-6235	-6242	-6296	MG	0.00	0.00	100.00
3333	-6614	-6536	-6535	-6613	MG	0.00	0.00	100.00
3333	-6754	-6690	-6678	-6753	MG	0.00	0.00	100.00
3333	-6477	-6364	-6363	-6476	MG	0.00	0.00	100.00
3333	-6375	-6307	-6306	-6374	MG	0.00	0.00	100.00
3333	-6998	-6915	-6914	-6997	MG	0.00	0.00	100.00
3333	-6619	-6547	-6538	-6618	MG	0.00	0.00	100.00
3333	-6995	-6912	-6911	-6994	MG	0.00	0.00	100.00
3333	-6246	-6245	-6303	-6304	MG	0.00	0.00	100.00
3333	-6830	-6745	-6744	-6829	MG	0.00	0.00	100.00
3333	-6482	-6369	-6368	-6481	MG	0.00	0.00	100.00
3333	-7053	-6994	-6993	-7052	MG	0.00	0.00	100.00
3333	-6377	-6309	-6308	-6376	MG	0.00	0.00	100.00
3333	-6538	-6481	-6480	-6546	MG	0.00	0.00	100.00
3333	-6835	-6834	-6916	-6917	MG	0.00	0.00	100.00
3333	-6829	-6744	-6743	-6828	MG	0.00	0.00	100.00
3333	-6481	-6368	-6367	-6480	MG	0.00	0.00	100.00
3333	-7007	-6901	-6923	-7006	MG	0.00	0.00	100.00
3333	-6300	-6243	-6237	-6299	MG	0.00	0.00	100.00
3333	-6668	-6617	-6616	-6668	MG	0.00	0.00	100.00
3333	-6757	-6693	-6692	-6756	MG	0.00	0.00	100.00
3333	-6546	-6480	-6479	-6537	MG	0.00	0.00	100.00
3333	-6307	-6239	-6248	-6306	MG	0.00	0.00	100.00
3333	-6751	-6673	-6672	-6750	MG	0.00	0.00	100.00
3333	-7131	-7051	-7050	-7130	MG	0.00	0.00	100.00
3333	-6915	-6833	-6832	-6914	MG	0.00	0.00	100.00
3333	-6537	-6479	-6478	-6545	MG	0.00	0.00	100.00
3333	-7059	-7058	-7138	-7139	MG	0.00	0.00	100.00
3333	-6742	-6687	-6666	-6741	MG	0.00	0.00	100.00
3333	-6997	-6914	-6913	-6996	MG	0.00	0.00	100.00
3333	-6922	-6840	-6839	-6921	MG	0.00	0.00	100.00
3333	-6556	-6492	-6491	-6555	MG	0.00	0.00	100.00
3333	-6840	-6755	-6754	-6839	MG	0.00	0.00	100.00
3333	-6545	-6478	-6477	-6536	MG	0.00	0.00	100.00
3333	-6311	-6252	-6251	-6310	MG	0.00	0.00	100.00
3333	-6365	-6297	-6296	-6364	MG	0.00	0.00	100.00
3333	-6921	-6839	-6838	-6920	MG	0.00	0.00	100.00
3333	-6839	-6754	-6753	-6838	MG	0.00	0.00	100.00
3333	-6491	-6378	-6377	-6490	MG	0.00	0.00	100.00
3333	-7142	-7062	-7061	-7141	MG	0.00	0.00	100.00
3333	-7134	-7054	-7053	-7133	MG	0.00	0.00	100.00
3333	-6310	-6251	-6250	-6309	MG	0.00	0.00	100.00
3333	-6912	-6830	-6829	-6911	MG	0.00	0.00	100.00
3333	-6490	-6377	-6376	-6489	MG	0.00	0.00	100.00
3333	-6753	-6678	-6677	-6752	MG	0.00	0.00	100.00
3333	-6621	-6620	-6689	-6671	MG	0.00	0.00	100.00
3333	-6549	-6548	-6620	-6621	MG	0.00	0.00	100.00
3333	-6673	-6623	-6622	-6672	MG	0.00	0.00	100.00
3333	-6618	-6538	-6546	-6617	MG	0.00	0.00	100.00
3333	-6670	-6619	-6618	-6669	MG	0.00	0.00	100.00
3333	-6752	-6677	-6673	-6751	MG	0.00	0.00	100.00
3333	-7001	-6918	-6917	-7000	MG	0.00	0.00	100.00
3333	-6376	-6308	-6307	-6375	MG	0.00	0.00	100.00
3333	-6372	-6371	-6484	-6485	MG	0.00	0.00	100.00
3333	-6550	-6549	-6621	-6622	MG	0.00	0.00	100.00
3333	-6552	-6488	-6487	-6539	MG	0.00	0.00	100.00
3333	-6488	-6375	-6374	-6487	MG	0.00	0.00	100.00
3333	-6480	-6367	-6366	-6479	MG	0.00	0.00	100.00
3333	-7145	-7065	-7064	-7144	MG	0.00	0.00	100.00
3333	-6367	-6299	-6298	-6366	MG	0.00	0.00	100.00
3333	-6992	-6909	-6900	-6991	MG	0.00	0.00	100.00
3333	-6616	-6537	-6545	-6615	MG	0.00	0.00	100.00
3333	-6539	-6487	-6486	-6551	MG	0.00	0.00	100.00

3333	-6827	-6742	-6741	-6826	MG	0.00	0.00	100.00
3333	-7058	-7057	-7137	-7138	MG	0.00	0.00	100.00
3333	-6914	-6832	-6831	-6913	MG	0.00	0.00	100.00
3333	-6623	-6551	-6550	-6622	MG	0.00	0.00	100.00
3333	-7135	-7055	-7054	-7134	MG	0.00	0.00	100.00
3333	-6551	-6486	-6485	-6550	MG	0.00	0.00	100.00
3333	-6373	-6305	-6304	-6372	MG	0.00	0.00	100.00
3333	-6996	-6913	-6912	-6995	MG	0.00	0.00	100.00
3333	-6913	-6831	-6830	-6912	MG	0.00	0.00	100.00
3333	-7137	-7057	-7056	-7136	MG	0.00	0.00	100.00
3333	-6548	-6483	-6482	-6547	MG	0.00	0.00	100.00
3333	-6620	-6548	-6547	-6619	MG	0.00	0.00	100.00
3333	-6370	-6302	-6301	-6369	MG	0.00	0.00	100.00
3333	-7054	-6995	-6994	-7053	MG	0.00	0.00	100.00
3333	-6296	-6242	-6234	-6295	MG	0.00	0.00	100.00
3333	-6622	-6621	-6671	-6672	MG	0.00	0.00	100.00
3333	-6745	-6668	-6688	-6744	MG	0.00	0.00	100.00
3333	-6838	-6753	-6752	-6837	MG	0.00	0.00	100.00
3333	-6627	-6554	-6553	-6626	MG	0.00	0.00	100.00
3333	-6690	-6626	-6625	-6678	MG	0.00	0.00	100.00
3333	-6911	-6829	-6828	-6910	MG	0.00	0.00	100.00
3333	-6626	-6553	-6552	-6625	MG	0.00	0.00	100.00
3333	-6672	-6671	-6749	-6750	MG	0.00	0.00	100.00
3333	-7066	-7007	-7006	-7065	MG	0.00	0.00	100.00
3333	-7052	-6993	-6992	-7051	MG	0.00	0.00	100.00
3333	-6489	-6376	-6375	-6488	MG	0.00	0.00	100.00
3333	-6910	-6828	-6827	-6909	MG	0.00	0.00	100.00
3333	-6617	-6546	-6537	-6616	MG	0.00	0.00	100.00
3333	-6687	-6614	-6613	-6666	MG	0.00	0.00	100.00
3333	-6746	-6669	-6668	-6745	MG	0.00	0.00	100.00
3333	-7065	-7006	-7005	-7064	MG	0.00	0.00	100.00
3333	-6743	-6667	-6668	-6742	MG	0.00	0.00	100.00
3333	-6923	-6841	-6840	-6922	MG	0.00	0.00	100.00
3333	-7144	-7064	-7063	-7143	MG	0.00	0.00	100.00
3333	-6756	-6692	-6691	-6755	MG	0.00	0.00	100.00
3333	-6841	-6756	-6755	-6840	MG	0.00	0.00	100.00
3333	-7005	-6922	-6921	-7004	MG	0.00	0.00	100.00
3333	-6298	-6236	-6235	-6297	MG	0.00	0.00	100.00
3333	-6366	-6298	-6297	-6365	MG	0.00	0.00	100.00
3333	-6755	-6691	-6690	-6754	MG	0.00	0.00	100.00
3333	-6615	-6545	-6536	-6614	MG	0.00	0.00	100.00
3333	-7063	-7004	-7003	-7062	MG	0.00	0.00	100.00
3333	-6692	-6628	-6627	-6691	MG	0.00	0.00	100.00
3333	-6628	-6555	-6554	-6627	MG	0.00	0.00	100.00
3333	-6555	-6491	-6490	-6554	MG	0.00	0.00	100.00
3333	-6750	-6749	-6834	-6835	MG	0.00	0.00	100.00
3333	-6831	-6746	-6745	-6830	MG	0.00	0.00	100.00
3333	-6483	-6370	-6369	-6482	MG	0.00	0.00	100.00
3333	-6245	-6238	-6302	-6303	MG	0.00	0.00	100.00
3333	-6693	-6629	-6628	-6692	MG	0.00	0.00	100.00
3333	-6554	-6490	-6489	-6553	MG	0.00	0.00	100.00
3333	-6691	-6627	-6626	-6690	MG	0.00	0.00	100.00
3333	-6688	-6616	-6615	-6667	MG	0.00	0.00	100.00
3333	-6836	-6751	-6750	-6835	MG	0.00	0.00	100.00
3333	-6919	-6837	-6836	-6918	MG	0.00	0.00	100.00
3333	-6669	-6618	-6617	-6668	MG	0.00	0.00	100.00
3333	-6749	-6748	-6833	-6834	MG	0.00	0.00	100.00
3333	-6747	-6670	-6669	-6746	MG	0.00	0.00	100.00
3333	-7060	-7001	-7000	-7059	MG	0.00	0.00	100.00
3333	-6305	-6247	-6246	-6304	MG	0.00	0.00	100.00
3333	-6918	-6836	-6835	-6917	MG	0.00	0.00	100.00
3333	-6689	-6620	-6619	-6670	MG	0.00	0.00	100.00
3333	-6478	-6365	-6364	-6477	MG	0.00	0.00	100.00
3333	-6479	-6366	-6365	-6478	MG	0.00	0.00	100.00
3333	-7002	-6919	-6918	-7001	MG	0.00	0.00	100.00
3333	-7006	-6923	-6922	-7005	MG	0.00	0.00	100.00
3333	-6667	-6615	-6614	-6668	MG	0.00	0.00	100.00
3333	-6909	-6827	-6826	-6908	MG	0.00	0.00	100.00
3333	-6920	-6838	-6837	-6919	MG	0.00	0.00	100.00
3333	-6553	-6489	-6488	-6552	MG	0.00	0.00	100.00
3333	-7004	-6921	-6920	-7003	MG	0.00	0.00	100.00
3333	-6486	-6373	-6372	-6485	MG	0.00	0.00	100.00
3333	-6744	-6688	-6667	-6743	MG	0.00	0.00	100.00
3333	-6837	-6752	-6751	-6836	MG	0.00	0.00	100.00
3333	-6309	-6250	-6249	-6308	MG	0.00	0.00	100.00
3333	-7064	-7005	-7004	-7063	MG	0.00	0.00	100.00
3334	-8230	-4887	-4953	-8318	MG	0.00	0.00	100.00
3334	-8481	-5002	-5255	-8539	MG	0.00	0.00	100.00
3334	-8318	-4953	-4885	-8379	MG	0.00	0.00	100.00

3334	-8030	-4503	-4842	-8156	MG	0.00	0.00	100.00
3334	-8721	-5355	-5287	-8841	MG	0.00	0.00	100.00
3334	-8156	-4842	-4887	-8230	MG	0.00	0.00	100.00
3334	-8379	-4885	-4816	-8426	MG	0.00	0.00	100.00
3334	-8426	-4816	-5002	-8481	MG	0.00	0.00	100.00
3334	-8841	-5287	-5216	-8910	MG	0.00	0.00	100.00
3334	-8629	-5305	-5355	-8721	MG	0.00	0.00	100.00
3334	-8910	-5216	-5398	-8984	MG	0.00	0.00	100.00
3334	-8539	-5255	-5305	-8629	MG	0.00	0.00	100.00
3335	-7498	-4492	-4459	-7497	MG	0.00	0.00	100.00
3339	-4362	-4169	-7973	-7974	MG	0.00	0.00	100.00
3342	-4421	-5418	-8423	-8423	MG	0.00	0.00	100.00
3345	-5781	-5854	-6493	-6493	MG	0.00	0.00	100.00
3346	-6170	-5356	-6259	-6259	MG	0.00	0.00	100.00
3364	-5747	-5053	-6249	-6250	MG	0.00	0.00	100.00
3364	-6251	-5747	-6250	-6250	MG	0.00	0.00	100.00
3372	-6152	-5448	-6690	-6691	MG	0.00	0.00	100.00
3380	-4460	-4493	-7502	-7503	MG	0.00	0.00	100.00
3384	-4170	-4363	-7976	-7977	MG	0.00	0.00	100.00
3386	-5397	-4422	-8427	-8427	MG	0.00	0.00	100.00
3388	-6494	-5855	-5773	-5773	MG	0.00	0.00	100.00
3390	-5357	-6269	-6171	-6171	MG	0.00	0.00	100.00
3424	-7021	-6174	-7156	-7156	MG	0.00	0.00	100.00
3426	-6175	-7157	-7022	-7022	MG	0.00	0.00	100.00
3435	-6151	-6687	-6667	-6667	MG	0.00	0.00	100.00
3436	-9550	-6104	-6172	-9598	MG	0.00	0.00	100.00
3436	-9073	-5620	-5701	-9149	MG	0.00	0.00	100.00
3436	-9440	-5808	-6036	-9479	MG	0.00	0.00	100.00
3436	-9727	-6001	-6206	-9855	MG	0.00	0.00	100.00
3436	-10194	-6495	-6380	-10249	MG	0.00	0.00	100.00
3436	-9968	-6437	-6501	-10034	MG	0.00	0.00	100.00
3436	-9374	-5605	-5808	-9440	MG	0.00	0.00	100.00
3436	-9207	-5783	-5689	-9283	MG	0.00	0.00	100.00
3436	-9283	-5689	-5605	-9374	MG	0.00	0.00	100.00
3436	-9479	-6036	-6104	-9550	MG	0.00	0.00	100.00
3436	-9149	-5701	-5783	-9207	MG	0.00	0.00	100.00
3436	-9598	-6172	-6102	-9640	MG	0.00	0.00	100.00
3436	-9640	-6102	-6001	-9727	MG	0.00	0.00	100.00
3436	-9855	-6206	-6437	-9968	MG	0.00	0.00	100.00
3436	-8982	-5387	-5620	-9073	MG	0.00	0.00	100.00
3436	-10034	-6501	-6597	-10126	MG	0.00	0.00	100.00
3436	-10126	-6597	-6495	-10194	MG	0.00	0.00	100.00
3437	-8229	-8228	-8316	-8317	MG	0.00	0.00	100.00
3437	-10199	-10133	-10132	-10198	MG	0.00	0.00	100.00
3437	-10257	-10201	-10200	-10256	MG	0.00	0.00	100.00
3437	-8427	-8380	-8379	-8426	MG	0.00	0.00	100.00
3437	-10122	-10030	-10029	-10121	MG	0.00	0.00	100.00
3437	-10038	-9946	-9962	-10037	MG	0.00	0.00	100.00
3437	-7974	-7928	-7927	-7973	MG	0.00	0.00	100.00
3437	-7502	-7466	-7465	-7501	MG	0.00	0.00	100.00
3437	-7971	-7925	-7924	-7970	MG	0.00	0.00	100.00
3437	-10129	-10037	-10036	-10128	MG	0.00	0.00	100.00
3437	-8911	-8808	-8841	-8910	MG	0.00	0.00	100.00
3437	-10255	-10199	-10198	-10254	MG	0.00	0.00	100.00
3437	-10041	-9972	-9971	-10040	MG	0.00	0.00	100.00
3437	-10036	-10035	-10127	-10128	MG	0.00	0.00	100.00
3437	-8424	-8377	-8376	-8423	MG	0.00	0.00	100.00
3437	3301	-10193	-10192	-10248	MG	0.00	0.00	100.00
3437	-9446	-9380	-9379	-9445	MG	0.00	0.00	100.00
3437	-10198	-10132	-10131	-10177	MG	0.00	0.00	100.00
3437	-10121	-10029	-10028	-10120	MG	0.00	0.00	100.00
3437	-7666	-7662	-7711	-7712	MG	0.00	0.00	100.00
3437	-10133	-10041	-10040	-10132	MG	0.00	0.00	100.00
3437	3302	-10176	-10196	-10251	MG	0.00	0.00	100.00
3437	-9972	-9849	-9848	-9971	MG	0.00	0.00	100.00
3437	-8984	-8983	-9095	-9074	MG	0.00	0.00	100.00
3437	-10132	-10040	-10039	-10131	MG	0.00	0.00	100.00
3437	-9968	-9855	-9854	-9945	MG	0.00	0.00	100.00
3437	-7269	-7206	-7205	-7268	MG	0.00	0.00	100.00
3437	-10030	-9944	-9943	-10029	MG	0.00	0.00	100.00
3437	-7571	-7497	-7496	-7576	MG	0.00	0.00	100.00
3437	-9557	-9505	-9493	-9556	MG	0.00	0.00	100.00
3437	-8230	-8229	-8317	-8318	MG	0.00	0.00	100.00
3437	-9447	-9381	-9380	-9446	MG	0.00	0.00	100.00
3437	-7349	-7348	-7464	-7465	MG	0.00	0.00	100.00
3437	-7257	-7194	-7193	-7256	MG	0.00	0.00	100.00
3437	-10175	-10121	-10120	-10189	MG	0.00	0.00	100.00
3437	-9493	-9446	-9445	-9488	MG	0.00	0.00	100.00
3437	-9600	-9599	-9641	-9642	MG	0.00	0.00	100.00

3437	-9962	-9857	-9847	-9970	MG	0.00	0.00	100.00
3437	-9857	-9741	-9740	-9847	MG	0.00	0.00	100.00
3437	-7348	-7347	-7463	-7464	MG	0.00	0.00	100.00
3437	-9974	-9863	-9840	-9973	MG	0.00	0.00	100.00
3437	-10127	-10126	-10194	-10195	MG	0.00	0.00	100.00
3437	-8983	-8982	-9073	-9095	MG	0.00	0.00	100.00
3437	-9445	-9379	-9378	-9444	MG	0.00	0.00	100.00
3437	-9742	-9644	-9643	-9741	MG	0.00	0.00	100.00
3437	-9644	-9602	-9601	-9643	MG	0.00	0.00	100.00
3437	-10195	-10194	-10249	-10250	MG	0.00	0.00	100.00
3437	-7468	-7352	-7351	-7467	MG	0.00	0.00	100.00
3437	-7265	-7264	-7298	-7299	MG	0.00	0.00	100.00
3437	-9444	-9378	-9377	-9443	MG	0.00	0.00	100.00
3437	-7801	-7705	-7697	-7800	MG	0.00	0.00	100.00
3437	-7705	-7655	-7654	-7697	MG	0.00	0.00	100.00
3437	-7459	-7343	-7342	-7458	MG	0.00	0.00	100.00
3437	-7501	-7500	-7572	-7579	MG	0.00	0.00	100.00
3437	-9727	-9640	-9639	-9739	MG	0.00	0.00	100.00
3437	-9648	-9606	-9605	-9647	MG	0.00	0.00	100.00
3437	-8420	-8373	-8372	-8419	MG	0.00	0.00	100.00
3437	-7472	-7356	-7355	-7471	MG	0.00	0.00	100.00
3437	-8917	-8809	-8827	-8916	MG	0.00	0.00	100.00
3437	-8433	-8386	-8385	-8432	MG	0.00	0.00	100.00
3437	-9373	-9282	-9281	-9372	MG	0.00	0.00	100.00
3437	-10246	-10190	-10175	-10245	MG	0.00	0.00	100.00
3437	-10134	-10042	-10041	-10133	MG	0.00	0.00	100.00
3437	-9747	-9649	-9648	-9746	MG	0.00	0.00	100.00
3437	-8372	-8311	-8310	-8371	MG	0.00	0.00	100.00
3437	-9485	-9479	-9550	-9551	MG	0.00	0.00	100.00
3437	-9744	-9646	-9645	-9743	MG	0.00	0.00	100.00
3437	-9646	-9604	-9603	-9645	MG	0.00	0.00	100.00
3437	-9604	-9556	-9555	-9603	MG	0.00	0.00	100.00
3437	-8423	-8376	-8375	-8422	MG	0.00	0.00	100.00
3437	-8907	-8824	-8807	-8906	MG	0.00	0.00	100.00
3437	-9740	-9728	-9856	-9847	MG	0.00	0.00	100.00
3437	-9743	-9645	-9644	-9742	MG	0.00	0.00	100.00
3437	-9645	-9603	-9602	-9644	MG	0.00	0.00	100.00
3437	-7505	-7469	-7468	-7504	MG	0.00	0.00	100.00
3437	-9555	-9488	-9504	-9554	MG	0.00	0.00	100.00
3437	-8426	-8425	-8480	-8481	MG	0.00	0.00	100.00
3437	-8539	-8538	-8621	-8629	MG	0.00	0.00	100.00
3437	-7813	-7723	-7722	-7812	MG	0.00	0.00	100.00
3437	-7723	-7671	-7670	-7722	MG	0.00	0.00	100.00
3437	-10196	-10195	-10250	-10251	MG	0.00	0.00	100.00
3437	-8424	-8423	-8472	-8479	MG	0.00	0.00	100.00
3437	-8910	-8909	-8983	-8984	MG	0.00	0.00	100.00
3437	-9074	-9095	-9150	-9151	MG	0.00	0.00	100.00
3437	-7812	-7722	-7716	-7811	MG	0.00	0.00	100.00
3437	-7722	-7670	-7669	-7716	MG	0.00	0.00	100.00
3437	-9377	-9286	-9285	-9376	MG	0.00	0.00	100.00
3437	-10254	-10198	-10177	-10253	MG	0.00	0.00	100.00
3437	-7495	-7459	-7458	-7494	MG	0.00	0.00	100.00
3437	-9847	-9856	-9969	-9970	MG	0.00	0.00	100.00
3437	-10040	-9971	-9963	-10039	MG	0.00	0.00	100.00
3437	-7807	-7806	-7929	-7930	MG	0.00	0.00	100.00
3437	-7711	-7710	-7805	-7806	MG	0.00	0.00	100.00
3437	-9506	-9448	-9447	-9505	MG	0.00	0.00	100.00
3437	-7264	-7263	-7297	-7298	MG	0.00	0.00	100.00
3437	-7138	-7137	-7200	-7201	MG	0.00	0.00	100.00
3437	-9739	-9639	-9638	-9738	MG	0.00	0.00	100.00
3437	-7715	-7668	-7643	-7721	MG	0.00	0.00	100.00
3437	-7668	-7583	-7582	-7643	MG	0.00	0.00	100.00
3437	-7583	-7505	-7504	-7582	MG	0.00	0.00	100.00
3437	-10197	-10130	-10129	-10176	MG	0.00	0.00	100.00
3437	-10130	-10038	-10037	-10129	MG	0.00	0.00	100.00
3437	-10200	-10134	-10133	-10199	MG	0.00	0.00	100.00
3437	-7291	-7257	-7256	-7290	MG	0.00	0.00	100.00
3437	-7643	-7582	-7581	-7667	MG	0.00	0.00	100.00
3437	-10176	-10129	-10128	-10196	MG	0.00	0.00	100.00
3437	-10256	-10200	-10199	-10255	MG	0.00	0.00	100.00
3437	-10037	-9962	-9970	-10036	MG	0.00	0.00	100.00
3437	-7299	-7298	-7348	-7349	MG	0.00	0.00	100.00
3437	-7714	-7667	-7663	-7713	MG	0.00	0.00	100.00
3437	-9863	-9747	-9746	-9840	MG	0.00	0.00	100.00
3437	-7581	-7503	-7502	-7580	MG	0.00	0.00	100.00
3437	-7931	-7808	-7807	-7930	MG	0.00	0.00	100.00
3437	-7808	-7713	-7712	-7807	MG	0.00	0.00	100.00
3437	-9855	-9727	-9739	-9854	MG	0.00	0.00	100.00
3437	-7663	-7580	-7579	-7666	MG	0.00	0.00	100.00

3437	-9554	-9504	-9487	-9553	MG	0.00	0.00	100.00
3437	-9504	-9444	-9443	-9487	MG	0.00	0.00	100.00
3437	-8029	-8028	-8154	-8155	MG	0.00	0.00	100.00
3437	-9643	-9601	-9600	-9642	MG	0.00	0.00	100.00
3437	-9849	-9745	-9744	-9848	MG	0.00	0.00	100.00
3437	-7710	-7661	-7660	-7709	MG	0.00	0.00	100.00
3437	-9487	-9443	-9442	-9486	MG	0.00	0.00	100.00
3437	-7935	-7811	-7810	-7934	MG	0.00	0.00	100.00
3437	-9961	-9839	-9853	-9967	MG	0.00	0.00	100.00
3437	-9856	-9855	-9968	-9969	MG	0.00	0.00	100.00
3437	-9640	-9598	-9597	-9639	MG	0.00	0.00	100.00
3437	-9598	-9550	-9549	-9597	MG	0.00	0.00	100.00
3437	-9550	-9479	-9503	-9549	MG	0.00	0.00	100.00
3437	-7499	-7463	-7462	-7498	MG	0.00	0.00	100.00
3437	-9383	-9292	-9291	-9382	MG	0.00	0.00	100.00
3437	-9853	-9737	-9736	-9838	MG	0.00	0.00	100.00
3437	-9209	-9208	-9284	-9285	MG	0.00	0.00	100.00
3437	-9208	-9207	-9283	-9284	MG	0.00	0.00	100.00
3437	-9095	-9073	-9149	-9150	MG	0.00	0.00	100.00
3437	-8721	-8720	-8825	-8841	MG	0.00	0.00	100.00
3437	-8720	-8719	-8840	-8825	MG	0.00	0.00	100.00
3437	-8538	-8537	-8628	-8621	MG	0.00	0.00	100.00
3437	-10245	-10175	-10189	-10244	MG	0.00	0.00	100.00
3437	-7658	-7576	-7570	-7657	MG	0.00	0.00	100.00
3437	-7576	-7496	-7495	-7570	MG	0.00	0.00	100.00
3437	-9943	-9852	-9837	-9942	MG	0.00	0.00	100.00
3437	-7924	-7802	-7779	-7923	MG	0.00	0.00	100.00
3437	-7802	-7698	-7706	-7779	MG	0.00	0.00	100.00
3437	-7698	-7657	-7656	-7706	MG	0.00	0.00	100.00
3437	-7657	-7570	-7569	-7656	MG	0.00	0.00	100.00
3437	-7570	-7495	-7494	-7569	MG	0.00	0.00	100.00
3437	-7969	-7923	-7922	-7968	MG	0.00	0.00	100.00
3437	-7923	-7779	-7801	-7922	MG	0.00	0.00	100.00
3437	-7671	-7586	-7585	-7670	MG	0.00	0.00	100.00
3437	-7706	-7656	-7655	-7705	MG	0.00	0.00	100.00
3437	-10249	-10194	-10193	3301	MG	0.00	0.00	100.00
3437	-7139	-7138	-7201	-7202	MG	0.00	0.00	100.00
3437	-7968	-7922	-7921	-7967	MG	0.00	0.00	100.00
3437	-7922	-7801	-7800	-7921	MG	0.00	0.00	100.00
3437	-9205	-9147	-9146	-9204	MG	0.00	0.00	100.00
3437	-8909	-8908	-8982	-8983	MG	0.00	0.00	100.00
3437	-7806	-7805	-7928	-7929	MG	0.00	0.00	100.00
3437	-7662	-7661	-7710	-7711	MG	0.00	0.00	100.00
3437	-7930	-7929	-7975	-7976	MG	0.00	0.00	100.00
3437	-8425	-8424	-8479	-8480	MG	0.00	0.00	100.00
3437	-7712	-7711	-7806	-7807	MG	0.00	0.00	100.00
3437	-9374	-9283	-9282	-9373	MG	0.00	0.00	100.00
3437	-10042	-9973	-9972	-10041	MG	0.00	0.00	100.00
3437	-7356	-7306	-7305	-7355	MG	0.00	0.00	100.00
3437	-7306	-7272	-7271	-7305	MG	0.00	0.00	100.00
3437	-7272	-7209	-7208	-7271	MG	0.00	0.00	100.00
3437	-9741	-9643	-9642	-9740	MG	0.00	0.00	100.00
3437	-10043	-9974	-9973	-10042	MG	0.00	0.00	100.00
3437	-10135	-10043	-10042	-10134	MG	0.00	0.00	100.00
3437	-10201	-10135	-10134	-10200	MG	0.00	0.00	100.00
3437	-7305	-7271	-7270	-7304	MG	0.00	0.00	100.00
3437	-7271	-7208	-7207	-7270	MG	0.00	0.00	100.00
3437	-7208	-7145	-7144	-7207	MG	0.00	0.00	100.00
3437	-9556	-9493	-9488	-9555	MG	0.00	0.00	100.00
3437	-7470	-7354	-7353	-7469	MG	0.00	0.00	100.00
3437	-8977	-8903	-8902	-8976	MG	0.00	0.00	100.00
3437	-9970	-9969	-10035	-10036	MG	0.00	0.00	100.00
3437	-10128	-10127	-10195	-10196	MG	0.00	0.00	100.00
3437	-9603	-9555	-9554	-9602	MG	0.00	0.00	100.00
3437	-9143	-9093	-9068	-9142	MG	0.00	0.00	100.00
3437	-9488	-9445	-9444	-9504	MG	0.00	0.00	100.00
3437	-8976	-8902	-8901	-8975	MG	0.00	0.00	100.00
3437	-7303	-7269	-7268	-7302	MG	0.00	0.00	100.00
3437	-9284	-9283	-9374	-9375	MG	0.00	0.00	100.00
3437	-9602	-9554	-9553	-9601	MG	0.00	0.00	100.00
3437	-7504	-7468	-7467	-7503	MG	0.00	0.00	100.00
3437	-8809	-8728	-8727	-8827	MG	0.00	0.00	100.00
3437	-8728	-8635	-8634	-8727	MG	0.00	0.00	100.00
3437	-7805	-7710	-7709	-7804	MG	0.00	0.00	100.00
3437	-9601	-9553	-9552	-9600	MG	0.00	0.00	100.00
3437	-9553	-9487	-9486	-9552	MG	0.00	0.00	100.00
3437	-9443	-9377	-9376	-9442	MG	0.00	0.00	100.00
3437	-7467	-7351	-7350	-7466	MG	0.00	0.00	100.00
3437	-7351	-7301	-7300	-7350	MG	0.00	0.00	100.00

3437	-7301	-7267	-7266	-7300	MG	0.00	0.00	100.00
3437	-7267	-7204	-7203	-7266	MG	0.00	0.00	100.00
3437	-8485	-8432	-8431	-8484	MG	0.00	0.00	100.00
3437	-8915	-8826	-8843	-8914	MG	0.00	0.00	100.00
3437	-9479	-9440	-9439	-9503	MG	0.00	0.00	100.00
3437	-9440	-9374	-9373	-9439	MG	0.00	0.00	100.00
3437	-9639	-9597	-9596	-9638	MG	0.00	0.00	100.00
3437	-9597	-9549	-9548	-9596	MG	0.00	0.00	100.00
3437	-9549	-9503	-9484	-9548	MG	0.00	0.00	100.00
3437	-8311	-8223	-8222	-8310	MG	0.00	0.00	100.00
3437	-7508	-7472	-7471	-7507	MG	0.00	0.00	100.00
3437	-7973	-7927	-7926	-7972	MG	0.00	0.00	100.00
3437	-7983	-7937	-7936	-7982	MG	0.00	0.00	100.00
3437	-7263	-7200	-7199	-7262	MG	0.00	0.00	100.00
3437	-7200	-7137	-7136	-7199	MG	0.00	0.00	100.00
3437	-10029	-9943	-9942	-10028	MG	0.00	0.00	100.00
3437	-7975	-7974	-8028	-8029	MG	0.00	0.00	100.00
3437	-7296	-7262	-7261	-7295	MG	0.00	0.00	100.00
3437	-7262	-7199	-7198	-7261	MG	0.00	0.00	100.00
3437	-8379	-8378	-8425	-8426	MG	0.00	0.00	100.00
3437	-7497	-7461	-7460	-7496	MG	0.00	0.00	100.00
3437	-7461	-7345	-7344	-7460	MG	0.00	0.00	100.00
3437	-7345	-7295	-7294	-7344	MG	0.00	0.00	100.00
3437	-7295	-7261	-7260	-7294	MG	0.00	0.00	100.00
3437	-7261	-7198	-7197	-7260	MG	0.00	0.00	100.00
3437	-7198	-7135	-7134	-7197	MG	0.00	0.00	100.00
3437	-7496	-7460	-7459	-7495	MG	0.00	0.00	100.00
3437	-7460	-7344	-7343	-7459	MG	0.00	0.00	100.00
3437	-7344	-7294	-7293	-7343	MG	0.00	0.00	100.00
3437	-7294	-7260	-7259	-7293	MG	0.00	0.00	100.00
3437	-7260	-7197	-7196	-7259	MG	0.00	0.00	100.00
3437	-7197	-7134	-7133	-7196	MG	0.00	0.00	100.00
3437	-6558	-7131	-7132	-7132	MG	0.00	0.00	100.00
3437	-6558	-7132	-7133	-5852	MG	0.00	0.00	100.00
3437	-7343	-7293	-7292	-7342	MG	0.00	0.00	100.00
3437	-7293	-7259	-7258	-7292	MG	0.00	0.00	100.00
3437	-7259	-7196	-7195	-7258	MG	0.00	0.00	100.00
3437	-7196	-7133	-7132	-7195	MG	0.00	0.00	100.00
3437	-7494	-7458	-7457	-7493	MG	0.00	0.00	100.00
3437	-7458	-7342	-7341	-7457	MG	0.00	0.00	100.00
3437	-7342	-7292	-7291	-7341	MG	0.00	0.00	100.00
3437	-7292	-7258	-7257	-7291	MG	0.00	0.00	100.00
3437	-7258	-7195	-7194	-7257	MG	0.00	0.00	100.00
3437	-7195	-7132	-7131	-7194	MG	0.00	0.00	100.00
3437	-7493	-7457	-7456	-7492	MG	0.00	0.00	100.00
3437	-7457	-7341	-7340	-7456	MG	0.00	0.00	100.00
3437	-7341	-7291	-7290	-7340	MG	0.00	0.00	100.00
3437	-8534	-8471	-8470	-8533	MG	0.00	0.00	100.00
3437	-8471	-8421	-8420	-8470	MG	0.00	0.00	100.00
3437	-7194	-7131	-7130	-7193	MG	0.00	0.00	100.00
3437	-7465	-7464	-7500	-7501	MG	0.00	0.00	100.00
3437	-7464	-7463	-7499	-7500	MG	0.00	0.00	100.00
3437	-8617	-8533	-8532	-8616	MG	0.00	0.00	100.00
3437	-7298	-7297	-7347	-7348	MG	0.00	0.00	100.00
3437	-10194	-10126	-10125	-10193	MG	0.00	0.00	100.00
3437	-10126	-10034	-10033	-10125	MG	0.00	0.00	100.00
3437	-10034	-9968	-9945	-10033	MG	0.00	0.00	100.00
3437	-8714	-8616	-8627	-8713	MG	0.00	0.00	100.00
3437	-8616	-8532	-8531	-8627	MG	0.00	0.00	100.00
3437	-8532	-8469	-8477	-8531	MG	0.00	0.00	100.00
3437	-7580	-7502	-7501	-7579	MG	0.00	0.00	100.00
3437	-8030	-8029	-8155	-8156	MG	0.00	0.00	100.00
3437	-8802	-8713	-8712	-8801	MG	0.00	0.00	100.00
3437	-7302	-7268	-7267	-7301	MG	0.00	0.00	100.00
3437	-9969	-9968	-10034	-10035	MG	0.00	0.00	100.00
3437	-9728	-9727	-9855	-9856	MG	0.00	0.00	100.00
3437	-7503	-7467	-7466	-7502	MG	0.00	0.00	100.00
3437	-8841	-8825	-8909	-8910	MG	0.00	0.00	100.00
3437	-8825	-8840	-8908	-8909	MG	0.00	0.00	100.00
3437	-9839	-9738	-9737	-9853	MG	0.00	0.00	100.00
3437	-10247	-10191	-10190	-10246	MG	0.00	0.00	100.00
3437	-10191	-10123	-10122	-10190	MG	0.00	0.00	100.00
3437	-10123	-10031	-10030	-10122	MG	0.00	0.00	100.00
3437	-8237	-8163	-8162	-8236	MG	0.00	0.00	100.00
3437	-7977	-7931	-7930	-7976	MG	0.00	0.00	100.00
3437	-8037	-7983	-7982	-8036	MG	0.00	0.00	100.00
3437	-8432	-8385	-8384	-8431	MG	0.00	0.00	100.00
3437	-10190	-10122	-10121	-10175	MG	0.00	0.00	100.00
3437	-9599	-9598	-9640	-9641	MG	0.00	0.00	100.00

3437	-8236	-8162	-8161	-8235	MG	0.00	0.00	100.00
3437	-9944	-9838	-9852	-9943	MG	0.00	0.00	100.00
3437	-9838	-9736	-9726	-9852	MG	0.00	0.00	100.00
3437	-8431	-8384	-8383	-8430	MG	0.00	0.00	100.00
3437	-8384	-8323	-8322	-8383	MG	0.00	0.00	100.00
3437	-8323	-8235	-8234	-8322	MG	0.00	0.00	100.00
3437	-8235	-8161	-8160	-8234	MG	0.00	0.00	100.00
3437	-8161	-8035	-8034	-8160	MG	0.00	0.00	100.00
3437	-9852	-9726	-9735	-9837	MG	0.00	0.00	100.00
3437	-10244	-10189	-10188	-10243	MG	0.00	0.00	100.00
3437	-10189	-10120	-10119	-10188	MG	0.00	0.00	100.00
3437	-10120	-10028	-10027	-10119	MG	0.00	0.00	100.00
3437	-10028	-9942	-9941	-10027	MG	0.00	0.00	100.00
3437	-9942	-9837	-9846	-9941	MG	0.00	0.00	100.00
3437	-9837	-9735	-9734	-9846	MG	0.00	0.00	100.00
3437	-7202	-7201	-7264	-7265	MG	0.00	0.00	100.00
3437	-7201	-7200	-7263	-7264	MG	0.00	0.00	100.00
3437	-9375	-9374	-9440	-9441	MG	0.00	0.00	100.00
3437	-10035	-10034	-10126	-10127	MG	0.00	0.00	100.00
3437	-9649	-9607	-9606	-9648	MG	0.00	0.00	100.00
3437	-9607	-9559	-9558	-9606	MG	0.00	0.00	100.00
3437	-9559	-9507	-9506	-9558	MG	0.00	0.00	100.00
3437	-9507	-9449	-9448	-9506	MG	0.00	0.00	100.00
3437	-9449	-9383	-9382	-9448	MG	0.00	0.00	100.00
3437	-9746	-9648	-9647	-9745	MG	0.00	0.00	100.00
3437	-9376	-9375	-9441	-9442	MG	0.00	0.00	100.00
3437	-9606	-9558	-9557	-9605	MG	0.00	0.00	100.00
3437	-9558	-9506	-9505	-9557	MG	0.00	0.00	100.00
3437	-9486	-9485	-9551	-9552	MG	0.00	0.00	100.00
3437	-9448	-9382	-9381	-9447	MG	0.00	0.00	100.00
3437	-9745	-9647	-9646	-9744	MG	0.00	0.00	100.00
3437	-9647	-9605	-9604	-9646	MG	0.00	0.00	100.00
3437	-9605	-9557	-9556	-9604	MG	0.00	0.00	100.00
3437	-7498	-7462	-7461	-7497	MG	0.00	0.00	100.00
3437	-9505	-9447	-9446	-9493	MG	0.00	0.00	100.00
3437	-7976	-7975	-8029	-8030	MG	0.00	0.00	100.00
3437	-8156	-8155	-8229	-8230	MG	0.00	0.00	100.00
3437	-8318	-8317	-8378	-8379	MG	0.00	0.00	100.00
3437	-8317	-8316	-8377	-8378	MG	0.00	0.00	100.00
3437	-8155	-8154	-8228	-8229	MG	0.00	0.00	100.00
3437	-8537	-8536	-8620	-8628	MG	0.00	0.00	100.00
3437	-8628	-8620	-8718	-8719	MG	0.00	0.00	100.00
3437	-8719	-8718	-8824	-8840	MG	0.00	0.00	100.00
3437	-8840	-8824	-8907	-8908	MG	0.00	0.00	100.00
3437	-8376	-8315	-8314	-8375	MG	0.00	0.00	100.00
3437	-8315	-8227	-8226	-8314	MG	0.00	0.00	100.00
3437	-8227	-8153	-8152	-8226	MG	0.00	0.00	100.00
3437	-8153	-8027	-8026	-8152	MG	0.00	0.00	100.00
3437	-8027	-7973	-7972	-8026	MG	0.00	0.00	100.00
3437	-8422	-8375	-8374	-8421	MG	0.00	0.00	100.00
3437	-8375	-8314	-8313	-8374	MG	0.00	0.00	100.00
3437	-8314	-8226	-8225	-8313	MG	0.00	0.00	100.00
3437	-8226	-8152	-8151	-8225	MG	0.00	0.00	100.00
3437	-8152	-8026	-8025	-8151	MG	0.00	0.00	100.00
3437	-8026	-7972	-7971	-8025	MG	0.00	0.00	100.00
3437	-8421	-8374	-8373	-8420	MG	0.00	0.00	100.00
3437	-8374	-8313	-8312	-8373	MG	0.00	0.00	100.00
3437	-8313	-8225	-8224	-8312	MG	0.00	0.00	100.00
3437	-8225	-8151	-8150	-8224	MG	0.00	0.00	100.00
3437	-8151	-8025	-8024	-8150	MG	0.00	0.00	100.00
3437	-8025	-7971	-7970	-8024	MG	0.00	0.00	100.00
3437	-8545	-8485	-8484	-8544	MG	0.00	0.00	100.00
3437	-8373	-8312	-8311	-8372	MG	0.00	0.00	100.00
3437	-8312	-8224	-8223	-8311	MG	0.00	0.00	100.00
3437	-8224	-8150	-8149	-8223	MG	0.00	0.00	100.00
3437	-8150	-8024	-8023	-8149	MG	0.00	0.00	100.00
3437	-8024	-7970	-7969	-8023	MG	0.00	0.00	100.00
3437	-8419	-8372	-8371	-8418	MG	0.00	0.00	100.00
3437	-7579	-7572	-7662	-7666	MG	0.00	0.00	100.00
3437	-9503	-9439	-9438	-9484	MG	0.00	0.00	100.00
3437	-8223	-8149	-8148	-8222	MG	0.00	0.00	100.00
3437	-8149	-8023	-8022	-8148	MG	0.00	0.00	100.00
3437	-8023	-7969	-7968	-8022	MG	0.00	0.00	100.00
3437	-8418	-8371	-8370	-8417	MG	0.00	0.00	100.00
3437	-8371	-8310	-8309	-8370	MG	0.00	0.00	100.00
3437	-8310	-8222	-8221	-8309	MG	0.00	0.00	100.00
3437	-8222	-8148	-8147	-8221	MG	0.00	0.00	100.00
3437	-8148	-8022	-8021	-8147	MG	0.00	0.00	100.00
3437	-8022	-7968	-7967	-8021	MG	0.00	0.00	100.00

3437	-9595	-9547	-9546	-9594	MG	0.00	0.00	100.00
3437	-8378	-8377	-8424	-8425	MG	0.00	0.00	100.00
3437	-7937	-7813	-7812	-7936	MG	0.00	0.00	100.00
3437	-9437	-9371	-9370	-9436	MG	0.00	0.00	100.00
3437	-9736	-9636	-9635	-9726	MG	0.00	0.00	100.00
3437	-9636	-9594	-9593	-9635	MG	0.00	0.00	100.00
3437	-7586	-7508	-7507	-7585	MG	0.00	0.00	100.00
3437	-7982	-7936	-7935	-7981	MG	0.00	0.00	100.00
3437	-7936	-7812	-7811	-7935	MG	0.00	0.00	100.00
3437	-9436	-9370	-9369	-9435	MG	0.00	0.00	100.00
3437	-9726	-9635	-9634	-9735	MG	0.00	0.00	100.00
3437	-7670	-7585	-7584	-7669	MG	0.00	0.00	100.00
3437	-7585	-7507	-7506	-7584	MG	0.00	0.00	100.00
3437	-7981	-7935	-7934	-7980	MG	0.00	0.00	100.00
3437	-9477	-9435	-9434	-9476	MG	0.00	0.00	100.00
3437	-7811	-7716	-7715	-7810	MG	0.00	0.00	100.00
3437	-7716	-7669	-7668	-7715	MG	0.00	0.00	100.00
3437	-7669	-7584	-7583	-7668	MG	0.00	0.00	100.00
3437	-7584	-7506	-7505	-7583	MG	0.00	0.00	100.00
3437	-7980	-7934	-7933	-7979	MG	0.00	0.00	100.00
3437	-7934	-7810	-7809	-7933	MG	0.00	0.00	100.00
3437	-7810	-7715	-7721	-7809	MG	0.00	0.00	100.00
3437	-9642	-9641	-9728	-9740	MG	0.00	0.00	100.00
3437	-9641	-9640	-9727	-9728	MG	0.00	0.00	100.00
3437	-9552	-9551	-9599	-9600	MG	0.00	0.00	100.00
3437	-7979	-7933	-7932	-7978	MG	0.00	0.00	100.00
3437	-7933	-7809	-7781	-7932	MG	0.00	0.00	100.00
3437	-7809	-7721	-7714	-7781	MG	0.00	0.00	100.00
3437	-7721	-7643	-7667	-7714	MG	0.00	0.00	100.00
3437	-9100	-8991	-8990	-9099	MG	0.00	0.00	100.00
3437	-7582	-7504	-7503	-7581	MG	0.00	0.00	100.00
3437	-7978	-7932	-7931	-7977	MG	0.00	0.00	100.00
3437	-7932	-7781	-7808	-7931	MG	0.00	0.00	100.00
3437	-7781	-7714	-7713	-7808	MG	0.00	0.00	100.00
3437	-9157	-9099	-9098	-9156	MG	0.00	0.00	100.00
3437	-7667	-7581	-7580	-7663	MG	0.00	0.00	100.00
3437	-8990	-8916	-8915	-8989	MG	0.00	0.00	100.00
3437	-9381	-9290	-9289	-9380	MG	0.00	0.00	100.00
3437	-9290	-9214	-9213	-9289	MG	0.00	0.00	100.00
3437	-7713	-7663	-7666	-7712	MG	0.00	0.00	100.00
3437	-9156	-9098	-9097	-9155	MG	0.00	0.00	100.00
3437	-9098	-8989	-8988	-9097	MG	0.00	0.00	100.00
3437	-7500	-7499	-7578	-7572	MG	0.00	0.00	100.00
3437	-9380	-9289	-9288	-9379	MG	0.00	0.00	100.00
3437	-7928	-7805	-7804	-7927	MG	0.00	0.00	100.00
3437	-9213	-9155	-9154	-9212	MG	0.00	0.00	100.00
3437	-9155	-9097	-9096	-9154	MG	0.00	0.00	100.00
3437	-7661	-7578	-7577	-7660	MG	0.00	0.00	100.00
3437	-7578	-7499	-7498	-7577	MG	0.00	0.00	100.00
3437	-7927	-7804	-7780	-7926	MG	0.00	0.00	100.00
3437	-7804	-7709	-7708	-7780	MG	0.00	0.00	100.00
3437	-7709	-7660	-7659	-7708	MG	0.00	0.00	100.00
3437	-7660	-7577	-7571	-7659	MG	0.00	0.00	100.00
3437	-7577	-7498	-7497	-7571	MG	0.00	0.00	100.00
3437	-7972	-7926	-7925	-7971	MG	0.00	0.00	100.00
3437	-7926	-7780	-7803	-7925	MG	0.00	0.00	100.00
3437	-7780	-7708	-7707	-7803	MG	0.00	0.00	100.00
3437	-7708	-7659	-7658	-7707	MG	0.00	0.00	100.00
3437	-7659	-7571	-7576	-7658	MG	0.00	0.00	100.00
3437	-9076	-8986	-8985	-9075	MG	0.00	0.00	100.00
3437	-8986	-8912	-8911	-8985	MG	0.00	0.00	100.00
3437	-7925	-7803	-7802	-7924	MG	0.00	0.00	100.00
3437	-7803	-7707	-7698	-7802	MG	0.00	0.00	100.00
3437	-7707	-7658	-7657	-7698	MG	0.00	0.00	100.00
3437	-9075	-8985	-8984	-9074	MG	0.00	0.00	100.00
3437	-8985	-8911	-8910	-8984	MG	0.00	0.00	100.00
3437	-7970	-7924	-7923	-7969	MG	0.00	0.00	100.00
3437	-9441	-9440	-9479	-9485	MG	0.00	0.00	100.00
3437	-9283	-9207	-9206	-9282	MG	0.00	0.00	100.00
3437	-9207	-9149	-9148	-9206	MG	0.00	0.00	100.00
3437	-9149	-9073	-9072	-9148	MG	0.00	0.00	100.00
3437	-9073	-8982	-8981	-9072	MG	0.00	0.00	100.00
3437	-8982	-8908	-8907	-8981	MG	0.00	0.00	100.00
3437	-9282	-9206	-9205	-9281	MG	0.00	0.00	100.00
3437	-7779	-7706	-7705	-7801	MG	0.00	0.00	100.00
3437	-9148	-9072	-9071	-9147	MG	0.00	0.00	100.00
3437	-7656	-7569	-7568	-7655	MG	0.00	0.00	100.00
3437	-7569	-7494	-7493	-7568	MG	0.00	0.00	100.00
3437	-9372	-9281	-9280	-9371	MG	0.00	0.00	100.00

3437	-9281	-9205	-9204	-9280	MG	0.00	0.00	100.00
3437	-8033	-7979	-7978	-8032	MG	0.00	0.00	100.00
3437	-9147	-9071	-9094	-9146	MG	0.00	0.00	100.00
3437	-7655	-7568	-7567	-7654	MG	0.00	0.00	100.00
3437	-7568	-7493	-7492	-7567	MG	0.00	0.00	100.00
3437	-9371	-9280	-9279	-9370	MG	0.00	0.00	100.00
3437	-7929	-7928	-7974	-7975	MG	0.00	0.00	100.00
3437	-9204	-9146	-9145	-9203	MG	0.00	0.00	100.00
3437	-9146	-9094	-9070	-9145	MG	0.00	0.00	100.00
3437	-9094	-8979	-8978	-9070	MG	0.00	0.00	100.00
3437	-8979	-8905	-8904	-8978	MG	0.00	0.00	100.00
3437	-9370	-9279	-9278	-9369	MG	0.00	0.00	100.00
3437	-9279	-9203	-9202	-9278	MG	0.00	0.00	100.00
3437	-7209	-7146	-7145	-7208	MG	0.00	0.00	100.00
3437	-7507	-7471	-7470	-7506	MG	0.00	0.00	100.00
3437	-7471	-7355	-7354	-7470	MG	0.00	0.00	100.00
3437	-7355	-7305	-7304	-7354	MG	0.00	0.00	100.00
3437	-9369	-9278	-9277	-9368	MG	0.00	0.00	100.00
3437	-9278	-9202	-9201	-9277	MG	0.00	0.00	100.00
3437	-9202	-9144	-9143	-9201	MG	0.00	0.00	100.00
3437	-7506	-7470	-7469	-7505	MG	0.00	0.00	100.00
3437	-9069	-8977	-8976	-9093	MG	0.00	0.00	100.00
3437	-7354	-7304	-7303	-7353	MG	0.00	0.00	100.00
3437	-7304	-7270	-7269	-7303	MG	0.00	0.00	100.00
3437	-7270	-7207	-7206	-7269	MG	0.00	0.00	100.00
3437	-7207	-7144	-7143	-7206	MG	0.00	0.00	100.00
3437	-8470	-8420	-8419	-8469	MG	0.00	0.00	100.00
3437	-7469	-7353	-7352	-7468	MG	0.00	0.00	100.00
3437	-7353	-7303	-7302	-7352	MG	0.00	0.00	100.00
3437	-9285	-9284	-9375	-9376	MG	0.00	0.00	100.00
3437	-9214	-9156	-9155	-9213	MG	0.00	0.00	100.00
3437	-7206	-7143	-7142	-7205	MG	0.00	0.00	100.00
3437	-9150	-9149	-9207	-9208	MG	0.00	0.00	100.00
3437	-10033	-9945	-9961	-10032	MG	0.00	0.00	100.00
3437	-7352	-7302	-7301	-7351	MG	0.00	0.00	100.00
3437	-8635	-8546	-8545	-8634	MG	0.00	0.00	100.00
3437	-7268	-7205	-7204	-7267	MG	0.00	0.00	100.00
3437	-7205	-7142	-7141	-7204	MG	0.00	0.00	100.00
3437	-8916	-8827	-8826	-8915	MG	0.00	0.00	100.00
3437	-8827	-8727	-8726	-8826	MG	0.00	0.00	100.00
3437	-8727	-8634	-8633	-8726	MG	0.00	0.00	100.00
3437	-8634	-8545	-8544	-8633	MG	0.00	0.00	100.00
3437	-8621	-8628	-8719	-8720	MG	0.00	0.00	100.00
3437	-7204	-7141	-7140	-7203	MG	0.00	0.00	100.00
3437	-7466	-7350	-7349	-7465	MG	0.00	0.00	100.00
3437	-7350	-7300	-7299	-7349	MG	0.00	0.00	100.00
3437	-7300	-7266	-7265	-7299	MG	0.00	0.00	100.00
3437	-7266	-7203	-7202	-7265	MG	0.00	0.00	100.00
3437	-7203	-7140	-7139	-7202	MG	0.00	0.00	100.00
3437	-8484	-8431	-8430	-8483	MG	0.00	0.00	100.00
3437	-7572	-7578	-7661	-7662	MG	0.00	0.00	100.00
3437	-7463	-7347	-7346	-7462	MG	0.00	0.00	100.00
3437	-7347	-7297	-7296	-7346	MG	0.00	0.00	100.00
3437	-7297	-7263	-7262	-7296	MG	0.00	0.00	100.00
3437	-8543	-8483	-8474	-8542	MG	0.00	0.00	100.00
3437	-8483	-8430	-8429	-8474	MG	0.00	0.00	100.00
3437	-7462	-7346	-7345	-7461	MG	0.00	0.00	100.00
3437	-7346	-7296	-7295	-7345	MG	0.00	0.00	100.00
3437	-8724	-8631	-8630	-8723	MG	0.00	0.00	100.00
3437	-8631	-8542	-8541	-8630	MG	0.00	0.00	100.00
3437	-7199	-7136	-7135	-7198	MG	0.00	0.00	100.00
3437	-8474	-8429	-8428	-8473	MG	0.00	0.00	100.00
3437	-8912	-8787	-8808	-8911	MG	0.00	0.00	100.00
3437	-8787	-8723	-8722	-8808	MG	0.00	0.00	100.00
3437	-9973	-9840	-9849	-9972	MG	0.00	0.00	100.00
3437	-9840	-9746	-9745	-9849	MG	0.00	0.00	100.00
3437	-8541	-8473	-8482	-8540	MG	0.00	0.00	100.00
3437	-8473	-8428	-8427	-8482	MG	0.00	0.00	100.00
3437	-8808	-8722	-8721	-8841	MG	0.00	0.00	100.00
3437	-8722	-8622	-8629	-8721	MG	0.00	0.00	100.00
3437	-8622	-8540	-8539	-8629	MG	0.00	0.00	100.00
3437	-8540	-8482	-8481	-8539	MG	0.00	0.00	100.00
3437	-8482	-8427	-8426	-8481	MG	0.00	0.00	100.00
3437	-8824	-8718	-8717	-8807	MG	0.00	0.00	100.00
3437	-8718	-8620	-8619	-8717	MG	0.00	0.00	100.00
3437	-8620	-8536	-8535	-8619	MG	0.00	0.00	100.00
3437	-9971	-9848	-9862	-9963	MG	0.00	0.00	100.00
3437	-9848	-9744	-9743	-9862	MG	0.00	0.00	100.00
3437	-10253	-10177	-10197	-10252	MG	0.00	0.00	100.00

3437	-10177	-10131	-10130	-10197	MG	0.00	0.00	100.00
3437	-10131	-10039	-10038	-10130	MG	0.00	0.00	100.00
3437	-10039	-9963	-9946	-10038	MG	0.00	0.00	100.00
3437	-9963	-9862	-9858	-9946	MG	0.00	0.00	100.00
3437	-9862	-9743	-9742	-9858	MG	0.00	0.00	100.00
3437	-10252	-10197	-10176	3302	MG	0.00	0.00	100.00
3437	-8806	-8716	-8715	-8839	MG	0.00	0.00	100.00
3437	-8716	-8618	-8617	-8715	MG	0.00	0.00	100.00
3437	-8618	-8534	-8533	-8617	MG	0.00	0.00	100.00
3437	-9946	-9858	-9857	-9962	MG	0.00	0.00	100.00
3437	-9858	-9742	-9741	-9857	MG	0.00	0.00	100.00
3437	-8904	-8839	-8803	-8903	MG	0.00	0.00	100.00
3437	-8839	-8715	-8714	-8803	MG	0.00	0.00	100.00
3437	-8715	-8617	-8616	-8714	MG	0.00	0.00	100.00
3437	-9215	-9157	-9156	-9214	MG	0.00	0.00	100.00
3437	-8533	-8470	-8469	-8532	MG	0.00	0.00	100.00
3437	-9201	-9143	-9142	-9200	MG	0.00	0.00	100.00
3437	-8903	-8803	-8802	-8902	MG	0.00	0.00	100.00
3437	-8803	-8714	-8713	-8802	MG	0.00	0.00	100.00
3437	-8234	-8160	-8159	-8233	MG	0.00	0.00	100.00
3437	-8160	-8034	-8033	-8159	MG	0.00	0.00	100.00
3437	-10193	-10125	-10124	-10192	MG	0.00	0.00	100.00
3437	-10125	-10033	-10032	-10124	MG	0.00	0.00	100.00
3437	-8469	-8419	-8418	-8477	MG	0.00	0.00	100.00
3437	-9945	-9854	-9839	-9961	MG	0.00	0.00	100.00
3437	-9854	-9739	-9738	-9839	MG	0.00	0.00	100.00
3437	-10248	-10192	-10191	-10247	MG	0.00	0.00	100.00
3437	-10192	-10124	-10123	-10191	MG	0.00	0.00	100.00
3437	-10124	-10032	-10031	-10123	MG	0.00	0.00	100.00
3437	-10032	-9961	-9967	-10031	MG	0.00	0.00	100.00
3437	-9379	-9288	-9287	-9378	MG	0.00	0.00	100.00
3437	-8629	-8621	-8720	-8721	MG	0.00	0.00	100.00
3437	-9288	-9212	-9211	-9287	MG	0.00	0.00	100.00
3437	-8386	-8325	-8324	-8385	MG	0.00	0.00	100.00
3437	-8325	-8237	-8236	-8324	MG	0.00	0.00	100.00
3437	-10031	-9967	-9944	-10030	MG	0.00	0.00	100.00
3437	-9967	-9853	-9838	-9944	MG	0.00	0.00	100.00
3437	-9287	-9211	-9210	-9286	MG	0.00	0.00	100.00
3437	-9211	-9153	-9152	-9210	MG	0.00	0.00	100.00
3437	-8385	-8324	-8323	-8384	MG	0.00	0.00	100.00
3437	-8324	-8236	-8235	-8323	MG	0.00	0.00	100.00
3437	-8914	-8843	-8842	-8913	MG	0.00	0.00	100.00
3437	-8162	-8036	-8035	-8161	MG	0.00	0.00	100.00
3437	-8036	-7982	-7981	-8035	MG	0.00	0.00	100.00
3437	-9152	-9075	-9074	-9151	MG	0.00	0.00	100.00
3437	-9596	-9548	-9547	-9595	MG	0.00	0.00	100.00
3437	-9548	-9484	-9483	-9547	MG	0.00	0.00	100.00
3437	-9442	-9441	-9485	-9486	MG	0.00	0.00	100.00
3437	-9438	-9372	-9371	-9437	MG	0.00	0.00	100.00
3437	-8035	-7981	-7980	-8034	MG	0.00	0.00	100.00
3437	-8430	-8383	-8382	-8429	MG	0.00	0.00	100.00
3437	-8383	-8322	-8321	-8382	MG	0.00	0.00	100.00
3437	-8322	-8234	-8233	-8321	MG	0.00	0.00	100.00
3437	-9093	-8976	-8975	-9068	MG	0.00	0.00	100.00
3437	-9483	-9437	-9436	-9478	MG	0.00	0.00	100.00
3437	-8034	-7980	-7979	-8033	MG	0.00	0.00	100.00
3437	-8429	-8382	-8381	-8428	MG	0.00	0.00	100.00
3437	-8382	-8321	-8320	-8381	MG	0.00	0.00	100.00
3437	-8321	-8233	-8232	-8320	MG	0.00	0.00	100.00
3437	-8233	-8159	-8158	-8232	MG	0.00	0.00	100.00
3437	-8159	-8033	-8032	-8158	MG	0.00	0.00	100.00
3437	-9289	-9213	-9212	-9288	MG	0.00	0.00	100.00
3437	-8428	-8381	-8380	-8427	MG	0.00	0.00	100.00
3437	-8381	-8320	-8319	-8380	MG	0.00	0.00	100.00
3437	-8320	-8232	-8231	-8319	MG	0.00	0.00	100.00
3437	-8232	-8158	-8157	-8231	MG	0.00	0.00	100.00
3437	-8158	-8032	-8031	-8157	MG	0.00	0.00	100.00
3437	-8032	-7978	-7977	-8031	MG	0.00	0.00	100.00
3437	-8380	-8319	-8318	-8379	MG	0.00	0.00	100.00
3437	-8319	-8231	-8230	-8318	MG	0.00	0.00	100.00
3437	-8231	-8157	-8156	-8230	MG	0.00	0.00	100.00
3437	-8157	-8031	-8030	-8156	MG	0.00	0.00	100.00
3437	-8031	-7977	-7976	-8030	MG	0.00	0.00	100.00
3437	-8481	-8480	-8538	-8539	MG	0.00	0.00	100.00
3437	-8480	-8479	-8537	-8538	MG	0.00	0.00	100.00
3437	-8377	-8316	-8315	-8376	MG	0.00	0.00	100.00
3437	-8316	-8228	-8227	-8315	MG	0.00	0.00	100.00
3437	-8228	-8154	-8153	-8227	MG	0.00	0.00	100.00
3437	-8154	-8028	-8027	-8153	MG	0.00	0.00	100.00

3437	-8028	-7974	-7973	-8027	MG	0.00	0.00	100.00
3437	-8479	-8472	-8536	-8537	MG	0.00	0.00	100.00
3437	-8991	-8917	-8916	-8990	MG	0.00	0.00	100.00
3437	-9382	-9291	-9290	-9381	MG	0.00	0.00	100.00
3437	-9368	-9277	-9276	-9367	MG	0.00	0.00	100.00
3437	-9277	-9201	-9200	-9276	MG	0.00	0.00	100.00
3437	-9637	-9595	-9594	-9636	MG	0.00	0.00	100.00
3437	-9099	-8990	-8989	-9098	MG	0.00	0.00	100.00
3437	-9547	-9483	-9478	-9546	MG	0.00	0.00	100.00
3437	-8826	-8726	-8725	-8843	MG	0.00	0.00	100.00
3437	-8726	-8633	-8632	-8725	MG	0.00	0.00	100.00
3437	-8723	-8630	-8622	-8722	MG	0.00	0.00	100.00
3437	-9151	-9150	-9208	-9209	MG	0.00	0.00	100.00
3437	-9594	-9546	-9545	-9593	MG	0.00	0.00	100.00
3437	-8989	-8915	-8914	-8988	MG	0.00	0.00	100.00
3437	-8902	-8802	-8801	-8901	MG	0.00	0.00	100.00
3437	-8981	-8907	-8906	-8980	MG	0.00	0.00	100.00
3437	-8546	-8486	-8485	-8545	MG	0.00	0.00	100.00
3437	-8486	-8433	-8432	-8485	MG	0.00	0.00	100.00
3437	-9097	-8988	-8987	-9096	MG	0.00	0.00	100.00
3437	-8988	-8914	-8913	-8987	MG	0.00	0.00	100.00
3437	-8980	-8906	-8905	-8979	MG	0.00	0.00	100.00
3437	-9435	-9369	-9368	-9434	MG	0.00	0.00	100.00
3437	-9212	-9154	-9153	-9211	MG	0.00	0.00	100.00
3437	-9154	-9096	-9076	-9153	MG	0.00	0.00	100.00
3437	-9096	-8987	-8986	-9076	MG	0.00	0.00	100.00
3437	-9544	-9476	-9502	-9543	MG	0.00	0.00	100.00
3437	-9476	-9434	-9433	-9502	MG	0.00	0.00	100.00
3437	-8633	-8544	-8543	-8632	MG	0.00	0.00	100.00
3437	-8544	-8484	-8483	-8543	MG	0.00	0.00	100.00
3437	-9153	-9076	-9075	-9152	MG	0.00	0.00	100.00
3437	-8905	-8806	-8839	-8904	MG	0.00	0.00	100.00
3437	-9439	-9373	-9372	-9438	MG	0.00	0.00	100.00
3437	-9738	-9638	-9637	-9737	MG	0.00	0.00	100.00
3437	-9638	-9596	-9595	-9637	MG	0.00	0.00	100.00
3437	-8632	-8543	-8542	-8631	MG	0.00	0.00	100.00
3437	-8725	-8632	-8631	-8724	MG	0.00	0.00	100.00
3437	-9484	-9438	-9437	-9483	MG	0.00	0.00	100.00
3437	-8913	-8842	-8787	-8912	MG	0.00	0.00	100.00
3437	-9737	-9637	-9636	-9736	MG	0.00	0.00	100.00
3437	-8842	-8724	-8723	-8787	MG	0.00	0.00	100.00
3437	-8542	-8474	-8473	-8541	MG	0.00	0.00	100.00
3437	-9592	-9544	-9543	-9591	MG	0.00	0.00	100.00
3437	-8472	-8423	-8422	-8478	MG	0.00	0.00	100.00
3437	-8987	-8913	-8912	-8986	MG	0.00	0.00	100.00
3437	-9434	-9368	-9367	-9433	MG	0.00	0.00	100.00
3437	-8630	-8541	-8540	-8622	MG	0.00	0.00	100.00
3437	-9206	-9148	-9147	-9205	MG	0.00	0.00	100.00
3437	-9546	-9478	-9477	-9545	MG	0.00	0.00	100.00
3437	-9478	-9436	-9435	-9477	MG	0.00	0.00	100.00
3437	-9292	-9216	-9215	-9291	MG	0.00	0.00	100.00
3437	-9216	-9158	-9157	-9215	MG	0.00	0.00	100.00
3437	-9635	-9593	-9592	-9634	MG	0.00	0.00	100.00
3437	-9593	-9545	-9544	-9592	MG	0.00	0.00	100.00
3437	-9545	-9477	-9476	-9544	MG	0.00	0.00	100.00
3437	-8477	-8418	-8417	-8468	MG	0.00	0.00	100.00
3437	-9291	-9215	-9214	-9290	MG	0.00	0.00	100.00
3437	-9735	-9634	-9633	-9734	MG	0.00	0.00	100.00
3437	-9634	-9592	-9591	-9633	MG	0.00	0.00	100.00
3437	-8536	-8472	-8478	-8535	MG	0.00	0.00	100.00
3437	-9286	-9210	-9209	-9285	MG	0.00	0.00	100.00
3437	-8906	-8807	-8806	-8905	MG	0.00	0.00	100.00
3437	-9378	-9287	-9286	-9377	MG	0.00	0.00	100.00
3437	-8535	-8478	-8471	-8534	MG	0.00	0.00	100.00
3437	-8478	-8422	-8421	-8471	MG	0.00	0.00	100.00
3437	-9203	-9145	-9144	-9202	MG	0.00	0.00	100.00
3437	-9551	-9550	-9598	-9599	MG	0.00	0.00	100.00
3437	-9070	-8978	-8977	-9069	MG	0.00	0.00	100.00
3437	-9145	-9070	-9069	-9144	MG	0.00	0.00	100.00
3437	-9158	-9100	-9099	-9157	MG	0.00	0.00	100.00
3437	-8531	-8477	-8468	-8530	MG	0.00	0.00	100.00
3437	-9144	-9069	-9093	-9143	MG	0.00	0.00	100.00
3437	-9071	-8980	-8979	-9094	MG	0.00	0.00	100.00
3437	-8619	-8535	-8534	-8618	MG	0.00	0.00	100.00
3437	-8627	-8531	-8530	-8615	MG	0.00	0.00	100.00
3437	-9280	-9204	-9203	-9279	MG	0.00	0.00	100.00
3437	-8163	-8037	-8036	-8162	MG	0.00	0.00	100.00
3437	-8978	-8904	-8903	-8977	MG	0.00	0.00	100.00
3437	-8843	-8725	-8724	-8842	MG	0.00	0.00	100.00

3437	-8807	-8717	-8716	-8806	MG	0.00	0.00	100.00
3437	-8717	-8619	-8618	-8716	MG	0.00	0.00	100.00
3437	-9072	-8981	-8980	-9071	MG	0.00	0.00	100.00
3437	-8713	-8627	-8615	-8712	MG	0.00	0.00	100.00
3437	-9210	-9152	-9151	-9209	MG	0.00	0.00	100.00
3438	-10036	-6505	-6598	-10128	MG	0.00	0.00	100.00
3438	-9376	-5606	-5818	-9442	MG	0.00	0.00	100.00
3438	-9642	-6103	-6002	-9740	MG	0.00	0.00	100.00
3438	-8984	-5398	-5621	-9074	MG	0.00	0.00	100.00
3438	-9847	-6222	-6438	-9970	MG	0.00	0.00	100.00
3438	-9486	-6037	-6105	-9552	MG	0.00	0.00	100.00
3438	-9552	-6105	-6173	-9600	MG	0.00	0.00	100.00
3438	-10196	-6496	-6382	-10251	MG	0.00	0.00	100.00
3438	-9209	-5774	-5690	-9285	MG	0.00	0.00	100.00
3438	-9285	-5690	-5606	-9376	MG	0.00	0.00	100.00
3438	-9151	-5702	-5774	-9209	MG	0.00	0.00	100.00
3438	-9740	-6002	-6222	-9847	MG	0.00	0.00	100.00
3438	-9074	-5621	-5702	-9151	MG	0.00	0.00	100.00
3438	-9970	-6438	-6505	-10036	MG	0.00	0.00	100.00
3438	-10128	-6598	-6496	-10196	MG	0.00	0.00	100.00
3438	-9442	-5818	-6037	-9486	MG	0.00	0.00	100.00
3438	-9600	-6173	-6103	-9642	MG	0.00	0.00	100.00
3440	-7008	-7494	-7495	-6240	MG	0.00	0.00	100.00
3443	-7973	-5013	-4950	-7972	MG	0.00	0.00	100.00
3447	-4815	-4421	-8423	-8424	MG	0.00	0.00	100.00
3448	-8423	-5418	-5352	-8422	MG	0.00	0.00	100.00
3451	-5215	-4888	-8907	-8908	MG	0.00	0.00	100.00
3451	-4888	-5807	-8907	-8907	MG	0.00	0.00	100.00
3452	-6170	-6259	-6926	-6926	MG	0.00	0.00	100.00
3453	-5306	-6221	-9373	-9373	MG	0.00	0.00	100.00
3471	-6692	-6152	-6691	-6691	MG	0.00	0.00	100.00
3474	-7145	-6559	-7144	-7144	MG	0.00	0.00	100.00
3474	-6559	-5853	-7143	-7144	MG	0.00	0.00	100.00
3478	-7009	-6253	-7505	-7506	MG	0.00	0.00	100.00
3482	-4951	-5014	-7977	-7978	MG	0.00	0.00	100.00
3484	-5353	-5397	-8427	-8428	MG	0.00	0.00	100.00
3485	-4422	-4816	-8426	-8427	MG	0.00	0.00	100.00
3487	-5817	-4897	-8911	-8911	MG	0.00	0.00	100.00
3487	-4897	-5216	-8910	-8911	MG	0.00	0.00	100.00
3490	-6927	-6269	-6171	-6171	MG	0.00	0.00	100.00
3491	-6230	-5307	-9377	-9377	MG	0.00	0.00	100.00
3494	-6578	-5784	-6699	-6699	MG	0.00	0.00	100.00
3494	-6578	-6699	-7309	-7309	MG	0.00	0.00	100.00
3495	-5766	-6700	-6579	-6579	MG	0.00	0.00	100.00
3495	-7310	-6700	-6579	-6579	MG	0.00	0.00	100.00
3553	-7021	-7156	-7727	-7727	MG	0.00	0.00	100.00
3554	-6107	-6382	-10251	3302	MG	0.00	0.00	100.00
3554	-7022	-7092	3302	-10252	MG	0.00	0.00	100.00
3554	-7092	-6107	3302	3302	MG	0.00	0.00	100.00
3555	3301	-7091	-7021	-10248	MG	0.00	0.00	100.00
3555	-6380	-6106	3301	-10249	MG	0.00	0.00	100.00
3555	-6106	-7091	3301	3301	MG	0.00	0.00	100.00
3556	-7728	-7157	-7022	-7022	MG	0.00	0.00	100.00
3569	-7008	-7493	-7494	-7494	MG	0.00	0.00	100.00
3572	-7357	-7968	-7969	-7969	MG	0.00	0.00	100.00
3572	-7357	-7969	-7970	-6674	MG	0.00	0.00	100.00
3577	-7814	-8419	-8420	-7147	MG	0.00	0.00	100.00
3577	-7814	-8418	-8419	-8419	MG	0.00	0.00	100.00
3579	-8907	-5807	-5781	-8906	MG	0.00	0.00	100.00
3581	-9373	-6221	-6170	-9372	MG	0.00	0.00	100.00
3582	-5605	-5306	-9373	-9374	MG	0.00	0.00	100.00
3583	-8326	-8902	-8903	-8903	MG	0.00	0.00	100.00
3583	-8326	-8903	-8904	-7509	MG	0.00	0.00	100.00
3599	-7507	-7009	-7506	-7506	MG	0.00	0.00	100.00
3601	-7358	-6694	-7980	-7981	MG	0.00	0.00	100.00
3601	-7982	-7358	-7981	-7981	MG	0.00	0.00	100.00
3605	-8432	-7815	-8431	-8431	MG	0.00	0.00	100.00
3605	-7815	-7148	-8430	-8431	MG	0.00	0.00	100.00
3607	-5773	-5817	-8911	-8912	MG	0.00	0.00	100.00
3609	-8916	-8327	-8915	-8915	MG	0.00	0.00	100.00
3609	-8327	-7510	-8914	-8915	MG	0.00	0.00	100.00
3611	-6171	-6230	-9377	-9378	MG	0.00	0.00	100.00
3612	-5307	-5606	-9376	-9377	MG	0.00	0.00	100.00
3614	-9382	-8730	-9381	-9381	MG	0.00	0.00	100.00
3614	-8730	-7985	-9380	-9381	MG	0.00	0.00	100.00
3616	-8729	-9368	-9369	-9369	MG	0.00	0.00	100.00
3616	-8729	-9369	-9370	-7984	MG	0.00	0.00	100.00
3618	-5691	-6659	-9739	-9739	MG	0.00	0.00	100.00
3618	-6001	-5691	-9739	-9727	MG	0.00	0.00	100.00

3618	-9739	-6659	-6578	-9738	MG	0.00	0.00	100.00
3620	-5692	-6002	-9740	-9741	MG	0.00	0.00	100.00
3620	-6579	-6660	-9741	-9742	MG	0.00	0.00	100.00
3620	-6660	-5692	-9741	-9741	MG	0.00	0.00	100.00
3622	-9746	-9218	-9745	-9745	MG	0.00	0.00	100.00
3622	-9218	-8435	-9744	-9745	MG	0.00	0.00	100.00
3624	-9217	-9735	-9726	-9726	MG	0.00	0.00	100.00
3624	-9217	-9726	-9736	-8434	MG	0.00	0.00	100.00
3627	-9608	-10244	-10245	-10245	MG	0.00	0.00	100.00
3627	-9608	-10245	-10246	-8918	MG	0.00	0.00	100.00
3629	-10256	-9609	-10255	-10255	MG	0.00	0.00	100.00
3629	-9609	-8919	-10254	-10255	MG	0.00	0.00	100.00
3824	-4583	-4588	-4572	-4571	MG	0.00	0.00	100.00
3824	-4611	-4594	-4597	-4625	MG	0.00	0.00	100.00
3824	-4626	-4611	-4625	-4625	MG	0.00	0.00	100.00
3824	-4621	-4603	-4601	-4620	MG	0.00	0.00	100.00
3824	-4652	-4635	-4634	-4651	MG	0.00	0.00	100.00
3824	-4589	-4598	-4608	-4592	MG	0.00	0.00	100.00
3824	-4607	-4583	-4592	-4608	MG	0.00	0.00	100.00
3824	-4573	-4570	-4558	-4555	MG	0.00	0.00	100.00
3824	-4651	-4634	-4633	-4650	MG	0.00	0.00	100.00
3824	-4536	-4527	-4531	-4531	MG	0.00	0.00	100.00
3824	-4594	-4579	-4590	-4597	MG	0.00	0.00	100.00
3824	-4579	-4569	-4574	-4590	MG	0.00	0.00	100.00
3824	-4569	-4554	-4562	-4574	MG	0.00	0.00	100.00
3824	-4554	-4541	-4551	-4562	MG	0.00	0.00	100.00
3824	-4541	-4539	-4545	-4551	MG	0.00	0.00	100.00
3824	-4583	-4607	-4604	-4588	MG	0.00	0.00	100.00
3824	-4649	-4632	-4631	-4648	MG	0.00	0.00	100.00
3824	-4634	-4620	-4619	-4633	MG	0.00	0.00	100.00
3824	-4648	-4631	-4636	-4653	MG	0.00	0.00	100.00
3824	-4631	-4617	-4616	-4636	MG	0.00	0.00	100.00
3824	-4636	-4616	-4615	-4638	MG	0.00	0.00	100.00
3824	-4615	-4614	-4640	-4638	MG	0.00	0.00	100.00
3824	-4614	-4613	-4629	-4640	MG	0.00	0.00	100.00
3824	-4613	-4612	-4627	-4629	MG	0.00	0.00	100.00
3824	-4627	-4642	-4644	-4629	MG	0.00	0.00	100.00
3824	-4642	-4659	-4663	-4644	MG	0.00	0.00	100.00
3824	-4562	-4551	-4558	-4570	MG	0.00	0.00	100.00
3824	-4545	-4555	-4558	-4551	MG	0.00	0.00	100.00
3824	-4570	-4573	-4587	-4586	MG	0.00	0.00	100.00
3824	-4650	-4633	-4632	-4649	MG	0.00	0.00	100.00
3824	-4633	-4619	-4618	-4632	MG	0.00	0.00	100.00
3824	-4597	-4590	-4591	-4609	MG	0.00	0.00	100.00
3824	-4591	-4590	-4574	-4586	MG	0.00	0.00	100.00
3824	-4586	-4587	-4605	-4606	MG	0.00	0.00	100.00
3824	-4632	-4618	-4617	-4631	MG	0.00	0.00	100.00
3824	-4629	-4644	-4646	-4640	MG	0.00	0.00	100.00
3824	-4644	-4663	-4661	-4646	MG	0.00	0.00	100.00
3824	-4646	-4661	-4657	-4640	MG	0.00	0.00	100.00
3824	-4532	-4528	-4537	-4537	MG	0.00	0.00	100.00
3824	-4635	-4621	-4620	-4634	MG	0.00	0.00	100.00
3824	-4653	-4636	-4638	-4655	MG	0.00	0.00	100.00
3824	-4655	-4638	-4640	-4657	MG	0.00	0.00	100.00
3824	-4660	-4643	-4645	-4664	MG	0.00	0.00	100.00
3824	-4643	-4628	-4630	-4645	MG	0.00	0.00	100.00
3824	-4628	-4626	-4625	-4630	MG	0.00	0.00	100.00
3824	-4625	-4624	-4641	-4630	MG	0.00	0.00	100.00
3824	-4624	-4623	-4639	-4641	MG	0.00	0.00	100.00
3824	-4623	-4622	-4637	-4639	MG	0.00	0.00	100.00
3824	-4637	-4622	-4621	-4635	MG	0.00	0.00	100.00
3824	-4654	-4637	-4635	-4652	MG	0.00	0.00	100.00
3824	-4539	-4532	-4537	-4545	MG	0.00	0.00	100.00
3824	-4537	-4550	-4555	-4545	MG	0.00	0.00	100.00
3824	-4550	-4567	-4573	-4555	MG	0.00	0.00	100.00
3824	-4567	-4585	-4587	-4573	MG	0.00	0.00	100.00
3824	-4585	-4603	-4605	-4587	MG	0.00	0.00	100.00
3824	-4603	-4621	-4622	-4605	MG	0.00	0.00	100.00
3824	-4622	-4623	-4606	-4605	MG	0.00	0.00	100.00
3824	-4623	-4624	-4609	-4606	MG	0.00	0.00	100.00
3824	-4624	-4625	-4597	-4609	MG	0.00	0.00	100.00
3824	-4658	-4662	-4647	-4641	MG	0.00	0.00	100.00
3824	-4662	-4664	-4645	-4647	MG	0.00	0.00	100.00
3824	-4647	-4645	-4630	-4641	MG	0.00	0.00	100.00
3824	-4639	-4637	-4654	-4656	MG	0.00	0.00	100.00
3824	-4639	-4656	-4658	-4641	MG	0.00	0.00	100.00
3824	-4570	-4586	-4574	-4562	MG	0.00	0.00	100.00
3824	-4606	-4609	-4591	-4586	MG	0.00	0.00	100.00
3824	-4603	-4585	-4582	-4601	MG	0.00	0.00	100.00

3824	-4585	-4567	-4565	-4582	MG	0.00	0.00	100.00
3824	-4567	-4550	-4548	-4565	MG	0.00	0.00	100.00
3824	-4550	-4537	-4535	-4548	MG	0.00	0.00	100.00
3824	-4537	-4528	-4526	-4535	MG	0.00	0.00	100.00
3824	-4620	-4601	-4599	-4619	MG	0.00	0.00	100.00
3824	-4601	-4582	-4580	-4599	MG	0.00	0.00	100.00
3824	-4582	-4565	-4563	-4580	MG	0.00	0.00	100.00
3824	-4565	-4548	-4546	-4563	MG	0.00	0.00	100.00
3824	-4548	-4535	-4533	-4546	MG	0.00	0.00	100.00
3824	-4535	-4526	-4524	-4533	MG	0.00	0.00	100.00
3824	-4619	-4599	-4600	-4618	MG	0.00	0.00	100.00
3824	-4599	-4580	-4581	-4600	MG	0.00	0.00	100.00
3824	-4580	-4563	-4564	-4581	MG	0.00	0.00	100.00
3824	-4563	-4546	-4547	-4564	MG	0.00	0.00	100.00
3824	-4546	-4533	-4534	-4547	MG	0.00	0.00	100.00
3824	-4533	-4524	-4525	-4534	MG	0.00	0.00	100.00
3824	-4618	-4600	-4602	-4617	MG	0.00	0.00	100.00
3824	-4600	-4581	-4584	-4602	MG	0.00	0.00	100.00
3824	-4581	-4564	-4566	-4584	MG	0.00	0.00	100.00
3824	-4564	-4547	-4549	-4566	MG	0.00	0.00	100.00
3824	-4547	-4534	-4536	-4549	MG	0.00	0.00	100.00
3824	-4534	-4525	-4527	-4536	MG	0.00	0.00	100.00
3824	-4610	-4612	-4613	-4613	MG	0.00	0.00	100.00
3824	-4602	-4584	-4588	-4604	MG	0.00	0.00	100.00
3824	-4584	-4566	-4572	-4588	MG	0.00	0.00	100.00
3824	-4566	-4549	-4556	-4572	MG	0.00	0.00	100.00
3824	-4549	-4536	-4544	-4556	MG	0.00	0.00	100.00
3824	-4536	-4531	-4538	-4544	MG	0.00	0.00	100.00
3824	-4538	-4540	-4552	-4544	MG	0.00	0.00	100.00
3824	-4540	-4553	-4561	-4552	MG	0.00	0.00	100.00
3824	-4553	-4568	-4575	-4561	MG	0.00	0.00	100.00
3824	-4568	-4578	-4589	-4575	MG	0.00	0.00	100.00
3824	-4578	-4593	-4598	-4589	MG	0.00	0.00	100.00
3824	-4593	-4610	-4613	-4598	MG	0.00	0.00	100.00
3824	-4613	-4614	-4608	-4598	MG	0.00	0.00	100.00
3824	-4614	-4615	-4607	-4608	MG	0.00	0.00	100.00
3824	-4615	-4616	-4604	-4607	MG	0.00	0.00	100.00
3824	-4617	-4602	-4604	-4616	MG	0.00	0.00	100.00
3824	-4544	-4552	-4557	-4556	MG	0.00	0.00	100.00
3824	-4561	-4571	-4557	-4552	MG	0.00	0.00	100.00
3824	-4572	-4556	-4557	-4571	MG	0.00	0.00	100.00
3824	-4575	-4583	-4571	-4561	MG	0.00	0.00	100.00
3824	-4575	-4589	-4592	-4583	MG	0.00	0.00	100.00

Elenco carichi elementi bidimensionali

Condizione di carico n. 4: Variabili impalc. (pieno)

Carichi uniformi

Bid.	N1	N2	N3	N4	TDC	Qx <daN/mq>	Qy <daN/mq>	Qz <daN/mq>
2718	-3859	-3858	-3909	-3910	MG	0.00	0.00	500.00
2718	-3676	-3664	-3712	-3719	MG	0.00	0.00	500.00
2718	-3665	-3676	-3719	-3720	MG	0.00	0.00	500.00
2718	-3572	-3571	-3610	-3611	MG	0.00	0.00	500.00
2718	-3719	-3712	-3768	-3769	MG	0.00	0.00	500.00
2718	-3720	-3719	-3769	-3765	MG	0.00	0.00	500.00
2718	-3610	-3609	-3664	-3676	MG	0.00	0.00	500.00
2718	-3571	-3570	-3609	-3610	MG	0.00	0.00	500.00
2718	-3769	-3768	-3810	-3811	MG	0.00	0.00	500.00
2718	-3765	-3769	-3811	-3812	MG	0.00	0.00	500.00
2718	-3858	-3857	-3908	-3909	MG	0.00	0.00	500.00
2718	-3957	-3950	-4000	-4001	MG	0.00	0.00	500.00
2718	-3812	-3811	-3858	-3859	MG	0.00	0.00	500.00
2718	-3909	-3908	-3950	-3957	MG	0.00	0.00	500.00
2718	-3958	-3957	-4001	-4002	MG	0.00	0.00	500.00
2718	-3811	-3810	-3857	-3858	MG	0.00	0.00	500.00
2718	-3525	-3524	-3571	-3572	MG	0.00	0.00	500.00
2718	-3910	-3909	-3957	-3958	MG	0.00	0.00	500.00
2718	-3524	-3523	-3570	-3571	MG	0.00	0.00	500.00
2718	-3611	-3610	-3676	-3665	MG	0.00	0.00	500.00
2816	-3655	-3748	-4148	-4148	MG	0.00	0.00	500.00
2817	-3947	-4038	-4403	-4403	MG	0.00	0.00	500.00
2822	-4219	-3663	-4295	-4295	MG	0.00	0.00	500.00
2843	-4149	-3749	-3656	-3656	MG	0.00	0.00	500.00
2847	-4404	-4039	-3948	-3948	MG	0.00	0.00	500.00
2848	-3659	-4296	-4220	-4220	MG	0.00	0.00	500.00
2921	-4198	-4683	-4684	-4684	MG	0.00	0.00	500.00
2921	-4198	-4684	-4685	-3732	MG	0.00	0.00	500.00
2931	-6370	-3558	-3605	-6483	MG	0.00	0.00	500.00

2933	-6102	-3664	-3712	-6001	MG	0.00	0.00	500.00
2933	-6036	-3523	-3570	-6104	MG	0.00	0.00	500.00
2933	-6104	-3570	-3609	-6172	MG	0.00	0.00	500.00
2933	-6172	-3609	-3664	-6102	MG	0.00	0.00	500.00
2933	-6001	-3712	-3768	-6206	MG	0.00	0.00	500.00
2934	-4219	-4295	-4870	-4870	MG	0.00	0.00	500.00
2935	-4670	-4653	-4655	-4672	MG	0.00	0.00	500.00
2935	-4676	-4661	-4663	-4679	MG	0.00	0.00	500.00
2935	-4804	-4747	-4746	-4803	MG	0.00	0.00	500.00
2935	-4746	-4687	-4686	-4745	MG	0.00	0.00	500.00
2935	-4858	-4803	-4802	-4857	MG	0.00	0.00	500.00
2935	-4676	-4674	-4657	-4661	MG	0.00	0.00	500.00
2935	-4864	-4809	-4808	-4863	MG	0.00	0.00	500.00
2935	-4671	-4654	-4652	-4669	MG	0.00	0.00	500.00
2935	-4747	-4688	-4687	-4746	MG	0.00	0.00	500.00
2935	-4690	-4689	-4748	-4749	MG	0.00	0.00	500.00
2935	-4697	-4680	-4677	-4696	MG	0.00	0.00	500.00
2935	-4672	-4655	-4657	-4674	MG	0.00	0.00	500.00
2935	-4855	-4800	-4799	-4854	MG	0.00	0.00	500.00
2935	-4803	-4746	-4745	-4802	MG	0.00	0.00	500.00
2935	-4669	-4652	-4651	-4668	MG	0.00	0.00	500.00
2935	-4754	-4695	-4694	-4753	MG	0.00	0.00	500.00
2935	-4859	-4804	-4803	-4858	MG	0.00	0.00	500.00
2935	-4755	-4696	-4695	-4754	MG	0.00	0.00	500.00
2935	-4813	-4756	-4755	-4812	MG	0.00	0.00	500.00
2935	-4802	-4745	-4744	-4801	MG	0.00	0.00	500.00
2935	-4656	-4673	-4675	-4658	MG	0.00	0.00	500.00
2935	-4812	-4755	-4754	-4811	MG	0.00	0.00	500.00
2935	-4867	-4812	-4811	-4866	MG	0.00	0.00	500.00
2935	-4748	-4689	-4688	-4747	MG	0.00	0.00	500.00
2935	-4666	-4649	-4648	-4665	MG	0.00	0.00	500.00
2935	-4688	-4665	-4670	-4687	MG	0.00	0.00	500.00
2935	-4694	-4695	-4675	-4673	MG	0.00	0.00	500.00
2935	-4698	-4681	-4680	-4697	MG	0.00	0.00	500.00
2935	-4749	-4748	-4805	-4806	MG	0.00	0.00	500.00
2935	-4752	-4693	-4692	-4751	MG	0.00	0.00	500.00
2935	-4809	-4752	-4751	-4808	MG	0.00	0.00	500.00
2935	-4751	-4692	-4691	-4750	MG	0.00	0.00	500.00
2935	-4807	-4806	-4861	-4862	MG	0.00	0.00	500.00
2935	-4745	-4686	-4685	-4744	MG	0.00	0.00	500.00
2935	-4692	-4669	-4668	-4691	MG	0.00	0.00	500.00
2935	-4857	-4802	-4801	-4856	MG	0.00	0.00	500.00
2935	-4667	-4650	-4649	-4666	MG	0.00	0.00	500.00
2935	-4689	-4666	-4665	-4688	MG	0.00	0.00	500.00
2935	-4810	-4753	-4752	-4809	MG	0.00	0.00	500.00
2935	-4686	-4687	-4670	-4672	MG	0.00	0.00	500.00
2935	-4856	-4801	-4800	-4855	MG	0.00	0.00	500.00
2935	-4668	-4651	-4650	-4667	MG	0.00	0.00	500.00
2935	-4669	-4692	-4693	-4671	MG	0.00	0.00	500.00
2935	-4665	-4648	-4653	-4670	MG	0.00	0.00	500.00
2935	-4696	-4677	-4675	-4695	MG	0.00	0.00	500.00
2935	-4744	-4685	-4684	-4743	MG	0.00	0.00	500.00
2935	-4805	-4748	-4747	-4804	MG	0.00	0.00	500.00
2935	-4756	-4697	-4696	-4755	MG	0.00	0.00	500.00
2935	-4677	-4680	-4664	-4662	MG	0.00	0.00	500.00
2935	-4686	-4672	-4674	-4685	MG	0.00	0.00	500.00
2935	-4681	-4660	-4664	-4680	MG	0.00	0.00	500.00
2935	-4753	-4694	-4693	-4752	MG	0.00	0.00	500.00
2935	-4684	-4685	-4674	-4676	MG	0.00	0.00	500.00
2935	-4656	-4654	-4671	-4673	MG	0.00	0.00	500.00
2935	-4750	-4749	-4806	-4807	MG	0.00	0.00	500.00
2935	-4690	-4667	-4666	-4689	MG	0.00	0.00	500.00
2935	-4742	-4683	-4682	-4741	MG	0.00	0.00	500.00
2935	-4868	-4813	-4812	-4867	MG	0.00	0.00	500.00
2935	-4808	-4751	-4750	-4807	MG	0.00	0.00	500.00
2935	-4866	-4811	-4810	-4865	MG	0.00	0.00	500.00
2935	-4691	-4668	-4667	-4690	MG	0.00	0.00	500.00
2935	-4694	-4673	-4671	-4693	MG	0.00	0.00	500.00
2935	-4691	-4690	-4749	-4750	MG	0.00	0.00	500.00
2935	-4801	-4744	-4743	-4800	MG	0.00	0.00	500.00
2935	-4865	-4810	-4809	-4864	MG	0.00	0.00	500.00
2935	-4814	-4757	-4756	-4813	MG	0.00	0.00	500.00
2935	-4659	-4678	-4679	-4663	MG	0.00	0.00	500.00
2935	-4869	-4814	-4813	-4868	MG	0.00	0.00	500.00
2935	-4811	-4754	-4753	-4810	MG	0.00	0.00	500.00
2935	-4799	-4742	-4741	-4798	MG	0.00	0.00	500.00
2935	-4854	-4799	-4798	-4853	MG	0.00	0.00	500.00
2935	-4684	-4676	-4679	-4683	MG	0.00	0.00	500.00
2935	-4683	-4679	-4678	-4682	MG	0.00	0.00	500.00

2935	-4757	-4698	-4697	-4756	MG	0.00	0.00	500.00
2935	-4743	-4684	-4683	-4742	MG	0.00	0.00	500.00
2935	-4677	-4662	-4658	-4675	MG	0.00	0.00	500.00
2935	-4860	-4805	-4804	-4859	MG	0.00	0.00	500.00
2935	-4806	-4805	-4860	-4861	MG	0.00	0.00	500.00
2935	-4800	-4743	-4742	-4799	MG	0.00	0.00	500.00
2935	-4863	-4808	-4807	-4862	MG	0.00	0.00	500.00
2937	-6372	-3559	-3606	-6485	MG	0.00	0.00	500.00
2939	-6105	-3572	-3611	-6173	MG	0.00	0.00	500.00
2939	-6037	-3525	-3572	-6105	MG	0.00	0.00	500.00
2939	-6002	-3720	-3765	-6222	MG	0.00	0.00	500.00
2939	-6173	-3611	-3665	-6103	MG	0.00	0.00	500.00
2939	-6103	-3665	-3720	-6002	MG	0.00	0.00	500.00
2940	-4459	-3955	-4711	-4711	MG	0.00	0.00	500.00
2944	-5352	-3764	-4471	-4471	MG	0.00	0.00	500.00
2945	-4697	-4199	-4696	-4696	MG	0.00	0.00	500.00
2945	-4199	-3733	-4695	-4696	MG	0.00	0.00	500.00
2953	-4871	-4296	-4220	-4220	MG	0.00	0.00	500.00
2954	-3949	-4712	-4460	-4460	MG	0.00	0.00	500.00
2955	-5353	-4463	-3767	-3767	MG	0.00	0.00	500.00
3007	-3763	-4003	-6107	-5257	MG	0.00	0.00	500.00
3008	-3999	-3766	-5256	-6106	MG	0.00	0.00	500.00
3022	-4445	-5039	-5040	-4019	MG	0.00	0.00	500.00
3031	-6689	-3536	-3698	-6748	MG	0.00	0.00	500.00
3031	-6620	-3590	-3536	-6689	MG	0.00	0.00	500.00
3031	-6483	-3605	-3657	-6548	MG	0.00	0.00	500.00
3031	-6548	-3657	-3590	-6620	MG	0.00	0.00	500.00
3032	-6206	-3768	-3810	-6437	MG	0.00	0.00	500.00
3032	-6437	-3810	-3857	-6501	MG	0.00	0.00	500.00
3033	-3607	-4251	-7136	-7136	MG	0.00	0.00	500.00
3034	-5041	-4976	-4992	-5040	MG	0.00	0.00	500.00
3034	-4918	-4855	-4854	-4917	MG	0.00	0.00	500.00
3034	-5042	-4968	-4976	-5041	MG	0.00	0.00	500.00
3034	-4932	-4866	-4865	-4931	MG	0.00	0.00	500.00
3034	-4967	-4918	-4917	-4966	MG	0.00	0.00	500.00
3034	-5048	-4995	-4979	-5047	MG	0.00	0.00	500.00
3034	-4926	-4860	-4859	-4925	MG	0.00	0.00	500.00
3034	-4861	-4860	-4926	-4927	MG	0.00	0.00	500.00
3034	-4994	-4930	-4929	-4978	MG	0.00	0.00	500.00
3034	-4929	-4863	-4862	-4928	MG	0.00	0.00	500.00
3034	-4924	-4858	-4857	-4919	MG	0.00	0.00	500.00
3034	-4978	-4929	-4928	-4970	MG	0.00	0.00	500.00
3034	-4927	-4926	-4969	-4993	MG	0.00	0.00	500.00
3034	-4925	-4859	-4858	-4924	MG	0.00	0.00	500.00
3034	-4976	-4919	-4923	-4992	MG	0.00	0.00	500.00
3034	-4995	-4932	-4931	-4979	MG	0.00	0.00	500.00
3034	-5046	-4994	-4978	2902	MG	0.00	0.00	500.00
3034	-4969	-4926	-4925	-4977	MG	0.00	0.00	500.00
3034	-4919	-4857	-4856	-4923	MG	0.00	0.00	500.00
3034	-5051	-4997	-4980	-5050	MG	0.00	0.00	500.00
3034	2902	-4978	-4970	-5045	MG	0.00	0.00	500.00
3034	-5043	-4969	-4977	2901	MG	0.00	0.00	500.00
3034	-4920	-4867	-4866	-4932	MG	0.00	0.00	500.00
3034	-4992	-4923	-4918	-4967	MG	0.00	0.00	500.00
3034	-4996	-4920	-4932	-4995	MG	0.00	0.00	500.00
3034	-4923	-4856	-4855	-4918	MG	0.00	0.00	500.00
3034	-4930	-4864	-4863	-4929	MG	0.00	0.00	500.00
3034	-4997	-4934	-4933	-4980	MG	0.00	0.00	500.00
3034	-5039	-4967	-4966	-5038	MG	0.00	0.00	500.00
3034	2901	-4977	-4968	-5042	MG	0.00	0.00	500.00
3034	-4993	-4969	-5043	-5044	MG	0.00	0.00	500.00
3034	-4931	-4865	-4864	-4930	MG	0.00	0.00	500.00
3034	-4862	-4861	-4927	-4928	MG	0.00	0.00	500.00
3034	-5040	-4992	-4967	-5039	MG	0.00	0.00	500.00
3034	-4970	-4993	-5044	-5045	MG	0.00	0.00	500.00
3034	-4934	-4869	-4868	-4933	MG	0.00	0.00	500.00
3034	-4968	-4924	-4919	-4976	MG	0.00	0.00	500.00
3034	-4917	-4854	-4853	-4916	MG	0.00	0.00	500.00
3034	-5050	-4980	-4996	-5049	MG	0.00	0.00	500.00
3034	-5047	-4979	-4994	-5046	MG	0.00	0.00	500.00
3034	-4928	-4927	-4993	-4970	MG	0.00	0.00	500.00
3034	-4979	-4931	-4930	-4994	MG	0.00	0.00	500.00
3034	-5049	-4996	-4995	-5048	MG	0.00	0.00	500.00
3034	-4977	-4925	-4924	-4968	MG	0.00	0.00	500.00
3034	-4933	-4868	-4867	-4920	MG	0.00	0.00	500.00
3034	-5038	-4966	-4991	-5037	MG	0.00	0.00	500.00
3034	-4966	-4917	-4916	-4991	MG	0.00	0.00	500.00
3034	-4980	-4933	-4920	-4996	MG	0.00	0.00	500.00
3036	-6485	-3606	-3658	-6550	MG	0.00	0.00	500.00

3036	-6550	-3658	-3591	-6622	MG	0.00	0.00	500.00
3036	-6672	-3537	-3699	-6750	MG	0.00	0.00	500.00
3036	-6622	-3591	-3537	-6672	MG	0.00	0.00	500.00
3038	-4459	-4711	-5284	-5284	MG	0.00	0.00	500.00
3039	-6438	-3812	-3859	-6505	MG	0.00	0.00	500.00
3039	-6222	-3765	-3812	-6438	MG	0.00	0.00	500.00
3041	-4950	-4223	-5065	-5065	MG	0.00	0.00	500.00
3052	-4446	-4020	-5048	-5049	MG	0.00	0.00	500.00
3060	-4252	-3608	-7140	-7140	MG	0.00	0.00	500.00
3061	-5285	-4712	-4460	-4460	MG	0.00	0.00	500.00
3062	-4224	-5066	-4951	-4951	MG	0.00	0.00	500.00
3106	-4000	-3999	-6106	-6380	MG	0.00	0.00	500.00
3107	-4003	-4002	-6382	-6107	MG	0.00	0.00	500.00
3119	-4445	-5038	-5039	-5039	MG	0.00	0.00	500.00
3120	-4935	-5432	-5433	-4281	MG	0.00	0.00	500.00
3121	-6244	-3696	-3655	-6243	MG	0.00	0.00	500.00
3129	-7297	-4167	-4221	-7347	MG	0.00	0.00	500.00
3129	-6915	-3904	-3963	-6998	MG	0.00	0.00	500.00
3129	-6833	-3842	-3904	-6915	MG	0.00	0.00	500.00
3129	-7463	-4164	-4104	-7499	MG	0.00	0.00	500.00
3129	-7200	-3987	-4124	-7263	MG	0.00	0.00	500.00
3129	-6998	-3963	-3887	-7057	MG	0.00	0.00	500.00
3129	-7499	-4104	-4253	-7578	MG	0.00	0.00	500.00
3129	-7263	-4124	-4167	-7297	MG	0.00	0.00	500.00
3129	-7347	-4221	-4164	-7463	MG	0.00	0.00	500.00
3129	-6748	-3698	-3842	-6833	MG	0.00	0.00	500.00
3129	-7057	-3887	-3825	-7137	MG	0.00	0.00	500.00
3129	-7137	-3825	-3987	-7200	MG	0.00	0.00	500.00
3130	-6501	-3857	-3908	-6597	MG	0.00	0.00	500.00
3130	-6495	-3950	-4000	-6380	MG	0.00	0.00	500.00
3130	-6597	-3908	-3950	-6495	MG	0.00	0.00	500.00
3131	-5116	-5040	-5039	-5115	MG	0.00	0.00	500.00
3131	-5671	-5602	-5601	-5670	MG	0.00	0.00	500.00
3131	-5663	-5594	-5593	-5662	MG	0.00	0.00	500.00
3131	-5435	-5373	-5372	-5434	MG	0.00	0.00	500.00
3131	-5741	-5732	-5797	-5798	MG	0.00	0.00	500.00
3131	-5119	2901	-5042	-5118	MG	0.00	0.00	500.00
3131	-5129	-5051	-5050	-5128	MG	0.00	0.00	500.00
3131	-5200	-5115	-5114	-5199	MG	0.00	0.00	500.00
3131	-5325	-5274	-5273	-5324	MG	0.00	0.00	500.00
3131	-5795	-5731	-5730	-5794	MG	0.00	0.00	500.00
3131	-5594	-5499	-5498	-5593	MG	0.00	0.00	500.00
3131	-5592	-5497	-5496	-5591	MG	0.00	0.00	500.00
3131	-5204	-5119	-5118	-5203	MG	0.00	0.00	500.00
3131	-5277	-5212	-5211	-5276	MG	0.00	0.00	500.00
3131	-5591	-5496	-5495	-5590	MG	0.00	0.00	500.00
3131	-5203	-5118	-5117	-5202	MG	0.00	0.00	500.00
3131	-5805	-5744	-5736	-5804	MG	0.00	0.00	500.00
3131	-5735	-5670	-5669	-5734	MG	0.00	0.00	500.00
3131	-5505	-5442	-5441	-5504	MG	0.00	0.00	500.00
3131	-5432	-5370	-5369	-5431	MG	0.00	0.00	500.00
3131	-5445	-5383	-5382	-5444	MG	0.00	0.00	500.00
3131	-5744	-5673	-5672	-5736	MG	0.00	0.00	500.00
3131	-5120	-5043	2901	-5119	MG	0.00	0.00	500.00
3131	-5379	-5325	-5324	-5378	MG	0.00	0.00	500.00
3131	-5439	-5438	-5501	-5502	MG	0.00	0.00	500.00
3131	-5731	-5663	-5662	-5730	MG	0.00	0.00	500.00
3131	-5508	-5445	-5444	-5507	MG	0.00	0.00	500.00
3131	-5728	-5660	-5659	-5727	MG	0.00	0.00	500.00
3131	-5660	-5591	-5590	-5659	MG	0.00	0.00	500.00
3131	-5496	-5433	-5432	-5495	MG	0.00	0.00	500.00
3131	-5665	-5664	-5740	-5732	MG	0.00	0.00	500.00
3131	-5802	-5735	-5734	-5801	MG	0.00	0.00	500.00
3131	-5730	-5662	-5661	-5729	MG	0.00	0.00	500.00
3131	-5370	-5316	-5315	-5369	MG	0.00	0.00	500.00
3131	-5214	-5129	-5128	-5213	MG	0.00	0.00	500.00
3131	-5803	-5743	-5735	-5802	MG	0.00	0.00	500.00
3131	-5743	-5671	-5670	-5735	MG	0.00	0.00	500.00
3131	-5210	-5125	-5124	-5209	MG	0.00	0.00	500.00
3131	-5128	-5050	-5049	-5127	MG	0.00	0.00	500.00
3131	-5801	-5734	-5742	-5800	MG	0.00	0.00	500.00
3131	-5661	-5592	-5591	-5660	MG	0.00	0.00	500.00
3131	-5734	-5669	-5668	-5742	MG	0.00	0.00	500.00
3131	-5320	-5269	-5268	-5319	MG	0.00	0.00	500.00
3131	-5269	-5204	-5203	-5268	MG	0.00	0.00	500.00
3131	-5497	-5434	-5433	-5496	MG	0.00	0.00	500.00
3131	-5201	-5116	-5115	-5200	MG	0.00	0.00	500.00
3131	-5206	-5205	-5270	-5271	MG	0.00	0.00	500.00
3131	-5207	-5206	-5271	-5272	MG	0.00	0.00	500.00

3131	-5327	-5276	-5275	-5326	MG	0.00	0.00	500.00
3131	-5436	-5374	-5373	-5435	MG	0.00	0.00	500.00
3131	-5276	-5211	-5210	-5275	MG	0.00	0.00	500.00
3131	-5727	-5659	-5658	-5726	MG	0.00	0.00	500.00
3131	-5590	-5495	-5494	-5589	MG	0.00	0.00	500.00
3131	-5045	-5044	-5121	-5122	MG	0.00	0.00	500.00
3131	-5315	-5264	-5263	-5314	MG	0.00	0.00	500.00
3131	-5275	-5210	-5209	-5274	MG	0.00	0.00	500.00
3131	-5446	-5384	-5383	-5445	MG	0.00	0.00	500.00
3131	-5125	-5047	-5046	-5124	MG	0.00	0.00	500.00
3131	-5664	-5595	-5594	-5663	MG	0.00	0.00	500.00
3131	-5437	-5375	-5374	-5436	MG	0.00	0.00	500.00
3131	-5500	-5437	-5436	-5499	MG	0.00	0.00	500.00
3131	-5597	-5596	-5665	-5666	MG	0.00	0.00	500.00
3131	-5440	-5378	-5377	-5439	MG	0.00	0.00	500.00
3131	-5274	-5209	-5208	-5273	MG	0.00	0.00	500.00
3131	-5499	-5436	-5435	-5498	MG	0.00	0.00	500.00
3131	-5265	-5200	-5199	-5264	MG	0.00	0.00	500.00
3131	-5316	-5265	-5264	-5315	MG	0.00	0.00	500.00
3131	-5794	-5730	-5729	-5793	MG	0.00	0.00	500.00
3131	-5273	-5208	-5207	-5272	MG	0.00	0.00	500.00
3131	-5279	-5214	-5213	-5278	MG	0.00	0.00	500.00
3131	-5670	-5601	-5600	-5669	MG	0.00	0.00	500.00
3131	-5601	-5506	-5505	-5600	MG	0.00	0.00	500.00
3131	-5278	-5213	-5212	-5277	MG	0.00	0.00	500.00
3131	-5369	-5315	-5314	-5368	MG	0.00	0.00	500.00
3131	-5213	-5128	-5127	-5212	MG	0.00	0.00	500.00
3131	-5270	-5205	-5204	-5269	MG	0.00	0.00	500.00
3131	-5264	-5199	-5198	-5263	MG	0.00	0.00	500.00
3131	-5328	-5277	-5276	-5327	MG	0.00	0.00	500.00
3131	-5382	-5328	-5327	-5381	MG	0.00	0.00	500.00
3131	-5377	-5376	-5438	-5439	MG	0.00	0.00	500.00
3131	-5792	-5728	-5727	-5791	MG	0.00	0.00	500.00
3131	-5212	-5127	-5126	-5211	MG	0.00	0.00	500.00
3131	-5127	-5049	-5048	-5126	MG	0.00	0.00	500.00
3131	-5443	-5381	-5380	-5442	MG	0.00	0.00	500.00
3131	-5373	-5319	-5318	-5372	MG	0.00	0.00	500.00
3131	-5791	-5727	-5726	-5790	MG	0.00	0.00	500.00
3131	-5268	-5203	-5202	-5267	MG	0.00	0.00	500.00
3131	-5501	-5500	-5595	-5596	MG	0.00	0.00	500.00
3131	-5380	-5326	-5325	-5379	MG	0.00	0.00	500.00
3131	-5495	-5432	-5431	-5494	MG	0.00	0.00	500.00
3131	-5790	-5726	-5725	-5789	MG	0.00	0.00	500.00
3131	-5796	-5740	-5731	-5795	MG	0.00	0.00	500.00
3131	-5726	-5658	-5657	-5725	MG	0.00	0.00	500.00
3131	-5595	-5500	-5499	-5594	MG	0.00	0.00	500.00
3131	-5371	-5317	-5316	-5370	MG	0.00	0.00	500.00
3131	-5494	-5431	-5430	-5493	MG	0.00	0.00	500.00
3131	-5441	-5379	-5378	-5440	MG	0.00	0.00	500.00
3131	-5266	-5201	-5200	-5265	MG	0.00	0.00	500.00
3131	-5666	-5665	-5732	-5741	MG	0.00	0.00	500.00
3131	-5272	-5271	-5322	-5323	MG	0.00	0.00	500.00
3131	-5324	-5273	-5272	-5323	MG	0.00	0.00	500.00
3131	-5507	-5444	-5443	-5506	MG	0.00	0.00	500.00
3131	-5330	-5279	-5278	-5329	MG	0.00	0.00	500.00
3131	-5124	-5046	2902	-5123	MG	0.00	0.00	500.00
3131	-5502	-5501	-5596	-5597	MG	0.00	0.00	500.00
3131	-5732	-5740	-5796	-5797	MG	0.00	0.00	500.00
3131	-5383	-5329	-5328	-5382	MG	0.00	0.00	500.00
3131	-5329	-5278	-5277	-5328	MG	0.00	0.00	500.00
3131	-5205	-5120	-5119	-5204	MG	0.00	0.00	500.00
3131	-5506	-5443	-5442	-5505	MG	0.00	0.00	500.00
3131	-5321	-5270	-5269	-5320	MG	0.00	0.00	500.00
3131	-5374	-5320	-5319	-5373	MG	0.00	0.00	500.00
3131	-5199	-5114	-5113	-5198	MG	0.00	0.00	500.00
3131	-5669	-5600	-5599	-5668	MG	0.00	0.00	500.00
3131	-5376	-5375	-5437	-5438	MG	0.00	0.00	500.00
3131	-5600	-5505	-5504	-5599	MG	0.00	0.00	500.00
3131	-5326	-5275	-5274	-5325	MG	0.00	0.00	500.00
3131	-5271	-5270	-5321	-5322	MG	0.00	0.00	500.00
3131	-5599	-5504	-5503	-5598	MG	0.00	0.00	500.00
3131	-5381	-5327	-5326	-5380	MG	0.00	0.00	500.00
3131	-5211	-5126	-5125	-5210	MG	0.00	0.00	500.00
3131	-5659	-5590	-5589	-5658	MG	0.00	0.00	500.00
3131	-5673	-5604	-5603	-5672	MG	0.00	0.00	500.00
3131	-5442	-5380	-5379	-5441	MG	0.00	0.00	500.00
3131	-5317	-5266	-5265	-5316	MG	0.00	0.00	500.00
3131	-5503	-5440	-5439	-5502	MG	0.00	0.00	500.00
3131	-5509	-5446	-5445	-5508	MG	0.00	0.00	500.00

3131	-5740	-5664	-5663	-5731	MG	0.00	0.00	500.00
3131	-5202	-5117	-5116	-5201	MG	0.00	0.00	500.00
3131	-5589	-5494	-5493	-5588	MG	0.00	0.00	500.00
3131	-5433	-5371	-5370	-5432	MG	0.00	0.00	500.00
3131	-5603	-5508	-5507	-5602	MG	0.00	0.00	500.00
3131	-5596	-5595	-5664	-5665	MG	0.00	0.00	500.00
3131	-5208	-5123	-5122	-5207	MG	0.00	0.00	500.00
3131	-5602	-5507	-5506	-5601	MG	0.00	0.00	500.00
3131	-5323	-5322	-5376	-5377	MG	0.00	0.00	500.00
3131	-5378	-5324	-5323	-5377	MG	0.00	0.00	500.00
3131	-5319	-5268	-5267	-5318	MG	0.00	0.00	500.00
3131	-5742	-5668	-5667	-5733	MG	0.00	0.00	500.00
3131	-5504	-5441	-5440	-5503	MG	0.00	0.00	500.00
3131	-5114	-5038	-5037	-5113	MG	0.00	0.00	500.00
3131	-5672	-5603	-5602	-5671	MG	0.00	0.00	500.00
3131	-5431	-5369	-5368	-5430	MG	0.00	0.00	500.00
3131	-5729	-5661	-5660	-5728	MG	0.00	0.00	500.00
3131	-5793	-5729	-5728	-5792	MG	0.00	0.00	500.00
3131	-5438	-5437	-5500	-5501	MG	0.00	0.00	500.00
3131	-5267	-5202	-5201	-5266	MG	0.00	0.00	500.00
3131	-5658	-5589	-5588	-5657	MG	0.00	0.00	500.00
3131	-5209	-5124	-5123	-5208	MG	0.00	0.00	500.00
3131	-5126	-5048	-5047	-5125	MG	0.00	0.00	500.00
3131	-5118	-5042	-5041	-5117	MG	0.00	0.00	500.00
3131	-5372	-5318	-5317	-5371	MG	0.00	0.00	500.00
3131	-5122	-5121	-5206	-5207	MG	0.00	0.00	500.00
3131	-5121	-5120	-5205	-5206	MG	0.00	0.00	500.00
3131	-5668	-5599	-5598	-5667	MG	0.00	0.00	500.00
3131	-5604	-5509	-5508	-5603	MG	0.00	0.00	500.00
3131	-5598	-5503	-5502	-5597	MG	0.00	0.00	500.00
3131	-5322	-5321	-5375	-5376	MG	0.00	0.00	500.00
3131	-5117	-5041	-5040	-5116	MG	0.00	0.00	500.00
3131	-5115	-5039	-5038	-5114	MG	0.00	0.00	500.00
3131	-5733	-5667	-5666	-5741	MG	0.00	0.00	500.00
3131	-5804	-5736	-5743	-5803	MG	0.00	0.00	500.00
3131	-5318	-5267	-5266	-5317	MG	0.00	0.00	500.00
3131	-5044	-5043	-5120	-5121	MG	0.00	0.00	500.00
3131	-5667	-5598	-5597	-5666	MG	0.00	0.00	500.00
3131	-5498	-5435	-5434	-5497	MG	0.00	0.00	500.00
3131	-5593	-5498	-5497	-5592	MG	0.00	0.00	500.00
3131	-5736	-5672	-5671	-5743	MG	0.00	0.00	500.00
3131	-5384	-5330	-5329	-5383	MG	0.00	0.00	500.00
3131	-5662	-5593	-5592	-5661	MG	0.00	0.00	500.00
3131	-5444	-5382	-5381	-5443	MG	0.00	0.00	500.00
3131	-5375	-5321	-5320	-5374	MG	0.00	0.00	500.00
3131	-5434	-5372	-5371	-5433	MG	0.00	0.00	500.00
3131	-5800	-5742	-5733	-5799	MG	0.00	0.00	500.00
3131	-5799	-5733	-5741	-5798	MG	0.00	0.00	500.00
3131	-5123	2902	-5045	-5122	MG	0.00	0.00	500.00
3132	-6598	-3910	-3958	-6496	MG	0.00	0.00	500.00
3132	-6496	-3958	-4002	-6382	MG	0.00	0.00	500.00
3132	-6505	-3859	-3910	-6598	MG	0.00	0.00	500.00
3133	-7139	-3826	-3988	-7202	MG	0.00	0.00	500.00
3133	-7465	-4165	-4105	-7501	MG	0.00	0.00	500.00
3133	-6835	-3843	-3905	-6917	MG	0.00	0.00	500.00
3133	-6917	-3905	-3964	-7000	MG	0.00	0.00	500.00
3133	-7202	-3988	-4125	-7265	MG	0.00	0.00	500.00
3133	-6750	-3699	-3843	-6835	MG	0.00	0.00	500.00
3133	-7059	-3888	-3826	-7139	MG	0.00	0.00	500.00
3133	-7299	-4168	-4222	-7349	MG	0.00	0.00	500.00
3133	-7349	-4222	-4165	-7465	MG	0.00	0.00	500.00
3133	-7000	-3964	-3888	-7059	MG	0.00	0.00	500.00
3133	-7501	-4105	-4254	-7579	MG	0.00	0.00	500.00
3133	-7265	-4125	-4168	-7299	MG	0.00	0.00	500.00
3138	-5781	-4065	-4964	-4964	MG	0.00	0.00	500.00
3139	-5306	-3674	-6221	-6221	MG	0.00	0.00	500.00
3147	-5050	-4446	-5049	-5049	MG	0.00	0.00	500.00
3150	-4936	-4282	-5443	-5444	MG	0.00	0.00	500.00
3152	-3656	-3697	-6247	-6248	MG	0.00	0.00	500.00
3156	-5773	-4965	-4066	-4066	MG	0.00	0.00	500.00
3157	-3675	-5307	-6230	-6230	MG	0.00	0.00	500.00
3205	-5256	-4235	-7091	-7091	MG	0.00	0.00	500.00
3206	-4236	-5257	-7092	-7092	MG	0.00	0.00	500.00
3207	-4001	-4000	-6380	-6381	MG	0.00	0.00	500.00
3207	-4002	-4001	-6381	-6382	MG	0.00	0.00	500.00
3219	-4935	-5431	-5432	-5432	MG	0.00	0.00	500.00
3222	-5333	-5837	-5838	-4699	MG	0.00	0.00	500.00
3222	-5333	-5836	-5837	-5837	MG	0.00	0.00	500.00
3229	-6670	-3985	-3947	-6669	MG	0.00	0.00	500.00

3231	-7710	-4419	-4461	-7805	MG	0.00	0.00	500.00
3231	-7928	-4417	-4362	-7974	MG	0.00	0.00	500.00
3231	-7974	-4362	-4494	-8028	MG	0.00	0.00	500.00
3231	-7805	-4461	-4417	-7928	MG	0.00	0.00	500.00
3231	-7661	-4378	-4419	-7710	MG	0.00	0.00	500.00
3231	-7578	-4253	-4378	-7661	MG	0.00	0.00	500.00
3232	-3825	-3607	-7136	-7137	MG	0.00	0.00	500.00
3233	-7136	-4251	-4219	-7135	MG	0.00	0.00	500.00
3234	-5987	-5878	-5877	-5986	MG	0.00	0.00	500.00
3234	-5888	-5846	-5845	-5887	MG	0.00	0.00	500.00
3234	-6067	-6066	-6134	-6135	MG	0.00	0.00	500.00
3234	-6060	-5987	-5986	-6059	MG	0.00	0.00	500.00
3234	-6070	-5996	-5995	-6069	MG	0.00	0.00	500.00
3234	-6130	-6062	-6061	-6129	MG	0.00	0.00	500.00
3234	-5989	-5880	-5879	-5988	MG	0.00	0.00	500.00
3234	-6249	-6197	-6196	-6239	MG	0.00	0.00	500.00
3234	-6193	-6194	-6137	-6136	MG	0.00	0.00	500.00
3234	-6250	-6198	-6197	-6249	MG	0.00	0.00	500.00
3234	-6142	-6074	-6073	-6141	MG	0.00	0.00	500.00
3234	-6073	-5999	-5998	-6072	MG	0.00	0.00	500.00
3234	-5878	-5836	-5835	-5877	MG	0.00	0.00	500.00
3234	-6185	-6128	-6127	-6184	MG	0.00	0.00	500.00
3234	-5891	-5849	-5848	-5890	MG	0.00	0.00	500.00
3234	-6252	-6200	-6199	-6251	MG	0.00	0.00	500.00
3234	-6000	-5892	-5891	-5999	MG	0.00	0.00	500.00
3234	-5838	-5792	-5791	-5837	MG	0.00	0.00	500.00
3234	-6199	-6142	-6141	-6198	MG	0.00	0.00	500.00
3234	-6068	-6067	-6135	-6136	MG	0.00	0.00	500.00
3234	-5999	-5891	-5890	-5998	MG	0.00	0.00	500.00
3234	-6248	-6195	-6194	-6247	MG	0.00	0.00	500.00
3234	-6136	-6135	-6192	-6193	MG	0.00	0.00	500.00
3234	-6138	-6070	-6069	-6137	MG	0.00	0.00	500.00
3234	-6187	-6130	-6129	-6186	MG	0.00	0.00	500.00
3234	-6236	-6187	-6186	-6235	MG	0.00	0.00	500.00
3234	-5798	-5797	-5843	-5844	MG	0.00	0.00	500.00
3234	-5847	-5801	-5800	-5846	MG	0.00	0.00	500.00
3234	-6198	-6141	-6140	-6197	MG	0.00	0.00	500.00
3234	-6068	-6069	-5995	-6025	MG	0.00	0.00	500.00
3234	-6242	-6185	-6184	-6234	MG	0.00	0.00	500.00
3234	-6246	-6247	-6194	-6193	MG	0.00	0.00	500.00
3234	-5886	-5887	-5845	-5844	MG	0.00	0.00	500.00
3234	-6128	-6060	-6059	-6127	MG	0.00	0.00	500.00
3234	-6238	-6191	-6190	-6244	MG	0.00	0.00	500.00
3234	-6074	-6000	-5999	-6073	MG	0.00	0.00	500.00
3234	-5892	-5850	-5849	-5891	MG	0.00	0.00	500.00
3234	-5884	-5842	-5841	-5883	MG	0.00	0.00	500.00
3234	-5846	-5800	-5799	-5845	MG	0.00	0.00	500.00
3234	-5848	-5802	-5801	-5847	MG	0.00	0.00	500.00
3234	-5837	-5791	-5790	-5836	MG	0.00	0.00	500.00
3234	-5885	-5884	-5993	-5994	MG	0.00	0.00	500.00
3234	-5992	-5883	-5882	-5991	MG	0.00	0.00	500.00
3234	-6140	-6072	-6071	-6139	MG	0.00	0.00	500.00
3234	-5839	-5793	-5792	-5838	MG	0.00	0.00	500.00
3234	-6025	-5995	-5887	-5886	MG	0.00	0.00	500.00
3234	-5882	-5840	-5839	-5881	MG	0.00	0.00	500.00
3234	-5890	-5848	-5847	-5889	MG	0.00	0.00	500.00
3234	-5851	-5805	-5804	-5850	MG	0.00	0.00	500.00
3234	-6244	-6190	-6189	-6243	MG	0.00	0.00	500.00
3234	-6063	-5990	-5989	-6062	MG	0.00	0.00	500.00
3234	-5990	-5881	-5880	-5989	MG	0.00	0.00	500.00
3234	-6196	-6139	-6138	-6195	MG	0.00	0.00	500.00
3234	-5881	-5839	-5838	-5880	MG	0.00	0.00	500.00
3234	-5843	-5842	-5884	-5885	MG	0.00	0.00	500.00
3234	-5797	-5796	-5842	-5843	MG	0.00	0.00	500.00
3234	-5842	-5796	-5795	-5841	MG	0.00	0.00	500.00
3234	-6062	-5989	-5988	-6061	MG	0.00	0.00	500.00
3234	-5840	-5794	-5793	-5839	MG	0.00	0.00	500.00
3234	-5988	-5879	-5878	-5987	MG	0.00	0.00	500.00
3234	-5996	-5888	-5887	-5995	MG	0.00	0.00	500.00
3234	-5998	-5890	-5889	-5997	MG	0.00	0.00	500.00
3234	-6129	-6061	-6060	-6128	MG	0.00	0.00	500.00
3234	-5972	-5893	-5892	-6000	MG	0.00	0.00	500.00
3234	-5880	-5838	-5837	-5879	MG	0.00	0.00	500.00
3234	-6075	-5972	-6000	-6074	MG	0.00	0.00	500.00
3234	-5879	-5837	-5836	-5878	MG	0.00	0.00	500.00
3234	-5883	-5841	-5840	-5882	MG	0.00	0.00	500.00
3234	-6061	-5988	-5987	-6060	MG	0.00	0.00	500.00
3234	-6134	-6066	-6065	-6133	MG	0.00	0.00	500.00
3234	-6066	-5993	-5992	-6065	MG	0.00	0.00	500.00

3234	-5993	-5884	-5883	-5992	MG	0.00	0.00	500.00
3234	-5997	-5889	-5888	-5996	MG	0.00	0.00	500.00
3234	-6141	-6073	-6072	-6140	MG	0.00	0.00	500.00
3234	-6133	-6065	-6064	-6132	MG	0.00	0.00	500.00
3234	-6239	-6196	-6195	-6248	MG	0.00	0.00	500.00
3234	-6188	-6131	-6130	-6187	MG	0.00	0.00	500.00
3234	-6065	-5992	-5991	-6064	MG	0.00	0.00	500.00
3234	-5845	-5799	-5798	-5844	MG	0.00	0.00	500.00
3234	-6064	-5991	-5990	-6063	MG	0.00	0.00	500.00
3234	-5994	-5993	-6066	-6067	MG	0.00	0.00	500.00
3234	-5991	-5882	-5881	-5990	MG	0.00	0.00	500.00
3234	-5841	-5795	-5794	-5840	MG	0.00	0.00	500.00
3234	-6195	-6138	-6137	-6194	MG	0.00	0.00	500.00
3234	-5886	-5885	-5994	-6025	MG	0.00	0.00	500.00
3234	-6131	-6063	-6062	-6130	MG	0.00	0.00	500.00
3234	-6237	-6188	-6187	-6236	MG	0.00	0.00	500.00
3234	-6192	-6191	-6238	-6245	MG	0.00	0.00	500.00
3234	-6071	-5997	-5996	-6070	MG	0.00	0.00	500.00
3234	-6193	-6192	-6245	-6246	MG	0.00	0.00	500.00
3234	-5889	-5847	-5846	-5888	MG	0.00	0.00	500.00
3234	-5836	-5790	-5789	-5835	MG	0.00	0.00	500.00
3234	-6251	-6199	-6198	-6250	MG	0.00	0.00	500.00
3234	-5893	-5851	-5850	-5892	MG	0.00	0.00	500.00
3234	-6200	-6143	-6142	-6199	MG	0.00	0.00	500.00
3234	-5844	-5843	-5885	-5886	MG	0.00	0.00	500.00
3234	-6186	-6129	-6128	-6185	MG	0.00	0.00	500.00
3234	-6136	-6137	-6069	-6068	MG	0.00	0.00	500.00
3234	-6132	-6064	-6063	-6131	MG	0.00	0.00	500.00
3234	-5849	-5803	-5802	-5848	MG	0.00	0.00	500.00
3234	-6025	-5994	-6067	-6068	MG	0.00	0.00	500.00
3234	-6190	-6133	-6132	-6189	MG	0.00	0.00	500.00
3234	-6243	-6189	-6188	-6237	MG	0.00	0.00	500.00
3234	-5850	-5804	-5803	-5849	MG	0.00	0.00	500.00
3234	-6191	-6134	-6133	-6190	MG	0.00	0.00	500.00
3234	-6139	-6071	-6070	-6138	MG	0.00	0.00	500.00
3234	-6189	-6132	-6131	-6188	MG	0.00	0.00	500.00
3234	-6072	-5998	-5997	-6071	MG	0.00	0.00	500.00
3234	-6135	-6134	-6191	-6192	MG	0.00	0.00	500.00
3234	-6143	-6075	-6074	-6142	MG	0.00	0.00	500.00
3234	-6197	-6140	-6139	-6196	MG	0.00	0.00	500.00
3234	-6235	-6186	-6185	-6242	MG	0.00	0.00	500.00
3235	-7579	-4254	-4379	-7666	MG	0.00	0.00	500.00
3235	-7666	-4379	-4420	-7712	MG	0.00	0.00	500.00
3235	-7976	-4363	-4503	-8030	MG	0.00	0.00	500.00
3235	-7930	-4418	-4363	-7976	MG	0.00	0.00	500.00
3235	-7807	-4462	-4418	-7930	MG	0.00	0.00	500.00
3235	-7712	-4420	-4462	-7807	MG	0.00	0.00	500.00
3236	-4104	-3906	-7498	-7499	MG	0.00	0.00	500.00
3236	-3906	-4492	-7498	-7498	MG	0.00	0.00	500.00
3239	-4950	-5065	-5674	-5674	MG	0.00	0.00	500.00
3240	-4169	-5013	-7973	-7973	MG	0.00	0.00	500.00
3242	-5352	-4471	-5458	-5458	MG	0.00	0.00	500.00
3242	-5352	-5458	-6100	-6100	MG	0.00	0.00	500.00
3245	-5781	-4964	-5854	-5854	MG	0.00	0.00	500.00
3246	-6170	-4322	-5356	-5356	MG	0.00	0.00	500.00
3246	-6221	-3674	-4322	-6170	MG	0.00	0.00	500.00
3255	-5445	-4936	-5444	-5444	MG	0.00	0.00	500.00
3257	-5334	-4700	-5848	-5849	MG	0.00	0.00	500.00
3257	-5850	-5334	-5849	-5849	MG	0.00	0.00	500.00
3259	-3948	-3986	-6673	-6677	MG	0.00	0.00	500.00
3264	-4220	-4252	-7140	-7141	MG	0.00	0.00	500.00
3266	-3608	-3826	-7139	-7140	MG	0.00	0.00	500.00
3267	-4493	-3907	-7502	-7502	MG	0.00	0.00	500.00
3267	-3907	-4105	-7501	-7502	MG	0.00	0.00	500.00
3268	-5681	-5066	-4951	-4951	MG	0.00	0.00	500.00
3269	-5014	-4170	-7977	-7977	MG	0.00	0.00	500.00
3270	-4463	-5459	-5353	-5353	MG	0.00	0.00	500.00
3270	-6101	-5459	-5353	-5353	MG	0.00	0.00	500.00
3271	-4965	-5855	-5773	-5773	MG	0.00	0.00	500.00
3272	-4323	-3675	-6230	-6171	MG	0.00	0.00	500.00
3272	-6171	-5357	-4323	-4323	MG	0.00	0.00	500.00
3273	-6578	-4758	-5784	-5784	MG	0.00	0.00	500.00
3273	-5691	-3956	-6659	-6659	MG	0.00	0.00	500.00
3273	-6659	-3956	-4758	-6578	MG	0.00	0.00	500.00
3274	-4759	-3969	-6660	-6579	MG	0.00	0.00	500.00
3274	-6579	-5766	-4759	-4759	MG	0.00	0.00	500.00
3274	-3969	-5692	-6660	-6660	MG	0.00	0.00	500.00
3305	-5257	-6107	-7092	-7092	MG	0.00	0.00	500.00
3307	-6106	-5256	-7091	-7091	MG	0.00	0.00	500.00

3308	-7022	-6175	-5131	-5131	MG	0.00	0.00	500.00
3308	-5131	-4236	-7092	-7022	MG	0.00	0.00	500.00
3309	-7091	-4235	-5130	-7021	MG	0.00	0.00	500.00
3309	-7021	-5130	-6174	-6174	MG	0.00	0.00	500.00
3325	-5746	-6242	-6235	-6235	MG	0.00	0.00	500.00
3325	-5746	-6235	-6236	-5052	MG	0.00	0.00	500.00
3331	-6151	-6667	-6688	-5447	MG	0.00	0.00	500.00
3332	-8719	-5354	-5286	-8840	MG	0.00	0.00	500.00
3332	-8840	-5286	-5215	-8908	MG	0.00	0.00	500.00
3332	-8908	-5215	-5387	-8982	MG	0.00	0.00	500.00
3332	-8479	-5001	-5254	-8537	MG	0.00	0.00	500.00
3332	-8377	-4884	-4815	-8424	MG	0.00	0.00	500.00
3332	-8228	-4886	-4952	-8316	MG	0.00	0.00	500.00
3332	-8537	-5254	-5304	-8628	MG	0.00	0.00	500.00
3332	-8028	-4494	-4841	-8154	MG	0.00	0.00	500.00
3332	-8316	-4952	-4884	-8377	MG	0.00	0.00	500.00
3332	-8154	-4841	-4886	-8228	MG	0.00	0.00	500.00
3332	-8424	-4815	-5001	-8479	MG	0.00	0.00	500.00
3332	-8628	-5304	-5354	-8719	MG	0.00	0.00	500.00
3333	-6304	-6303	-6371	-6372	MG	0.00	0.00	500.00
3333	-6999	-6998	-7057	-7058	MG	0.00	0.00	500.00
3333	-6917	-6916	-6999	-7000	MG	0.00	0.00	500.00
3333	-6378	-6310	-6309	-6377	MG	0.00	0.00	500.00
3333	-6828	-6743	-6742	-6827	MG	0.00	0.00	500.00
3333	-6301	-6244	-6243	-6300	MG	0.00	0.00	500.00
3333	-6303	-6302	-6370	-6371	MG	0.00	0.00	500.00
3333	-6916	-6915	-6998	-6999	MG	0.00	0.00	500.00
3333	-7061	-7002	-7001	-7060	MG	0.00	0.00	500.00
3333	-6833	-6748	-6747	-6832	MG	0.00	0.00	500.00
3333	-7141	-7061	-7060	-7140	MG	0.00	0.00	500.00
3333	-6834	-6833	-6915	-6916	MG	0.00	0.00	500.00
3333	-6374	-6306	-6305	-6373	MG	0.00	0.00	500.00
3333	-6624	-6539	-6551	-6623	MG	0.00	0.00	500.00
3333	-6994	-6911	-6910	-6993	MG	0.00	0.00	500.00
3333	-7140	-7060	-7059	-7139	MG	0.00	0.00	500.00
3333	-6993	-6910	-6909	-6992	MG	0.00	0.00	500.00
3333	-6379	-6311	-6310	-6378	MG	0.00	0.00	500.00
3333	-6842	-6757	-6756	-6841	MG	0.00	0.00	500.00
3333	-6364	-6296	-6295	-6363	MG	0.00	0.00	500.00
3333	-7062	-7003	-7002	-7061	MG	0.00	0.00	500.00
3333	-7003	-6920	-6919	-7002	MG	0.00	0.00	500.00
3333	-6536	-6477	-6476	-6535	MG	0.00	0.00	500.00
3333	-6484	-6483	-6548	-6549	MG	0.00	0.00	500.00
3333	-7057	-6998	-6997	-7056	MG	0.00	0.00	500.00
3333	-6302	-6238	-6244	-6301	MG	0.00	0.00	500.00
3333	-6547	-6482	-6481	-6538	MG	0.00	0.00	500.00
3333	-6369	-6301	-6300	-6368	MG	0.00	0.00	500.00
3333	-6371	-6370	-6483	-6484	MG	0.00	0.00	500.00
3333	-6485	-6484	-6549	-6550	MG	0.00	0.00	500.00
3333	-7133	-7053	-7052	-7132	MG	0.00	0.00	500.00
3333	-7000	-6999	-7058	-7059	MG	0.00	0.00	500.00
3333	-6492	-6379	-6378	-6491	MG	0.00	0.00	500.00
3333	-6368	-6300	-6299	-6367	MG	0.00	0.00	500.00
3333	-7132	-7052	-7051	-7131	MG	0.00	0.00	500.00
3333	-7136	-7056	-7055	-7135	MG	0.00	0.00	500.00
3333	-6308	-6249	-6239	-6307	MG	0.00	0.00	500.00
3333	-6678	-6625	-6624	-6677	MG	0.00	0.00	500.00
3333	-6625	-6552	-6539	-6624	MG	0.00	0.00	500.00
3333	-6671	-6689	-6748	-6749	MG	0.00	0.00	500.00
3333	-6677	-6624	-6623	-6673	MG	0.00	0.00	500.00
3333	-7146	-7066	-7065	-7145	MG	0.00	0.00	500.00
3333	-7051	-6992	-6991	-7050	MG	0.00	0.00	500.00
3333	-6299	-6237	-6236	-6298	MG	0.00	0.00	500.00
3333	-6306	-6248	-6247	-6305	MG	0.00	0.00	500.00
3333	-6748	-6689	-6670	-6747	MG	0.00	0.00	500.00
3333	-6487	-6374	-6373	-6486	MG	0.00	0.00	500.00
3333	-7056	-6997	-6996	-7055	MG	0.00	0.00	500.00
3333	-6629	-6556	-6555	-6628	MG	0.00	0.00	500.00
3333	-6832	-6747	-6746	-6831	MG	0.00	0.00	500.00
3333	-7143	-7063	-7062	-7142	MG	0.00	0.00	500.00
3333	-7055	-6996	-6995	-7054	MG	0.00	0.00	500.00
3333	-6901	-6842	-6841	-6923	MG	0.00	0.00	500.00
3333	-6297	-6235	-6242	-6296	MG	0.00	0.00	500.00
3333	-6614	-6536	-6535	-6613	MG	0.00	0.00	500.00
3333	-6754	-6690	-6678	-6753	MG	0.00	0.00	500.00
3333	-6477	-6364	-6363	-6476	MG	0.00	0.00	500.00
3333	-6375	-6307	-6306	-6374	MG	0.00	0.00	500.00
3333	-6998	-6915	-6914	-6997	MG	0.00	0.00	500.00
3333	-6619	-6547	-6538	-6618	MG	0.00	0.00	500.00

3333	-6995	-6912	-6911	-6994	MG	0.00	0.00	500.00
3333	-6246	-6245	-6303	-6304	MG	0.00	0.00	500.00
3333	-6830	-6745	-6744	-6829	MG	0.00	0.00	500.00
3333	-6482	-6369	-6368	-6481	MG	0.00	0.00	500.00
3333	-7053	-6994	-6993	-7052	MG	0.00	0.00	500.00
3333	-6377	-6309	-6308	-6376	MG	0.00	0.00	500.00
3333	-6538	-6481	-6480	-6546	MG	0.00	0.00	500.00
3333	-6835	-6834	-6916	-6917	MG	0.00	0.00	500.00
3333	-6829	-6744	-6743	-6828	MG	0.00	0.00	500.00
3333	-6481	-6368	-6367	-6480	MG	0.00	0.00	500.00
3333	-7007	-6901	-6923	-7006	MG	0.00	0.00	500.00
3333	-6300	-6243	-6237	-6299	MG	0.00	0.00	500.00
3333	-6668	-6617	-6616	-6688	MG	0.00	0.00	500.00
3333	-6757	-6693	-6692	-6756	MG	0.00	0.00	500.00
3333	-6546	-6480	-6479	-6537	MG	0.00	0.00	500.00
3333	-6307	-6239	-6248	-6306	MG	0.00	0.00	500.00
3333	-6751	-6673	-6672	-6750	MG	0.00	0.00	500.00
3333	-7131	-7051	-7050	-7130	MG	0.00	0.00	500.00
3333	-6915	-6833	-6832	-6914	MG	0.00	0.00	500.00
3333	-6537	-6479	-6478	-6545	MG	0.00	0.00	500.00
3333	-7059	-7058	-7138	-7139	MG	0.00	0.00	500.00
3333	-6742	-6687	-6666	-6741	MG	0.00	0.00	500.00
3333	-6997	-6914	-6913	-6996	MG	0.00	0.00	500.00
3333	-6922	-6840	-6839	-6921	MG	0.00	0.00	500.00
3333	-6556	-6492	-6491	-6555	MG	0.00	0.00	500.00
3333	-6840	-6755	-6754	-6839	MG	0.00	0.00	500.00
3333	-6545	-6478	-6477	-6536	MG	0.00	0.00	500.00
3333	-6311	-6252	-6251	-6310	MG	0.00	0.00	500.00
3333	-6365	-6297	-6296	-6364	MG	0.00	0.00	500.00
3333	-6921	-6839	-6838	-6920	MG	0.00	0.00	500.00
3333	-6839	-6754	-6753	-6838	MG	0.00	0.00	500.00
3333	-6491	-6378	-6377	-6490	MG	0.00	0.00	500.00
3333	-7142	-7062	-7061	-7141	MG	0.00	0.00	500.00
3333	-7134	-7054	-7053	-7133	MG	0.00	0.00	500.00
3333	-6310	-6251	-6250	-6309	MG	0.00	0.00	500.00
3333	-6912	-6830	-6829	-6911	MG	0.00	0.00	500.00
3333	-6490	-6377	-6376	-6489	MG	0.00	0.00	500.00
3333	-6753	-6678	-6677	-6752	MG	0.00	0.00	500.00
3333	-6621	-6620	-6689	-6671	MG	0.00	0.00	500.00
3333	-6549	-6548	-6620	-6621	MG	0.00	0.00	500.00
3333	-6673	-6623	-6622	-6672	MG	0.00	0.00	500.00
3333	-6618	-6538	-6546	-6617	MG	0.00	0.00	500.00
3333	-6670	-6619	-6618	-6669	MG	0.00	0.00	500.00
3333	-6752	-6677	-6673	-6751	MG	0.00	0.00	500.00
3333	-7001	-6918	-6917	-7000	MG	0.00	0.00	500.00
3333	-6376	-6308	-6307	-6375	MG	0.00	0.00	500.00
3333	-6372	-6371	-6484	-6485	MG	0.00	0.00	500.00
3333	-6550	-6549	-6621	-6622	MG	0.00	0.00	500.00
3333	-6552	-6488	-6487	-6539	MG	0.00	0.00	500.00
3333	-6488	-6375	-6374	-6487	MG	0.00	0.00	500.00
3333	-6480	-6367	-6366	-6479	MG	0.00	0.00	500.00
3333	-7145	-7065	-7064	-7144	MG	0.00	0.00	500.00
3333	-6367	-6299	-6298	-6366	MG	0.00	0.00	500.00
3333	-6992	-6909	-6900	-6991	MG	0.00	0.00	500.00
3333	-6616	-6537	-6545	-6615	MG	0.00	0.00	500.00
3333	-6539	-6487	-6486	-6551	MG	0.00	0.00	500.00
3333	-6827	-6742	-6741	-6826	MG	0.00	0.00	500.00
3333	-7058	-7057	-7137	-7138	MG	0.00	0.00	500.00
3333	-6914	-6832	-6831	-6913	MG	0.00	0.00	500.00
3333	-6623	-6551	-6550	-6622	MG	0.00	0.00	500.00
3333	-7135	-7055	-7054	-7134	MG	0.00	0.00	500.00
3333	-6551	-6486	-6485	-6550	MG	0.00	0.00	500.00
3333	-6373	-6305	-6304	-6372	MG	0.00	0.00	500.00
3333	-6996	-6913	-6912	-6995	MG	0.00	0.00	500.00
3333	-6913	-6831	-6830	-6912	MG	0.00	0.00	500.00
3333	-7137	-7057	-7056	-7136	MG	0.00	0.00	500.00
3333	-6548	-6483	-6482	-6547	MG	0.00	0.00	500.00
3333	-6620	-6548	-6547	-6619	MG	0.00	0.00	500.00
3333	-6370	-6302	-6301	-6369	MG	0.00	0.00	500.00
3333	-7054	-6995	-6994	-7053	MG	0.00	0.00	500.00
3333	-6296	-6242	-6234	-6295	MG	0.00	0.00	500.00
3333	-6622	-6621	-6671	-6672	MG	0.00	0.00	500.00
3333	-6745	-6668	-6688	-6744	MG	0.00	0.00	500.00
3333	-6838	-6753	-6752	-6837	MG	0.00	0.00	500.00
3333	-6627	-6554	-6553	-6626	MG	0.00	0.00	500.00
3333	-6690	-6626	-6625	-6678	MG	0.00	0.00	500.00
3333	-6911	-6829	-6828	-6910	MG	0.00	0.00	500.00
3333	-6626	-6553	-6552	-6625	MG	0.00	0.00	500.00
3333	-6672	-6671	-6749	-6750	MG	0.00	0.00	500.00

3333	-7066	-7007	-7006	-7065	MG	0.00	0.00	500.00
3333	-7052	-6993	-6992	-7051	MG	0.00	0.00	500.00
3333	-6489	-6376	-6375	-6488	MG	0.00	0.00	500.00
3333	-6910	-6828	-6827	-6909	MG	0.00	0.00	500.00
3333	-6617	-6546	-6537	-6616	MG	0.00	0.00	500.00
3333	-6687	-6614	-6613	-6666	MG	0.00	0.00	500.00
3333	-6746	-6669	-6668	-6745	MG	0.00	0.00	500.00
3333	-7065	-7006	-7005	-7064	MG	0.00	0.00	500.00
3333	-6743	-6667	-6687	-6742	MG	0.00	0.00	500.00
3333	-6923	-6841	-6840	-6922	MG	0.00	0.00	500.00
3333	-7144	-7064	-7063	-7143	MG	0.00	0.00	500.00
3333	-6756	-6692	-6691	-6755	MG	0.00	0.00	500.00
3333	-6841	-6756	-6755	-6840	MG	0.00	0.00	500.00
3333	-7005	-6922	-6921	-7004	MG	0.00	0.00	500.00
3333	-6298	-6236	-6235	-6297	MG	0.00	0.00	500.00
3333	-6366	-6298	-6297	-6365	MG	0.00	0.00	500.00
3333	-6755	-6691	-6690	-6754	MG	0.00	0.00	500.00
3333	-6615	-6545	-6536	-6614	MG	0.00	0.00	500.00
3333	-7063	-7004	-7003	-7062	MG	0.00	0.00	500.00
3333	-6692	-6628	-6627	-6691	MG	0.00	0.00	500.00
3333	-6628	-6555	-6554	-6627	MG	0.00	0.00	500.00
3333	-6555	-6491	-6490	-6554	MG	0.00	0.00	500.00
3333	-6750	-6749	-6834	-6835	MG	0.00	0.00	500.00
3333	-6831	-6746	-6745	-6830	MG	0.00	0.00	500.00
3333	-6483	-6370	-6369	-6482	MG	0.00	0.00	500.00
3333	-6245	-6238	-6302	-6303	MG	0.00	0.00	500.00
3333	-6693	-6629	-6628	-6692	MG	0.00	0.00	500.00
3333	-6554	-6490	-6489	-6553	MG	0.00	0.00	500.00
3333	-6691	-6627	-6626	-6690	MG	0.00	0.00	500.00
3333	-6688	-6616	-6615	-6667	MG	0.00	0.00	500.00
3333	-6836	-6751	-6750	-6835	MG	0.00	0.00	500.00
3333	-6919	-6837	-6836	-6918	MG	0.00	0.00	500.00
3333	-6669	-6618	-6617	-6668	MG	0.00	0.00	500.00
3333	-6749	-6748	-6833	-6834	MG	0.00	0.00	500.00
3333	-6747	-6670	-6669	-6746	MG	0.00	0.00	500.00
3333	-7060	-7001	-7000	-7059	MG	0.00	0.00	500.00
3333	-6305	-6247	-6246	-6304	MG	0.00	0.00	500.00
3333	-6918	-6836	-6835	-6917	MG	0.00	0.00	500.00
3333	-6689	-6620	-6619	-6670	MG	0.00	0.00	500.00
3333	-6478	-6365	-6364	-6477	MG	0.00	0.00	500.00
3333	-6479	-6366	-6365	-6478	MG	0.00	0.00	500.00
3333	-7002	-6919	-6918	-7001	MG	0.00	0.00	500.00
3333	-7006	-6923	-6922	-7005	MG	0.00	0.00	500.00
3333	-6667	-6615	-6614	-6687	MG	0.00	0.00	500.00
3333	-6909	-6827	-6826	-6900	MG	0.00	0.00	500.00
3333	-6920	-6838	-6837	-6919	MG	0.00	0.00	500.00
3333	-6553	-6489	-6488	-6552	MG	0.00	0.00	500.00
3333	-7004	-6921	-6920	-7003	MG	0.00	0.00	500.00
3333	-6486	-6373	-6372	-6485	MG	0.00	0.00	500.00
3333	-6744	-6688	-6667	-6743	MG	0.00	0.00	500.00
3333	-6837	-6752	-6751	-6836	MG	0.00	0.00	500.00
3333	-6309	-6250	-6249	-6308	MG	0.00	0.00	500.00
3333	-7064	-7005	-7004	-7063	MG	0.00	0.00	500.00
3334	-8230	-4887	-4953	-8318	MG	0.00	0.00	500.00
3334	-8481	-5002	-5255	-8539	MG	0.00	0.00	500.00
3334	-8318	-4953	-4885	-8379	MG	0.00	0.00	500.00
3334	-8030	-4503	-4842	-8156	MG	0.00	0.00	500.00
3334	-8721	-5355	-5287	-8841	MG	0.00	0.00	500.00
3334	-8156	-4842	-4887	-8230	MG	0.00	0.00	500.00
3334	-8379	-4885	-4816	-8426	MG	0.00	0.00	500.00
3334	-8426	-4816	-5002	-8481	MG	0.00	0.00	500.00
3334	-8841	-5287	-5216	-8910	MG	0.00	0.00	500.00
3334	-8629	-5305	-5355	-8721	MG	0.00	0.00	500.00
3334	-8910	-5216	-5398	-8984	MG	0.00	0.00	500.00
3334	-8539	-5255	-5305	-8629	MG	0.00	0.00	500.00
3335	-7498	-4492	-4459	-7497	MG	0.00	0.00	500.00
3339	-4362	-4169	-7973	-7974	MG	0.00	0.00	500.00
3342	-4421	-5418	-8423	-8423	MG	0.00	0.00	500.00
3345	-5781	-5854	-6493	-6493	MG	0.00	0.00	500.00
3346	-6170	-5356	-6259	-6259	MG	0.00	0.00	500.00
3364	-5747	-5053	-6249	-6250	MG	0.00	0.00	500.00
3364	-6251	-5747	-6250	-6250	MG	0.00	0.00	500.00
3372	-6152	-5448	-6690	-6691	MG	0.00	0.00	500.00
3380	-4460	-4493	-7502	-7503	MG	0.00	0.00	500.00
3384	-4170	-4363	-7976	-7977	MG	0.00	0.00	500.00
3386	-5397	-4422	-8427	-8427	MG	0.00	0.00	500.00
3388	-6494	-5855	-5773	-5773	MG	0.00	0.00	500.00
3390	-5357	-6269	-6171	-6171	MG	0.00	0.00	500.00
3424	-7021	-6174	-7156	-7156	MG	0.00	0.00	500.00

3426	-6175	-7157	-7022	-7022	MG	0.00	0.00	500.00
3435	-6151	-6687	-6667	-6667	MG	0.00	0.00	500.00
3436	-9550	-6104	-6172	-9598	MG	0.00	0.00	500.00
3436	-9073	-5620	-5701	-9149	MG	0.00	0.00	500.00
3436	-9440	-5808	-6036	-9479	MG	0.00	0.00	500.00
3436	-9727	-6001	-6206	-9855	MG	0.00	0.00	500.00
3436	-10194	-6495	-6380	-10249	MG	0.00	0.00	500.00
3436	-9968	-6437	-6501	-10034	MG	0.00	0.00	500.00
3436	-9374	-5605	-5808	-9440	MG	0.00	0.00	500.00
3436	-9207	-5783	-5689	-9283	MG	0.00	0.00	500.00
3436	-9283	-5689	-5605	-9374	MG	0.00	0.00	500.00
3436	-9479	-6036	-6104	-9550	MG	0.00	0.00	500.00
3436	-9149	-5701	-5783	-9207	MG	0.00	0.00	500.00
3436	-9598	-6172	-6102	-9640	MG	0.00	0.00	500.00
3436	-9640	-6102	-6001	-9727	MG	0.00	0.00	500.00
3436	-9855	-6206	-6437	-9968	MG	0.00	0.00	500.00
3436	-8982	-5387	-5620	-9073	MG	0.00	0.00	500.00
3436	-10034	-6501	-6597	-10126	MG	0.00	0.00	500.00
3436	-10126	-6597	-6495	-10194	MG	0.00	0.00	500.00
3437	-8229	-8228	-8316	-8317	MG	0.00	0.00	500.00
3437	-10199	-10133	-10132	-10198	MG	0.00	0.00	500.00
3437	-10257	-10201	-10200	-10256	MG	0.00	0.00	500.00
3437	-8427	-8380	-8379	-8426	MG	0.00	0.00	500.00
3437	-10122	-10030	-10029	-10121	MG	0.00	0.00	500.00
3437	-10038	-9946	-9962	-10037	MG	0.00	0.00	500.00
3437	-7974	-7928	-7927	-7973	MG	0.00	0.00	500.00
3437	-7502	-7466	-7465	-7501	MG	0.00	0.00	500.00
3437	-7971	-7925	-7924	-7970	MG	0.00	0.00	500.00
3437	-10129	-10037	-10036	-10128	MG	0.00	0.00	500.00
3437	-8911	-8808	-8841	-8910	MG	0.00	0.00	500.00
3437	-10255	-10199	-10198	-10254	MG	0.00	0.00	500.00
3437	-10041	-9972	-9971	-10040	MG	0.00	0.00	500.00
3437	-10036	-10035	-10127	-10128	MG	0.00	0.00	500.00
3437	-8424	-8377	-8376	-8423	MG	0.00	0.00	500.00
3437	3301	-10193	-10192	-10248	MG	0.00	0.00	500.00
3437	-9446	-9380	-9379	-9445	MG	0.00	0.00	500.00
3437	-10198	-10132	-10131	-10177	MG	0.00	0.00	500.00
3437	-10121	-10029	-10028	-10120	MG	0.00	0.00	500.00
3437	-7666	-7662	-7711	-7712	MG	0.00	0.00	500.00
3437	-10133	-10041	-10040	-10132	MG	0.00	0.00	500.00
3437	3302	-10176	-10196	-10251	MG	0.00	0.00	500.00
3437	-9972	-9849	-9848	-9971	MG	0.00	0.00	500.00
3437	-8984	-8983	-9095	-9074	MG	0.00	0.00	500.00
3437	-10132	-10040	-10039	-10131	MG	0.00	0.00	500.00
3437	-9968	-9855	-9854	-9945	MG	0.00	0.00	500.00
3437	-7269	-7206	-7205	-7268	MG	0.00	0.00	500.00
3437	-10030	-9944	-9943	-10029	MG	0.00	0.00	500.00
3437	-7571	-7497	-7496	-7576	MG	0.00	0.00	500.00
3437	-9557	-9505	-9493	-9556	MG	0.00	0.00	500.00
3437	-8230	-8229	-8317	-8318	MG	0.00	0.00	500.00
3437	-9447	-9381	-9380	-9446	MG	0.00	0.00	500.00
3437	-7349	-7348	-7464	-7465	MG	0.00	0.00	500.00
3437	-7257	-7194	-7193	-7256	MG	0.00	0.00	500.00
3437	-10175	-10121	-10120	-10189	MG	0.00	0.00	500.00
3437	-9493	-9446	-9445	-9488	MG	0.00	0.00	500.00
3437	-9600	-9599	-9641	-9642	MG	0.00	0.00	500.00
3437	-9962	-9857	-9847	-9970	MG	0.00	0.00	500.00
3437	-9857	-9741	-9740	-9847	MG	0.00	0.00	500.00
3437	-7348	-7347	-7463	-7464	MG	0.00	0.00	500.00
3437	-9974	-9863	-9840	-9973	MG	0.00	0.00	500.00
3437	-10127	-10126	-10194	-10195	MG	0.00	0.00	500.00
3437	-8983	-8982	-9073	-9095	MG	0.00	0.00	500.00
3437	-9445	-9379	-9378	-9444	MG	0.00	0.00	500.00
3437	-9742	-9644	-9643	-9741	MG	0.00	0.00	500.00
3437	-9644	-9602	-9601	-9643	MG	0.00	0.00	500.00
3437	-10195	-10194	-10249	-10250	MG	0.00	0.00	500.00
3437	-7468	-7352	-7351	-7467	MG	0.00	0.00	500.00
3437	-7265	-7264	-7298	-7299	MG	0.00	0.00	500.00
3437	-9444	-9378	-9377	-9443	MG	0.00	0.00	500.00
3437	-7801	-7705	-7697	-7800	MG	0.00	0.00	500.00
3437	-7705	-7655	-7654	-7697	MG	0.00	0.00	500.00
3437	-7459	-7343	-7342	-7458	MG	0.00	0.00	500.00
3437	-7501	-7500	-7572	-7579	MG	0.00	0.00	500.00
3437	-9727	-9640	-9639	-9739	MG	0.00	0.00	500.00
3437	-9648	-9606	-9605	-9647	MG	0.00	0.00	500.00
3437	-8420	-8373	-8372	-8419	MG	0.00	0.00	500.00
3437	-7472	-7356	-7355	-7471	MG	0.00	0.00	500.00
3437	-8917	-8809	-8827	-8916	MG	0.00	0.00	500.00
3437	-8433	-8386	-8385	-8432	MG	0.00	0.00	500.00

3437	-9373	-9282	-9281	-9372	MG	0.00	0.00	500.00
3437	-10246	-10190	-10175	-10245	MG	0.00	0.00	500.00
3437	-10134	-10042	-10041	-10133	MG	0.00	0.00	500.00
3437	-9747	-9649	-9648	-9746	MG	0.00	0.00	500.00
3437	-8372	-8311	-8310	-8371	MG	0.00	0.00	500.00
3437	-9485	-9479	-9550	-9551	MG	0.00	0.00	500.00
3437	-9744	-9646	-9645	-9743	MG	0.00	0.00	500.00
3437	-9646	-9604	-9603	-9645	MG	0.00	0.00	500.00
3437	-9604	-9556	-9555	-9603	MG	0.00	0.00	500.00
3437	-8423	-8376	-8375	-8422	MG	0.00	0.00	500.00
3437	-8907	-8824	-8807	-8906	MG	0.00	0.00	500.00
3437	-9740	-9728	-9856	-9847	MG	0.00	0.00	500.00
3437	-9743	-9645	-9644	-9742	MG	0.00	0.00	500.00
3437	-9645	-9603	-9602	-9644	MG	0.00	0.00	500.00
3437	-7505	-7469	-7468	-7504	MG	0.00	0.00	500.00
3437	-9555	-9488	-9504	-9554	MG	0.00	0.00	500.00
3437	-8426	-8425	-8480	-8481	MG	0.00	0.00	500.00
3437	-8539	-8538	-8621	-8629	MG	0.00	0.00	500.00
3437	-7813	-7723	-7722	-7812	MG	0.00	0.00	500.00
3437	-7723	-7671	-7670	-7722	MG	0.00	0.00	500.00
3437	-10196	-10195	-10250	-10251	MG	0.00	0.00	500.00
3437	-8424	-8423	-8472	-8479	MG	0.00	0.00	500.00
3437	-8910	-8909	-8983	-8984	MG	0.00	0.00	500.00
3437	-9074	-9095	-9150	-9151	MG	0.00	0.00	500.00
3437	-7812	-7722	-7716	-7811	MG	0.00	0.00	500.00
3437	-7722	-7670	-7669	-7716	MG	0.00	0.00	500.00
3437	-9377	-9286	-9285	-9376	MG	0.00	0.00	500.00
3437	-10254	-10198	-10177	-10253	MG	0.00	0.00	500.00
3437	-7495	-7459	-7458	-7494	MG	0.00	0.00	500.00
3437	-9847	-9856	-9969	-9970	MG	0.00	0.00	500.00
3437	-10040	-9971	-9963	-10039	MG	0.00	0.00	500.00
3437	-7807	-7806	-7929	-7930	MG	0.00	0.00	500.00
3437	-7711	-7710	-7805	-7806	MG	0.00	0.00	500.00
3437	-9506	-9448	-9447	-9505	MG	0.00	0.00	500.00
3437	-7264	-7263	-7297	-7298	MG	0.00	0.00	500.00
3437	-7138	-7137	-7200	-7201	MG	0.00	0.00	500.00
3437	-9739	-9639	-9638	-9738	MG	0.00	0.00	500.00
3437	-7715	-7668	-7643	-7721	MG	0.00	0.00	500.00
3437	-7668	-7583	-7582	-7643	MG	0.00	0.00	500.00
3437	-7583	-7505	-7504	-7582	MG	0.00	0.00	500.00
3437	-10197	-10130	-10129	-10176	MG	0.00	0.00	500.00
3437	-10130	-10038	-10037	-10129	MG	0.00	0.00	500.00
3437	-10200	-10134	-10133	-10199	MG	0.00	0.00	500.00
3437	-7291	-7257	-7256	-7290	MG	0.00	0.00	500.00
3437	-7643	-7582	-7581	-7667	MG	0.00	0.00	500.00
3437	-10176	-10129	-10128	-10196	MG	0.00	0.00	500.00
3437	-10256	-10200	-10199	-10255	MG	0.00	0.00	500.00
3437	-10037	-9962	-9970	-10036	MG	0.00	0.00	500.00
3437	-7299	-7298	-7348	-7349	MG	0.00	0.00	500.00
3437	-7714	-7667	-7663	-7713	MG	0.00	0.00	500.00
3437	-9863	-9747	-9746	-9840	MG	0.00	0.00	500.00
3437	-7581	-7503	-7502	-7580	MG	0.00	0.00	500.00
3437	-7931	-7808	-7807	-7930	MG	0.00	0.00	500.00
3437	-7808	-7713	-7712	-7807	MG	0.00	0.00	500.00
3437	-9855	-9727	-9739	-9854	MG	0.00	0.00	500.00
3437	-7663	-7580	-7579	-7666	MG	0.00	0.00	500.00
3437	-9554	-9504	-9487	-9553	MG	0.00	0.00	500.00
3437	-9504	-9444	-9443	-9487	MG	0.00	0.00	500.00
3437	-8029	-8028	-8154	-8155	MG	0.00	0.00	500.00
3437	-9643	-9601	-9600	-9642	MG	0.00	0.00	500.00
3437	-9849	-9745	-9744	-9848	MG	0.00	0.00	500.00
3437	-7710	-7661	-7660	-7709	MG	0.00	0.00	500.00
3437	-9487	-9443	-9442	-9486	MG	0.00	0.00	500.00
3437	-7935	-7811	-7810	-7934	MG	0.00	0.00	500.00
3437	-9961	-9839	-9853	-9967	MG	0.00	0.00	500.00
3437	-9856	-9855	-9968	-9969	MG	0.00	0.00	500.00
3437	-9640	-9598	-9597	-9639	MG	0.00	0.00	500.00
3437	-9598	-9550	-9549	-9597	MG	0.00	0.00	500.00
3437	-9550	-9479	-9503	-9549	MG	0.00	0.00	500.00
3437	-7499	-7463	-7462	-7498	MG	0.00	0.00	500.00
3437	-9383	-9292	-9291	-9382	MG	0.00	0.00	500.00
3437	-9853	-9737	-9736	-9838	MG	0.00	0.00	500.00
3437	-9209	-9208	-9284	-9285	MG	0.00	0.00	500.00
3437	-9208	-9207	-9283	-9284	MG	0.00	0.00	500.00
3437	-9095	-9073	-9149	-9150	MG	0.00	0.00	500.00
3437	-8721	-8720	-8825	-8841	MG	0.00	0.00	500.00
3437	-8720	-8719	-8840	-8825	MG	0.00	0.00	500.00
3437	-8538	-8537	-8628	-8621	MG	0.00	0.00	500.00
3437	-10245	-10175	-10189	-10244	MG	0.00	0.00	500.00

3437	-7658	-7576	-7570	-7657	MG	0.00	0.00	500.00
3437	-7576	-7496	-7495	-7570	MG	0.00	0.00	500.00
3437	-9943	-9852	-9837	-9942	MG	0.00	0.00	500.00
3437	-7924	-7802	-7779	-7923	MG	0.00	0.00	500.00
3437	-7802	-7698	-7706	-7779	MG	0.00	0.00	500.00
3437	-7698	-7657	-7656	-7706	MG	0.00	0.00	500.00
3437	-7657	-7570	-7569	-7656	MG	0.00	0.00	500.00
3437	-7570	-7495	-7494	-7569	MG	0.00	0.00	500.00
3437	-7969	-7923	-7922	-7968	MG	0.00	0.00	500.00
3437	-7923	-7779	-7801	-7922	MG	0.00	0.00	500.00
3437	-7671	-7586	-7585	-7670	MG	0.00	0.00	500.00
3437	-7706	-7656	-7655	-7705	MG	0.00	0.00	500.00
3437	-10249	-10194	-10193	3301	MG	0.00	0.00	500.00
3437	-7139	-7138	-7201	-7202	MG	0.00	0.00	500.00
3437	-7968	-7922	-7921	-7967	MG	0.00	0.00	500.00
3437	-7922	-7801	-7800	-7921	MG	0.00	0.00	500.00
3437	-9205	-9147	-9146	-9204	MG	0.00	0.00	500.00
3437	-8909	-8908	-8982	-8983	MG	0.00	0.00	500.00
3437	-7806	-7805	-7928	-7929	MG	0.00	0.00	500.00
3437	-7662	-7661	-7710	-7711	MG	0.00	0.00	500.00
3437	-7930	-7929	-7975	-7976	MG	0.00	0.00	500.00
3437	-8425	-8424	-8479	-8480	MG	0.00	0.00	500.00
3437	-7712	-7711	-7806	-7807	MG	0.00	0.00	500.00
3437	-9374	-9283	-9282	-9373	MG	0.00	0.00	500.00
3437	-10042	-9973	-9972	-10041	MG	0.00	0.00	500.00
3437	-7356	-7306	-7305	-7355	MG	0.00	0.00	500.00
3437	-7306	-7272	-7271	-7305	MG	0.00	0.00	500.00
3437	-7272	-7209	-7208	-7271	MG	0.00	0.00	500.00
3437	-9741	-9643	-9642	-9740	MG	0.00	0.00	500.00
3437	-10043	-9974	-9973	-10042	MG	0.00	0.00	500.00
3437	-10135	-10043	-10042	-10134	MG	0.00	0.00	500.00
3437	-10201	-10135	-10134	-10200	MG	0.00	0.00	500.00
3437	-7305	-7271	-7270	-7304	MG	0.00	0.00	500.00
3437	-7271	-7208	-7207	-7270	MG	0.00	0.00	500.00
3437	-7208	-7145	-7144	-7207	MG	0.00	0.00	500.00
3437	-9556	-9493	-9488	-9555	MG	0.00	0.00	500.00
3437	-7470	-7354	-7353	-7469	MG	0.00	0.00	500.00
3437	-8977	-8903	-8902	-8976	MG	0.00	0.00	500.00
3437	-9970	-9969	-10035	-10036	MG	0.00	0.00	500.00
3437	-10128	-10127	-10195	-10196	MG	0.00	0.00	500.00
3437	-9603	-9555	-9554	-9602	MG	0.00	0.00	500.00
3437	-9143	-9093	-9068	-9142	MG	0.00	0.00	500.00
3437	-9488	-9445	-9444	-9504	MG	0.00	0.00	500.00
3437	-8976	-8902	-8901	-8975	MG	0.00	0.00	500.00
3437	-7303	-7269	-7268	-7302	MG	0.00	0.00	500.00
3437	-9284	-9283	-9374	-9375	MG	0.00	0.00	500.00
3437	-9602	-9554	-9553	-9601	MG	0.00	0.00	500.00
3437	-7504	-7468	-7467	-7503	MG	0.00	0.00	500.00
3437	-8809	-8728	-8727	-8827	MG	0.00	0.00	500.00
3437	-8728	-8635	-8634	-8727	MG	0.00	0.00	500.00
3437	-7805	-7710	-7709	-7804	MG	0.00	0.00	500.00
3437	-9601	-9553	-9552	-9600	MG	0.00	0.00	500.00
3437	-9553	-9487	-9486	-9552	MG	0.00	0.00	500.00
3437	-9443	-9377	-9376	-9442	MG	0.00	0.00	500.00
3437	-7467	-7351	-7350	-7466	MG	0.00	0.00	500.00
3437	-7351	-7301	-7300	-7350	MG	0.00	0.00	500.00
3437	-7301	-7267	-7266	-7300	MG	0.00	0.00	500.00
3437	-7267	-7204	-7203	-7266	MG	0.00	0.00	500.00
3437	-8485	-8432	-8431	-8484	MG	0.00	0.00	500.00
3437	-8915	-8826	-8843	-8914	MG	0.00	0.00	500.00
3437	-9479	-9440	-9439	-9503	MG	0.00	0.00	500.00
3437	-9440	-9374	-9373	-9439	MG	0.00	0.00	500.00
3437	-9639	-9597	-9596	-9638	MG	0.00	0.00	500.00
3437	-9597	-9549	-9548	-9596	MG	0.00	0.00	500.00
3437	-9549	-9503	-9484	-9548	MG	0.00	0.00	500.00
3437	-8311	-8223	-8222	-8310	MG	0.00	0.00	500.00
3437	-7508	-7472	-7471	-7507	MG	0.00	0.00	500.00
3437	-7973	-7927	-7926	-7972	MG	0.00	0.00	500.00
3437	-7983	-7937	-7936	-7982	MG	0.00	0.00	500.00
3437	-7263	-7200	-7199	-7262	MG	0.00	0.00	500.00
3437	-7200	-7137	-7136	-7199	MG	0.00	0.00	500.00
3437	-10029	-9943	-9942	-10028	MG	0.00	0.00	500.00
3437	-7975	-7974	-8028	-8029	MG	0.00	0.00	500.00
3437	-7296	-7262	-7261	-7295	MG	0.00	0.00	500.00
3437	-7262	-7199	-7198	-7261	MG	0.00	0.00	500.00
3437	-8379	-8378	-8425	-8426	MG	0.00	0.00	500.00
3437	-7497	-7461	-7460	-7496	MG	0.00	0.00	500.00
3437	-7461	-7345	-7344	-7460	MG	0.00	0.00	500.00
3437	-7345	-7295	-7294	-7344	MG	0.00	0.00	500.00

3437	-7295	-7261	-7260	-7294	MG	0.00	0.00	500.00
3437	-7261	-7198	-7197	-7260	MG	0.00	0.00	500.00
3437	-7198	-7135	-7134	-7197	MG	0.00	0.00	500.00
3437	-7496	-7460	-7459	-7495	MG	0.00	0.00	500.00
3437	-7460	-7344	-7343	-7459	MG	0.00	0.00	500.00
3437	-7344	-7294	-7293	-7343	MG	0.00	0.00	500.00
3437	-7294	-7260	-7259	-7293	MG	0.00	0.00	500.00
3437	-7260	-7197	-7196	-7259	MG	0.00	0.00	500.00
3437	-7197	-7134	-7133	-7196	MG	0.00	0.00	500.00
3437	-6558	-7131	-7132	-7132	MG	0.00	0.00	500.00
3437	-6558	-7132	-7133	-5852	MG	0.00	0.00	500.00
3437	-7343	-7293	-7292	-7342	MG	0.00	0.00	500.00
3437	-7293	-7259	-7258	-7292	MG	0.00	0.00	500.00
3437	-7259	-7196	-7195	-7258	MG	0.00	0.00	500.00
3437	-7196	-7133	-7132	-7195	MG	0.00	0.00	500.00
3437	-7494	-7458	-7457	-7493	MG	0.00	0.00	500.00
3437	-7458	-7342	-7341	-7457	MG	0.00	0.00	500.00
3437	-7342	-7292	-7291	-7341	MG	0.00	0.00	500.00
3437	-7292	-7258	-7257	-7291	MG	0.00	0.00	500.00
3437	-7258	-7195	-7194	-7257	MG	0.00	0.00	500.00
3437	-7195	-7132	-7131	-7194	MG	0.00	0.00	500.00
3437	-7493	-7457	-7456	-7492	MG	0.00	0.00	500.00
3437	-7457	-7341	-7340	-7456	MG	0.00	0.00	500.00
3437	-7341	-7291	-7290	-7340	MG	0.00	0.00	500.00
3437	-8534	-8471	-8470	-8533	MG	0.00	0.00	500.00
3437	-8471	-8421	-8420	-8470	MG	0.00	0.00	500.00
3437	-7194	-7131	-7130	-7193	MG	0.00	0.00	500.00
3437	-7465	-7464	-7500	-7501	MG	0.00	0.00	500.00
3437	-7464	-7463	-7499	-7500	MG	0.00	0.00	500.00
3437	-8617	-8533	-8532	-8616	MG	0.00	0.00	500.00
3437	-7298	-7297	-7347	-7348	MG	0.00	0.00	500.00
3437	-10194	-10126	-10125	-10193	MG	0.00	0.00	500.00
3437	-10126	-10034	-10033	-10125	MG	0.00	0.00	500.00
3437	-10034	-9968	-9945	-10033	MG	0.00	0.00	500.00
3437	-8714	-8616	-8627	-8713	MG	0.00	0.00	500.00
3437	-8616	-8532	-8531	-8627	MG	0.00	0.00	500.00
3437	-8532	-8469	-8477	-8531	MG	0.00	0.00	500.00
3437	-7580	-7502	-7501	-7579	MG	0.00	0.00	500.00
3437	-8030	-8029	-8155	-8156	MG	0.00	0.00	500.00
3437	-8802	-8713	-8712	-8801	MG	0.00	0.00	500.00
3437	-7302	-7268	-7267	-7301	MG	0.00	0.00	500.00
3437	-9969	-9968	-10034	-10035	MG	0.00	0.00	500.00
3437	-9728	-9727	-9855	-9856	MG	0.00	0.00	500.00
3437	-7503	-7467	-7466	-7502	MG	0.00	0.00	500.00
3437	-8841	-8825	-8909	-8910	MG	0.00	0.00	500.00
3437	-8825	-8840	-8908	-8909	MG	0.00	0.00	500.00
3437	-9839	-9738	-9737	-9853	MG	0.00	0.00	500.00
3437	-10247	-10191	-10190	-10246	MG	0.00	0.00	500.00
3437	-10191	-10123	-10122	-10190	MG	0.00	0.00	500.00
3437	-10123	-10031	-10030	-10122	MG	0.00	0.00	500.00
3437	-8237	-8163	-8162	-8236	MG	0.00	0.00	500.00
3437	-7977	-7931	-7930	-7976	MG	0.00	0.00	500.00
3437	-8037	-7983	-7982	-8036	MG	0.00	0.00	500.00
3437	-8432	-8385	-8384	-8431	MG	0.00	0.00	500.00
3437	-10190	-10122	-10121	-10175	MG	0.00	0.00	500.00
3437	-9599	-9598	-9640	-9641	MG	0.00	0.00	500.00
3437	-8236	-8162	-8161	-8235	MG	0.00	0.00	500.00
3437	-9944	-9838	-9852	-9943	MG	0.00	0.00	500.00
3437	-9838	-9736	-9726	-9852	MG	0.00	0.00	500.00
3437	-8431	-8384	-8383	-8430	MG	0.00	0.00	500.00
3437	-8384	-8323	-8322	-8383	MG	0.00	0.00	500.00
3437	-8323	-8235	-8234	-8322	MG	0.00	0.00	500.00
3437	-8235	-8161	-8160	-8234	MG	0.00	0.00	500.00
3437	-8161	-8035	-8034	-8160	MG	0.00	0.00	500.00
3437	-9852	-9726	-9735	-9837	MG	0.00	0.00	500.00
3437	-10244	-10189	-10188	-10243	MG	0.00	0.00	500.00
3437	-10189	-10120	-10119	-10188	MG	0.00	0.00	500.00
3437	-10120	-10028	-10027	-10119	MG	0.00	0.00	500.00
3437	-10028	-9942	-9941	-10027	MG	0.00	0.00	500.00
3437	-9942	-9837	-9846	-9941	MG	0.00	0.00	500.00
3437	-9837	-9735	-9734	-9846	MG	0.00	0.00	500.00
3437	-7202	-7201	-7264	-7265	MG	0.00	0.00	500.00
3437	-7201	-7200	-7263	-7264	MG	0.00	0.00	500.00
3437	-9375	-9374	-9440	-9441	MG	0.00	0.00	500.00
3437	-10035	-10034	-10126	-10127	MG	0.00	0.00	500.00
3437	-9649	-9607	-9606	-9648	MG	0.00	0.00	500.00
3437	-9607	-9559	-9558	-9606	MG	0.00	0.00	500.00
3437	-9559	-9507	-9506	-9558	MG	0.00	0.00	500.00
3437	-9507	-9449	-9448	-9506	MG	0.00	0.00	500.00

3437	-9449	-9383	-9382	-9448	MG	0.00	0.00	500.00
3437	-9746	-9648	-9647	-9745	MG	0.00	0.00	500.00
3437	-9376	-9375	-9441	-9442	MG	0.00	0.00	500.00
3437	-9606	-9558	-9557	-9605	MG	0.00	0.00	500.00
3437	-9558	-9506	-9505	-9557	MG	0.00	0.00	500.00
3437	-9486	-9485	-9551	-9552	MG	0.00	0.00	500.00
3437	-9448	-9382	-9381	-9447	MG	0.00	0.00	500.00
3437	-9745	-9647	-9646	-9744	MG	0.00	0.00	500.00
3437	-9647	-9605	-9604	-9646	MG	0.00	0.00	500.00
3437	-9605	-9557	-9556	-9604	MG	0.00	0.00	500.00
3437	-7498	-7462	-7461	-7497	MG	0.00	0.00	500.00
3437	-9505	-9447	-9446	-9493	MG	0.00	0.00	500.00
3437	-7976	-7975	-8029	-8030	MG	0.00	0.00	500.00
3437	-8156	-8155	-8229	-8230	MG	0.00	0.00	500.00
3437	-8318	-8317	-8378	-8379	MG	0.00	0.00	500.00
3437	-8317	-8316	-8377	-8378	MG	0.00	0.00	500.00
3437	-8155	-8154	-8228	-8229	MG	0.00	0.00	500.00
3437	-8537	-8536	-8620	-8628	MG	0.00	0.00	500.00
3437	-8628	-8620	-8718	-8719	MG	0.00	0.00	500.00
3437	-8719	-8718	-8824	-8840	MG	0.00	0.00	500.00
3437	-8840	-8824	-8907	-8908	MG	0.00	0.00	500.00
3437	-8376	-8315	-8314	-8375	MG	0.00	0.00	500.00
3437	-8315	-8227	-8226	-8314	MG	0.00	0.00	500.00
3437	-8227	-8153	-8152	-8226	MG	0.00	0.00	500.00
3437	-8153	-8027	-8026	-8152	MG	0.00	0.00	500.00
3437	-8027	-7973	-7972	-8026	MG	0.00	0.00	500.00
3437	-8422	-8375	-8374	-8421	MG	0.00	0.00	500.00
3437	-8375	-8314	-8313	-8374	MG	0.00	0.00	500.00
3437	-8314	-8226	-8225	-8313	MG	0.00	0.00	500.00
3437	-8226	-8152	-8151	-8225	MG	0.00	0.00	500.00
3437	-8152	-8026	-8025	-8151	MG	0.00	0.00	500.00
3437	-8026	-7972	-7971	-8025	MG	0.00	0.00	500.00
3437	-8421	-8374	-8373	-8420	MG	0.00	0.00	500.00
3437	-8374	-8313	-8312	-8373	MG	0.00	0.00	500.00
3437	-8313	-8225	-8224	-8312	MG	0.00	0.00	500.00
3437	-8225	-8151	-8150	-8224	MG	0.00	0.00	500.00
3437	-8151	-8025	-8024	-8150	MG	0.00	0.00	500.00
3437	-8025	-7971	-7970	-8024	MG	0.00	0.00	500.00
3437	-8545	-8485	-8484	-8544	MG	0.00	0.00	500.00
3437	-8373	-8312	-8311	-8372	MG	0.00	0.00	500.00
3437	-8312	-8224	-8223	-8311	MG	0.00	0.00	500.00
3437	-8224	-8150	-8149	-8223	MG	0.00	0.00	500.00
3437	-8150	-8024	-8023	-8149	MG	0.00	0.00	500.00
3437	-8024	-7970	-7969	-8023	MG	0.00	0.00	500.00
3437	-8419	-8372	-8371	-8418	MG	0.00	0.00	500.00
3437	-7579	-7572	-7662	-7666	MG	0.00	0.00	500.00
3437	-9503	-9439	-9438	-9484	MG	0.00	0.00	500.00
3437	-8223	-8149	-8148	-8222	MG	0.00	0.00	500.00
3437	-8149	-8023	-8022	-8148	MG	0.00	0.00	500.00
3437	-8023	-7969	-7968	-8022	MG	0.00	0.00	500.00
3437	-8418	-8371	-8370	-8417	MG	0.00	0.00	500.00
3437	-8371	-8310	-8309	-8370	MG	0.00	0.00	500.00
3437	-8310	-8222	-8221	-8309	MG	0.00	0.00	500.00
3437	-8222	-8148	-8147	-8221	MG	0.00	0.00	500.00
3437	-8148	-8022	-8021	-8147	MG	0.00	0.00	500.00
3437	-8022	-7968	-7967	-8021	MG	0.00	0.00	500.00
3437	-9595	-9547	-9546	-9594	MG	0.00	0.00	500.00
3437	-8378	-8377	-8424	-8425	MG	0.00	0.00	500.00
3437	-7937	-7813	-7812	-7936	MG	0.00	0.00	500.00
3437	-9437	-9371	-9370	-9436	MG	0.00	0.00	500.00
3437	-9736	-9636	-9635	-9726	MG	0.00	0.00	500.00
3437	-9636	-9594	-9593	-9635	MG	0.00	0.00	500.00
3437	-7586	-7508	-7507	-7585	MG	0.00	0.00	500.00
3437	-7982	-7936	-7935	-7981	MG	0.00	0.00	500.00
3437	-7936	-7812	-7811	-7935	MG	0.00	0.00	500.00
3437	-9436	-9370	-9369	-9435	MG	0.00	0.00	500.00
3437	-9726	-9635	-9634	-9735	MG	0.00	0.00	500.00
3437	-7670	-7585	-7584	-7669	MG	0.00	0.00	500.00
3437	-7585	-7507	-7506	-7584	MG	0.00	0.00	500.00
3437	-7981	-7935	-7934	-7980	MG	0.00	0.00	500.00
3437	-9477	-9435	-9434	-9476	MG	0.00	0.00	500.00
3437	-7811	-7716	-7715	-7810	MG	0.00	0.00	500.00
3437	-7716	-7669	-7668	-7715	MG	0.00	0.00	500.00
3437	-7669	-7584	-7583	-7668	MG	0.00	0.00	500.00
3437	-7584	-7506	-7505	-7583	MG	0.00	0.00	500.00
3437	-7980	-7934	-7933	-7979	MG	0.00	0.00	500.00
3437	-7934	-7810	-7809	-7933	MG	0.00	0.00	500.00
3437	-7810	-7715	-7721	-7809	MG	0.00	0.00	500.00
3437	-9642	-9641	-9728	-9740	MG	0.00	0.00	500.00

3437	-9641	-9640	-9727	-9728	MG	0.00	0.00	500.00
3437	-9552	-9551	-9599	-9600	MG	0.00	0.00	500.00
3437	-7979	-7933	-7932	-7978	MG	0.00	0.00	500.00
3437	-7933	-7809	-7781	-7932	MG	0.00	0.00	500.00
3437	-7809	-7721	-7714	-7781	MG	0.00	0.00	500.00
3437	-7721	-7643	-7667	-7714	MG	0.00	0.00	500.00
3437	-9100	-8991	-8990	-9099	MG	0.00	0.00	500.00
3437	-7582	-7504	-7503	-7581	MG	0.00	0.00	500.00
3437	-7978	-7932	-7931	-7977	MG	0.00	0.00	500.00
3437	-7932	-7781	-7808	-7931	MG	0.00	0.00	500.00
3437	-7781	-7714	-7713	-7808	MG	0.00	0.00	500.00
3437	-9157	-9099	-9098	-9156	MG	0.00	0.00	500.00
3437	-7667	-7581	-7580	-7663	MG	0.00	0.00	500.00
3437	-8990	-8916	-8915	-8989	MG	0.00	0.00	500.00
3437	-9381	-9290	-9289	-9380	MG	0.00	0.00	500.00
3437	-9290	-9214	-9213	-9289	MG	0.00	0.00	500.00
3437	-7713	-7663	-7666	-7712	MG	0.00	0.00	500.00
3437	-9156	-9098	-9097	-9155	MG	0.00	0.00	500.00
3437	-9098	-8989	-8988	-9097	MG	0.00	0.00	500.00
3437	-7500	-7499	-7578	-7572	MG	0.00	0.00	500.00
3437	-9380	-9289	-9288	-9379	MG	0.00	0.00	500.00
3437	-7928	-7805	-7804	-7927	MG	0.00	0.00	500.00
3437	-9213	-9155	-9154	-9212	MG	0.00	0.00	500.00
3437	-9155	-9097	-9096	-9154	MG	0.00	0.00	500.00
3437	-7661	-7578	-7577	-7660	MG	0.00	0.00	500.00
3437	-7578	-7499	-7498	-7577	MG	0.00	0.00	500.00
3437	-7927	-7804	-7780	-7926	MG	0.00	0.00	500.00
3437	-7804	-7709	-7708	-7780	MG	0.00	0.00	500.00
3437	-7709	-7660	-7659	-7708	MG	0.00	0.00	500.00
3437	-7660	-7577	-7571	-7659	MG	0.00	0.00	500.00
3437	-7577	-7498	-7497	-7571	MG	0.00	0.00	500.00
3437	-7972	-7926	-7925	-7971	MG	0.00	0.00	500.00
3437	-7926	-7780	-7803	-7925	MG	0.00	0.00	500.00
3437	-7780	-7708	-7707	-7803	MG	0.00	0.00	500.00
3437	-7708	-7659	-7658	-7707	MG	0.00	0.00	500.00
3437	-7659	-7571	-7576	-7658	MG	0.00	0.00	500.00
3437	-9076	-8986	-8985	-9075	MG	0.00	0.00	500.00
3437	-8986	-8912	-8911	-8985	MG	0.00	0.00	500.00
3437	-7925	-7803	-7802	-7924	MG	0.00	0.00	500.00
3437	-7803	-7707	-7698	-7802	MG	0.00	0.00	500.00
3437	-7707	-7658	-7657	-7698	MG	0.00	0.00	500.00
3437	-9075	-8985	-8984	-9074	MG	0.00	0.00	500.00
3437	-8985	-8911	-8910	-8984	MG	0.00	0.00	500.00
3437	-7970	-7924	-7923	-7969	MG	0.00	0.00	500.00
3437	-9441	-9440	-9479	-9485	MG	0.00	0.00	500.00
3437	-9283	-9207	-9206	-9282	MG	0.00	0.00	500.00
3437	-9207	-9149	-9148	-9206	MG	0.00	0.00	500.00
3437	-9149	-9073	-9072	-9148	MG	0.00	0.00	500.00
3437	-9073	-8982	-8981	-9072	MG	0.00	0.00	500.00
3437	-8982	-8908	-8907	-8981	MG	0.00	0.00	500.00
3437	-9282	-9206	-9205	-9281	MG	0.00	0.00	500.00
3437	-7779	-7706	-7705	-7801	MG	0.00	0.00	500.00
3437	-9148	-9072	-9071	-9147	MG	0.00	0.00	500.00
3437	-7656	-7569	-7568	-7655	MG	0.00	0.00	500.00
3437	-7569	-7494	-7493	-7568	MG	0.00	0.00	500.00
3437	-9372	-9281	-9280	-9371	MG	0.00	0.00	500.00
3437	-9281	-9205	-9204	-9280	MG	0.00	0.00	500.00
3437	-8033	-7979	-7978	-8032	MG	0.00	0.00	500.00
3437	-9147	-9071	-9094	-9146	MG	0.00	0.00	500.00
3437	-7655	-7568	-7567	-7654	MG	0.00	0.00	500.00
3437	-7568	-7493	-7492	-7567	MG	0.00	0.00	500.00
3437	-9371	-9280	-9279	-9370	MG	0.00	0.00	500.00
3437	-7929	-7928	-7974	-7975	MG	0.00	0.00	500.00
3437	-9204	-9146	-9145	-9203	MG	0.00	0.00	500.00
3437	-9146	-9094	-9070	-9145	MG	0.00	0.00	500.00
3437	-9094	-8979	-8978	-9070	MG	0.00	0.00	500.00
3437	-8979	-8905	-8904	-8978	MG	0.00	0.00	500.00
3437	-9370	-9279	-9278	-9369	MG	0.00	0.00	500.00
3437	-9279	-9203	-9202	-9278	MG	0.00	0.00	500.00
3437	-7209	-7146	-7145	-7208	MG	0.00	0.00	500.00
3437	-7507	-7471	-7470	-7506	MG	0.00	0.00	500.00
3437	-7471	-7355	-7354	-7470	MG	0.00	0.00	500.00
3437	-7355	-7305	-7304	-7354	MG	0.00	0.00	500.00
3437	-9369	-9278	-9277	-9368	MG	0.00	0.00	500.00
3437	-9278	-9202	-9201	-9277	MG	0.00	0.00	500.00
3437	-9202	-9144	-9143	-9201	MG	0.00	0.00	500.00
3437	-7506	-7470	-7469	-7505	MG	0.00	0.00	500.00
3437	-9069	-8977	-8976	-9093	MG	0.00	0.00	500.00
3437	-7354	-7304	-7303	-7353	MG	0.00	0.00	500.00

3437	-7304	-7270	-7269	-7303	MG	0.00	0.00	500.00
3437	-7270	-7207	-7206	-7269	MG	0.00	0.00	500.00
3437	-7207	-7144	-7143	-7206	MG	0.00	0.00	500.00
3437	-8470	-8420	-8419	-8469	MG	0.00	0.00	500.00
3437	-7469	-7353	-7352	-7468	MG	0.00	0.00	500.00
3437	-7353	-7303	-7302	-7352	MG	0.00	0.00	500.00
3437	-9285	-9284	-9375	-9376	MG	0.00	0.00	500.00
3437	-9214	-9156	-9155	-9213	MG	0.00	0.00	500.00
3437	-7206	-7143	-7142	-7205	MG	0.00	0.00	500.00
3437	-9150	-9149	-9207	-9208	MG	0.00	0.00	500.00
3437	-10033	-9945	-9961	-10032	MG	0.00	0.00	500.00
3437	-7352	-7302	-7301	-7351	MG	0.00	0.00	500.00
3437	-8635	-8546	-8545	-8634	MG	0.00	0.00	500.00
3437	-7268	-7205	-7204	-7267	MG	0.00	0.00	500.00
3437	-7205	-7142	-7141	-7204	MG	0.00	0.00	500.00
3437	-8916	-8827	-8826	-8915	MG	0.00	0.00	500.00
3437	-8827	-8727	-8726	-8826	MG	0.00	0.00	500.00
3437	-8727	-8634	-8633	-8726	MG	0.00	0.00	500.00
3437	-8634	-8545	-8544	-8633	MG	0.00	0.00	500.00
3437	-8621	-8628	-8719	-8720	MG	0.00	0.00	500.00
3437	-7204	-7141	-7140	-7203	MG	0.00	0.00	500.00
3437	-7466	-7350	-7349	-7465	MG	0.00	0.00	500.00
3437	-7350	-7300	-7299	-7349	MG	0.00	0.00	500.00
3437	-7300	-7266	-7265	-7299	MG	0.00	0.00	500.00
3437	-7266	-7203	-7202	-7265	MG	0.00	0.00	500.00
3437	-7203	-7140	-7139	-7202	MG	0.00	0.00	500.00
3437	-8484	-8431	-8430	-8483	MG	0.00	0.00	500.00
3437	-7572	-7578	-7661	-7662	MG	0.00	0.00	500.00
3437	-7463	-7347	-7346	-7462	MG	0.00	0.00	500.00
3437	-7347	-7297	-7296	-7346	MG	0.00	0.00	500.00
3437	-7297	-7263	-7262	-7296	MG	0.00	0.00	500.00
3437	-8543	-8483	-8474	-8542	MG	0.00	0.00	500.00
3437	-8483	-8430	-8429	-8474	MG	0.00	0.00	500.00
3437	-7462	-7346	-7345	-7461	MG	0.00	0.00	500.00
3437	-7346	-7296	-7295	-7345	MG	0.00	0.00	500.00
3437	-8724	-8631	-8630	-8723	MG	0.00	0.00	500.00
3437	-8631	-8542	-8541	-8630	MG	0.00	0.00	500.00
3437	-7199	-7136	-7135	-7198	MG	0.00	0.00	500.00
3437	-8474	-8429	-8428	-8473	MG	0.00	0.00	500.00
3437	-8912	-8787	-8808	-8911	MG	0.00	0.00	500.00
3437	-8787	-8723	-8722	-8808	MG	0.00	0.00	500.00
3437	-9973	-9840	-9849	-9972	MG	0.00	0.00	500.00
3437	-9840	-9746	-9745	-9849	MG	0.00	0.00	500.00
3437	-8541	-8473	-8482	-8540	MG	0.00	0.00	500.00
3437	-8473	-8428	-8427	-8482	MG	0.00	0.00	500.00
3437	-8808	-8722	-8721	-8841	MG	0.00	0.00	500.00
3437	-8722	-8622	-8629	-8721	MG	0.00	0.00	500.00
3437	-8622	-8540	-8539	-8629	MG	0.00	0.00	500.00
3437	-8540	-8482	-8481	-8539	MG	0.00	0.00	500.00
3437	-8482	-8427	-8426	-8481	MG	0.00	0.00	500.00
3437	-8824	-8718	-8717	-8807	MG	0.00	0.00	500.00
3437	-8718	-8620	-8619	-8717	MG	0.00	0.00	500.00
3437	-8620	-8536	-8535	-8619	MG	0.00	0.00	500.00
3437	-9971	-9848	-9862	-9963	MG	0.00	0.00	500.00
3437	-9848	-9744	-9743	-9862	MG	0.00	0.00	500.00
3437	-10253	-10177	-10197	-10252	MG	0.00	0.00	500.00
3437	-10177	-10131	-10130	-10197	MG	0.00	0.00	500.00
3437	-10131	-10039	-10038	-10130	MG	0.00	0.00	500.00
3437	-10039	-9963	-9946	-10038	MG	0.00	0.00	500.00
3437	-9963	-9862	-9858	-9946	MG	0.00	0.00	500.00
3437	-9862	-9743	-9742	-9858	MG	0.00	0.00	500.00
3437	-10252	-10197	-10176	3302	MG	0.00	0.00	500.00
3437	-8806	-8716	-8715	-8839	MG	0.00	0.00	500.00
3437	-8716	-8618	-8617	-8715	MG	0.00	0.00	500.00
3437	-8618	-8534	-8533	-8617	MG	0.00	0.00	500.00
3437	-9946	-9858	-9857	-9962	MG	0.00	0.00	500.00
3437	-9858	-9742	-9741	-9857	MG	0.00	0.00	500.00
3437	-8904	-8839	-8803	-8903	MG	0.00	0.00	500.00
3437	-8839	-8715	-8714	-8803	MG	0.00	0.00	500.00
3437	-8715	-8617	-8616	-8714	MG	0.00	0.00	500.00
3437	-9215	-9157	-9156	-9214	MG	0.00	0.00	500.00
3437	-8533	-8470	-8469	-8532	MG	0.00	0.00	500.00
3437	-9201	-9143	-9142	-9200	MG	0.00	0.00	500.00
3437	-8903	-8803	-8802	-8902	MG	0.00	0.00	500.00
3437	-8803	-8714	-8713	-8802	MG	0.00	0.00	500.00
3437	-8234	-8160	-8159	-8233	MG	0.00	0.00	500.00
3437	-8160	-8034	-8033	-8159	MG	0.00	0.00	500.00
3437	-10193	-10125	-10124	-10192	MG	0.00	0.00	500.00
3437	-10125	-10033	-10032	-10124	MG	0.00	0.00	500.00

3437	-8469	-8419	-8418	-8477	MG	0.00	0.00	500.00
3437	-9945	-9854	-9839	-9961	MG	0.00	0.00	500.00
3437	-9854	-9739	-9738	-9839	MG	0.00	0.00	500.00
3437	-10248	-10192	-10191	-10247	MG	0.00	0.00	500.00
3437	-10192	-10124	-10123	-10191	MG	0.00	0.00	500.00
3437	-10124	-10032	-10031	-10123	MG	0.00	0.00	500.00
3437	-10032	-9961	-9967	-10031	MG	0.00	0.00	500.00
3437	-9379	-9288	-9287	-9378	MG	0.00	0.00	500.00
3437	-8629	-8621	-8720	-8721	MG	0.00	0.00	500.00
3437	-9288	-9212	-9211	-9287	MG	0.00	0.00	500.00
3437	-8386	-8325	-8324	-8385	MG	0.00	0.00	500.00
3437	-8325	-8237	-8236	-8324	MG	0.00	0.00	500.00
3437	-10031	-9967	-9944	-10030	MG	0.00	0.00	500.00
3437	-9967	-9853	-9838	-9944	MG	0.00	0.00	500.00
3437	-9287	-9211	-9210	-9286	MG	0.00	0.00	500.00
3437	-9211	-9153	-9152	-9210	MG	0.00	0.00	500.00
3437	-8385	-8324	-8323	-8384	MG	0.00	0.00	500.00
3437	-8324	-8236	-8235	-8323	MG	0.00	0.00	500.00
3437	-8914	-8843	-8842	-8913	MG	0.00	0.00	500.00
3437	-8162	-8036	-8035	-8161	MG	0.00	0.00	500.00
3437	-8036	-7982	-7981	-8035	MG	0.00	0.00	500.00
3437	-9152	-9075	-9074	-9151	MG	0.00	0.00	500.00
3437	-9596	-9548	-9547	-9595	MG	0.00	0.00	500.00
3437	-9548	-9484	-9483	-9547	MG	0.00	0.00	500.00
3437	-9442	-9441	-9485	-9486	MG	0.00	0.00	500.00
3437	-9438	-9372	-9371	-9437	MG	0.00	0.00	500.00
3437	-8035	-7981	-7980	-8034	MG	0.00	0.00	500.00
3437	-8430	-8383	-8382	-8429	MG	0.00	0.00	500.00
3437	-8383	-8322	-8321	-8382	MG	0.00	0.00	500.00
3437	-8322	-8234	-8233	-8321	MG	0.00	0.00	500.00
3437	-9093	-8976	-8975	-9068	MG	0.00	0.00	500.00
3437	-9483	-9437	-9436	-9478	MG	0.00	0.00	500.00
3437	-8034	-7980	-7979	-8033	MG	0.00	0.00	500.00
3437	-8429	-8382	-8381	-8428	MG	0.00	0.00	500.00
3437	-8382	-8321	-8320	-8381	MG	0.00	0.00	500.00
3437	-8321	-8233	-8232	-8320	MG	0.00	0.00	500.00
3437	-8233	-8159	-8158	-8232	MG	0.00	0.00	500.00
3437	-8159	-8033	-8032	-8158	MG	0.00	0.00	500.00
3437	-9289	-9213	-9212	-9288	MG	0.00	0.00	500.00
3437	-8428	-8381	-8380	-8427	MG	0.00	0.00	500.00
3437	-8381	-8320	-8319	-8380	MG	0.00	0.00	500.00
3437	-8320	-8232	-8231	-8319	MG	0.00	0.00	500.00
3437	-8232	-8158	-8157	-8231	MG	0.00	0.00	500.00
3437	-8158	-8032	-8031	-8157	MG	0.00	0.00	500.00
3437	-8032	-7978	-7977	-8031	MG	0.00	0.00	500.00
3437	-8380	-8319	-8318	-8379	MG	0.00	0.00	500.00
3437	-8319	-8231	-8230	-8318	MG	0.00	0.00	500.00
3437	-8231	-8157	-8156	-8230	MG	0.00	0.00	500.00
3437	-8157	-8031	-8030	-8156	MG	0.00	0.00	500.00
3437	-8031	-7977	-7976	-8030	MG	0.00	0.00	500.00
3437	-8481	-8480	-8538	-8539	MG	0.00	0.00	500.00
3437	-8480	-8479	-8537	-8538	MG	0.00	0.00	500.00
3437	-8377	-8316	-8315	-8376	MG	0.00	0.00	500.00
3437	-8316	-8228	-8227	-8315	MG	0.00	0.00	500.00
3437	-8228	-8154	-8153	-8227	MG	0.00	0.00	500.00
3437	-8154	-8028	-8027	-8153	MG	0.00	0.00	500.00
3437	-8028	-7974	-7973	-8027	MG	0.00	0.00	500.00
3437	-8479	-8472	-8536	-8537	MG	0.00	0.00	500.00
3437	-8991	-8917	-8916	-8990	MG	0.00	0.00	500.00
3437	-9382	-9291	-9290	-9381	MG	0.00	0.00	500.00
3437	-9368	-9277	-9276	-9367	MG	0.00	0.00	500.00
3437	-9277	-9201	-9200	-9276	MG	0.00	0.00	500.00
3437	-9637	-9595	-9594	-9636	MG	0.00	0.00	500.00
3437	-9099	-8990	-8989	-9098	MG	0.00	0.00	500.00
3437	-9547	-9483	-9478	-9546	MG	0.00	0.00	500.00
3437	-8826	-8726	-8725	-8843	MG	0.00	0.00	500.00
3437	-8726	-8633	-8632	-8725	MG	0.00	0.00	500.00
3437	-8723	-8630	-8622	-8722	MG	0.00	0.00	500.00
3437	-9151	-9150	-9208	-9209	MG	0.00	0.00	500.00
3437	-9594	-9546	-9545	-9593	MG	0.00	0.00	500.00
3437	-8989	-8915	-8914	-8988	MG	0.00	0.00	500.00
3437	-8902	-8802	-8801	-8901	MG	0.00	0.00	500.00
3437	-8981	-8907	-8906	-8980	MG	0.00	0.00	500.00
3437	-8546	-8486	-8485	-8545	MG	0.00	0.00	500.00
3437	-8486	-8433	-8432	-8485	MG	0.00	0.00	500.00
3437	-9097	-8988	-8987	-9096	MG	0.00	0.00	500.00
3437	-8988	-8914	-8913	-8987	MG	0.00	0.00	500.00
3437	-8980	-8906	-8905	-8979	MG	0.00	0.00	500.00
3437	-9435	-9369	-9368	-9434	MG	0.00	0.00	500.00

3437	-9212	-9154	-9153	-9211	MG	0.00	0.00	500.00
3437	-9154	-9096	-9076	-9153	MG	0.00	0.00	500.00
3437	-9096	-8987	-8986	-9076	MG	0.00	0.00	500.00
3437	-9544	-9476	-9502	-9543	MG	0.00	0.00	500.00
3437	-9476	-9434	-9433	-9502	MG	0.00	0.00	500.00
3437	-8633	-8544	-8543	-8632	MG	0.00	0.00	500.00
3437	-8544	-8484	-8483	-8543	MG	0.00	0.00	500.00
3437	-9153	-9076	-9075	-9152	MG	0.00	0.00	500.00
3437	-8905	-8806	-8839	-8904	MG	0.00	0.00	500.00
3437	-9439	-9373	-9372	-9438	MG	0.00	0.00	500.00
3437	-9738	-9638	-9637	-9737	MG	0.00	0.00	500.00
3437	-9638	-9596	-9595	-9637	MG	0.00	0.00	500.00
3437	-8632	-8543	-8542	-8631	MG	0.00	0.00	500.00
3437	-8725	-8632	-8631	-8724	MG	0.00	0.00	500.00
3437	-9484	-9438	-9437	-9483	MG	0.00	0.00	500.00
3437	-8913	-8842	-8787	-8912	MG	0.00	0.00	500.00
3437	-9737	-9637	-9636	-9736	MG	0.00	0.00	500.00
3437	-8842	-8724	-8723	-8787	MG	0.00	0.00	500.00
3437	-8542	-8474	-8473	-8541	MG	0.00	0.00	500.00
3437	-9592	-9544	-9543	-9591	MG	0.00	0.00	500.00
3437	-8472	-8423	-8422	-8478	MG	0.00	0.00	500.00
3437	-8987	-8913	-8912	-8986	MG	0.00	0.00	500.00
3437	-9434	-9368	-9367	-9433	MG	0.00	0.00	500.00
3437	-8630	-8541	-8540	-8622	MG	0.00	0.00	500.00
3437	-9206	-9148	-9147	-9205	MG	0.00	0.00	500.00
3437	-9546	-9478	-9477	-9545	MG	0.00	0.00	500.00
3437	-9478	-9436	-9435	-9477	MG	0.00	0.00	500.00
3437	-9292	-9216	-9215	-9291	MG	0.00	0.00	500.00
3437	-9216	-9158	-9157	-9215	MG	0.00	0.00	500.00
3437	-9635	-9593	-9592	-9634	MG	0.00	0.00	500.00
3437	-9593	-9545	-9544	-9592	MG	0.00	0.00	500.00
3437	-9545	-9477	-9476	-9544	MG	0.00	0.00	500.00
3437	-8477	-8418	-8417	-8468	MG	0.00	0.00	500.00
3437	-9291	-9215	-9214	-9290	MG	0.00	0.00	500.00
3437	-9735	-9634	-9633	-9734	MG	0.00	0.00	500.00
3437	-9634	-9592	-9591	-9633	MG	0.00	0.00	500.00
3437	-8536	-8472	-8478	-8535	MG	0.00	0.00	500.00
3437	-9286	-9210	-9209	-9285	MG	0.00	0.00	500.00
3437	-8906	-8807	-8806	-8905	MG	0.00	0.00	500.00
3437	-9378	-9287	-9286	-9377	MG	0.00	0.00	500.00
3437	-8535	-8478	-8471	-8534	MG	0.00	0.00	500.00
3437	-8478	-8422	-8421	-8471	MG	0.00	0.00	500.00
3437	-9203	-9145	-9144	-9202	MG	0.00	0.00	500.00
3437	-9551	-9550	-9598	-9599	MG	0.00	0.00	500.00
3437	-9070	-8978	-8977	-9069	MG	0.00	0.00	500.00
3437	-9145	-9070	-9069	-9144	MG	0.00	0.00	500.00
3437	-9158	-9100	-9099	-9157	MG	0.00	0.00	500.00
3437	-8531	-8477	-8468	-8530	MG	0.00	0.00	500.00
3437	-9144	-9069	-9093	-9143	MG	0.00	0.00	500.00
3437	-9071	-8980	-8979	-9094	MG	0.00	0.00	500.00
3437	-8619	-8535	-8534	-8618	MG	0.00	0.00	500.00
3437	-8627	-8531	-8530	-8615	MG	0.00	0.00	500.00
3437	-9280	-9204	-9203	-9279	MG	0.00	0.00	500.00
3437	-8163	-8037	-8036	-8162	MG	0.00	0.00	500.00
3437	-8978	-8904	-8903	-8977	MG	0.00	0.00	500.00
3437	-8843	-8725	-8724	-8842	MG	0.00	0.00	500.00
3437	-8807	-8717	-8716	-8806	MG	0.00	0.00	500.00
3437	-8717	-8619	-8618	-8716	MG	0.00	0.00	500.00
3437	-9072	-8981	-8980	-9071	MG	0.00	0.00	500.00
3437	-8713	-8627	-8615	-8712	MG	0.00	0.00	500.00
3437	-9210	-9152	-9151	-9209	MG	0.00	0.00	500.00
3438	-10036	-6505	-6598	-10128	MG	0.00	0.00	500.00
3438	-9376	-5606	-5818	-9442	MG	0.00	0.00	500.00
3438	-9642	-6103	-6002	-9740	MG	0.00	0.00	500.00
3438	-8984	-5398	-5621	-9074	MG	0.00	0.00	500.00
3438	-9847	-6222	-6438	-9970	MG	0.00	0.00	500.00
3438	-9486	-6037	-6105	-9552	MG	0.00	0.00	500.00
3438	-9552	-6105	-6173	-9600	MG	0.00	0.00	500.00
3438	-10196	-6496	-6382	-10251	MG	0.00	0.00	500.00
3438	-9209	-5774	-5690	-9285	MG	0.00	0.00	500.00
3438	-9285	-5690	-5606	-9376	MG	0.00	0.00	500.00
3438	-9151	-5702	-5774	-9209	MG	0.00	0.00	500.00
3438	-9740	-6002	-6222	-9847	MG	0.00	0.00	500.00
3438	-9074	-5621	-5702	-9151	MG	0.00	0.00	500.00
3438	-9970	-6438	-6505	-10036	MG	0.00	0.00	500.00
3438	-10128	-6598	-6496	-10196	MG	0.00	0.00	500.00
3438	-9442	-5818	-6037	-9486	MG	0.00	0.00	500.00
3438	-9600	-6173	-6103	-9642	MG	0.00	0.00	500.00
3440	-7008	-7494	-7495	-6240	MG	0.00	0.00	500.00

3443	-7973	-5013	-4950	-7972	MG	0.00	0.00	500.00
3447	-4815	-4421	-8423	-8424	MG	0.00	0.00	500.00
3448	-8423	-5418	-5352	-8422	MG	0.00	0.00	500.00
3451	-5215	-4888	-8907	-8908	MG	0.00	0.00	500.00
3451	-4888	-5807	-8907	-8907	MG	0.00	0.00	500.00
3452	-6170	-6259	-6926	-6926	MG	0.00	0.00	500.00
3453	-5306	-6221	-9373	-9373	MG	0.00	0.00	500.00
3471	-6692	-6152	-6691	-6691	MG	0.00	0.00	500.00
3474	-7145	-6559	-7144	-7144	MG	0.00	0.00	500.00
3474	-6559	-5853	-7143	-7144	MG	0.00	0.00	500.00
3478	-7009	-6253	-7505	-7506	MG	0.00	0.00	500.00
3482	-4951	-5014	-7977	-7978	MG	0.00	0.00	500.00
3484	-5353	-5397	-8427	-8428	MG	0.00	0.00	500.00
3485	-4422	-4816	-8426	-8427	MG	0.00	0.00	500.00
3487	-5817	-4897	-8911	-8911	MG	0.00	0.00	500.00
3487	-4897	-5216	-8910	-8911	MG	0.00	0.00	500.00
3490	-6927	-6269	-6171	-6171	MG	0.00	0.00	500.00
3491	-6230	-5307	-9377	-9377	MG	0.00	0.00	500.00
3494	-6578	-5784	-6699	-6699	MG	0.00	0.00	500.00
3494	-6578	-6699	-7309	-7309	MG	0.00	0.00	500.00
3495	-5766	-6700	-6579	-6579	MG	0.00	0.00	500.00
3495	-7310	-6700	-6579	-6579	MG	0.00	0.00	500.00
3553	-7021	-7156	-7727	-7727	MG	0.00	0.00	500.00
3554	-6107	-6382	-10251	3302	MG	0.00	0.00	500.00
3554	-7022	-7092	3302	-10252	MG	0.00	0.00	500.00
3554	-7092	-6107	3302	3302	MG	0.00	0.00	500.00
3555	3301	-7091	-7021	-10248	MG	0.00	0.00	500.00
3555	-6380	-6106	3301	-10249	MG	0.00	0.00	500.00
3555	-6106	-7091	3301	3301	MG	0.00	0.00	500.00
3556	-7728	-7157	-7022	-7022	MG	0.00	0.00	500.00
3569	-7008	-7493	-7494	-7494	MG	0.00	0.00	500.00
3572	-7357	-7968	-7969	-7969	MG	0.00	0.00	500.00
3572	-7357	-7969	-7970	-6674	MG	0.00	0.00	500.00
3577	-7814	-8419	-8420	-7147	MG	0.00	0.00	500.00
3577	-7814	-8418	-8419	-8419	MG	0.00	0.00	500.00
3579	-8907	-5807	-5781	-8906	MG	0.00	0.00	500.00
3581	-9373	-6221	-6170	-9372	MG	0.00	0.00	500.00
3582	-5605	-5306	-9373	-9374	MG	0.00	0.00	500.00
3583	-8326	-8902	-8903	-8903	MG	0.00	0.00	500.00
3583	-8326	-8903	-8904	-7509	MG	0.00	0.00	500.00
3599	-7507	-7009	-7506	-7506	MG	0.00	0.00	500.00
3601	-7358	-6694	-7980	-7981	MG	0.00	0.00	500.00
3601	-7982	-7358	-7981	-7981	MG	0.00	0.00	500.00
3605	-8432	-7815	-8431	-8431	MG	0.00	0.00	500.00
3605	-7815	-7148	-8430	-8431	MG	0.00	0.00	500.00
3607	-5773	-5817	-8911	-8912	MG	0.00	0.00	500.00
3609	-8916	-8327	-8915	-8915	MG	0.00	0.00	500.00
3609	-8327	-7510	-8914	-8915	MG	0.00	0.00	500.00
3611	-6171	-6230	-9377	-9378	MG	0.00	0.00	500.00
3612	-5307	-5606	-9376	-9377	MG	0.00	0.00	500.00
3614	-9382	-8730	-9381	-9381	MG	0.00	0.00	500.00
3614	-8730	-7985	-9380	-9381	MG	0.00	0.00	500.00
3616	-8729	-9368	-9369	-9369	MG	0.00	0.00	500.00
3616	-8729	-9369	-9370	-7984	MG	0.00	0.00	500.00
3618	-5691	-6659	-9739	-9739	MG	0.00	0.00	500.00
3618	-6001	-5691	-9739	-9727	MG	0.00	0.00	500.00
3618	-9739	-6659	-6578	-9738	MG	0.00	0.00	500.00
3620	-5692	-6002	-9740	-9741	MG	0.00	0.00	500.00
3620	-6579	-6660	-9741	-9742	MG	0.00	0.00	500.00
3620	-6660	-5692	-9741	-9741	MG	0.00	0.00	500.00
3622	-9746	-9218	-9745	-9745	MG	0.00	0.00	500.00
3622	-9218	-8435	-9744	-9745	MG	0.00	0.00	500.00
3624	-9217	-9735	-9726	-9726	MG	0.00	0.00	500.00
3624	-9217	-9726	-9736	-8434	MG	0.00	0.00	500.00
3627	-9608	-10244	-10245	-10245	MG	0.00	0.00	500.00
3627	-9608	-10245	-10246	-8918	MG	0.00	0.00	500.00
3629	-10256	-9609	-10255	-10255	MG	0.00	0.00	500.00
3629	-9609	-8919	-10254	-10255	MG	0.00	0.00	500.00
3824	-4583	-4588	-4572	-4571	MG	0.00	0.00	500.00
3824	-4611	-4594	-4597	-4625	MG	0.00	0.00	500.00
3824	-4626	-4611	-4625	-4625	MG	0.00	0.00	500.00
3824	-4621	-4603	-4601	-4620	MG	0.00	0.00	500.00
3824	-4652	-4635	-4634	-4651	MG	0.00	0.00	500.00
3824	-4589	-4598	-4608	-4592	MG	0.00	0.00	500.00
3824	-4607	-4583	-4592	-4608	MG	0.00	0.00	500.00
3824	-4573	-4570	-4558	-4555	MG	0.00	0.00	500.00
3824	-4651	-4634	-4633	-4650	MG	0.00	0.00	500.00
3824	-4536	-4527	-4531	-4531	MG	0.00	0.00	500.00
3824	-4594	-4579	-4590	-4597	MG	0.00	0.00	500.00

3824	-4579	-4569	-4574	-4590	MG	0.00	0.00	500.00
3824	-4569	-4554	-4562	-4574	MG	0.00	0.00	500.00
3824	-4554	-4541	-4551	-4562	MG	0.00	0.00	500.00
3824	-4541	-4539	-4545	-4551	MG	0.00	0.00	500.00
3824	-4583	-4607	-4604	-4588	MG	0.00	0.00	500.00
3824	-4649	-4632	-4631	-4648	MG	0.00	0.00	500.00
3824	-4634	-4620	-4619	-4633	MG	0.00	0.00	500.00
3824	-4648	-4631	-4636	-4653	MG	0.00	0.00	500.00
3824	-4631	-4617	-4616	-4636	MG	0.00	0.00	500.00
3824	-4636	-4616	-4615	-4638	MG	0.00	0.00	500.00
3824	-4615	-4614	-4640	-4638	MG	0.00	0.00	500.00
3824	-4614	-4613	-4629	-4640	MG	0.00	0.00	500.00
3824	-4613	-4612	-4627	-4629	MG	0.00	0.00	500.00
3824	-4627	-4642	-4644	-4629	MG	0.00	0.00	500.00
3824	-4642	-4659	-4663	-4644	MG	0.00	0.00	500.00
3824	-4562	-4551	-4558	-4570	MG	0.00	0.00	500.00
3824	-4545	-4555	-4558	-4551	MG	0.00	0.00	500.00
3824	-4570	-4573	-4587	-4586	MG	0.00	0.00	500.00
3824	-4650	-4633	-4632	-4649	MG	0.00	0.00	500.00
3824	-4633	-4619	-4618	-4632	MG	0.00	0.00	500.00
3824	-4597	-4590	-4591	-4609	MG	0.00	0.00	500.00
3824	-4591	-4590	-4574	-4586	MG	0.00	0.00	500.00
3824	-4586	-4587	-4605	-4606	MG	0.00	0.00	500.00
3824	-4632	-4618	-4617	-4631	MG	0.00	0.00	500.00
3824	-4629	-4644	-4646	-4640	MG	0.00	0.00	500.00
3824	-4644	-4663	-4661	-4646	MG	0.00	0.00	500.00
3824	-4646	-4661	-4657	-4640	MG	0.00	0.00	500.00
3824	-4532	-4528	-4537	-4537	MG	0.00	0.00	500.00
3824	-4635	-4621	-4620	-4634	MG	0.00	0.00	500.00
3824	-4653	-4636	-4638	-4655	MG	0.00	0.00	500.00
3824	-4655	-4638	-4640	-4657	MG	0.00	0.00	500.00
3824	-4660	-4643	-4645	-4664	MG	0.00	0.00	500.00
3824	-4643	-4628	-4630	-4645	MG	0.00	0.00	500.00
3824	-4628	-4626	-4625	-4630	MG	0.00	0.00	500.00
3824	-4625	-4624	-4641	-4630	MG	0.00	0.00	500.00
3824	-4624	-4623	-4639	-4641	MG	0.00	0.00	500.00
3824	-4623	-4622	-4637	-4639	MG	0.00	0.00	500.00
3824	-4637	-4622	-4621	-4635	MG	0.00	0.00	500.00
3824	-4654	-4637	-4635	-4652	MG	0.00	0.00	500.00
3824	-4539	-4532	-4537	-4545	MG	0.00	0.00	500.00
3824	-4537	-4550	-4555	-4545	MG	0.00	0.00	500.00
3824	-4550	-4567	-4573	-4555	MG	0.00	0.00	500.00
3824	-4567	-4585	-4587	-4573	MG	0.00	0.00	500.00
3824	-4585	-4603	-4605	-4587	MG	0.00	0.00	500.00
3824	-4603	-4621	-4622	-4605	MG	0.00	0.00	500.00
3824	-4622	-4623	-4606	-4605	MG	0.00	0.00	500.00
3824	-4623	-4624	-4609	-4606	MG	0.00	0.00	500.00
3824	-4624	-4625	-4597	-4609	MG	0.00	0.00	500.00
3824	-4658	-4662	-4647	-4641	MG	0.00	0.00	500.00
3824	-4662	-4664	-4645	-4647	MG	0.00	0.00	500.00
3824	-4647	-4645	-4630	-4641	MG	0.00	0.00	500.00
3824	-4639	-4637	-4654	-4656	MG	0.00	0.00	500.00
3824	-4639	-4656	-4658	-4641	MG	0.00	0.00	500.00
3824	-4570	-4586	-4574	-4562	MG	0.00	0.00	500.00
3824	-4606	-4609	-4591	-4586	MG	0.00	0.00	500.00
3824	-4603	-4585	-4582	-4601	MG	0.00	0.00	500.00
3824	-4585	-4567	-4565	-4582	MG	0.00	0.00	500.00
3824	-4567	-4550	-4548	-4565	MG	0.00	0.00	500.00
3824	-4550	-4537	-4535	-4548	MG	0.00	0.00	500.00
3824	-4537	-4528	-4526	-4535	MG	0.00	0.00	500.00
3824	-4620	-4601	-4599	-4619	MG	0.00	0.00	500.00
3824	-4601	-4582	-4580	-4599	MG	0.00	0.00	500.00
3824	-4582	-4565	-4563	-4580	MG	0.00	0.00	500.00
3824	-4565	-4548	-4546	-4563	MG	0.00	0.00	500.00
3824	-4548	-4535	-4533	-4546	MG	0.00	0.00	500.00
3824	-4535	-4526	-4524	-4533	MG	0.00	0.00	500.00
3824	-4619	-4599	-4600	-4618	MG	0.00	0.00	500.00
3824	-4599	-4580	-4581	-4600	MG	0.00	0.00	500.00
3824	-4580	-4563	-4564	-4581	MG	0.00	0.00	500.00
3824	-4563	-4546	-4547	-4564	MG	0.00	0.00	500.00
3824	-4546	-4533	-4534	-4547	MG	0.00	0.00	500.00
3824	-4533	-4524	-4525	-4534	MG	0.00	0.00	500.00
3824	-4618	-4600	-4602	-4617	MG	0.00	0.00	500.00
3824	-4600	-4581	-4584	-4602	MG	0.00	0.00	500.00
3824	-4581	-4564	-4566	-4584	MG	0.00	0.00	500.00
3824	-4564	-4547	-4549	-4566	MG	0.00	0.00	500.00
3824	-4547	-4534	-4536	-4549	MG	0.00	0.00	500.00
3824	-4534	-4525	-4527	-4536	MG	0.00	0.00	500.00
3824	-4610	-4612	-4613	-4613	MG	0.00	0.00	500.00

3824	-4602	-4584	-4588	-4604	MG	0.00	0.00	500.00
3824	-4584	-4566	-4572	-4588	MG	0.00	0.00	500.00
3824	-4566	-4549	-4556	-4572	MG	0.00	0.00	500.00
3824	-4549	-4536	-4544	-4556	MG	0.00	0.00	500.00
3824	-4536	-4531	-4538	-4544	MG	0.00	0.00	500.00
3824	-4538	-4540	-4552	-4544	MG	0.00	0.00	500.00
3824	-4540	-4553	-4561	-4552	MG	0.00	0.00	500.00
3824	-4553	-4568	-4575	-4561	MG	0.00	0.00	500.00
3824	-4568	-4578	-4589	-4575	MG	0.00	0.00	500.00
3824	-4578	-4593	-4598	-4589	MG	0.00	0.00	500.00
3824	-4593	-4610	-4613	-4598	MG	0.00	0.00	500.00
3824	-4613	-4614	-4608	-4598	MG	0.00	0.00	500.00
3824	-4614	-4615	-4607	-4608	MG	0.00	0.00	500.00
3824	-4615	-4616	-4604	-4607	MG	0.00	0.00	500.00
3824	-4617	-4602	-4604	-4616	MG	0.00	0.00	500.00
3824	-4544	-4552	-4557	-4556	MG	0.00	0.00	500.00
3824	-4561	-4571	-4557	-4552	MG	0.00	0.00	500.00
3824	-4572	-4556	-4557	-4571	MG	0.00	0.00	500.00
3824	-4575	-4583	-4571	-4561	MG	0.00	0.00	500.00
3824	-4575	-4589	-4592	-4583	MG	0.00	0.00	500.00

Elenco carichi elementi bidimensionali

Condizione di carico n. 5: Variabili impalc. (caso 1)

Carichi uniformi

Bid.	N1	N2	N3	N4	TDC	Qx <daN/mq>	Qy <daN/mq>	Qz <daN/mq>
2718	-3859	-3858	-3909	-3910	MG	0.00	0.00	500.00
2718	-3676	-3664	-3712	-3719	MG	0.00	0.00	500.00
2718	-3665	-3676	-3719	-3720	MG	0.00	0.00	500.00
2718	-3572	-3571	-3610	-3611	MG	0.00	0.00	500.00
2718	-3719	-3712	-3768	-3769	MG	0.00	0.00	500.00
2718	-3720	-3719	-3769	-3765	MG	0.00	0.00	500.00
2718	-3610	-3609	-3664	-3676	MG	0.00	0.00	500.00
2718	-3571	-3570	-3609	-3610	MG	0.00	0.00	500.00
2718	-3769	-3768	-3810	-3811	MG	0.00	0.00	500.00
2718	-3765	-3769	-3811	-3812	MG	0.00	0.00	500.00
2718	-3858	-3857	-3908	-3909	MG	0.00	0.00	500.00
2718	-3957	-3950	-4000	-4001	MG	0.00	0.00	500.00
2718	-3812	-3811	-3858	-3859	MG	0.00	0.00	500.00
2718	-3909	-3908	-3950	-3957	MG	0.00	0.00	500.00
2718	-3958	-3957	-4001	-4002	MG	0.00	0.00	500.00
2718	-3811	-3810	-3857	-3858	MG	0.00	0.00	500.00
2718	-3525	-3524	-3571	-3572	MG	0.00	0.00	500.00
2718	-3910	-3909	-3957	-3958	MG	0.00	0.00	500.00
2718	-3524	-3523	-3570	-3571	MG	0.00	0.00	500.00
2718	-3611	-3610	-3676	-3665	MG	0.00	0.00	500.00
2816	-3655	-3748	-4148	-4148	MG	0.00	0.00	500.00
2817	-3947	-4038	-4403	-4403	MG	0.00	0.00	500.00
2822	-4219	-3663	-4295	-4295	MG	0.00	0.00	500.00
2843	-4149	-3749	-3656	-3656	MG	0.00	0.00	500.00
2847	-4404	-4039	-3948	-3948	MG	0.00	0.00	500.00
2848	-3659	-4296	-4220	-4220	MG	0.00	0.00	500.00
2921	-4198	-4683	-4684	-4684	MG	0.00	0.00	500.00
2921	-4198	-4684	-4685	-3732	MG	0.00	0.00	500.00
2931	-6370	-3558	-3605	-6483	MG	0.00	0.00	500.00
2933	-6102	-3664	-3712	-6001	MG	0.00	0.00	500.00
2933	-6036	-3523	-3570	-6104	MG	0.00	0.00	500.00
2933	-6104	-3570	-3609	-6172	MG	0.00	0.00	500.00
2933	-6172	-3609	-3664	-6102	MG	0.00	0.00	500.00
2933	-6001	-3712	-3768	-6206	MG	0.00	0.00	500.00
2934	-4219	-4295	-4870	-4870	MG	0.00	0.00	500.00
2935	-4670	-4653	-4655	-4672	MG	0.00	0.00	500.00
2935	-4676	-4661	-4663	-4679	MG	0.00	0.00	500.00
2935	-4804	-4747	-4746	-4803	MG	0.00	0.00	500.00
2935	-4746	-4687	-4686	-4745	MG	0.00	0.00	500.00
2935	-4858	-4803	-4802	-4857	MG	0.00	0.00	500.00
2935	-4676	-4674	-4657	-4661	MG	0.00	0.00	500.00
2935	-4864	-4809	-4808	-4863	MG	0.00	0.00	500.00
2935	-4671	-4654	-4652	-4669	MG	0.00	0.00	500.00
2935	-4747	-4688	-4687	-4746	MG	0.00	0.00	500.00
2935	-4690	-4689	-4748	-4749	MG	0.00	0.00	500.00
2935	-4697	-4680	-4677	-4696	MG	0.00	0.00	500.00
2935	-4672	-4655	-4657	-4674	MG	0.00	0.00	500.00
2935	-4855	-4800	-4799	-4854	MG	0.00	0.00	500.00
2935	-4803	-4746	-4745	-4802	MG	0.00	0.00	500.00
2935	-4669	-4652	-4651	-4668	MG	0.00	0.00	500.00
2935	-4754	-4695	-4694	-4753	MG	0.00	0.00	500.00
2935	-4859	-4804	-4803	-4858	MG	0.00	0.00	500.00

2935	-4755	-4696	-4695	-4754	MG	0.00	0.00	500.00
2935	-4813	-4756	-4755	-4812	MG	0.00	0.00	500.00
2935	-4802	-4745	-4744	-4801	MG	0.00	0.00	500.00
2935	-4656	-4673	-4675	-4658	MG	0.00	0.00	500.00
2935	-4812	-4755	-4754	-4811	MG	0.00	0.00	500.00
2935	-4867	-4812	-4811	-4866	MG	0.00	0.00	500.00
2935	-4748	-4689	-4688	-4747	MG	0.00	0.00	500.00
2935	-4666	-4649	-4648	-4665	MG	0.00	0.00	500.00
2935	-4688	-4665	-4670	-4687	MG	0.00	0.00	500.00
2935	-4694	-4695	-4675	-4673	MG	0.00	0.00	500.00
2935	-4698	-4681	-4680	-4697	MG	0.00	0.00	500.00
2935	-4749	-4748	-4805	-4806	MG	0.00	0.00	500.00
2935	-4752	-4693	-4692	-4751	MG	0.00	0.00	500.00
2935	-4809	-4752	-4751	-4808	MG	0.00	0.00	500.00
2935	-4751	-4692	-4691	-4750	MG	0.00	0.00	500.00
2935	-4807	-4806	-4861	-4862	MG	0.00	0.00	500.00
2935	-4745	-4686	-4685	-4744	MG	0.00	0.00	500.00
2935	-4692	-4669	-4668	-4691	MG	0.00	0.00	500.00
2935	-4857	-4802	-4801	-4856	MG	0.00	0.00	500.00
2935	-4667	-4650	-4649	-4666	MG	0.00	0.00	500.00
2935	-4689	-4666	-4665	-4688	MG	0.00	0.00	500.00
2935	-4810	-4753	-4752	-4809	MG	0.00	0.00	500.00
2935	-4686	-4687	-4670	-4672	MG	0.00	0.00	500.00
2935	-4856	-4801	-4800	-4855	MG	0.00	0.00	500.00
2935	-4668	-4651	-4650	-4667	MG	0.00	0.00	500.00
2935	-4669	-4692	-4693	-4671	MG	0.00	0.00	500.00
2935	-4665	-4648	-4653	-4670	MG	0.00	0.00	500.00
2935	-4696	-4677	-4675	-4695	MG	0.00	0.00	500.00
2935	-4744	-4685	-4684	-4743	MG	0.00	0.00	500.00
2935	-4805	-4748	-4747	-4804	MG	0.00	0.00	500.00
2935	-4756	-4697	-4696	-4755	MG	0.00	0.00	500.00
2935	-4677	-4680	-4664	-4662	MG	0.00	0.00	500.00
2935	-4686	-4672	-4674	-4685	MG	0.00	0.00	500.00
2935	-4681	-4660	-4664	-4680	MG	0.00	0.00	500.00
2935	-4753	-4694	-4693	-4752	MG	0.00	0.00	500.00
2935	-4684	-4685	-4674	-4676	MG	0.00	0.00	500.00
2935	-4656	-4654	-4671	-4673	MG	0.00	0.00	500.00
2935	-4750	-4749	-4806	-4807	MG	0.00	0.00	500.00
2935	-4690	-4667	-4666	-4689	MG	0.00	0.00	500.00
2935	-4742	-4683	-4682	-4741	MG	0.00	0.00	500.00
2935	-4868	-4813	-4812	-4867	MG	0.00	0.00	500.00
2935	-4808	-4751	-4750	-4807	MG	0.00	0.00	500.00
2935	-4866	-4811	-4810	-4865	MG	0.00	0.00	500.00
2935	-4691	-4668	-4667	-4690	MG	0.00	0.00	500.00
2935	-4694	-4673	-4671	-4693	MG	0.00	0.00	500.00
2935	-4691	-4690	-4749	-4750	MG	0.00	0.00	500.00
2935	-4801	-4744	-4743	-4800	MG	0.00	0.00	500.00
2935	-4865	-4810	-4809	-4864	MG	0.00	0.00	500.00
2935	-4814	-4757	-4756	-4813	MG	0.00	0.00	500.00
2935	-4659	-4678	-4679	-4663	MG	0.00	0.00	500.00
2935	-4869	-4814	-4813	-4868	MG	0.00	0.00	500.00
2935	-4811	-4754	-4753	-4810	MG	0.00	0.00	500.00
2935	-4799	-4742	-4741	-4798	MG	0.00	0.00	500.00
2935	-4854	-4799	-4798	-4853	MG	0.00	0.00	500.00
2935	-4684	-4676	-4679	-4683	MG	0.00	0.00	500.00
2935	-4683	-4679	-4678	-4682	MG	0.00	0.00	500.00
2935	-4757	-4698	-4697	-4756	MG	0.00	0.00	500.00
2935	-4743	-4684	-4683	-4742	MG	0.00	0.00	500.00
2935	-4677	-4662	-4658	-4675	MG	0.00	0.00	500.00
2935	-4860	-4805	-4804	-4859	MG	0.00	0.00	500.00
2935	-4806	-4805	-4860	-4861	MG	0.00	0.00	500.00
2935	-4800	-4743	-4742	-4799	MG	0.00	0.00	500.00
2935	-4863	-4808	-4807	-4862	MG	0.00	0.00	500.00
2937	-6372	-3559	-3606	-6485	MG	0.00	0.00	500.00
2939	-6105	-3572	-3611	-6173	MG	0.00	0.00	500.00
2939	-6037	-3525	-3572	-6105	MG	0.00	0.00	500.00
2939	-6002	-3720	-3765	-6222	MG	0.00	0.00	500.00
2939	-6173	-3611	-3665	-6103	MG	0.00	0.00	500.00
2939	-6103	-3665	-3720	-6002	MG	0.00	0.00	500.00
2940	-4459	-3955	-4711	-4711	MG	0.00	0.00	500.00
2944	-5352	-3764	-4471	-4471	MG	0.00	0.00	500.00
2945	-4697	-4199	-4696	-4696	MG	0.00	0.00	500.00
2945	-4199	-3733	-4695	-4696	MG	0.00	0.00	500.00
2953	-4871	-4296	-4220	-4220	MG	0.00	0.00	500.00
2954	-3949	-4712	-4460	-4460	MG	0.00	0.00	500.00
2955	-5353	-4463	-3767	-3767	MG	0.00	0.00	500.00
3007	-3763	-4003	-6107	-5257	MG	0.00	0.00	500.00
3008	-3999	-3766	-5256	-6106	MG	0.00	0.00	500.00
3022	-4445	-5039	-5040	-4019	MG	0.00	0.00	500.00

3031	-6689	-3536	-3698	-6748	MG	0.00	0.00	500.00
3031	-6620	-3590	-3536	-6689	MG	0.00	0.00	500.00
3031	-6483	-3605	-3657	-6548	MG	0.00	0.00	500.00
3031	-6548	-3657	-3590	-6620	MG	0.00	0.00	500.00
3032	-6206	-3768	-3810	-6437	MG	0.00	0.00	500.00
3032	-6437	-3810	-3857	-6501	MG	0.00	0.00	500.00
3033	-3607	-4251	-7136	-7136	MG	0.00	0.00	500.00
3034	-5041	-4976	-4992	-5040	MG	0.00	0.00	500.00
3034	-4918	-4855	-4854	-4917	MG	0.00	0.00	500.00
3034	-5042	-4968	-4976	-5041	MG	0.00	0.00	500.00
3034	-4932	-4866	-4865	-4931	MG	0.00	0.00	500.00
3034	-4967	-4918	-4917	-4966	MG	0.00	0.00	500.00
3034	-5048	-4995	-4979	-5047	MG	0.00	0.00	500.00
3034	-4926	-4860	-4859	-4925	MG	0.00	0.00	500.00
3034	-4861	-4860	-4926	-4927	MG	0.00	0.00	500.00
3034	-4994	-4930	-4929	-4978	MG	0.00	0.00	500.00
3034	-4929	-4863	-4862	-4928	MG	0.00	0.00	500.00
3034	-4924	-4858	-4857	-4919	MG	0.00	0.00	500.00
3034	-4978	-4929	-4928	-4970	MG	0.00	0.00	500.00
3034	-4927	-4926	-4969	-4993	MG	0.00	0.00	500.00
3034	-4925	-4859	-4858	-4924	MG	0.00	0.00	500.00
3034	-4976	-4919	-4923	-4992	MG	0.00	0.00	500.00
3034	-4995	-4932	-4931	-4979	MG	0.00	0.00	500.00
3034	-5046	-4994	-4978	2902	MG	0.00	0.00	500.00
3034	-4969	-4926	-4925	-4977	MG	0.00	0.00	500.00
3034	-4919	-4857	-4856	-4923	MG	0.00	0.00	500.00
3034	-5051	-4997	-4980	-5050	MG	0.00	0.00	500.00
3034	2902	-4978	-4970	-5045	MG	0.00	0.00	500.00
3034	-5043	-4969	-4977	2901	MG	0.00	0.00	500.00
3034	-4920	-4867	-4866	-4932	MG	0.00	0.00	500.00
3034	-4992	-4923	-4918	-4967	MG	0.00	0.00	500.00
3034	-4996	-4920	-4932	-4995	MG	0.00	0.00	500.00
3034	-4923	-4856	-4855	-4918	MG	0.00	0.00	500.00
3034	-4930	-4864	-4863	-4929	MG	0.00	0.00	500.00
3034	-4997	-4934	-4933	-4980	MG	0.00	0.00	500.00
3034	-5039	-4967	-4966	-5038	MG	0.00	0.00	500.00
3034	2901	-4977	-4968	-5042	MG	0.00	0.00	500.00
3034	-4993	-4969	-5043	-5044	MG	0.00	0.00	500.00
3034	-4931	-4865	-4864	-4930	MG	0.00	0.00	500.00
3034	-4862	-4861	-4927	-4928	MG	0.00	0.00	500.00
3034	-5040	-4992	-4967	-5039	MG	0.00	0.00	500.00
3034	-4970	-4993	-5044	-5045	MG	0.00	0.00	500.00
3034	-4934	-4869	-4868	-4933	MG	0.00	0.00	500.00
3034	-4968	-4924	-4919	-4976	MG	0.00	0.00	500.00
3034	-4917	-4854	-4853	-4916	MG	0.00	0.00	500.00
3034	-5050	-4980	-4996	-5049	MG	0.00	0.00	500.00
3034	-5047	-4979	-4994	-5046	MG	0.00	0.00	500.00
3034	-4928	-4927	-4993	-4970	MG	0.00	0.00	500.00
3034	-4979	-4931	-4930	-4994	MG	0.00	0.00	500.00
3034	-5049	-4996	-4995	-5048	MG	0.00	0.00	500.00
3034	-4977	-4925	-4924	-4968	MG	0.00	0.00	500.00
3034	-4933	-4868	-4867	-4920	MG	0.00	0.00	500.00
3034	-5038	-4966	-4991	-5037	MG	0.00	0.00	500.00
3034	-4966	-4917	-4916	-4991	MG	0.00	0.00	500.00
3034	-4980	-4933	-4920	-4996	MG	0.00	0.00	500.00
3036	-6485	-3606	-3658	-6550	MG	0.00	0.00	500.00
3036	-6550	-3658	-3591	-6622	MG	0.00	0.00	500.00
3036	-6672	-3537	-3699	-6750	MG	0.00	0.00	500.00
3036	-6622	-3591	-3537	-6672	MG	0.00	0.00	500.00
3038	-4459	-4711	-5284	-5284	MG	0.00	0.00	500.00
3039	-6438	-3812	-3859	-6505	MG	0.00	0.00	500.00
3039	-6222	-3765	-3812	-6438	MG	0.00	0.00	500.00
3041	-4950	-4223	-5065	-5065	MG	0.00	0.00	500.00
3052	-4446	-4020	-5048	-5049	MG	0.00	0.00	500.00
3060	-4252	-3608	-7140	-7140	MG	0.00	0.00	500.00
3061	-5285	-4712	-4460	-4460	MG	0.00	0.00	500.00
3062	-4224	-5066	-4951	-4951	MG	0.00	0.00	500.00
3106	-4000	-3999	-6106	-6380	MG	0.00	0.00	500.00
3107	-4003	-4002	-6382	-6107	MG	0.00	0.00	500.00
3119	-4445	-5038	-5039	-5039	MG	0.00	0.00	500.00
3120	-4935	-5432	-5433	-4281	MG	0.00	0.00	500.00
3121	-6244	-3696	-3655	-6243	MG	0.00	0.00	500.00
3129	-7297	-4167	-4221	-7347	MG	0.00	0.00	500.00
3129	-6915	-3904	-3963	-6998	MG	0.00	0.00	500.00
3129	-6833	-3842	-3904	-6915	MG	0.00	0.00	500.00
3129	-7463	-4164	-4104	-7499	MG	0.00	0.00	500.00
3129	-7200	-3987	-4124	-7263	MG	0.00	0.00	500.00
3129	-6998	-3963	-3887	-7057	MG	0.00	0.00	500.00
3129	-7499	-4104	-4253	-7578	MG	0.00	0.00	500.00

3129	-7263	-4124	-4167	-7297	MG	0.00	0.00	500.00
3129	-7347	-4221	-4164	-7463	MG	0.00	0.00	500.00
3129	-6748	-3698	-3842	-6833	MG	0.00	0.00	500.00
3129	-7057	-3887	-3825	-7137	MG	0.00	0.00	500.00
3129	-7137	-3825	-3987	-7200	MG	0.00	0.00	500.00
3130	-6501	-3857	-3908	-6597	MG	0.00	0.00	500.00
3130	-6495	-3950	-4000	-6380	MG	0.00	0.00	500.00
3130	-6597	-3908	-3950	-6495	MG	0.00	0.00	500.00
3131	-5116	-5040	-5039	-5115	MG	0.00	0.00	500.00
3131	-5671	-5602	-5601	-5670	MG	0.00	0.00	500.00
3131	-5663	-5594	-5593	-5662	MG	0.00	0.00	500.00
3131	-5435	-5373	-5372	-5434	MG	0.00	0.00	500.00
3131	-5741	-5732	-5797	-5798	MG	0.00	0.00	500.00
3131	-5119	2901	-5042	-5118	MG	0.00	0.00	500.00
3131	-5129	-5051	-5050	-5128	MG	0.00	0.00	500.00
3131	-5200	-5115	-5114	-5199	MG	0.00	0.00	500.00
3131	-5325	-5274	-5273	-5324	MG	0.00	0.00	500.00
3131	-5795	-5731	-5730	-5794	MG	0.00	0.00	500.00
3131	-5594	-5499	-5498	-5593	MG	0.00	0.00	500.00
3131	-5592	-5497	-5496	-5591	MG	0.00	0.00	500.00
3131	-5204	-5119	-5118	-5203	MG	0.00	0.00	500.00
3131	-5277	-5212	-5211	-5276	MG	0.00	0.00	500.00
3131	-5591	-5496	-5495	-5590	MG	0.00	0.00	500.00
3131	-5203	-5118	-5117	-5202	MG	0.00	0.00	500.00
3131	-5805	-5744	-5736	-5804	MG	0.00	0.00	500.00
3131	-5735	-5670	-5669	-5734	MG	0.00	0.00	500.00
3131	-5505	-5442	-5441	-5504	MG	0.00	0.00	500.00
3131	-5432	-5370	-5369	-5431	MG	0.00	0.00	500.00
3131	-5445	-5383	-5382	-5444	MG	0.00	0.00	500.00
3131	-5744	-5673	-5672	-5736	MG	0.00	0.00	500.00
3131	-5120	-5043	2901	-5119	MG	0.00	0.00	500.00
3131	-5379	-5325	-5324	-5378	MG	0.00	0.00	500.00
3131	-5439	-5438	-5501	-5502	MG	0.00	0.00	500.00
3131	-5731	-5663	-5662	-5730	MG	0.00	0.00	500.00
3131	-5508	-5445	-5444	-5507	MG	0.00	0.00	500.00
3131	-5728	-5660	-5659	-5727	MG	0.00	0.00	500.00
3131	-5660	-5591	-5590	-5659	MG	0.00	0.00	500.00
3131	-5496	-5433	-5432	-5495	MG	0.00	0.00	500.00
3131	-5665	-5664	-5740	-5732	MG	0.00	0.00	500.00
3131	-5802	-5735	-5734	-5801	MG	0.00	0.00	500.00
3131	-5730	-5662	-5661	-5729	MG	0.00	0.00	500.00
3131	-5370	-5316	-5315	-5369	MG	0.00	0.00	500.00
3131	-5214	-5129	-5128	-5213	MG	0.00	0.00	500.00
3131	-5803	-5743	-5735	-5802	MG	0.00	0.00	500.00
3131	-5743	-5671	-5670	-5735	MG	0.00	0.00	500.00
3131	-5210	-5125	-5124	-5209	MG	0.00	0.00	500.00
3131	-5128	-5050	-5049	-5127	MG	0.00	0.00	500.00
3131	-5801	-5734	-5742	-5800	MG	0.00	0.00	500.00
3131	-5661	-5592	-5591	-5660	MG	0.00	0.00	500.00
3131	-5734	-5669	-5668	-5742	MG	0.00	0.00	500.00
3131	-5320	-5269	-5268	-5319	MG	0.00	0.00	500.00
3131	-5269	-5204	-5203	-5268	MG	0.00	0.00	500.00
3131	-5497	-5434	-5433	-5496	MG	0.00	0.00	500.00
3131	-5201	-5116	-5115	-5200	MG	0.00	0.00	500.00
3131	-5206	-5205	-5270	-5271	MG	0.00	0.00	500.00
3131	-5207	-5206	-5271	-5272	MG	0.00	0.00	500.00
3131	-5327	-5276	-5275	-5326	MG	0.00	0.00	500.00
3131	-5436	-5374	-5373	-5435	MG	0.00	0.00	500.00
3131	-5276	-5211	-5210	-5275	MG	0.00	0.00	500.00
3131	-5727	-5659	-5658	-5726	MG	0.00	0.00	500.00
3131	-5590	-5495	-5494	-5589	MG	0.00	0.00	500.00
3131	-5045	-5044	-5121	-5122	MG	0.00	0.00	500.00
3131	-5315	-5264	-5263	-5314	MG	0.00	0.00	500.00
3131	-5275	-5210	-5209	-5274	MG	0.00	0.00	500.00
3131	-5446	-5384	-5383	-5445	MG	0.00	0.00	500.00
3131	-5125	-5047	-5046	-5124	MG	0.00	0.00	500.00
3131	-5664	-5595	-5594	-5663	MG	0.00	0.00	500.00
3131	-5437	-5375	-5374	-5436	MG	0.00	0.00	500.00
3131	-5500	-5437	-5436	-5499	MG	0.00	0.00	500.00
3131	-5597	-5596	-5665	-5666	MG	0.00	0.00	500.00
3131	-5440	-5378	-5377	-5439	MG	0.00	0.00	500.00
3131	-5274	-5209	-5208	-5273	MG	0.00	0.00	500.00
3131	-5499	-5436	-5435	-5498	MG	0.00	0.00	500.00
3131	-5265	-5200	-5199	-5264	MG	0.00	0.00	500.00
3131	-5316	-5265	-5264	-5315	MG	0.00	0.00	500.00
3131	-5794	-5730	-5729	-5793	MG	0.00	0.00	500.00
3131	-5273	-5208	-5207	-5272	MG	0.00	0.00	500.00
3131	-5279	-5214	-5213	-5278	MG	0.00	0.00	500.00
3131	-5670	-5601	-5600	-5669	MG	0.00	0.00	500.00

3131	-5601	-5506	-5505	-5600	MG	0.00	0.00	500.00
3131	-5278	-5213	-5212	-5277	MG	0.00	0.00	500.00
3131	-5369	-5315	-5314	-5368	MG	0.00	0.00	500.00
3131	-5213	-5128	-5127	-5212	MG	0.00	0.00	500.00
3131	-5270	-5205	-5204	-5269	MG	0.00	0.00	500.00
3131	-5264	-5199	-5198	-5263	MG	0.00	0.00	500.00
3131	-5328	-5277	-5276	-5327	MG	0.00	0.00	500.00
3131	-5382	-5328	-5327	-5381	MG	0.00	0.00	500.00
3131	-5377	-5376	-5438	-5439	MG	0.00	0.00	500.00
3131	-5792	-5728	-5727	-5791	MG	0.00	0.00	500.00
3131	-5212	-5127	-5126	-5211	MG	0.00	0.00	500.00
3131	-5127	-5049	-5048	-5126	MG	0.00	0.00	500.00
3131	-5443	-5381	-5380	-5442	MG	0.00	0.00	500.00
3131	-5373	-5319	-5318	-5372	MG	0.00	0.00	500.00
3131	-5791	-5727	-5726	-5790	MG	0.00	0.00	500.00
3131	-5268	-5203	-5202	-5267	MG	0.00	0.00	500.00
3131	-5501	-5500	-5595	-5596	MG	0.00	0.00	500.00
3131	-5380	-5326	-5325	-5379	MG	0.00	0.00	500.00
3131	-5495	-5432	-5431	-5494	MG	0.00	0.00	500.00
3131	-5790	-5726	-5725	-5789	MG	0.00	0.00	500.00
3131	-5796	-5740	-5731	-5795	MG	0.00	0.00	500.00
3131	-5726	-5658	-5657	-5725	MG	0.00	0.00	500.00
3131	-5595	-5500	-5499	-5594	MG	0.00	0.00	500.00
3131	-5371	-5317	-5316	-5370	MG	0.00	0.00	500.00
3131	-5494	-5431	-5430	-5493	MG	0.00	0.00	500.00
3131	-5441	-5379	-5378	-5440	MG	0.00	0.00	500.00
3131	-5266	-5201	-5200	-5265	MG	0.00	0.00	500.00
3131	-5666	-5665	-5732	-5741	MG	0.00	0.00	500.00
3131	-5272	-5271	-5322	-5323	MG	0.00	0.00	500.00
3131	-5324	-5273	-5272	-5323	MG	0.00	0.00	500.00
3131	-5507	-5444	-5443	-5506	MG	0.00	0.00	500.00
3131	-5330	-5279	-5278	-5329	MG	0.00	0.00	500.00
3131	-5124	-5046	2902	-5123	MG	0.00	0.00	500.00
3131	-5502	-5501	-5596	-5597	MG	0.00	0.00	500.00
3131	-5732	-5740	-5796	-5797	MG	0.00	0.00	500.00
3131	-5383	-5329	-5328	-5382	MG	0.00	0.00	500.00
3131	-5329	-5278	-5277	-5328	MG	0.00	0.00	500.00
3131	-5205	-5120	-5119	-5204	MG	0.00	0.00	500.00
3131	-5506	-5443	-5442	-5505	MG	0.00	0.00	500.00
3131	-5321	-5270	-5269	-5320	MG	0.00	0.00	500.00
3131	-5374	-5320	-5319	-5373	MG	0.00	0.00	500.00
3131	-5199	-5114	-5113	-5198	MG	0.00	0.00	500.00
3131	-5669	-5600	-5599	-5668	MG	0.00	0.00	500.00
3131	-5376	-5375	-5437	-5438	MG	0.00	0.00	500.00
3131	-5600	-5505	-5504	-5599	MG	0.00	0.00	500.00
3131	-5326	-5275	-5274	-5325	MG	0.00	0.00	500.00
3131	-5271	-5270	-5321	-5322	MG	0.00	0.00	500.00
3131	-5599	-5504	-5503	-5598	MG	0.00	0.00	500.00
3131	-5381	-5327	-5326	-5380	MG	0.00	0.00	500.00
3131	-5211	-5126	-5125	-5210	MG	0.00	0.00	500.00
3131	-5659	-5590	-5589	-5658	MG	0.00	0.00	500.00
3131	-5673	-5604	-5603	-5672	MG	0.00	0.00	500.00
3131	-5442	-5380	-5379	-5441	MG	0.00	0.00	500.00
3131	-5317	-5266	-5265	-5316	MG	0.00	0.00	500.00
3131	-5503	-5440	-5439	-5502	MG	0.00	0.00	500.00
3131	-5509	-5446	-5445	-5508	MG	0.00	0.00	500.00
3131	-5740	-5664	-5663	-5731	MG	0.00	0.00	500.00
3131	-5202	-5117	-5116	-5201	MG	0.00	0.00	500.00
3131	-5589	-5494	-5493	-5588	MG	0.00	0.00	500.00
3131	-5433	-5371	-5370	-5432	MG	0.00	0.00	500.00
3131	-5603	-5508	-5507	-5602	MG	0.00	0.00	500.00
3131	-5596	-5595	-5664	-5665	MG	0.00	0.00	500.00
3131	-5208	-5123	-5122	-5207	MG	0.00	0.00	500.00
3131	-5602	-5507	-5506	-5601	MG	0.00	0.00	500.00
3131	-5323	-5322	-5376	-5377	MG	0.00	0.00	500.00
3131	-5378	-5324	-5323	-5377	MG	0.00	0.00	500.00
3131	-5319	-5268	-5267	-5318	MG	0.00	0.00	500.00
3131	-5742	-5668	-5667	-5733	MG	0.00	0.00	500.00
3131	-5504	-5441	-5440	-5503	MG	0.00	0.00	500.00
3131	-5114	-5038	-5037	-5113	MG	0.00	0.00	500.00
3131	-5672	-5603	-5602	-5671	MG	0.00	0.00	500.00
3131	-5431	-5369	-5368	-5430	MG	0.00	0.00	500.00
3131	-5729	-5661	-5660	-5728	MG	0.00	0.00	500.00
3131	-5793	-5729	-5728	-5792	MG	0.00	0.00	500.00
3131	-5438	-5437	-5500	-5501	MG	0.00	0.00	500.00
3131	-5267	-5202	-5201	-5266	MG	0.00	0.00	500.00
3131	-5658	-5589	-5588	-5657	MG	0.00	0.00	500.00
3131	-5209	-5124	-5123	-5208	MG	0.00	0.00	500.00
3131	-5126	-5048	-5047	-5125	MG	0.00	0.00	500.00

3131	-5118	-5042	-5041	-5117	MG	0.00	0.00	500.00
3131	-5372	-5318	-5317	-5371	MG	0.00	0.00	500.00
3131	-5122	-5121	-5206	-5207	MG	0.00	0.00	500.00
3131	-5121	-5120	-5205	-5206	MG	0.00	0.00	500.00
3131	-5668	-5599	-5598	-5667	MG	0.00	0.00	500.00
3131	-5604	-5509	-5508	-5603	MG	0.00	0.00	500.00
3131	-5598	-5503	-5502	-5597	MG	0.00	0.00	500.00
3131	-5322	-5321	-5375	-5376	MG	0.00	0.00	500.00
3131	-5117	-5041	-5040	-5116	MG	0.00	0.00	500.00
3131	-5115	-5039	-5038	-5114	MG	0.00	0.00	500.00
3131	-5733	-5667	-5666	-5741	MG	0.00	0.00	500.00
3131	-5804	-5736	-5743	-5803	MG	0.00	0.00	500.00
3131	-5318	-5267	-5266	-5317	MG	0.00	0.00	500.00
3131	-5044	-5043	-5120	-5121	MG	0.00	0.00	500.00
3131	-5667	-5598	-5597	-5666	MG	0.00	0.00	500.00
3131	-5498	-5435	-5434	-5497	MG	0.00	0.00	500.00
3131	-5593	-5498	-5497	-5592	MG	0.00	0.00	500.00
3131	-5736	-5672	-5671	-5743	MG	0.00	0.00	500.00
3131	-5384	-5330	-5329	-5383	MG	0.00	0.00	500.00
3131	-5662	-5593	-5592	-5661	MG	0.00	0.00	500.00
3131	-5444	-5382	-5381	-5443	MG	0.00	0.00	500.00
3131	-5375	-5321	-5320	-5374	MG	0.00	0.00	500.00
3131	-5434	-5372	-5371	-5433	MG	0.00	0.00	500.00
3131	-5800	-5742	-5733	-5799	MG	0.00	0.00	500.00
3131	-5799	-5733	-5741	-5798	MG	0.00	0.00	500.00
3131	-5123	2902	-5045	-5122	MG	0.00	0.00	500.00
3132	-6598	-3910	-3958	-6496	MG	0.00	0.00	500.00
3132	-6496	-3958	-4002	-6382	MG	0.00	0.00	500.00
3132	-6505	-3859	-3910	-6598	MG	0.00	0.00	500.00
3133	-7139	-3826	-3988	-7202	MG	0.00	0.00	500.00
3133	-7465	-4165	-4105	-7501	MG	0.00	0.00	500.00
3133	-6835	-3843	-3905	-6917	MG	0.00	0.00	500.00
3133	-6917	-3905	-3964	-7000	MG	0.00	0.00	500.00
3133	-7202	-3988	-4125	-7265	MG	0.00	0.00	500.00
3133	-6750	-3699	-3843	-6835	MG	0.00	0.00	500.00
3133	-7059	-3888	-3826	-7139	MG	0.00	0.00	500.00
3133	-7299	-4168	-4222	-7349	MG	0.00	0.00	500.00
3133	-7349	-4222	-4165	-7465	MG	0.00	0.00	500.00
3133	-7000	-3964	-3888	-7059	MG	0.00	0.00	500.00
3133	-7501	-4105	-4254	-7579	MG	0.00	0.00	500.00
3133	-7265	-4125	-4168	-7299	MG	0.00	0.00	500.00
3138	-5781	-4065	-4964	-4964	MG	0.00	0.00	500.00
3139	-5306	-3674	-6221	-6221	MG	0.00	0.00	500.00
3147	-5050	-4446	-5049	-5049	MG	0.00	0.00	500.00
3150	-4936	-4282	-5443	-5444	MG	0.00	0.00	500.00
3152	-3656	-3697	-6247	-6248	MG	0.00	0.00	500.00
3156	-5773	-4965	-4066	-4066	MG	0.00	0.00	500.00
3157	-3675	-5307	-6230	-6230	MG	0.00	0.00	500.00
3205	-5256	-4235	-7091	-7091	MG	0.00	0.00	500.00
3206	-4236	-5257	-7092	-7092	MG	0.00	0.00	500.00
3207	-4001	-4000	-6380	-6381	MG	0.00	0.00	500.00
3207	-4002	-4001	-6381	-6382	MG	0.00	0.00	500.00
3219	-4935	-5431	-5432	-5432	MG	0.00	0.00	500.00
3222	-5333	-5837	-5838	-4699	MG	0.00	0.00	500.00
3222	-5333	-5836	-5837	-5837	MG	0.00	0.00	500.00
3229	-6670	-3985	-3947	-6669	MG	0.00	0.00	500.00
3231	-7710	-4419	-4461	-7805	MG	0.00	0.00	500.00
3231	-7928	-4417	-4362	-7974	MG	0.00	0.00	500.00
3231	-7974	-4362	-4494	-8028	MG	0.00	0.00	500.00
3231	-7805	-4461	-4417	-7928	MG	0.00	0.00	500.00
3231	-7661	-4378	-4419	-7710	MG	0.00	0.00	500.00
3231	-7578	-4253	-4378	-7661	MG	0.00	0.00	500.00
3232	-3825	-3607	-7136	-7137	MG	0.00	0.00	500.00
3233	-7136	-4251	-4219	-7135	MG	0.00	0.00	500.00
3234	-5987	-5878	-5877	-5986	MG	0.00	0.00	500.00
3234	-5888	-5846	-5845	-5887	MG	0.00	0.00	500.00
3234	-6067	-6066	-6134	-6135	MG	0.00	0.00	500.00
3234	-6060	-5987	-5986	-6059	MG	0.00	0.00	500.00
3234	-6070	-5996	-5995	-6069	MG	0.00	0.00	500.00
3234	-6130	-6062	-6061	-6129	MG	0.00	0.00	500.00
3234	-5989	-5880	-5879	-5988	MG	0.00	0.00	500.00
3234	-6249	-6197	-6196	-6239	MG	0.00	0.00	500.00
3234	-6193	-6194	-6137	-6136	MG	0.00	0.00	500.00
3234	-6250	-6198	-6197	-6249	MG	0.00	0.00	500.00
3234	-6142	-6074	-6073	-6141	MG	0.00	0.00	500.00
3234	-6073	-5999	-5998	-6072	MG	0.00	0.00	500.00
3234	-5878	-5836	-5835	-5877	MG	0.00	0.00	500.00
3234	-6185	-6128	-6127	-6184	MG	0.00	0.00	500.00
3234	-5891	-5849	-5848	-5890	MG	0.00	0.00	500.00

3234	-6252	-6200	-6199	-6251	MG	0.00	0.00	500.00
3234	-6000	-5892	-5891	-5999	MG	0.00	0.00	500.00
3234	-5838	-5792	-5791	-5837	MG	0.00	0.00	500.00
3234	-6199	-6142	-6141	-6198	MG	0.00	0.00	500.00
3234	-6068	-6067	-6135	-6136	MG	0.00	0.00	500.00
3234	-5999	-5891	-5890	-5998	MG	0.00	0.00	500.00
3234	-6248	-6195	-6194	-6247	MG	0.00	0.00	500.00
3234	-6136	-6135	-6192	-6193	MG	0.00	0.00	500.00
3234	-6138	-6070	-6069	-6137	MG	0.00	0.00	500.00
3234	-6187	-6130	-6129	-6186	MG	0.00	0.00	500.00
3234	-6236	-6187	-6186	-6235	MG	0.00	0.00	500.00
3234	-5798	-5797	-5843	-5844	MG	0.00	0.00	500.00
3234	-5847	-5801	-5800	-5846	MG	0.00	0.00	500.00
3234	-6198	-6141	-6140	-6197	MG	0.00	0.00	500.00
3234	-6068	-6069	-5995	-6025	MG	0.00	0.00	500.00
3234	-6242	-6185	-6184	-6234	MG	0.00	0.00	500.00
3234	-6246	-6247	-6194	-6193	MG	0.00	0.00	500.00
3234	-5886	-5887	-5845	-5844	MG	0.00	0.00	500.00
3234	-6128	-6060	-6059	-6127	MG	0.00	0.00	500.00
3234	-6238	-6191	-6190	-6244	MG	0.00	0.00	500.00
3234	-6074	-6000	-5999	-6073	MG	0.00	0.00	500.00
3234	-5892	-5850	-5849	-5891	MG	0.00	0.00	500.00
3234	-5884	-5842	-5841	-5883	MG	0.00	0.00	500.00
3234	-5846	-5800	-5799	-5845	MG	0.00	0.00	500.00
3234	-5848	-5802	-5801	-5847	MG	0.00	0.00	500.00
3234	-5837	-5791	-5790	-5836	MG	0.00	0.00	500.00
3234	-5885	-5884	-5993	-5994	MG	0.00	0.00	500.00
3234	-5992	-5883	-5882	-5991	MG	0.00	0.00	500.00
3234	-6140	-6072	-6071	-6139	MG	0.00	0.00	500.00
3234	-5839	-5793	-5792	-5838	MG	0.00	0.00	500.00
3234	-6025	-5995	-5887	-5886	MG	0.00	0.00	500.00
3234	-5882	-5840	-5839	-5881	MG	0.00	0.00	500.00
3234	-5890	-5848	-5847	-5889	MG	0.00	0.00	500.00
3234	-5851	-5805	-5804	-5850	MG	0.00	0.00	500.00
3234	-6244	-6190	-6189	-6243	MG	0.00	0.00	500.00
3234	-6063	-5990	-5989	-6062	MG	0.00	0.00	500.00
3234	-5990	-5881	-5880	-5989	MG	0.00	0.00	500.00
3234	-6196	-6139	-6138	-6195	MG	0.00	0.00	500.00
3234	-5881	-5839	-5838	-5880	MG	0.00	0.00	500.00
3234	-5843	-5842	-5884	-5885	MG	0.00	0.00	500.00
3234	-5797	-5796	-5842	-5843	MG	0.00	0.00	500.00
3234	-5842	-5796	-5795	-5841	MG	0.00	0.00	500.00
3234	-6062	-5989	-5988	-6061	MG	0.00	0.00	500.00
3234	-5840	-5794	-5793	-5839	MG	0.00	0.00	500.00
3234	-5988	-5879	-5878	-5987	MG	0.00	0.00	500.00
3234	-5996	-5888	-5887	-5995	MG	0.00	0.00	500.00
3234	-5998	-5890	-5889	-5997	MG	0.00	0.00	500.00
3234	-6129	-6061	-6060	-6128	MG	0.00	0.00	500.00
3234	-5972	-5893	-5892	-6000	MG	0.00	0.00	500.00
3234	-5880	-5838	-5837	-5879	MG	0.00	0.00	500.00
3234	-6075	-5972	-6000	-6074	MG	0.00	0.00	500.00
3234	-5879	-5837	-5836	-5878	MG	0.00	0.00	500.00
3234	-5883	-5841	-5840	-5882	MG	0.00	0.00	500.00
3234	-6061	-5988	-5987	-6060	MG	0.00	0.00	500.00
3234	-6134	-6066	-6065	-6133	MG	0.00	0.00	500.00
3234	-6066	-5993	-5992	-6065	MG	0.00	0.00	500.00
3234	-5993	-5884	-5883	-5992	MG	0.00	0.00	500.00
3234	-5997	-5889	-5888	-5996	MG	0.00	0.00	500.00
3234	-6141	-6073	-6072	-6140	MG	0.00	0.00	500.00
3234	-6133	-6065	-6064	-6132	MG	0.00	0.00	500.00
3234	-6239	-6196	-6195	-6248	MG	0.00	0.00	500.00
3234	-6188	-6131	-6130	-6187	MG	0.00	0.00	500.00
3234	-6065	-5992	-5991	-6064	MG	0.00	0.00	500.00
3234	-5845	-5799	-5798	-5844	MG	0.00	0.00	500.00
3234	-6064	-5991	-5990	-6063	MG	0.00	0.00	500.00
3234	-5994	-5993	-6066	-6067	MG	0.00	0.00	500.00
3234	-5991	-5882	-5881	-5990	MG	0.00	0.00	500.00
3234	-5841	-5795	-5794	-5840	MG	0.00	0.00	500.00
3234	-6195	-6138	-6137	-6194	MG	0.00	0.00	500.00
3234	-5886	-5885	-5994	-6025	MG	0.00	0.00	500.00
3234	-6131	-6063	-6062	-6130	MG	0.00	0.00	500.00
3234	-6237	-6188	-6187	-6236	MG	0.00	0.00	500.00
3234	-6192	-6191	-6238	-6245	MG	0.00	0.00	500.00
3234	-6071	-5997	-5996	-6070	MG	0.00	0.00	500.00
3234	-6193	-6192	-6245	-6246	MG	0.00	0.00	500.00
3234	-5889	-5847	-5846	-5888	MG	0.00	0.00	500.00
3234	-5836	-5790	-5789	-5835	MG	0.00	0.00	500.00
3234	-6251	-6199	-6198	-6250	MG	0.00	0.00	500.00
3234	-5893	-5851	-5850	-5892	MG	0.00	0.00	500.00

3234	-6200	-6143	-6142	-6199	MG	0.00	0.00	500.00
3234	-5844	-5843	-5885	-5886	MG	0.00	0.00	500.00
3234	-6186	-6129	-6128	-6185	MG	0.00	0.00	500.00
3234	-6136	-6137	-6069	-6068	MG	0.00	0.00	500.00
3234	-6132	-6064	-6063	-6131	MG	0.00	0.00	500.00
3234	-5849	-5803	-5802	-5848	MG	0.00	0.00	500.00
3234	-6025	-5994	-6067	-6068	MG	0.00	0.00	500.00
3234	-6190	-6133	-6132	-6189	MG	0.00	0.00	500.00
3234	-6243	-6189	-6188	-6237	MG	0.00	0.00	500.00
3234	-5850	-5804	-5803	-5849	MG	0.00	0.00	500.00
3234	-6191	-6134	-6133	-6190	MG	0.00	0.00	500.00
3234	-6139	-6071	-6070	-6138	MG	0.00	0.00	500.00
3234	-6189	-6132	-6131	-6188	MG	0.00	0.00	500.00
3234	-6072	-5998	-5997	-6071	MG	0.00	0.00	500.00
3234	-6135	-6134	-6191	-6192	MG	0.00	0.00	500.00
3234	-6143	-6075	-6074	-6142	MG	0.00	0.00	500.00
3234	-6197	-6140	-6139	-6196	MG	0.00	0.00	500.00
3234	-6235	-6186	-6185	-6242	MG	0.00	0.00	500.00
3235	-7579	-4254	-4379	-7666	MG	0.00	0.00	500.00
3235	-7666	-4379	-4420	-7712	MG	0.00	0.00	500.00
3235	-7976	-4363	-4503	-8030	MG	0.00	0.00	500.00
3235	-7930	-4418	-4363	-7976	MG	0.00	0.00	500.00
3235	-7807	-4462	-4418	-7930	MG	0.00	0.00	500.00
3235	-7712	-4420	-4462	-7807	MG	0.00	0.00	500.00
3236	-4104	-3906	-7498	-7499	MG	0.00	0.00	500.00
3236	-3906	-4492	-7498	-7498	MG	0.00	0.00	500.00
3239	-4950	-5065	-5674	-5674	MG	0.00	0.00	500.00
3240	-4169	-5013	-7973	-7973	MG	0.00	0.00	500.00
3242	-5352	-4471	-5458	-5458	MG	0.00	0.00	500.00
3242	-5352	-5458	-6100	-6100	MG	0.00	0.00	500.00
3245	-5781	-4964	-5854	-5854	MG	0.00	0.00	500.00
3246	-6170	-4322	-5356	-5356	MG	0.00	0.00	500.00
3246	-6221	-3674	-4322	-6170	MG	0.00	0.00	500.00
3255	-5445	-4936	-5444	-5444	MG	0.00	0.00	500.00
3257	-5334	-4700	-5848	-5849	MG	0.00	0.00	500.00
3257	-5850	-5334	-5849	-5849	MG	0.00	0.00	500.00
3259	-3948	-3986	-6673	-6677	MG	0.00	0.00	500.00
3264	-4220	-4252	-7140	-7141	MG	0.00	0.00	500.00
3266	-3608	-3826	-7139	-7140	MG	0.00	0.00	500.00
3267	-4493	-3907	-7502	-7502	MG	0.00	0.00	500.00
3267	-3907	-4105	-7501	-7502	MG	0.00	0.00	500.00
3268	-5681	-5066	-4951	-4951	MG	0.00	0.00	500.00
3269	-5014	-4170	-7977	-7977	MG	0.00	0.00	500.00
3270	-4463	-5459	-5353	-5353	MG	0.00	0.00	500.00
3270	-6101	-5459	-5353	-5353	MG	0.00	0.00	500.00
3271	-4965	-5855	-5773	-5773	MG	0.00	0.00	500.00
3272	-4323	-3675	-6230	-6171	MG	0.00	0.00	500.00
3272	-6171	-5357	-4323	-4323	MG	0.00	0.00	500.00
3273	-6578	-4758	-5784	-5784	MG	0.00	0.00	500.00
3273	-5691	-3956	-6659	-6659	MG	0.00	0.00	500.00
3273	-6659	-3956	-4758	-6578	MG	0.00	0.00	500.00
3274	-4759	-3969	-6660	-6579	MG	0.00	0.00	500.00
3274	-6579	-5766	-4759	-4759	MG	0.00	0.00	500.00
3274	-3969	-5692	-6660	-6660	MG	0.00	0.00	500.00
3305	-5257	-6107	-7092	-7092	MG	0.00	0.00	500.00
3307	-6106	-5256	-7091	-7091	MG	0.00	0.00	500.00
3308	-7022	-6175	-5131	-5131	MG	0.00	0.00	500.00
3308	-5131	-4236	-7092	-7022	MG	0.00	0.00	500.00
3309	-7091	-4235	-5130	-7021	MG	0.00	0.00	500.00
3309	-7021	-5130	-6174	-6174	MG	0.00	0.00	500.00
3325	-5746	-6242	-6235	-6235	MG	0.00	0.00	500.00
3325	-5746	-6235	-6236	-5052	MG	0.00	0.00	500.00
3331	-6151	-6667	-6688	-5447	MG	0.00	0.00	500.00
3332	-8719	-5354	-5286	-8840	MG	0.00	0.00	500.00
3332	-8840	-5286	-5215	-8908	MG	0.00	0.00	500.00
3332	-8908	-5215	-5387	-8982	MG	0.00	0.00	500.00
3332	-8479	-5001	-5254	-8537	MG	0.00	0.00	500.00
3332	-8377	-4884	-4815	-8424	MG	0.00	0.00	500.00
3332	-8228	-4886	-4952	-8316	MG	0.00	0.00	500.00
3332	-8537	-5254	-5304	-8628	MG	0.00	0.00	500.00
3332	-8028	-4494	-4841	-8154	MG	0.00	0.00	500.00
3332	-8316	-4952	-4884	-8377	MG	0.00	0.00	500.00
3332	-8154	-4841	-4886	-8228	MG	0.00	0.00	500.00
3332	-8424	-4815	-5001	-8479	MG	0.00	0.00	500.00
3332	-8628	-5304	-5354	-8719	MG	0.00	0.00	500.00
3333	-6304	-6303	-6371	-6372	MG	0.00	0.00	500.00
3333	-6999	-6998	-7057	-7058	MG	0.00	0.00	500.00
3333	-6917	-6916	-6999	-7000	MG	0.00	0.00	500.00
3333	-6378	-6310	-6309	-6377	MG	0.00	0.00	500.00

3333	-6828	-6743	-6742	-6827	MG	0.00	0.00	500.00
3333	-6301	-6244	-6243	-6300	MG	0.00	0.00	500.00
3333	-6303	-6302	-6370	-6371	MG	0.00	0.00	500.00
3333	-6916	-6915	-6998	-6999	MG	0.00	0.00	500.00
3333	-7061	-7002	-7001	-7060	MG	0.00	0.00	500.00
3333	-6833	-6748	-6747	-6832	MG	0.00	0.00	500.00
3333	-7141	-7061	-7060	-7140	MG	0.00	0.00	500.00
3333	-6834	-6833	-6915	-6916	MG	0.00	0.00	500.00
3333	-6374	-6306	-6305	-6373	MG	0.00	0.00	500.00
3333	-6624	-6539	-6551	-6623	MG	0.00	0.00	500.00
3333	-6994	-6911	-6910	-6993	MG	0.00	0.00	500.00
3333	-7140	-7060	-7059	-7139	MG	0.00	0.00	500.00
3333	-6993	-6910	-6909	-6992	MG	0.00	0.00	500.00
3333	-6379	-6311	-6310	-6378	MG	0.00	0.00	500.00
3333	-6842	-6757	-6756	-6841	MG	0.00	0.00	500.00
3333	-6364	-6296	-6295	-6363	MG	0.00	0.00	500.00
3333	-7062	-7003	-7002	-7061	MG	0.00	0.00	500.00
3333	-7003	-6920	-6919	-7002	MG	0.00	0.00	500.00
3333	-6536	-6477	-6476	-6535	MG	0.00	0.00	500.00
3333	-6484	-6483	-6548	-6549	MG	0.00	0.00	500.00
3333	-7057	-6998	-6997	-7056	MG	0.00	0.00	500.00
3333	-6302	-6238	-6244	-6301	MG	0.00	0.00	500.00
3333	-6547	-6482	-6481	-6538	MG	0.00	0.00	500.00
3333	-6369	-6301	-6300	-6368	MG	0.00	0.00	500.00
3333	-6371	-6370	-6483	-6484	MG	0.00	0.00	500.00
3333	-6485	-6484	-6549	-6550	MG	0.00	0.00	500.00
3333	-7133	-7053	-7052	-7132	MG	0.00	0.00	500.00
3333	-7000	-6999	-7058	-7059	MG	0.00	0.00	500.00
3333	-6492	-6379	-6378	-6491	MG	0.00	0.00	500.00
3333	-6368	-6300	-6299	-6367	MG	0.00	0.00	500.00
3333	-7132	-7052	-7051	-7131	MG	0.00	0.00	500.00
3333	-7136	-7056	-7055	-7135	MG	0.00	0.00	500.00
3333	-6308	-6249	-6239	-6307	MG	0.00	0.00	500.00
3333	-6678	-6625	-6624	-6677	MG	0.00	0.00	500.00
3333	-6625	-6552	-6539	-6624	MG	0.00	0.00	500.00
3333	-6671	-6689	-6748	-6749	MG	0.00	0.00	500.00
3333	-6677	-6624	-6623	-6673	MG	0.00	0.00	500.00
3333	-7146	-7066	-7065	-7145	MG	0.00	0.00	500.00
3333	-7051	-6992	-6991	-7050	MG	0.00	0.00	500.00
3333	-6299	-6237	-6236	-6298	MG	0.00	0.00	500.00
3333	-6306	-6248	-6247	-6305	MG	0.00	0.00	500.00
3333	-6748	-6689	-6670	-6747	MG	0.00	0.00	500.00
3333	-6487	-6374	-6373	-6486	MG	0.00	0.00	500.00
3333	-7056	-6997	-6996	-7055	MG	0.00	0.00	500.00
3333	-6629	-6556	-6555	-6628	MG	0.00	0.00	500.00
3333	-6832	-6747	-6746	-6831	MG	0.00	0.00	500.00
3333	-7143	-7063	-7062	-7142	MG	0.00	0.00	500.00
3333	-7055	-6996	-6995	-7054	MG	0.00	0.00	500.00
3333	-6901	-6842	-6841	-6923	MG	0.00	0.00	500.00
3333	-6297	-6235	-6242	-6296	MG	0.00	0.00	500.00
3333	-6614	-6536	-6535	-6613	MG	0.00	0.00	500.00
3333	-6754	-6690	-6678	-6753	MG	0.00	0.00	500.00
3333	-6477	-6364	-6363	-6476	MG	0.00	0.00	500.00
3333	-6375	-6307	-6306	-6374	MG	0.00	0.00	500.00
3333	-6998	-6915	-6914	-6997	MG	0.00	0.00	500.00
3333	-6619	-6547	-6538	-6618	MG	0.00	0.00	500.00
3333	-6995	-6912	-6911	-6994	MG	0.00	0.00	500.00
3333	-6246	-6245	-6303	-6304	MG	0.00	0.00	500.00
3333	-6830	-6745	-6744	-6829	MG	0.00	0.00	500.00
3333	-6482	-6369	-6368	-6481	MG	0.00	0.00	500.00
3333	-7053	-6994	-6993	-7052	MG	0.00	0.00	500.00
3333	-6377	-6309	-6308	-6376	MG	0.00	0.00	500.00
3333	-6538	-6481	-6480	-6546	MG	0.00	0.00	500.00
3333	-6835	-6834	-6916	-6917	MG	0.00	0.00	500.00
3333	-6829	-6744	-6743	-6828	MG	0.00	0.00	500.00
3333	-6481	-6368	-6367	-6480	MG	0.00	0.00	500.00
3333	-7007	-6901	-6923	-7006	MG	0.00	0.00	500.00
3333	-6300	-6243	-6237	-6299	MG	0.00	0.00	500.00
3333	-6668	-6617	-6616	-6688	MG	0.00	0.00	500.00
3333	-6757	-6693	-6692	-6756	MG	0.00	0.00	500.00
3333	-6546	-6480	-6479	-6537	MG	0.00	0.00	500.00
3333	-6307	-6239	-6248	-6306	MG	0.00	0.00	500.00
3333	-6751	-6673	-6672	-6750	MG	0.00	0.00	500.00
3333	-7131	-7051	-7050	-7130	MG	0.00	0.00	500.00
3333	-6915	-6833	-6832	-6914	MG	0.00	0.00	500.00
3333	-6537	-6479	-6478	-6545	MG	0.00	0.00	500.00
3333	-7059	-7058	-7138	-7139	MG	0.00	0.00	500.00
3333	-6742	-6687	-6666	-6741	MG	0.00	0.00	500.00
3333	-6997	-6914	-6913	-6996	MG	0.00	0.00	500.00

3333	-6922	-6840	-6839	-6921	MG	0.00	0.00	500.00
3333	-6556	-6492	-6491	-6555	MG	0.00	0.00	500.00
3333	-6840	-6755	-6754	-6839	MG	0.00	0.00	500.00
3333	-6545	-6478	-6477	-6536	MG	0.00	0.00	500.00
3333	-6311	-6252	-6251	-6310	MG	0.00	0.00	500.00
3333	-6365	-6297	-6296	-6364	MG	0.00	0.00	500.00
3333	-6921	-6839	-6838	-6920	MG	0.00	0.00	500.00
3333	-6839	-6754	-6753	-6838	MG	0.00	0.00	500.00
3333	-6491	-6378	-6377	-6490	MG	0.00	0.00	500.00
3333	-7142	-7062	-7061	-7141	MG	0.00	0.00	500.00
3333	-7134	-7054	-7053	-7133	MG	0.00	0.00	500.00
3333	-6310	-6251	-6250	-6309	MG	0.00	0.00	500.00
3333	-6912	-6830	-6829	-6911	MG	0.00	0.00	500.00
3333	-6490	-6377	-6376	-6489	MG	0.00	0.00	500.00
3333	-6753	-6678	-6677	-6752	MG	0.00	0.00	500.00
3333	-6621	-6620	-6689	-6671	MG	0.00	0.00	500.00
3333	-6549	-6548	-6620	-6621	MG	0.00	0.00	500.00
3333	-6673	-6623	-6622	-6672	MG	0.00	0.00	500.00
3333	-6618	-6538	-6546	-6617	MG	0.00	0.00	500.00
3333	-6670	-6619	-6618	-6669	MG	0.00	0.00	500.00
3333	-6752	-6677	-6673	-6751	MG	0.00	0.00	500.00
3333	-7001	-6918	-6917	-7000	MG	0.00	0.00	500.00
3333	-6376	-6308	-6307	-6375	MG	0.00	0.00	500.00
3333	-6372	-6371	-6484	-6485	MG	0.00	0.00	500.00
3333	-6550	-6549	-6621	-6622	MG	0.00	0.00	500.00
3333	-6552	-6488	-6487	-6539	MG	0.00	0.00	500.00
3333	-6488	-6375	-6374	-6487	MG	0.00	0.00	500.00
3333	-6480	-6367	-6366	-6479	MG	0.00	0.00	500.00
3333	-7145	-7065	-7064	-7144	MG	0.00	0.00	500.00
3333	-6367	-6299	-6298	-6366	MG	0.00	0.00	500.00
3333	-6992	-6909	-6900	-6991	MG	0.00	0.00	500.00
3333	-6616	-6537	-6545	-6615	MG	0.00	0.00	500.00
3333	-6539	-6487	-6486	-6551	MG	0.00	0.00	500.00
3333	-6827	-6742	-6741	-6826	MG	0.00	0.00	500.00
3333	-7058	-7057	-7137	-7138	MG	0.00	0.00	500.00
3333	-6914	-6832	-6831	-6913	MG	0.00	0.00	500.00
3333	-6623	-6551	-6550	-6622	MG	0.00	0.00	500.00
3333	-7135	-7055	-7054	-7134	MG	0.00	0.00	500.00
3333	-6551	-6486	-6485	-6550	MG	0.00	0.00	500.00
3333	-6373	-6305	-6304	-6372	MG	0.00	0.00	500.00
3333	-6996	-6913	-6912	-6995	MG	0.00	0.00	500.00
3333	-6913	-6831	-6830	-6912	MG	0.00	0.00	500.00
3333	-7137	-7057	-7056	-7136	MG	0.00	0.00	500.00
3333	-6548	-6483	-6482	-6547	MG	0.00	0.00	500.00
3333	-6620	-6548	-6547	-6619	MG	0.00	0.00	500.00
3333	-6370	-6302	-6301	-6369	MG	0.00	0.00	500.00
3333	-7054	-6995	-6994	-7053	MG	0.00	0.00	500.00
3333	-6296	-6242	-6234	-6295	MG	0.00	0.00	500.00
3333	-6622	-6621	-6671	-6672	MG	0.00	0.00	500.00
3333	-6745	-6668	-6668	-6744	MG	0.00	0.00	500.00
3333	-6838	-6753	-6752	-6837	MG	0.00	0.00	500.00
3333	-6627	-6554	-6553	-6626	MG	0.00	0.00	500.00
3333	-6690	-6626	-6625	-6678	MG	0.00	0.00	500.00
3333	-6911	-6829	-6828	-6910	MG	0.00	0.00	500.00
3333	-6626	-6553	-6552	-6625	MG	0.00	0.00	500.00
3333	-6672	-6671	-6749	-6750	MG	0.00	0.00	500.00
3333	-7066	-7007	-7006	-7065	MG	0.00	0.00	500.00
3333	-7052	-6993	-6992	-7051	MG	0.00	0.00	500.00
3333	-6489	-6376	-6375	-6488	MG	0.00	0.00	500.00
3333	-6910	-6828	-6827	-6909	MG	0.00	0.00	500.00
3333	-6617	-6546	-6537	-6616	MG	0.00	0.00	500.00
3333	-6687	-6614	-6613	-6666	MG	0.00	0.00	500.00
3333	-6746	-6669	-6668	-6745	MG	0.00	0.00	500.00
3333	-7065	-7006	-7005	-7064	MG	0.00	0.00	500.00
3333	-6743	-6667	-6687	-6742	MG	0.00	0.00	500.00
3333	-6923	-6841	-6840	-6922	MG	0.00	0.00	500.00
3333	-7144	-7064	-7063	-7143	MG	0.00	0.00	500.00
3333	-6756	-6692	-6691	-6755	MG	0.00	0.00	500.00
3333	-6841	-6756	-6755	-6840	MG	0.00	0.00	500.00
3333	-7005	-6922	-6921	-7004	MG	0.00	0.00	500.00
3333	-6298	-6236	-6235	-6297	MG	0.00	0.00	500.00
3333	-6366	-6298	-6297	-6365	MG	0.00	0.00	500.00
3333	-6755	-6691	-6690	-6754	MG	0.00	0.00	500.00
3333	-6615	-6545	-6536	-6614	MG	0.00	0.00	500.00
3333	-7063	-7004	-7003	-7062	MG	0.00	0.00	500.00
3333	-6692	-6628	-6627	-6691	MG	0.00	0.00	500.00
3333	-6628	-6555	-6554	-6627	MG	0.00	0.00	500.00
3333	-6555	-6491	-6490	-6554	MG	0.00	0.00	500.00
3333	-6750	-6749	-6834	-6835	MG	0.00	0.00	500.00

3333	-6831	-6746	-6745	-6830	MG	0.00	0.00	500.00
3333	-6483	-6370	-6369	-6482	MG	0.00	0.00	500.00
3333	-6245	-6238	-6302	-6303	MG	0.00	0.00	500.00
3333	-6693	-6629	-6628	-6692	MG	0.00	0.00	500.00
3333	-6554	-6490	-6489	-6553	MG	0.00	0.00	500.00
3333	-6691	-6627	-6626	-6690	MG	0.00	0.00	500.00
3333	-6688	-6616	-6615	-6667	MG	0.00	0.00	500.00
3333	-6836	-6751	-6750	-6835	MG	0.00	0.00	500.00
3333	-6919	-6837	-6836	-6918	MG	0.00	0.00	500.00
3333	-6669	-6618	-6617	-6668	MG	0.00	0.00	500.00
3333	-6749	-6748	-6833	-6834	MG	0.00	0.00	500.00
3333	-6747	-6670	-6669	-6746	MG	0.00	0.00	500.00
3333	-7060	-7001	-7000	-7059	MG	0.00	0.00	500.00
3333	-6305	-6247	-6246	-6304	MG	0.00	0.00	500.00
3333	-6918	-6836	-6835	-6917	MG	0.00	0.00	500.00
3333	-6689	-6620	-6619	-6670	MG	0.00	0.00	500.00
3333	-6478	-6365	-6364	-6477	MG	0.00	0.00	500.00
3333	-6479	-6366	-6365	-6478	MG	0.00	0.00	500.00
3333	-7002	-6919	-6918	-7001	MG	0.00	0.00	500.00
3333	-7006	-6923	-6922	-7005	MG	0.00	0.00	500.00
3333	-6667	-6615	-6614	-6668	MG	0.00	0.00	500.00
3333	-6909	-6827	-6826	-6908	MG	0.00	0.00	500.00
3333	-6920	-6838	-6837	-6919	MG	0.00	0.00	500.00
3333	-6553	-6489	-6488	-6552	MG	0.00	0.00	500.00
3333	-7004	-6921	-6920	-7003	MG	0.00	0.00	500.00
3333	-6486	-6373	-6372	-6485	MG	0.00	0.00	500.00
3333	-6744	-6688	-6667	-6743	MG	0.00	0.00	500.00
3333	-6837	-6752	-6751	-6836	MG	0.00	0.00	500.00
3333	-6309	-6250	-6249	-6308	MG	0.00	0.00	500.00
3333	-7064	-7005	-7004	-7063	MG	0.00	0.00	500.00
3334	-8230	-4887	-4953	-8318	MG	0.00	0.00	500.00
3334	-8481	-5002	-5255	-8539	MG	0.00	0.00	500.00
3334	-8318	-4953	-4885	-8379	MG	0.00	0.00	500.00
3334	-8030	-4503	-4842	-8156	MG	0.00	0.00	500.00
3334	-8721	-5355	-5287	-8841	MG	0.00	0.00	500.00
3334	-8156	-4842	-4887	-8230	MG	0.00	0.00	500.00
3334	-8379	-4885	-4816	-8426	MG	0.00	0.00	500.00
3334	-8426	-4816	-5002	-8481	MG	0.00	0.00	500.00
3334	-8841	-5287	-5216	-8910	MG	0.00	0.00	500.00
3334	-8629	-5305	-5355	-8721	MG	0.00	0.00	500.00
3334	-8910	-5216	-5398	-8984	MG	0.00	0.00	500.00
3334	-8539	-5255	-5305	-8629	MG	0.00	0.00	500.00
3335	-7498	-4492	-4459	-7497	MG	0.00	0.00	500.00
3339	-4362	-4169	-7973	-7974	MG	0.00	0.00	500.00
3342	-4421	-5418	-8423	-8423	MG	0.00	0.00	500.00
3345	-5781	-5854	-6493	-6493	MG	0.00	0.00	500.00
3346	-6170	-5356	-6259	-6259	MG	0.00	0.00	500.00
3364	-5747	-5053	-6249	-6250	MG	0.00	0.00	500.00
3364	-6251	-5747	-6250	-6250	MG	0.00	0.00	500.00
3372	-6152	-5448	-6690	-6691	MG	0.00	0.00	500.00
3380	-4460	-4493	-7502	-7503	MG	0.00	0.00	500.00
3384	-4170	-4363	-7976	-7977	MG	0.00	0.00	500.00
3386	-5397	-4422	-8427	-8427	MG	0.00	0.00	500.00
3388	-6494	-5855	-5773	-5773	MG	0.00	0.00	500.00
3390	-5357	-6269	-6171	-6171	MG	0.00	0.00	500.00
3424	-7021	-6174	-7156	-7156	MG	0.00	0.00	500.00
3426	-6175	-7157	-7022	-7022	MG	0.00	0.00	500.00
3435	-6151	-6687	-6667	-6667	MG	0.00	0.00	500.00
3436	-9550	-6104	-6172	-9598	MG	0.00	0.00	500.00
3436	-9073	-5620	-5701	-9149	MG	0.00	0.00	500.00
3436	-9440	-5808	-6036	-9479	MG	0.00	0.00	500.00
3436	-9727	-6001	-6206	-9855	MG	0.00	0.00	500.00
3436	-10194	-6495	-6380	-10249	MG	0.00	0.00	500.00
3436	-9968	-6437	-6501	-10034	MG	0.00	0.00	500.00
3436	-9374	-5605	-5808	-9440	MG	0.00	0.00	500.00
3436	-9207	-5783	-5689	-9283	MG	0.00	0.00	500.00
3436	-9283	-5689	-5605	-9374	MG	0.00	0.00	500.00
3436	-9479	-6036	-6104	-9550	MG	0.00	0.00	500.00
3436	-9149	-5701	-5783	-9207	MG	0.00	0.00	500.00
3436	-9598	-6172	-6102	-9640	MG	0.00	0.00	500.00
3436	-9640	-6102	-6001	-9727	MG	0.00	0.00	500.00
3436	-9855	-6206	-6437	-9968	MG	0.00	0.00	500.00
3436	-8982	-5387	-5620	-9073	MG	0.00	0.00	500.00
3436	-10034	-6501	-6597	-10126	MG	0.00	0.00	500.00
3436	-10126	-6597	-6495	-10194	MG	0.00	0.00	500.00
3437	-8229	-8228	-8316	-8317	MG	0.00	0.00	500.00
3437	-10199	-10133	-10132	-10198	MG	0.00	0.00	500.00
3437	-10257	-10201	-10200	-10256	MG	0.00	0.00	500.00
3437	-8427	-8380	-8379	-8426	MG	0.00	0.00	500.00

3437	-10122	-10030	-10029	-10121	MG	0.00	0.00	500.00
3437	-10038	-9946	-9962	-10037	MG	0.00	0.00	500.00
3437	-7974	-7928	-7927	-7973	MG	0.00	0.00	500.00
3437	-7502	-7466	-7465	-7501	MG	0.00	0.00	500.00
3437	-7971	-7925	-7924	-7970	MG	0.00	0.00	500.00
3437	-10129	-10037	-10036	-10128	MG	0.00	0.00	500.00
3437	-8911	-8808	-8841	-8910	MG	0.00	0.00	500.00
3437	-10255	-10199	-10198	-10254	MG	0.00	0.00	500.00
3437	-10041	-9972	-9971	-10040	MG	0.00	0.00	500.00
3437	-10036	-10035	-10127	-10128	MG	0.00	0.00	500.00
3437	-8424	-8377	-8376	-8423	MG	0.00	0.00	500.00
3437	3301	-10193	-10192	-10248	MG	0.00	0.00	500.00
3437	-9446	-9380	-9379	-9445	MG	0.00	0.00	500.00
3437	-10198	-10132	-10131	-10177	MG	0.00	0.00	500.00
3437	-10121	-10029	-10028	-10120	MG	0.00	0.00	500.00
3437	-7666	-7662	-7711	-7712	MG	0.00	0.00	500.00
3437	-10133	-10041	-10040	-10132	MG	0.00	0.00	500.00
3437	3302	-10176	-10196	-10251	MG	0.00	0.00	500.00
3437	-9972	-9849	-9848	-9971	MG	0.00	0.00	500.00
3437	-8984	-8983	-9095	-9074	MG	0.00	0.00	500.00
3437	-10132	-10040	-10039	-10131	MG	0.00	0.00	500.00
3437	-9968	-9855	-9854	-9945	MG	0.00	0.00	500.00
3437	-7269	-7206	-7205	-7268	MG	0.00	0.00	500.00
3437	-10030	-9944	-9943	-10029	MG	0.00	0.00	500.00
3437	-7571	-7497	-7496	-7576	MG	0.00	0.00	500.00
3437	-9557	-9505	-9493	-9556	MG	0.00	0.00	500.00
3437	-8230	-8229	-8317	-8318	MG	0.00	0.00	500.00
3437	-9447	-9381	-9380	-9446	MG	0.00	0.00	500.00
3437	-7349	-7348	-7464	-7465	MG	0.00	0.00	500.00
3437	-7257	-7194	-7193	-7256	MG	0.00	0.00	500.00
3437	-10175	-10121	-10120	-10189	MG	0.00	0.00	500.00
3437	-9493	-9446	-9445	-9488	MG	0.00	0.00	500.00
3437	-9600	-9599	-9641	-9642	MG	0.00	0.00	500.00
3437	-9962	-9857	-9847	-9970	MG	0.00	0.00	500.00
3437	-9857	-9741	-9740	-9847	MG	0.00	0.00	500.00
3437	-7348	-7347	-7463	-7464	MG	0.00	0.00	500.00
3437	-9974	-9863	-9840	-9973	MG	0.00	0.00	500.00
3437	-10127	-10126	-10194	-10195	MG	0.00	0.00	500.00
3437	-8983	-8982	-9073	-9095	MG	0.00	0.00	500.00
3437	-9445	-9379	-9378	-9444	MG	0.00	0.00	500.00
3437	-9742	-9644	-9643	-9741	MG	0.00	0.00	500.00
3437	-9644	-9602	-9601	-9643	MG	0.00	0.00	500.00
3437	-10195	-10194	-10249	-10250	MG	0.00	0.00	500.00
3437	-7468	-7352	-7351	-7467	MG	0.00	0.00	500.00
3437	-7265	-7264	-7298	-7299	MG	0.00	0.00	500.00
3437	-9444	-9378	-9377	-9443	MG	0.00	0.00	500.00
3437	-7801	-7705	-7697	-7800	MG	0.00	0.00	500.00
3437	-7705	-7655	-7654	-7697	MG	0.00	0.00	500.00
3437	-7459	-7343	-7342	-7458	MG	0.00	0.00	500.00
3437	-7501	-7500	-7572	-7579	MG	0.00	0.00	500.00
3437	-9727	-9640	-9639	-9739	MG	0.00	0.00	500.00
3437	-9648	-9606	-9605	-9647	MG	0.00	0.00	500.00
3437	-8420	-8373	-8372	-8419	MG	0.00	0.00	500.00
3437	-7472	-7356	-7355	-7471	MG	0.00	0.00	500.00
3437	-8917	-8809	-8827	-8916	MG	0.00	0.00	500.00
3437	-8433	-8386	-8385	-8432	MG	0.00	0.00	500.00
3437	-9373	-9282	-9281	-9372	MG	0.00	0.00	500.00
3437	-10246	-10190	-10175	-10245	MG	0.00	0.00	500.00
3437	-10134	-10042	-10041	-10133	MG	0.00	0.00	500.00
3437	-9747	-9649	-9648	-9746	MG	0.00	0.00	500.00
3437	-8372	-8311	-8310	-8371	MG	0.00	0.00	500.00
3437	-9485	-9479	-9550	-9551	MG	0.00	0.00	500.00
3437	-9744	-9646	-9645	-9743	MG	0.00	0.00	500.00
3437	-9646	-9604	-9603	-9645	MG	0.00	0.00	500.00
3437	-9604	-9556	-9555	-9603	MG	0.00	0.00	500.00
3437	-8423	-8376	-8375	-8422	MG	0.00	0.00	500.00
3437	-8907	-8824	-8807	-8906	MG	0.00	0.00	500.00
3437	-9740	-9728	-9856	-9847	MG	0.00	0.00	500.00
3437	-9743	-9645	-9644	-9742	MG	0.00	0.00	500.00
3437	-9645	-9603	-9602	-9644	MG	0.00	0.00	500.00
3437	-7505	-7469	-7468	-7504	MG	0.00	0.00	500.00
3437	-9555	-9488	-9504	-9554	MG	0.00	0.00	500.00
3437	-8426	-8425	-8480	-8481	MG	0.00	0.00	500.00
3437	-8539	-8538	-8621	-8629	MG	0.00	0.00	500.00
3437	-7813	-7723	-7722	-7812	MG	0.00	0.00	500.00
3437	-7723	-7671	-7670	-7722	MG	0.00	0.00	500.00
3437	-10196	-10195	-10250	-10251	MG	0.00	0.00	500.00
3437	-8424	-8423	-8472	-8479	MG	0.00	0.00	500.00
3437	-8910	-8909	-8983	-8984	MG	0.00	0.00	500.00

3437	-9074	-9095	-9150	-9151	MG	0.00	0.00	500.00
3437	-7812	-7722	-7716	-7811	MG	0.00	0.00	500.00
3437	-7722	-7670	-7669	-7716	MG	0.00	0.00	500.00
3437	-9377	-9286	-9285	-9376	MG	0.00	0.00	500.00
3437	-10254	-10198	-10177	-10253	MG	0.00	0.00	500.00
3437	-7495	-7459	-7458	-7494	MG	0.00	0.00	500.00
3437	-9847	-9856	-9969	-9970	MG	0.00	0.00	500.00
3437	-10040	-9971	-9963	-10039	MG	0.00	0.00	500.00
3437	-7807	-7806	-7929	-7930	MG	0.00	0.00	500.00
3437	-7711	-7710	-7805	-7806	MG	0.00	0.00	500.00
3437	-9506	-9448	-9447	-9505	MG	0.00	0.00	500.00
3437	-7264	-7263	-7297	-7298	MG	0.00	0.00	500.00
3437	-7138	-7137	-7200	-7201	MG	0.00	0.00	500.00
3437	-9739	-9639	-9638	-9738	MG	0.00	0.00	500.00
3437	-7715	-7668	-7643	-7721	MG	0.00	0.00	500.00
3437	-7668	-7583	-7582	-7643	MG	0.00	0.00	500.00
3437	-7583	-7505	-7504	-7582	MG	0.00	0.00	500.00
3437	-10197	-10130	-10129	-10176	MG	0.00	0.00	500.00
3437	-10130	-10038	-10037	-10129	MG	0.00	0.00	500.00
3437	-10200	-10134	-10133	-10199	MG	0.00	0.00	500.00
3437	-7291	-7257	-7256	-7290	MG	0.00	0.00	500.00
3437	-7643	-7582	-7581	-7667	MG	0.00	0.00	500.00
3437	-10176	-10129	-10128	-10196	MG	0.00	0.00	500.00
3437	-10256	-10200	-10199	-10255	MG	0.00	0.00	500.00
3437	-10037	-9962	-9970	-10036	MG	0.00	0.00	500.00
3437	-7299	-7298	-7348	-7349	MG	0.00	0.00	500.00
3437	-7714	-7667	-7663	-7713	MG	0.00	0.00	500.00
3437	-9863	-9747	-9746	-9840	MG	0.00	0.00	500.00
3437	-7581	-7503	-7502	-7580	MG	0.00	0.00	500.00
3437	-7931	-7808	-7807	-7930	MG	0.00	0.00	500.00
3437	-7808	-7713	-7712	-7807	MG	0.00	0.00	500.00
3437	-9855	-9727	-9739	-9854	MG	0.00	0.00	500.00
3437	-7663	-7580	-7579	-7666	MG	0.00	0.00	500.00
3437	-9554	-9504	-9487	-9553	MG	0.00	0.00	500.00
3437	-9504	-9444	-9443	-9487	MG	0.00	0.00	500.00
3437	-8029	-8028	-8154	-8155	MG	0.00	0.00	500.00
3437	-9643	-9601	-9600	-9642	MG	0.00	0.00	500.00
3437	-9849	-9745	-9744	-9848	MG	0.00	0.00	500.00
3437	-7710	-7661	-7660	-7709	MG	0.00	0.00	500.00
3437	-9487	-9443	-9442	-9486	MG	0.00	0.00	500.00
3437	-7935	-7811	-7810	-7934	MG	0.00	0.00	500.00
3437	-9961	-9839	-9853	-9967	MG	0.00	0.00	500.00
3437	-9856	-9855	-9968	-9969	MG	0.00	0.00	500.00
3437	-9640	-9598	-9597	-9639	MG	0.00	0.00	500.00
3437	-9598	-9550	-9549	-9597	MG	0.00	0.00	500.00
3437	-9550	-9479	-9503	-9549	MG	0.00	0.00	500.00
3437	-7499	-7463	-7462	-7498	MG	0.00	0.00	500.00
3437	-9383	-9292	-9291	-9382	MG	0.00	0.00	500.00
3437	-9853	-9737	-9736	-9838	MG	0.00	0.00	500.00
3437	-9209	-9208	-9284	-9285	MG	0.00	0.00	500.00
3437	-9208	-9207	-9283	-9284	MG	0.00	0.00	500.00
3437	-9095	-9073	-9149	-9150	MG	0.00	0.00	500.00
3437	-8721	-8720	-8825	-8841	MG	0.00	0.00	500.00
3437	-8720	-8719	-8840	-8825	MG	0.00	0.00	500.00
3437	-8538	-8537	-8628	-8621	MG	0.00	0.00	500.00
3437	-10245	-10175	-10189	-10244	MG	0.00	0.00	500.00
3437	-7658	-7576	-7570	-7657	MG	0.00	0.00	500.00
3437	-7576	-7496	-7495	-7570	MG	0.00	0.00	500.00
3437	-9943	-9852	-9837	-9942	MG	0.00	0.00	500.00
3437	-7924	-7802	-7779	-7923	MG	0.00	0.00	500.00
3437	-7802	-7698	-7706	-7779	MG	0.00	0.00	500.00
3437	-7698	-7657	-7656	-7706	MG	0.00	0.00	500.00
3437	-7657	-7570	-7569	-7656	MG	0.00	0.00	500.00
3437	-7570	-7495	-7494	-7569	MG	0.00	0.00	500.00
3437	-7969	-7923	-7922	-7968	MG	0.00	0.00	500.00
3437	-7923	-7779	-7801	-7922	MG	0.00	0.00	500.00
3437	-7671	-7586	-7585	-7670	MG	0.00	0.00	500.00
3437	-7706	-7656	-7655	-7705	MG	0.00	0.00	500.00
3437	-10249	-10194	-10193	3301	MG	0.00	0.00	500.00
3437	-7139	-7138	-7201	-7202	MG	0.00	0.00	500.00
3437	-7968	-7922	-7921	-7967	MG	0.00	0.00	500.00
3437	-7922	-7801	-7800	-7921	MG	0.00	0.00	500.00
3437	-9205	-9147	-9146	-9204	MG	0.00	0.00	500.00
3437	-8909	-8908	-8982	-8983	MG	0.00	0.00	500.00
3437	-7806	-7805	-7928	-7929	MG	0.00	0.00	500.00
3437	-7662	-7661	-7710	-7711	MG	0.00	0.00	500.00
3437	-7930	-7929	-7975	-7976	MG	0.00	0.00	500.00
3437	-8425	-8424	-8479	-8480	MG	0.00	0.00	500.00
3437	-7712	-7711	-7806	-7807	MG	0.00	0.00	500.00

3437	-9374	-9283	-9282	-9373	MG	0.00	0.00	500.00
3437	-10042	-9973	-9972	-10041	MG	0.00	0.00	500.00
3437	-7356	-7306	-7305	-7355	MG	0.00	0.00	500.00
3437	-7306	-7272	-7271	-7305	MG	0.00	0.00	500.00
3437	-7272	-7209	-7208	-7271	MG	0.00	0.00	500.00
3437	-9741	-9643	-9642	-9740	MG	0.00	0.00	500.00
3437	-10043	-9974	-9973	-10042	MG	0.00	0.00	500.00
3437	-10135	-10043	-10042	-10134	MG	0.00	0.00	500.00
3437	-10201	-10135	-10134	-10200	MG	0.00	0.00	500.00
3437	-7305	-7271	-7270	-7304	MG	0.00	0.00	500.00
3437	-7271	-7208	-7207	-7270	MG	0.00	0.00	500.00
3437	-7208	-7145	-7144	-7207	MG	0.00	0.00	500.00
3437	-9556	-9493	-9488	-9555	MG	0.00	0.00	500.00
3437	-7470	-7354	-7353	-7469	MG	0.00	0.00	500.00
3437	-8977	-8903	-8902	-8976	MG	0.00	0.00	500.00
3437	-9970	-9969	-10035	-10036	MG	0.00	0.00	500.00
3437	-10128	-10127	-10195	-10196	MG	0.00	0.00	500.00
3437	-9603	-9555	-9554	-9602	MG	0.00	0.00	500.00
3437	-9143	-9093	-9068	-9142	MG	0.00	0.00	500.00
3437	-9488	-9445	-9444	-9504	MG	0.00	0.00	500.00
3437	-8976	-8902	-8901	-8975	MG	0.00	0.00	500.00
3437	-7303	-7269	-7268	-7302	MG	0.00	0.00	500.00
3437	-9284	-9283	-9374	-9375	MG	0.00	0.00	500.00
3437	-9602	-9554	-9553	-9601	MG	0.00	0.00	500.00
3437	-7504	-7468	-7467	-7503	MG	0.00	0.00	500.00
3437	-8809	-8728	-8727	-8827	MG	0.00	0.00	500.00
3437	-8728	-8635	-8634	-8727	MG	0.00	0.00	500.00
3437	-7805	-7710	-7709	-7804	MG	0.00	0.00	500.00
3437	-9601	-9553	-9552	-9600	MG	0.00	0.00	500.00
3437	-9553	-9487	-9486	-9552	MG	0.00	0.00	500.00
3437	-9443	-9377	-9376	-9442	MG	0.00	0.00	500.00
3437	-7467	-7351	-7350	-7466	MG	0.00	0.00	500.00
3437	-7351	-7301	-7300	-7350	MG	0.00	0.00	500.00
3437	-7301	-7267	-7266	-7300	MG	0.00	0.00	500.00
3437	-7267	-7204	-7203	-7266	MG	0.00	0.00	500.00
3437	-8485	-8432	-8431	-8484	MG	0.00	0.00	500.00
3437	-8915	-8826	-8843	-8914	MG	0.00	0.00	500.00
3437	-9479	-9440	-9439	-9503	MG	0.00	0.00	500.00
3437	-9440	-9374	-9373	-9439	MG	0.00	0.00	500.00
3437	-9639	-9597	-9596	-9638	MG	0.00	0.00	500.00
3437	-9597	-9549	-9548	-9596	MG	0.00	0.00	500.00
3437	-9549	-9503	-9484	-9548	MG	0.00	0.00	500.00
3437	-8311	-8223	-8222	-8310	MG	0.00	0.00	500.00
3437	-7508	-7472	-7471	-7507	MG	0.00	0.00	500.00
3437	-7973	-7927	-7926	-7972	MG	0.00	0.00	500.00
3437	-7983	-7937	-7936	-7982	MG	0.00	0.00	500.00
3437	-7263	-7200	-7199	-7262	MG	0.00	0.00	500.00
3437	-7200	-7137	-7136	-7199	MG	0.00	0.00	500.00
3437	-10029	-9943	-9942	-10028	MG	0.00	0.00	500.00
3437	-7975	-7974	-8028	-8029	MG	0.00	0.00	500.00
3437	-7296	-7262	-7261	-7295	MG	0.00	0.00	500.00
3437	-7262	-7199	-7198	-7261	MG	0.00	0.00	500.00
3437	-8379	-8378	-8425	-8426	MG	0.00	0.00	500.00
3437	-7497	-7461	-7460	-7496	MG	0.00	0.00	500.00
3437	-7461	-7345	-7344	-7460	MG	0.00	0.00	500.00
3437	-7345	-7295	-7294	-7344	MG	0.00	0.00	500.00
3437	-7295	-7261	-7260	-7294	MG	0.00	0.00	500.00
3437	-7261	-7198	-7197	-7260	MG	0.00	0.00	500.00
3437	-7198	-7135	-7134	-7197	MG	0.00	0.00	500.00
3437	-7496	-7460	-7459	-7495	MG	0.00	0.00	500.00
3437	-7460	-7344	-7343	-7459	MG	0.00	0.00	500.00
3437	-7344	-7294	-7293	-7343	MG	0.00	0.00	500.00
3437	-7294	-7260	-7259	-7293	MG	0.00	0.00	500.00
3437	-7260	-7197	-7196	-7259	MG	0.00	0.00	500.00
3437	-7197	-7134	-7133	-7196	MG	0.00	0.00	500.00
3437	-6558	-7131	-7132	-7132	MG	0.00	0.00	500.00
3437	-6558	-7132	-7133	-5852	MG	0.00	0.00	500.00
3437	-7343	-7293	-7292	-7342	MG	0.00	0.00	500.00
3437	-7293	-7259	-7258	-7292	MG	0.00	0.00	500.00
3437	-7259	-7196	-7195	-7258	MG	0.00	0.00	500.00
3437	-7196	-7133	-7132	-7195	MG	0.00	0.00	500.00
3437	-7494	-7458	-7457	-7493	MG	0.00	0.00	500.00
3437	-7458	-7342	-7341	-7457	MG	0.00	0.00	500.00
3437	-7342	-7292	-7291	-7341	MG	0.00	0.00	500.00
3437	-7292	-7258	-7257	-7291	MG	0.00	0.00	500.00
3437	-7258	-7195	-7194	-7257	MG	0.00	0.00	500.00
3437	-7195	-7132	-7131	-7194	MG	0.00	0.00	500.00
3437	-7493	-7457	-7456	-7492	MG	0.00	0.00	500.00
3437	-7457	-7341	-7340	-7456	MG	0.00	0.00	500.00

3437	-7341	-7291	-7290	-7340	MG	0.00	0.00	500.00
3437	-8534	-8471	-8470	-8533	MG	0.00	0.00	500.00
3437	-8471	-8421	-8420	-8470	MG	0.00	0.00	500.00
3437	-7194	-7131	-7130	-7193	MG	0.00	0.00	500.00
3437	-7465	-7464	-7500	-7501	MG	0.00	0.00	500.00
3437	-7464	-7463	-7499	-7500	MG	0.00	0.00	500.00
3437	-8617	-8533	-8532	-8616	MG	0.00	0.00	500.00
3437	-7298	-7297	-7347	-7348	MG	0.00	0.00	500.00
3437	-10194	-10126	-10125	-10193	MG	0.00	0.00	500.00
3437	-10126	-10034	-10033	-10125	MG	0.00	0.00	500.00
3437	-10034	-9968	-9945	-10033	MG	0.00	0.00	500.00
3437	-8714	-8616	-8627	-8713	MG	0.00	0.00	500.00
3437	-8616	-8532	-8531	-8627	MG	0.00	0.00	500.00
3437	-8532	-8469	-8477	-8531	MG	0.00	0.00	500.00
3437	-7580	-7502	-7501	-7579	MG	0.00	0.00	500.00
3437	-8030	-8029	-8155	-8156	MG	0.00	0.00	500.00
3437	-8802	-8713	-8712	-8801	MG	0.00	0.00	500.00
3437	-7302	-7268	-7267	-7301	MG	0.00	0.00	500.00
3437	-9969	-9968	-10034	-10035	MG	0.00	0.00	500.00
3437	-9728	-9727	-9855	-9856	MG	0.00	0.00	500.00
3437	-7503	-7467	-7466	-7502	MG	0.00	0.00	500.00
3437	-8841	-8825	-8909	-8910	MG	0.00	0.00	500.00
3437	-8825	-8840	-8908	-8909	MG	0.00	0.00	500.00
3437	-9839	-9738	-9737	-9853	MG	0.00	0.00	500.00
3437	-10247	-10191	-10190	-10246	MG	0.00	0.00	500.00
3437	-10191	-10123	-10122	-10190	MG	0.00	0.00	500.00
3437	-10123	-10031	-10030	-10122	MG	0.00	0.00	500.00
3437	-8237	-8163	-8162	-8236	MG	0.00	0.00	500.00
3437	-7977	-7931	-7930	-7976	MG	0.00	0.00	500.00
3437	-8037	-7983	-7982	-8036	MG	0.00	0.00	500.00
3437	-8432	-8385	-8384	-8431	MG	0.00	0.00	500.00
3437	-10190	-10122	-10121	-10175	MG	0.00	0.00	500.00
3437	-9599	-9598	-9640	-9641	MG	0.00	0.00	500.00
3437	-8236	-8162	-8161	-8235	MG	0.00	0.00	500.00
3437	-9944	-9838	-9852	-9943	MG	0.00	0.00	500.00
3437	-9838	-9736	-9726	-9852	MG	0.00	0.00	500.00
3437	-8431	-8384	-8383	-8430	MG	0.00	0.00	500.00
3437	-8384	-8323	-8322	-8383	MG	0.00	0.00	500.00
3437	-8323	-8235	-8234	-8322	MG	0.00	0.00	500.00
3437	-8235	-8161	-8160	-8234	MG	0.00	0.00	500.00
3437	-8161	-8035	-8034	-8160	MG	0.00	0.00	500.00
3437	-9852	-9726	-9735	-9837	MG	0.00	0.00	500.00
3437	-10244	-10189	-10188	-10243	MG	0.00	0.00	500.00
3437	-10189	-10120	-10119	-10188	MG	0.00	0.00	500.00
3437	-10120	-10028	-10027	-10119	MG	0.00	0.00	500.00
3437	-10028	-9942	-9941	-10027	MG	0.00	0.00	500.00
3437	-9942	-9837	-9846	-9941	MG	0.00	0.00	500.00
3437	-9837	-9735	-9734	-9846	MG	0.00	0.00	500.00
3437	-7202	-7201	-7264	-7265	MG	0.00	0.00	500.00
3437	-7201	-7200	-7263	-7264	MG	0.00	0.00	500.00
3437	-9375	-9374	-9440	-9441	MG	0.00	0.00	500.00
3437	-10035	-10034	-10126	-10127	MG	0.00	0.00	500.00
3437	-9649	-9607	-9606	-9648	MG	0.00	0.00	500.00
3437	-9607	-9559	-9558	-9606	MG	0.00	0.00	500.00
3437	-9559	-9507	-9506	-9558	MG	0.00	0.00	500.00
3437	-9507	-9449	-9448	-9506	MG	0.00	0.00	500.00
3437	-9449	-9383	-9382	-9448	MG	0.00	0.00	500.00
3437	-9746	-9648	-9647	-9745	MG	0.00	0.00	500.00
3437	-9376	-9375	-9441	-9442	MG	0.00	0.00	500.00
3437	-9606	-9558	-9557	-9605	MG	0.00	0.00	500.00
3437	-9558	-9506	-9505	-9557	MG	0.00	0.00	500.00
3437	-9486	-9485	-9551	-9552	MG	0.00	0.00	500.00
3437	-9448	-9382	-9381	-9447	MG	0.00	0.00	500.00
3437	-9745	-9647	-9646	-9744	MG	0.00	0.00	500.00
3437	-9647	-9605	-9604	-9646	MG	0.00	0.00	500.00
3437	-9605	-9557	-9556	-9604	MG	0.00	0.00	500.00
3437	-7498	-7462	-7461	-7497	MG	0.00	0.00	500.00
3437	-9505	-9447	-9446	-9493	MG	0.00	0.00	500.00
3437	-7976	-7975	-8029	-8030	MG	0.00	0.00	500.00
3437	-8156	-8155	-8229	-8230	MG	0.00	0.00	500.00
3437	-8318	-8317	-8378	-8379	MG	0.00	0.00	500.00
3437	-8317	-8316	-8377	-8378	MG	0.00	0.00	500.00
3437	-8155	-8154	-8228	-8229	MG	0.00	0.00	500.00
3437	-8537	-8536	-8620	-8628	MG	0.00	0.00	500.00
3437	-8628	-8620	-8718	-8719	MG	0.00	0.00	500.00
3437	-8719	-8718	-8824	-8840	MG	0.00	0.00	500.00
3437	-8840	-8824	-8907	-8908	MG	0.00	0.00	500.00
3437	-8376	-8315	-8314	-8375	MG	0.00	0.00	500.00
3437	-8315	-8227	-8226	-8314	MG	0.00	0.00	500.00

3437	-8227	-8153	-8152	-8226	MG	0.00	0.00	500.00
3437	-8153	-8027	-8026	-8152	MG	0.00	0.00	500.00
3437	-8027	-7973	-7972	-8026	MG	0.00	0.00	500.00
3437	-8422	-8375	-8374	-8421	MG	0.00	0.00	500.00
3437	-8375	-8314	-8313	-8374	MG	0.00	0.00	500.00
3437	-8314	-8226	-8225	-8313	MG	0.00	0.00	500.00
3437	-8226	-8152	-8151	-8225	MG	0.00	0.00	500.00
3437	-8152	-8026	-8025	-8151	MG	0.00	0.00	500.00
3437	-8026	-7972	-7971	-8025	MG	0.00	0.00	500.00
3437	-8421	-8374	-8373	-8420	MG	0.00	0.00	500.00
3437	-8374	-8313	-8312	-8373	MG	0.00	0.00	500.00
3437	-8313	-8225	-8224	-8312	MG	0.00	0.00	500.00
3437	-8225	-8151	-8150	-8224	MG	0.00	0.00	500.00
3437	-8151	-8025	-8024	-8150	MG	0.00	0.00	500.00
3437	-8025	-7971	-7970	-8024	MG	0.00	0.00	500.00
3437	-8545	-8485	-8484	-8544	MG	0.00	0.00	500.00
3437	-8373	-8312	-8311	-8372	MG	0.00	0.00	500.00
3437	-8312	-8224	-8223	-8311	MG	0.00	0.00	500.00
3437	-8224	-8150	-8149	-8223	MG	0.00	0.00	500.00
3437	-8150	-8024	-8023	-8149	MG	0.00	0.00	500.00
3437	-8024	-7970	-7969	-8023	MG	0.00	0.00	500.00
3437	-8419	-8372	-8371	-8418	MG	0.00	0.00	500.00
3437	-7579	-7572	-7662	-7666	MG	0.00	0.00	500.00
3437	-9503	-9439	-9438	-9484	MG	0.00	0.00	500.00
3437	-8223	-8149	-8148	-8222	MG	0.00	0.00	500.00
3437	-8149	-8023	-8022	-8148	MG	0.00	0.00	500.00
3437	-8023	-7969	-7968	-8022	MG	0.00	0.00	500.00
3437	-8418	-8371	-8370	-8417	MG	0.00	0.00	500.00
3437	-8371	-8310	-8309	-8370	MG	0.00	0.00	500.00
3437	-8310	-8222	-8221	-8309	MG	0.00	0.00	500.00
3437	-8222	-8148	-8147	-8221	MG	0.00	0.00	500.00
3437	-8148	-8022	-8021	-8147	MG	0.00	0.00	500.00
3437	-8022	-7968	-7967	-8021	MG	0.00	0.00	500.00
3437	-9595	-9547	-9546	-9594	MG	0.00	0.00	500.00
3437	-8378	-8377	-8424	-8425	MG	0.00	0.00	500.00
3437	-7937	-7813	-7812	-7936	MG	0.00	0.00	500.00
3437	-9437	-9371	-9370	-9436	MG	0.00	0.00	500.00
3437	-9736	-9636	-9635	-9726	MG	0.00	0.00	500.00
3437	-9636	-9594	-9593	-9635	MG	0.00	0.00	500.00
3437	-7586	-7508	-7507	-7585	MG	0.00	0.00	500.00
3437	-7982	-7936	-7935	-7981	MG	0.00	0.00	500.00
3437	-7936	-7812	-7811	-7935	MG	0.00	0.00	500.00
3437	-9436	-9370	-9369	-9435	MG	0.00	0.00	500.00
3437	-9726	-9635	-9634	-9735	MG	0.00	0.00	500.00
3437	-7670	-7585	-7584	-7669	MG	0.00	0.00	500.00
3437	-7585	-7507	-7506	-7584	MG	0.00	0.00	500.00
3437	-7981	-7935	-7934	-7980	MG	0.00	0.00	500.00
3437	-9477	-9435	-9434	-9476	MG	0.00	0.00	500.00
3437	-7811	-7716	-7715	-7810	MG	0.00	0.00	500.00
3437	-7716	-7669	-7668	-7715	MG	0.00	0.00	500.00
3437	-7669	-7584	-7583	-7668	MG	0.00	0.00	500.00
3437	-7584	-7506	-7505	-7583	MG	0.00	0.00	500.00
3437	-7980	-7934	-7933	-7979	MG	0.00	0.00	500.00
3437	-7934	-7810	-7809	-7933	MG	0.00	0.00	500.00
3437	-7810	-7715	-7721	-7809	MG	0.00	0.00	500.00
3437	-9642	-9641	-9728	-9740	MG	0.00	0.00	500.00
3437	-9641	-9640	-9727	-9728	MG	0.00	0.00	500.00
3437	-9552	-9551	-9599	-9600	MG	0.00	0.00	500.00
3437	-7979	-7933	-7932	-7978	MG	0.00	0.00	500.00
3437	-7933	-7809	-7781	-7932	MG	0.00	0.00	500.00
3437	-7809	-7721	-7714	-7781	MG	0.00	0.00	500.00
3437	-7721	-7643	-7667	-7714	MG	0.00	0.00	500.00
3437	-9100	-8991	-8990	-9099	MG	0.00	0.00	500.00
3437	-7582	-7504	-7503	-7581	MG	0.00	0.00	500.00
3437	-7978	-7932	-7931	-7977	MG	0.00	0.00	500.00
3437	-7932	-7781	-7808	-7931	MG	0.00	0.00	500.00
3437	-7781	-7714	-7713	-7808	MG	0.00	0.00	500.00
3437	-9157	-9099	-9098	-9156	MG	0.00	0.00	500.00
3437	-7667	-7581	-7580	-7663	MG	0.00	0.00	500.00
3437	-8990	-8916	-8915	-8989	MG	0.00	0.00	500.00
3437	-9381	-9290	-9289	-9380	MG	0.00	0.00	500.00
3437	-9290	-9214	-9213	-9289	MG	0.00	0.00	500.00
3437	-7713	-7663	-7666	-7712	MG	0.00	0.00	500.00
3437	-9156	-9098	-9097	-9155	MG	0.00	0.00	500.00
3437	-9098	-8989	-8988	-9097	MG	0.00	0.00	500.00
3437	-7500	-7499	-7578	-7572	MG	0.00	0.00	500.00
3437	-9380	-9289	-9288	-9379	MG	0.00	0.00	500.00
3437	-7928	-7805	-7804	-7927	MG	0.00	0.00	500.00
3437	-9213	-9155	-9154	-9212	MG	0.00	0.00	500.00

3437	-9155	-9097	-9096	-9154	MG	0.00	0.00	500.00
3437	-7661	-7578	-7577	-7660	MG	0.00	0.00	500.00
3437	-7578	-7499	-7498	-7577	MG	0.00	0.00	500.00
3437	-7927	-7804	-7780	-7926	MG	0.00	0.00	500.00
3437	-7804	-7709	-7708	-7780	MG	0.00	0.00	500.00
3437	-7709	-7660	-7659	-7708	MG	0.00	0.00	500.00
3437	-7660	-7577	-7571	-7659	MG	0.00	0.00	500.00
3437	-7577	-7498	-7497	-7571	MG	0.00	0.00	500.00
3437	-7972	-7926	-7925	-7971	MG	0.00	0.00	500.00
3437	-7926	-7780	-7803	-7925	MG	0.00	0.00	500.00
3437	-7780	-7708	-7707	-7803	MG	0.00	0.00	500.00
3437	-7708	-7659	-7658	-7707	MG	0.00	0.00	500.00
3437	-7659	-7571	-7576	-7658	MG	0.00	0.00	500.00
3437	-9076	-8986	-8985	-9075	MG	0.00	0.00	500.00
3437	-8986	-8912	-8911	-8985	MG	0.00	0.00	500.00
3437	-7925	-7803	-7802	-7924	MG	0.00	0.00	500.00
3437	-7803	-7707	-7698	-7802	MG	0.00	0.00	500.00
3437	-7707	-7658	-7657	-7698	MG	0.00	0.00	500.00
3437	-9075	-8985	-8984	-9074	MG	0.00	0.00	500.00
3437	-8985	-8911	-8910	-8984	MG	0.00	0.00	500.00
3437	-7970	-7924	-7923	-7969	MG	0.00	0.00	500.00
3437	-9441	-9440	-9479	-9485	MG	0.00	0.00	500.00
3437	-9283	-9207	-9206	-9282	MG	0.00	0.00	500.00
3437	-9207	-9149	-9148	-9206	MG	0.00	0.00	500.00
3437	-9149	-9073	-9072	-9148	MG	0.00	0.00	500.00
3437	-9073	-8982	-8981	-9072	MG	0.00	0.00	500.00
3437	-8982	-8908	-8907	-8981	MG	0.00	0.00	500.00
3437	-9282	-9206	-9205	-9281	MG	0.00	0.00	500.00
3437	-7779	-7706	-7705	-7801	MG	0.00	0.00	500.00
3437	-9148	-9072	-9071	-9147	MG	0.00	0.00	500.00
3437	-7656	-7569	-7568	-7655	MG	0.00	0.00	500.00
3437	-7569	-7494	-7493	-7568	MG	0.00	0.00	500.00
3437	-9372	-9281	-9280	-9371	MG	0.00	0.00	500.00
3437	-9281	-9205	-9204	-9280	MG	0.00	0.00	500.00
3437	-8033	-7979	-7978	-8032	MG	0.00	0.00	500.00
3437	-9147	-9071	-9094	-9146	MG	0.00	0.00	500.00
3437	-7655	-7568	-7567	-7654	MG	0.00	0.00	500.00
3437	-7568	-7493	-7492	-7567	MG	0.00	0.00	500.00
3437	-9371	-9280	-9279	-9370	MG	0.00	0.00	500.00
3437	-7929	-7928	-7974	-7975	MG	0.00	0.00	500.00
3437	-9204	-9146	-9145	-9203	MG	0.00	0.00	500.00
3437	-9146	-9094	-9070	-9145	MG	0.00	0.00	500.00
3437	-9094	-8979	-8978	-9070	MG	0.00	0.00	500.00
3437	-8979	-8905	-8904	-8978	MG	0.00	0.00	500.00
3437	-9370	-9279	-9278	-9369	MG	0.00	0.00	500.00
3437	-9279	-9203	-9202	-9278	MG	0.00	0.00	500.00
3437	-7209	-7146	-7145	-7208	MG	0.00	0.00	500.00
3437	-7507	-7471	-7470	-7506	MG	0.00	0.00	500.00
3437	-7471	-7355	-7354	-7470	MG	0.00	0.00	500.00
3437	-7355	-7305	-7304	-7354	MG	0.00	0.00	500.00
3437	-9369	-9278	-9277	-9368	MG	0.00	0.00	500.00
3437	-9278	-9202	-9201	-9277	MG	0.00	0.00	500.00
3437	-9202	-9144	-9143	-9201	MG	0.00	0.00	500.00
3437	-7506	-7470	-7469	-7505	MG	0.00	0.00	500.00
3437	-9069	-8977	-8976	-9093	MG	0.00	0.00	500.00
3437	-7354	-7304	-7303	-7353	MG	0.00	0.00	500.00
3437	-7304	-7270	-7269	-7303	MG	0.00	0.00	500.00
3437	-7270	-7207	-7206	-7269	MG	0.00	0.00	500.00
3437	-7207	-7144	-7143	-7206	MG	0.00	0.00	500.00
3437	-8470	-8420	-8419	-8469	MG	0.00	0.00	500.00
3437	-7469	-7353	-7352	-7468	MG	0.00	0.00	500.00
3437	-7353	-7303	-7302	-7352	MG	0.00	0.00	500.00
3437	-9285	-9284	-9375	-9376	MG	0.00	0.00	500.00
3437	-9214	-9156	-9155	-9213	MG	0.00	0.00	500.00
3437	-7206	-7143	-7142	-7205	MG	0.00	0.00	500.00
3437	-9150	-9149	-9207	-9208	MG	0.00	0.00	500.00
3437	-10033	-9945	-9961	-10032	MG	0.00	0.00	500.00
3437	-7352	-7302	-7301	-7351	MG	0.00	0.00	500.00
3437	-8635	-8546	-8545	-8634	MG	0.00	0.00	500.00
3437	-7268	-7205	-7204	-7267	MG	0.00	0.00	500.00
3437	-7205	-7142	-7141	-7204	MG	0.00	0.00	500.00
3437	-8916	-8827	-8826	-8915	MG	0.00	0.00	500.00
3437	-8827	-8727	-8726	-8826	MG	0.00	0.00	500.00
3437	-8727	-8634	-8633	-8726	MG	0.00	0.00	500.00
3437	-8634	-8545	-8544	-8633	MG	0.00	0.00	500.00
3437	-8621	-8628	-8719	-8720	MG	0.00	0.00	500.00
3437	-7204	-7141	-7140	-7203	MG	0.00	0.00	500.00
3437	-7466	-7350	-7349	-7465	MG	0.00	0.00	500.00
3437	-7350	-7300	-7299	-7349	MG	0.00	0.00	500.00

3437	-7300	-7266	-7265	-7299	MG	0.00	0.00	500.00
3437	-7266	-7203	-7202	-7265	MG	0.00	0.00	500.00
3437	-7203	-7140	-7139	-7202	MG	0.00	0.00	500.00
3437	-8484	-8431	-8430	-8483	MG	0.00	0.00	500.00
3437	-7572	-7578	-7661	-7662	MG	0.00	0.00	500.00
3437	-7463	-7347	-7346	-7462	MG	0.00	0.00	500.00
3437	-7347	-7297	-7296	-7346	MG	0.00	0.00	500.00
3437	-7297	-7263	-7262	-7296	MG	0.00	0.00	500.00
3437	-8543	-8483	-8474	-8542	MG	0.00	0.00	500.00
3437	-8483	-8430	-8429	-8474	MG	0.00	0.00	500.00
3437	-7462	-7346	-7345	-7461	MG	0.00	0.00	500.00
3437	-7346	-7296	-7295	-7345	MG	0.00	0.00	500.00
3437	-8724	-8631	-8630	-8723	MG	0.00	0.00	500.00
3437	-8631	-8542	-8541	-8630	MG	0.00	0.00	500.00
3437	-7199	-7136	-7135	-7198	MG	0.00	0.00	500.00
3437	-8474	-8429	-8428	-8473	MG	0.00	0.00	500.00
3437	-8912	-8787	-8808	-8911	MG	0.00	0.00	500.00
3437	-8787	-8723	-8722	-8808	MG	0.00	0.00	500.00
3437	-9973	-9840	-9849	-9972	MG	0.00	0.00	500.00
3437	-9840	-9746	-9745	-9849	MG	0.00	0.00	500.00
3437	-8541	-8473	-8482	-8540	MG	0.00	0.00	500.00
3437	-8473	-8428	-8427	-8482	MG	0.00	0.00	500.00
3437	-8808	-8722	-8721	-8841	MG	0.00	0.00	500.00
3437	-8722	-8622	-8629	-8721	MG	0.00	0.00	500.00
3437	-8622	-8540	-8539	-8629	MG	0.00	0.00	500.00
3437	-8540	-8482	-8481	-8539	MG	0.00	0.00	500.00
3437	-8482	-8427	-8426	-8481	MG	0.00	0.00	500.00
3437	-8824	-8718	-8717	-8807	MG	0.00	0.00	500.00
3437	-8718	-8620	-8619	-8717	MG	0.00	0.00	500.00
3437	-8620	-8536	-8535	-8619	MG	0.00	0.00	500.00
3437	-9971	-9848	-9862	-9963	MG	0.00	0.00	500.00
3437	-9848	-9744	-9743	-9862	MG	0.00	0.00	500.00
3437	-10253	-10177	-10197	-10252	MG	0.00	0.00	500.00
3437	-10177	-10131	-10130	-10197	MG	0.00	0.00	500.00
3437	-10131	-10039	-10038	-10130	MG	0.00	0.00	500.00
3437	-10039	-9963	-9946	-10038	MG	0.00	0.00	500.00
3437	-9963	-9862	-9858	-9946	MG	0.00	0.00	500.00
3437	-9862	-9743	-9742	-9858	MG	0.00	0.00	500.00
3437	-10252	-10197	-10176	3302	MG	0.00	0.00	500.00
3437	-8806	-8716	-8715	-8839	MG	0.00	0.00	500.00
3437	-8716	-8618	-8617	-8715	MG	0.00	0.00	500.00
3437	-8618	-8534	-8533	-8617	MG	0.00	0.00	500.00
3437	-9946	-9858	-9857	-9962	MG	0.00	0.00	500.00
3437	-9858	-9742	-9741	-9857	MG	0.00	0.00	500.00
3437	-8904	-8839	-8803	-8903	MG	0.00	0.00	500.00
3437	-8839	-8715	-8714	-8803	MG	0.00	0.00	500.00
3437	-8715	-8617	-8616	-8714	MG	0.00	0.00	500.00
3437	-9215	-9157	-9156	-9214	MG	0.00	0.00	500.00
3437	-8533	-8470	-8469	-8532	MG	0.00	0.00	500.00
3437	-9201	-9143	-9142	-9200	MG	0.00	0.00	500.00
3437	-8903	-8803	-8802	-8902	MG	0.00	0.00	500.00
3437	-8803	-8714	-8713	-8802	MG	0.00	0.00	500.00
3437	-8234	-8160	-8159	-8233	MG	0.00	0.00	500.00
3437	-8160	-8034	-8033	-8159	MG	0.00	0.00	500.00
3437	-10193	-10125	-10124	-10192	MG	0.00	0.00	500.00
3437	-10125	-10033	-10032	-10124	MG	0.00	0.00	500.00
3437	-8469	-8419	-8418	-8477	MG	0.00	0.00	500.00
3437	-9945	-9854	-9839	-9961	MG	0.00	0.00	500.00
3437	-9854	-9739	-9738	-9839	MG	0.00	0.00	500.00
3437	-10248	-10192	-10191	-10247	MG	0.00	0.00	500.00
3437	-10192	-10124	-10123	-10191	MG	0.00	0.00	500.00
3437	-10124	-10032	-10031	-10123	MG	0.00	0.00	500.00
3437	-10032	-9961	-9967	-10031	MG	0.00	0.00	500.00
3437	-9379	-9288	-9287	-9378	MG	0.00	0.00	500.00
3437	-8629	-8621	-8720	-8721	MG	0.00	0.00	500.00
3437	-9288	-9212	-9211	-9287	MG	0.00	0.00	500.00
3437	-8386	-8325	-8324	-8385	MG	0.00	0.00	500.00
3437	-8325	-8237	-8236	-8324	MG	0.00	0.00	500.00
3437	-10031	-9967	-9944	-10030	MG	0.00	0.00	500.00
3437	-9967	-9853	-9838	-9944	MG	0.00	0.00	500.00
3437	-9287	-9211	-9210	-9286	MG	0.00	0.00	500.00
3437	-9211	-9153	-9152	-9210	MG	0.00	0.00	500.00
3437	-8385	-8324	-8323	-8384	MG	0.00	0.00	500.00
3437	-8324	-8236	-8235	-8323	MG	0.00	0.00	500.00
3437	-8914	-8843	-8842	-8913	MG	0.00	0.00	500.00
3437	-8162	-8036	-8035	-8161	MG	0.00	0.00	500.00
3437	-8036	-7982	-7981	-8035	MG	0.00	0.00	500.00
3437	-9152	-9075	-9074	-9151	MG	0.00	0.00	500.00
3437	-9596	-9548	-9547	-9595	MG	0.00	0.00	500.00

3437	-9548	-9484	-9483	-9547	MG	0.00	0.00	500.00
3437	-9442	-9441	-9485	-9486	MG	0.00	0.00	500.00
3437	-9438	-9372	-9371	-9437	MG	0.00	0.00	500.00
3437	-8035	-7981	-7980	-8034	MG	0.00	0.00	500.00
3437	-8430	-8383	-8382	-8429	MG	0.00	0.00	500.00
3437	-8383	-8322	-8321	-8382	MG	0.00	0.00	500.00
3437	-8322	-8234	-8233	-8321	MG	0.00	0.00	500.00
3437	-9093	-8976	-8975	-9068	MG	0.00	0.00	500.00
3437	-9483	-9437	-9436	-9478	MG	0.00	0.00	500.00
3437	-8034	-7980	-7979	-8033	MG	0.00	0.00	500.00
3437	-8429	-8382	-8381	-8428	MG	0.00	0.00	500.00
3437	-8382	-8321	-8320	-8381	MG	0.00	0.00	500.00
3437	-8321	-8233	-8232	-8320	MG	0.00	0.00	500.00
3437	-8233	-8159	-8158	-8232	MG	0.00	0.00	500.00
3437	-8159	-8033	-8032	-8158	MG	0.00	0.00	500.00
3437	-9289	-9213	-9212	-9288	MG	0.00	0.00	500.00
3437	-8428	-8381	-8380	-8427	MG	0.00	0.00	500.00
3437	-8381	-8320	-8319	-8380	MG	0.00	0.00	500.00
3437	-8320	-8232	-8231	-8319	MG	0.00	0.00	500.00
3437	-8232	-8158	-8157	-8231	MG	0.00	0.00	500.00
3437	-8158	-8032	-8031	-8157	MG	0.00	0.00	500.00
3437	-8032	-7978	-7977	-8031	MG	0.00	0.00	500.00
3437	-8380	-8319	-8318	-8379	MG	0.00	0.00	500.00
3437	-8319	-8231	-8230	-8318	MG	0.00	0.00	500.00
3437	-8231	-8157	-8156	-8230	MG	0.00	0.00	500.00
3437	-8157	-8031	-8030	-8156	MG	0.00	0.00	500.00
3437	-8031	-7977	-7976	-8030	MG	0.00	0.00	500.00
3437	-8481	-8480	-8538	-8539	MG	0.00	0.00	500.00
3437	-8480	-8479	-8537	-8538	MG	0.00	0.00	500.00
3437	-8377	-8316	-8315	-8376	MG	0.00	0.00	500.00
3437	-8316	-8228	-8227	-8315	MG	0.00	0.00	500.00
3437	-8228	-8154	-8153	-8227	MG	0.00	0.00	500.00
3437	-8154	-8028	-8027	-8153	MG	0.00	0.00	500.00
3437	-8028	-7974	-7973	-8027	MG	0.00	0.00	500.00
3437	-8479	-8472	-8536	-8537	MG	0.00	0.00	500.00
3437	-8991	-8917	-8916	-8990	MG	0.00	0.00	500.00
3437	-9382	-9291	-9290	-9381	MG	0.00	0.00	500.00
3437	-9368	-9277	-9276	-9367	MG	0.00	0.00	500.00
3437	-9277	-9201	-9200	-9276	MG	0.00	0.00	500.00
3437	-9637	-9595	-9594	-9636	MG	0.00	0.00	500.00
3437	-9099	-8990	-8989	-9098	MG	0.00	0.00	500.00
3437	-9547	-9483	-9478	-9546	MG	0.00	0.00	500.00
3437	-8826	-8726	-8725	-8843	MG	0.00	0.00	500.00
3437	-8726	-8633	-8632	-8725	MG	0.00	0.00	500.00
3437	-8723	-8630	-8622	-8722	MG	0.00	0.00	500.00
3437	-9151	-9150	-9208	-9209	MG	0.00	0.00	500.00
3437	-9594	-9546	-9545	-9593	MG	0.00	0.00	500.00
3437	-8989	-8915	-8914	-8988	MG	0.00	0.00	500.00
3437	-8902	-8802	-8801	-8901	MG	0.00	0.00	500.00
3437	-8981	-8907	-8906	-8980	MG	0.00	0.00	500.00
3437	-8546	-8486	-8485	-8545	MG	0.00	0.00	500.00
3437	-8486	-8433	-8432	-8485	MG	0.00	0.00	500.00
3437	-9097	-8988	-8987	-9096	MG	0.00	0.00	500.00
3437	-8988	-8914	-8913	-8987	MG	0.00	0.00	500.00
3437	-8980	-8906	-8905	-8979	MG	0.00	0.00	500.00
3437	-9435	-9369	-9368	-9434	MG	0.00	0.00	500.00
3437	-9212	-9154	-9153	-9211	MG	0.00	0.00	500.00
3437	-9154	-9096	-9076	-9153	MG	0.00	0.00	500.00
3437	-9096	-8987	-8986	-9076	MG	0.00	0.00	500.00
3437	-9544	-9476	-9502	-9543	MG	0.00	0.00	500.00
3437	-9476	-9434	-9433	-9502	MG	0.00	0.00	500.00
3437	-8633	-8544	-8543	-8632	MG	0.00	0.00	500.00
3437	-8544	-8484	-8483	-8543	MG	0.00	0.00	500.00
3437	-9153	-9076	-9075	-9152	MG	0.00	0.00	500.00
3437	-8905	-8806	-8839	-8904	MG	0.00	0.00	500.00
3437	-9439	-9373	-9372	-9438	MG	0.00	0.00	500.00
3437	-9738	-9638	-9637	-9737	MG	0.00	0.00	500.00
3437	-9638	-9596	-9595	-9637	MG	0.00	0.00	500.00
3437	-8632	-8543	-8542	-8631	MG	0.00	0.00	500.00
3437	-8725	-8632	-8631	-8724	MG	0.00	0.00	500.00
3437	-9484	-9438	-9437	-9483	MG	0.00	0.00	500.00
3437	-8913	-8842	-8787	-8912	MG	0.00	0.00	500.00
3437	-9737	-9637	-9636	-9736	MG	0.00	0.00	500.00
3437	-8842	-8724	-8723	-8787	MG	0.00	0.00	500.00
3437	-8542	-8474	-8473	-8541	MG	0.00	0.00	500.00
3437	-9592	-9544	-9543	-9591	MG	0.00	0.00	500.00
3437	-8472	-8423	-8422	-8478	MG	0.00	0.00	500.00
3437	-8987	-8913	-8912	-8986	MG	0.00	0.00	500.00
3437	-9434	-9368	-9367	-9433	MG	0.00	0.00	500.00

3437	-8630	-8541	-8540	-8622	MG	0.00	0.00	500.00
3437	-9206	-9148	-9147	-9205	MG	0.00	0.00	500.00
3437	-9546	-9478	-9477	-9545	MG	0.00	0.00	500.00
3437	-9478	-9436	-9435	-9477	MG	0.00	0.00	500.00
3437	-9292	-9216	-9215	-9291	MG	0.00	0.00	500.00
3437	-9216	-9158	-9157	-9215	MG	0.00	0.00	500.00
3437	-9635	-9593	-9592	-9634	MG	0.00	0.00	500.00
3437	-9593	-9545	-9544	-9592	MG	0.00	0.00	500.00
3437	-9545	-9477	-9476	-9544	MG	0.00	0.00	500.00
3437	-8477	-8418	-8417	-8468	MG	0.00	0.00	500.00
3437	-9291	-9215	-9214	-9290	MG	0.00	0.00	500.00
3437	-9735	-9634	-9633	-9734	MG	0.00	0.00	500.00
3437	-9634	-9592	-9591	-9633	MG	0.00	0.00	500.00
3437	-8536	-8472	-8478	-8535	MG	0.00	0.00	500.00
3437	-9286	-9210	-9209	-9285	MG	0.00	0.00	500.00
3437	-8906	-8807	-8806	-8905	MG	0.00	0.00	500.00
3437	-9378	-9287	-9286	-9377	MG	0.00	0.00	500.00
3437	-8535	-8478	-8471	-8534	MG	0.00	0.00	500.00
3437	-8478	-8422	-8421	-8471	MG	0.00	0.00	500.00
3437	-9203	-9145	-9144	-9202	MG	0.00	0.00	500.00
3437	-9551	-9550	-9598	-9599	MG	0.00	0.00	500.00
3437	-9070	-8978	-8977	-9069	MG	0.00	0.00	500.00
3437	-9145	-9070	-9069	-9144	MG	0.00	0.00	500.00
3437	-9158	-9100	-9099	-9157	MG	0.00	0.00	500.00
3437	-8531	-8477	-8468	-8530	MG	0.00	0.00	500.00
3437	-9144	-9069	-9093	-9143	MG	0.00	0.00	500.00
3437	-9071	-8980	-8979	-9094	MG	0.00	0.00	500.00
3437	-8619	-8535	-8534	-8618	MG	0.00	0.00	500.00
3437	-8627	-8531	-8530	-8615	MG	0.00	0.00	500.00
3437	-9280	-9204	-9203	-9279	MG	0.00	0.00	500.00
3437	-8163	-8037	-8036	-8162	MG	0.00	0.00	500.00
3437	-8978	-8904	-8903	-8977	MG	0.00	0.00	500.00
3437	-8843	-8725	-8724	-8842	MG	0.00	0.00	500.00
3437	-8807	-8717	-8716	-8806	MG	0.00	0.00	500.00
3437	-8717	-8619	-8618	-8716	MG	0.00	0.00	500.00
3437	-9072	-8981	-8980	-9071	MG	0.00	0.00	500.00
3437	-8713	-8627	-8615	-8712	MG	0.00	0.00	500.00
3437	-9210	-9152	-9151	-9209	MG	0.00	0.00	500.00
3438	-10036	-6505	-6598	-10128	MG	0.00	0.00	500.00
3438	-9376	-5606	-5818	-9442	MG	0.00	0.00	500.00
3438	-9642	-6103	-6002	-9740	MG	0.00	0.00	500.00
3438	-8984	-5398	-5621	-9074	MG	0.00	0.00	500.00
3438	-9847	-6222	-6438	-9970	MG	0.00	0.00	500.00
3438	-9486	-6037	-6105	-9552	MG	0.00	0.00	500.00
3438	-9552	-6105	-6173	-9600	MG	0.00	0.00	500.00
3438	-10196	-6496	-6382	-10251	MG	0.00	0.00	500.00
3438	-9209	-5774	-5690	-9285	MG	0.00	0.00	500.00
3438	-9285	-5690	-5606	-9376	MG	0.00	0.00	500.00
3438	-9151	-5702	-5774	-9209	MG	0.00	0.00	500.00
3438	-9740	-6002	-6222	-9847	MG	0.00	0.00	500.00
3438	-9074	-5621	-5702	-9151	MG	0.00	0.00	500.00
3438	-9970	-6438	-6505	-10036	MG	0.00	0.00	500.00
3438	-10128	-6598	-6496	-10196	MG	0.00	0.00	500.00
3438	-9442	-5818	-6037	-9486	MG	0.00	0.00	500.00
3438	-9600	-6173	-6103	-9642	MG	0.00	0.00	500.00
3440	-7008	-7494	-7495	-6240	MG	0.00	0.00	500.00
3443	-7973	-5013	-4950	-7972	MG	0.00	0.00	500.00
3447	-4815	-4421	-8423	-8424	MG	0.00	0.00	500.00
3448	-8423	-5418	-5352	-8422	MG	0.00	0.00	500.00
3451	-5215	-4888	-8907	-8908	MG	0.00	0.00	500.00
3451	-4888	-5807	-8907	-8907	MG	0.00	0.00	500.00
3452	-6170	-6259	-6926	-6926	MG	0.00	0.00	500.00
3453	-5306	-6221	-9373	-9373	MG	0.00	0.00	500.00
3471	-6692	-6152	-6691	-6691	MG	0.00	0.00	500.00
3474	-7145	-6559	-7144	-7144	MG	0.00	0.00	500.00
3474	-6559	-5853	-7143	-7144	MG	0.00	0.00	500.00
3478	-7009	-6253	-7505	-7506	MG	0.00	0.00	500.00
3482	-4951	-5014	-7977	-7978	MG	0.00	0.00	500.00
3484	-5353	-5397	-8427	-8428	MG	0.00	0.00	500.00
3485	-4422	-4816	-8426	-8427	MG	0.00	0.00	500.00
3487	-5817	-4897	-8911	-8911	MG	0.00	0.00	500.00
3487	-4897	-5216	-8910	-8911	MG	0.00	0.00	500.00
3490	-6927	-6269	-6171	-6171	MG	0.00	0.00	500.00
3491	-6230	-5307	-9377	-9377	MG	0.00	0.00	500.00
3494	-6578	-5784	-6699	-6699	MG	0.00	0.00	500.00
3494	-6578	-6699	-7309	-7309	MG	0.00	0.00	500.00
3495	-5766	-6700	-6579	-6579	MG	0.00	0.00	500.00
3495	-7310	-6700	-6579	-6579	MG	0.00	0.00	500.00
3553	-7021	-7156	-7727	-7727	MG	0.00	0.00	500.00

3554	-6107	-6382	-10251	3302	MG	0.00	0.00	500.00
3554	-7022	-7092	3302	-10252	MG	0.00	0.00	500.00
3554	-7092	-6107	3302	3302	MG	0.00	0.00	500.00
3555	3301	-7091	-7021	-10248	MG	0.00	0.00	500.00
3555	-6380	-6106	3301	-10249	MG	0.00	0.00	500.00
3555	-6106	-7091	3301	3301	MG	0.00	0.00	500.00
3556	-7728	-7157	-7022	-7022	MG	0.00	0.00	500.00
3569	-7008	-7493	-7494	-7494	MG	0.00	0.00	500.00
3572	-7357	-7968	-7969	-7969	MG	0.00	0.00	500.00
3572	-7357	-7969	-7970	-6674	MG	0.00	0.00	500.00
3577	-7814	-8419	-8420	-7147	MG	0.00	0.00	500.00
3577	-7814	-8418	-8419	-8419	MG	0.00	0.00	500.00
3579	-8907	-5807	-5781	-8906	MG	0.00	0.00	500.00
3581	-9373	-6221	-6170	-9372	MG	0.00	0.00	500.00
3582	-5605	-5306	-9373	-9374	MG	0.00	0.00	500.00
3583	-8326	-8902	-8903	-8903	MG	0.00	0.00	500.00
3583	-8326	-8903	-8904	-7509	MG	0.00	0.00	500.00
3599	-7507	-7009	-7506	-7506	MG	0.00	0.00	500.00
3601	-7358	-6694	-7980	-7981	MG	0.00	0.00	500.00
3601	-7982	-7358	-7981	-7981	MG	0.00	0.00	500.00
3605	-8432	-7815	-8431	-8431	MG	0.00	0.00	500.00
3605	-7815	-7148	-8430	-8431	MG	0.00	0.00	500.00
3607	-5773	-5817	-8911	-8912	MG	0.00	0.00	500.00
3609	-8916	-8327	-8915	-8915	MG	0.00	0.00	500.00
3609	-8327	-7510	-8914	-8915	MG	0.00	0.00	500.00
3611	-6171	-6230	-9377	-9378	MG	0.00	0.00	500.00
3612	-5307	-5606	-9376	-9377	MG	0.00	0.00	500.00
3614	-9382	-8730	-9381	-9381	MG	0.00	0.00	500.00
3614	-8730	-7985	-9380	-9381	MG	0.00	0.00	500.00
3616	-8729	-9368	-9369	-9369	MG	0.00	0.00	500.00
3616	-8729	-9369	-9370	-7984	MG	0.00	0.00	500.00
3618	-5691	-6659	-9739	-9739	MG	0.00	0.00	500.00
3618	-6001	-5691	-9739	-9727	MG	0.00	0.00	500.00
3618	-9739	-6659	-6578	-9738	MG	0.00	0.00	500.00
3620	-5692	-6002	-9740	-9741	MG	0.00	0.00	500.00
3620	-6579	-6660	-9741	-9742	MG	0.00	0.00	500.00
3620	-6660	-5692	-9741	-9741	MG	0.00	0.00	500.00
3622	-9746	-9218	-9745	-9745	MG	0.00	0.00	500.00
3622	-9218	-8435	-9744	-9745	MG	0.00	0.00	500.00
3624	-9217	-9735	-9726	-9726	MG	0.00	0.00	500.00
3624	-9217	-9726	-9736	-8434	MG	0.00	0.00	500.00
3627	-9608	-10244	-10245	-10245	MG	0.00	0.00	500.00
3627	-9608	-10245	-10246	-8918	MG	0.00	0.00	500.00
3629	-10256	-9609	-10255	-10255	MG	0.00	0.00	500.00
3629	-9609	-8919	-10254	-10255	MG	0.00	0.00	500.00
3824	-4583	-4588	-4572	-4571	MG	0.00	0.00	500.00
3824	-4611	-4594	-4597	-4625	MG	0.00	0.00	500.00
3824	-4626	-4611	-4625	-4625	MG	0.00	0.00	500.00
3824	-4621	-4603	-4601	-4620	MG	0.00	0.00	500.00
3824	-4652	-4635	-4634	-4651	MG	0.00	0.00	500.00
3824	-4589	-4598	-4608	-4592	MG	0.00	0.00	500.00
3824	-4607	-4583	-4592	-4608	MG	0.00	0.00	500.00
3824	-4573	-4570	-4558	-4555	MG	0.00	0.00	500.00
3824	-4651	-4634	-4633	-4650	MG	0.00	0.00	500.00
3824	-4536	-4527	-4531	-4531	MG	0.00	0.00	500.00
3824	-4594	-4579	-4590	-4597	MG	0.00	0.00	500.00
3824	-4579	-4569	-4574	-4590	MG	0.00	0.00	500.00
3824	-4569	-4554	-4562	-4574	MG	0.00	0.00	500.00
3824	-4554	-4541	-4551	-4562	MG	0.00	0.00	500.00
3824	-4541	-4539	-4545	-4551	MG	0.00	0.00	500.00
3824	-4583	-4607	-4604	-4588	MG	0.00	0.00	500.00
3824	-4649	-4632	-4631	-4648	MG	0.00	0.00	500.00
3824	-4634	-4620	-4619	-4633	MG	0.00	0.00	500.00
3824	-4648	-4631	-4636	-4653	MG	0.00	0.00	500.00
3824	-4631	-4617	-4616	-4636	MG	0.00	0.00	500.00
3824	-4636	-4616	-4615	-4638	MG	0.00	0.00	500.00
3824	-4615	-4614	-4640	-4638	MG	0.00	0.00	500.00
3824	-4614	-4613	-4629	-4640	MG	0.00	0.00	500.00
3824	-4613	-4612	-4627	-4629	MG	0.00	0.00	500.00
3824	-4627	-4642	-4644	-4629	MG	0.00	0.00	500.00
3824	-4642	-4659	-4663	-4644	MG	0.00	0.00	500.00
3824	-4562	-4551	-4558	-4570	MG	0.00	0.00	500.00
3824	-4545	-4555	-4558	-4551	MG	0.00	0.00	500.00
3824	-4570	-4573	-4587	-4586	MG	0.00	0.00	500.00
3824	-4650	-4633	-4632	-4649	MG	0.00	0.00	500.00
3824	-4633	-4619	-4618	-4632	MG	0.00	0.00	500.00
3824	-4597	-4590	-4591	-4609	MG	0.00	0.00	500.00
3824	-4591	-4590	-4574	-4586	MG	0.00	0.00	500.00
3824	-4586	-4587	-4605	-4606	MG	0.00	0.00	500.00

3824	-4632	-4618	-4617	-4631	MG	0.00	0.00	500.00
3824	-4629	-4644	-4646	-4640	MG	0.00	0.00	500.00
3824	-4644	-4663	-4661	-4646	MG	0.00	0.00	500.00
3824	-4646	-4661	-4657	-4640	MG	0.00	0.00	500.00
3824	-4532	-4528	-4537	-4537	MG	0.00	0.00	500.00
3824	-4635	-4621	-4620	-4634	MG	0.00	0.00	500.00
3824	-4653	-4636	-4638	-4655	MG	0.00	0.00	500.00
3824	-4655	-4638	-4640	-4657	MG	0.00	0.00	500.00
3824	-4660	-4643	-4645	-4664	MG	0.00	0.00	500.00
3824	-4643	-4628	-4630	-4645	MG	0.00	0.00	500.00
3824	-4628	-4626	-4625	-4630	MG	0.00	0.00	500.00
3824	-4625	-4624	-4641	-4630	MG	0.00	0.00	500.00
3824	-4624	-4623	-4639	-4641	MG	0.00	0.00	500.00
3824	-4623	-4622	-4637	-4639	MG	0.00	0.00	500.00
3824	-4637	-4622	-4621	-4635	MG	0.00	0.00	500.00
3824	-4654	-4637	-4635	-4652	MG	0.00	0.00	500.00
3824	-4539	-4532	-4537	-4545	MG	0.00	0.00	500.00
3824	-4537	-4550	-4555	-4545	MG	0.00	0.00	500.00
3824	-4550	-4567	-4573	-4555	MG	0.00	0.00	500.00
3824	-4567	-4585	-4587	-4573	MG	0.00	0.00	500.00
3824	-4585	-4603	-4605	-4587	MG	0.00	0.00	500.00
3824	-4603	-4621	-4622	-4605	MG	0.00	0.00	500.00
3824	-4622	-4623	-4606	-4605	MG	0.00	0.00	500.00
3824	-4623	-4624	-4609	-4606	MG	0.00	0.00	500.00
3824	-4624	-4625	-4597	-4609	MG	0.00	0.00	500.00
3824	-4658	-4662	-4647	-4641	MG	0.00	0.00	500.00
3824	-4662	-4664	-4645	-4647	MG	0.00	0.00	500.00
3824	-4647	-4645	-4630	-4641	MG	0.00	0.00	500.00
3824	-4639	-4637	-4654	-4656	MG	0.00	0.00	500.00
3824	-4639	-4656	-4658	-4641	MG	0.00	0.00	500.00
3824	-4570	-4586	-4574	-4562	MG	0.00	0.00	500.00
3824	-4606	-4609	-4591	-4586	MG	0.00	0.00	500.00
3824	-4603	-4585	-4582	-4601	MG	0.00	0.00	500.00
3824	-4585	-4567	-4565	-4582	MG	0.00	0.00	500.00
3824	-4567	-4550	-4548	-4565	MG	0.00	0.00	500.00
3824	-4550	-4537	-4535	-4548	MG	0.00	0.00	500.00
3824	-4537	-4528	-4526	-4535	MG	0.00	0.00	500.00
3824	-4620	-4601	-4599	-4619	MG	0.00	0.00	500.00
3824	-4601	-4582	-4580	-4599	MG	0.00	0.00	500.00
3824	-4582	-4565	-4563	-4580	MG	0.00	0.00	500.00
3824	-4565	-4548	-4546	-4563	MG	0.00	0.00	500.00
3824	-4548	-4535	-4533	-4546	MG	0.00	0.00	500.00
3824	-4535	-4526	-4524	-4533	MG	0.00	0.00	500.00
3824	-4619	-4599	-4600	-4618	MG	0.00	0.00	500.00
3824	-4599	-4580	-4581	-4600	MG	0.00	0.00	500.00
3824	-4580	-4563	-4564	-4581	MG	0.00	0.00	500.00
3824	-4563	-4546	-4547	-4564	MG	0.00	0.00	500.00
3824	-4546	-4533	-4534	-4547	MG	0.00	0.00	500.00
3824	-4533	-4524	-4525	-4534	MG	0.00	0.00	500.00
3824	-4618	-4600	-4602	-4617	MG	0.00	0.00	500.00
3824	-4600	-4581	-4584	-4602	MG	0.00	0.00	500.00
3824	-4581	-4564	-4566	-4584	MG	0.00	0.00	500.00
3824	-4564	-4547	-4549	-4566	MG	0.00	0.00	500.00
3824	-4547	-4534	-4536	-4549	MG	0.00	0.00	500.00
3824	-4534	-4525	-4527	-4536	MG	0.00	0.00	500.00
3824	-4610	-4612	-4613	-4613	MG	0.00	0.00	500.00
3824	-4602	-4584	-4588	-4604	MG	0.00	0.00	500.00
3824	-4584	-4566	-4572	-4588	MG	0.00	0.00	500.00
3824	-4566	-4549	-4556	-4572	MG	0.00	0.00	500.00
3824	-4549	-4536	-4544	-4556	MG	0.00	0.00	500.00
3824	-4536	-4531	-4538	-4544	MG	0.00	0.00	500.00
3824	-4538	-4540	-4552	-4544	MG	0.00	0.00	500.00
3824	-4540	-4553	-4561	-4552	MG	0.00	0.00	500.00
3824	-4553	-4568	-4575	-4561	MG	0.00	0.00	500.00
3824	-4568	-4578	-4589	-4575	MG	0.00	0.00	500.00
3824	-4578	-4593	-4598	-4589	MG	0.00	0.00	500.00
3824	-4593	-4610	-4613	-4598	MG	0.00	0.00	500.00
3824	-4613	-4614	-4608	-4598	MG	0.00	0.00	500.00
3824	-4614	-4615	-4607	-4608	MG	0.00	0.00	500.00
3824	-4615	-4616	-4604	-4607	MG	0.00	0.00	500.00
3824	-4617	-4602	-4604	-4616	MG	0.00	0.00	500.00
3824	-4544	-4552	-4557	-4556	MG	0.00	0.00	500.00
3824	-4561	-4571	-4557	-4552	MG	0.00	0.00	500.00
3824	-4572	-4556	-4557	-4571	MG	0.00	0.00	500.00
3824	-4575	-4583	-4571	-4561	MG	0.00	0.00	500.00
3824	-4575	-4589	-4592	-4583	MG	0.00	0.00	500.00

Elenco carichi elementi bidimensionali

Condizione di carico n. 7: Variabili impalc. (caso 3)

Carichi uniformi

Bid.	N1	N2	N3	N4	TDC	Qx	Qy	Qz
						<daN/mq>	<daN/mq>	<daN/mq>
2816	-3655	-3748	-4148	-4148	MG	0.00	0.00	500.00
2817	-3947	-4038	-4403	-4403	MG	0.00	0.00	500.00
2822	-4219	-3663	-4295	-4295	MG	0.00	0.00	500.00
2843	-4149	-3749	-3656	-3656	MG	0.00	0.00	500.00
2847	-4404	-4039	-3948	-3948	MG	0.00	0.00	500.00
2848	-3659	-4296	-4220	-4220	MG	0.00	0.00	500.00
2921	-4198	-4683	-4684	-4684	MG	0.00	0.00	500.00
2921	-4198	-4684	-4685	-3732	MG	0.00	0.00	500.00
2931	-6370	-3558	-3605	-6483	MG	0.00	0.00	500.00
2934	-4219	-4295	-4870	-4870	MG	0.00	0.00	500.00
2935	-4670	-4653	-4655	-4672	MG	0.00	0.00	500.00
2935	-4676	-4661	-4663	-4679	MG	0.00	0.00	500.00
2935	-4804	-4747	-4746	-4803	MG	0.00	0.00	500.00
2935	-4746	-4687	-4686	-4745	MG	0.00	0.00	500.00
2935	-4858	-4803	-4802	-4857	MG	0.00	0.00	500.00
2935	-4676	-4674	-4657	-4661	MG	0.00	0.00	500.00
2935	-4864	-4809	-4808	-4863	MG	0.00	0.00	500.00
2935	-4671	-4654	-4652	-4669	MG	0.00	0.00	500.00
2935	-4747	-4688	-4687	-4746	MG	0.00	0.00	500.00
2935	-4690	-4689	-4748	-4749	MG	0.00	0.00	500.00
2935	-4697	-4680	-4677	-4696	MG	0.00	0.00	500.00
2935	-4672	-4655	-4657	-4674	MG	0.00	0.00	500.00
2935	-4855	-4800	-4799	-4854	MG	0.00	0.00	500.00
2935	-4803	-4746	-4745	-4802	MG	0.00	0.00	500.00
2935	-4669	-4652	-4651	-4668	MG	0.00	0.00	500.00
2935	-4754	-4695	-4694	-4753	MG	0.00	0.00	500.00
2935	-4859	-4804	-4803	-4858	MG	0.00	0.00	500.00
2935	-4755	-4696	-4695	-4754	MG	0.00	0.00	500.00
2935	-4813	-4756	-4755	-4812	MG	0.00	0.00	500.00
2935	-4802	-4745	-4744	-4801	MG	0.00	0.00	500.00
2935	-4656	-4673	-4675	-4658	MG	0.00	0.00	500.00
2935	-4812	-4755	-4754	-4811	MG	0.00	0.00	500.00
2935	-4867	-4812	-4811	-4866	MG	0.00	0.00	500.00
2935	-4748	-4689	-4688	-4747	MG	0.00	0.00	500.00
2935	-4666	-4649	-4648	-4665	MG	0.00	0.00	500.00
2935	-4688	-4665	-4670	-4687	MG	0.00	0.00	500.00
2935	-4694	-4695	-4675	-4673	MG	0.00	0.00	500.00
2935	-4698	-4681	-4680	-4697	MG	0.00	0.00	500.00
2935	-4749	-4748	-4805	-4806	MG	0.00	0.00	500.00
2935	-4752	-4693	-4692	-4751	MG	0.00	0.00	500.00
2935	-4809	-4752	-4751	-4808	MG	0.00	0.00	500.00
2935	-4751	-4692	-4691	-4750	MG	0.00	0.00	500.00
2935	-4807	-4806	-4861	-4862	MG	0.00	0.00	500.00
2935	-4745	-4686	-4685	-4744	MG	0.00	0.00	500.00
2935	-4692	-4669	-4668	-4691	MG	0.00	0.00	500.00
2935	-4857	-4802	-4801	-4856	MG	0.00	0.00	500.00
2935	-4667	-4650	-4649	-4666	MG	0.00	0.00	500.00
2935	-4689	-4666	-4665	-4688	MG	0.00	0.00	500.00
2935	-4810	-4753	-4752	-4809	MG	0.00	0.00	500.00
2935	-4686	-4687	-4670	-4672	MG	0.00	0.00	500.00
2935	-4856	-4801	-4800	-4855	MG	0.00	0.00	500.00
2935	-4668	-4651	-4650	-4667	MG	0.00	0.00	500.00
2935	-4669	-4692	-4693	-4671	MG	0.00	0.00	500.00
2935	-4665	-4648	-4653	-4670	MG	0.00	0.00	500.00
2935	-4696	-4677	-4675	-4695	MG	0.00	0.00	500.00
2935	-4744	-4685	-4684	-4743	MG	0.00	0.00	500.00
2935	-4805	-4748	-4747	-4804	MG	0.00	0.00	500.00
2935	-4756	-4697	-4696	-4755	MG	0.00	0.00	500.00
2935	-4677	-4680	-4664	-4662	MG	0.00	0.00	500.00
2935	-4686	-4672	-4674	-4685	MG	0.00	0.00	500.00
2935	-4681	-4660	-4664	-4680	MG	0.00	0.00	500.00
2935	-4753	-4694	-4693	-4752	MG	0.00	0.00	500.00
2935	-4684	-4685	-4674	-4676	MG	0.00	0.00	500.00
2935	-4656	-4654	-4671	-4673	MG	0.00	0.00	500.00
2935	-4750	-4749	-4806	-4807	MG	0.00	0.00	500.00
2935	-4690	-4667	-4666	-4689	MG	0.00	0.00	500.00
2935	-4742	-4683	-4682	-4741	MG	0.00	0.00	500.00
2935	-4868	-4813	-4812	-4867	MG	0.00	0.00	500.00
2935	-4808	-4751	-4750	-4807	MG	0.00	0.00	500.00
2935	-4866	-4811	-4810	-4865	MG	0.00	0.00	500.00
2935	-4691	-4668	-4667	-4690	MG	0.00	0.00	500.00
2935	-4694	-4673	-4671	-4693	MG	0.00	0.00	500.00
2935	-4691	-4690	-4749	-4750	MG	0.00	0.00	500.00
2935	-4801	-4744	-4743	-4800	MG	0.00	0.00	500.00
2935	-4865	-4810	-4809	-4864	MG	0.00	0.00	500.00

2935	-4814	-4757	-4756	-4813	MG	0.00	0.00	500.00
2935	-4659	-4678	-4679	-4663	MG	0.00	0.00	500.00
2935	-4869	-4814	-4813	-4868	MG	0.00	0.00	500.00
2935	-4811	-4754	-4753	-4810	MG	0.00	0.00	500.00
2935	-4799	-4742	-4741	-4798	MG	0.00	0.00	500.00
2935	-4854	-4799	-4798	-4853	MG	0.00	0.00	500.00
2935	-4684	-4676	-4679	-4683	MG	0.00	0.00	500.00
2935	-4683	-4679	-4678	-4682	MG	0.00	0.00	500.00
2935	-4757	-4698	-4697	-4756	MG	0.00	0.00	500.00
2935	-4743	-4684	-4683	-4742	MG	0.00	0.00	500.00
2935	-4677	-4662	-4658	-4675	MG	0.00	0.00	500.00
2935	-4860	-4805	-4804	-4859	MG	0.00	0.00	500.00
2935	-4806	-4805	-4860	-4861	MG	0.00	0.00	500.00
2935	-4800	-4743	-4742	-4799	MG	0.00	0.00	500.00
2935	-4863	-4808	-4807	-4862	MG	0.00	0.00	500.00
2937	-6372	-3559	-3606	-6485	MG	0.00	0.00	500.00
2945	-4697	-4199	-4696	-4696	MG	0.00	0.00	500.00
2945	-4199	-3733	-4695	-4696	MG	0.00	0.00	500.00
2953	-4871	-4296	-4220	-4220	MG	0.00	0.00	500.00
3022	-4445	-5039	-5040	-4019	MG	0.00	0.00	500.00
3031	-6689	-3536	-3698	-6748	MG	0.00	0.00	500.00
3031	-6620	-3590	-3536	-6689	MG	0.00	0.00	500.00
3031	-6483	-3605	-3657	-6548	MG	0.00	0.00	500.00
3031	-6548	-3657	-3590	-6620	MG	0.00	0.00	500.00
3033	-3607	-4251	-7136	-7136	MG	0.00	0.00	500.00
3034	-5041	-4976	-4992	-5040	MG	0.00	0.00	500.00
3034	-4918	-4855	-4854	-4917	MG	0.00	0.00	500.00
3034	-5042	-4968	-4976	-5041	MG	0.00	0.00	500.00
3034	-4932	-4866	-4865	-4931	MG	0.00	0.00	500.00
3034	-4967	-4918	-4917	-4966	MG	0.00	0.00	500.00
3034	-5048	-4995	-4979	-5047	MG	0.00	0.00	500.00
3034	-4926	-4860	-4859	-4925	MG	0.00	0.00	500.00
3034	-4861	-4860	-4926	-4927	MG	0.00	0.00	500.00
3034	-4994	-4930	-4929	-4978	MG	0.00	0.00	500.00
3034	-4929	-4863	-4862	-4928	MG	0.00	0.00	500.00
3034	-4924	-4858	-4857	-4919	MG	0.00	0.00	500.00
3034	-4978	-4929	-4928	-4970	MG	0.00	0.00	500.00
3034	-4927	-4926	-4969	-4993	MG	0.00	0.00	500.00
3034	-4925	-4859	-4858	-4924	MG	0.00	0.00	500.00
3034	-4976	-4919	-4923	-4992	MG	0.00	0.00	500.00
3034	-4995	-4932	-4931	-4979	MG	0.00	0.00	500.00
3034	-5046	-4994	-4978	2902	MG	0.00	0.00	500.00
3034	-4969	-4926	-4925	-4977	MG	0.00	0.00	500.00
3034	-4919	-4857	-4856	-4923	MG	0.00	0.00	500.00
3034	-5051	-4997	-4980	-5050	MG	0.00	0.00	500.00
3034	2902	-4978	-4970	-5045	MG	0.00	0.00	500.00
3034	-5043	-4969	-4977	2901	MG	0.00	0.00	500.00
3034	-4920	-4867	-4866	-4932	MG	0.00	0.00	500.00
3034	-4992	-4923	-4918	-4967	MG	0.00	0.00	500.00
3034	-4996	-4920	-4932	-4995	MG	0.00	0.00	500.00
3034	-4923	-4856	-4855	-4918	MG	0.00	0.00	500.00
3034	-4930	-4864	-4863	-4929	MG	0.00	0.00	500.00
3034	-4997	-4934	-4933	-4980	MG	0.00	0.00	500.00
3034	-5039	-4967	-4966	-5038	MG	0.00	0.00	500.00
3034	2901	-4977	-4968	-5042	MG	0.00	0.00	500.00
3034	-4993	-4969	-5043	-5044	MG	0.00	0.00	500.00
3034	-4931	-4865	-4864	-4930	MG	0.00	0.00	500.00
3034	-4862	-4861	-4927	-4928	MG	0.00	0.00	500.00
3034	-5040	-4992	-4967	-5039	MG	0.00	0.00	500.00
3034	-4970	-4993	-5044	-5045	MG	0.00	0.00	500.00
3034	-4934	-4869	-4868	-4933	MG	0.00	0.00	500.00
3034	-4968	-4924	-4919	-4976	MG	0.00	0.00	500.00
3034	-4917	-4854	-4853	-4916	MG	0.00	0.00	500.00
3034	-5050	-4980	-4996	-5049	MG	0.00	0.00	500.00
3034	-5047	-4979	-4994	-5046	MG	0.00	0.00	500.00
3034	-4928	-4927	-4993	-4970	MG	0.00	0.00	500.00
3034	-4979	-4931	-4930	-4994	MG	0.00	0.00	500.00
3034	-5049	-4996	-4995	-5048	MG	0.00	0.00	500.00
3034	-4977	-4925	-4924	-4968	MG	0.00	0.00	500.00
3034	-4933	-4868	-4867	-4920	MG	0.00	0.00	500.00
3034	-5038	-4966	-4991	-5037	MG	0.00	0.00	500.00
3034	-4966	-4917	-4916	-4991	MG	0.00	0.00	500.00
3034	-4980	-4933	-4920	-4996	MG	0.00	0.00	500.00
3036	-6485	-3606	-3658	-6550	MG	0.00	0.00	500.00
3036	-6550	-3658	-3591	-6622	MG	0.00	0.00	500.00
3036	-6672	-3537	-3699	-6750	MG	0.00	0.00	500.00
3036	-6622	-3591	-3537	-6672	MG	0.00	0.00	500.00
3052	-4446	-4020	-5048	-5049	MG	0.00	0.00	500.00
3060	-4252	-3608	-7140	-7140	MG	0.00	0.00	500.00

3119	-4445	-5038	-5039	-5039	MG	0.00	0.00	500.00
3120	-4935	-5432	-5433	-4281	MG	0.00	0.00	500.00
3121	-6244	-3696	-3655	-6243	MG	0.00	0.00	500.00
3129	-6915	-3904	-3963	-6998	MG	0.00	0.00	500.00
3129	-6833	-3842	-3904	-6915	MG	0.00	0.00	500.00
3129	-7200	-3987	-4124	-7263	MG	0.00	0.00	500.00
3129	-6998	-3963	-3887	-7057	MG	0.00	0.00	500.00
3129	-6748	-3698	-3842	-6833	MG	0.00	0.00	500.00
3129	-7057	-3887	-3825	-7137	MG	0.00	0.00	500.00
3129	-7137	-3825	-3987	-7200	MG	0.00	0.00	500.00
3131	-5116	-5040	-5039	-5115	MG	0.00	0.00	500.00
3131	-5671	-5602	-5601	-5670	MG	0.00	0.00	500.00
3131	-5663	-5594	-5593	-5662	MG	0.00	0.00	500.00
3131	-5435	-5373	-5372	-5434	MG	0.00	0.00	500.00
3131	-5741	-5732	-5797	-5798	MG	0.00	0.00	500.00
3131	-5119	2901	-5042	-5118	MG	0.00	0.00	500.00
3131	-5129	-5051	-5050	-5128	MG	0.00	0.00	500.00
3131	-5200	-5115	-5114	-5199	MG	0.00	0.00	500.00
3131	-5325	-5274	-5273	-5324	MG	0.00	0.00	500.00
3131	-5795	-5731	-5730	-5794	MG	0.00	0.00	500.00
3131	-5594	-5499	-5498	-5593	MG	0.00	0.00	500.00
3131	-5592	-5497	-5496	-5591	MG	0.00	0.00	500.00
3131	-5204	-5119	-5118	-5203	MG	0.00	0.00	500.00
3131	-5277	-5212	-5211	-5276	MG	0.00	0.00	500.00
3131	-5591	-5496	-5495	-5590	MG	0.00	0.00	500.00
3131	-5203	-5118	-5117	-5202	MG	0.00	0.00	500.00
3131	-5805	-5744	-5736	-5804	MG	0.00	0.00	500.00
3131	-5735	-5670	-5669	-5734	MG	0.00	0.00	500.00
3131	-5505	-5442	-5441	-5504	MG	0.00	0.00	500.00
3131	-5432	-5370	-5369	-5431	MG	0.00	0.00	500.00
3131	-5445	-5383	-5382	-5444	MG	0.00	0.00	500.00
3131	-5744	-5673	-5672	-5736	MG	0.00	0.00	500.00
3131	-5120	-5043	2901	-5119	MG	0.00	0.00	500.00
3131	-5379	-5325	-5324	-5378	MG	0.00	0.00	500.00
3131	-5439	-5438	-5501	-5502	MG	0.00	0.00	500.00
3131	-5731	-5663	-5662	-5730	MG	0.00	0.00	500.00
3131	-5508	-5445	-5444	-5507	MG	0.00	0.00	500.00
3131	-5728	-5660	-5659	-5727	MG	0.00	0.00	500.00
3131	-5660	-5591	-5590	-5659	MG	0.00	0.00	500.00
3131	-5496	-5433	-5432	-5495	MG	0.00	0.00	500.00
3131	-5665	-5664	-5740	-5732	MG	0.00	0.00	500.00
3131	-5802	-5735	-5734	-5801	MG	0.00	0.00	500.00
3131	-5730	-5662	-5661	-5729	MG	0.00	0.00	500.00
3131	-5370	-5316	-5315	-5369	MG	0.00	0.00	500.00
3131	-5214	-5129	-5128	-5213	MG	0.00	0.00	500.00
3131	-5803	-5743	-5735	-5802	MG	0.00	0.00	500.00
3131	-5743	-5671	-5670	-5735	MG	0.00	0.00	500.00
3131	-5210	-5125	-5124	-5209	MG	0.00	0.00	500.00
3131	-5128	-5050	-5049	-5127	MG	0.00	0.00	500.00
3131	-5801	-5734	-5742	-5800	MG	0.00	0.00	500.00
3131	-5661	-5592	-5591	-5660	MG	0.00	0.00	500.00
3131	-5734	-5669	-5668	-5742	MG	0.00	0.00	500.00
3131	-5320	-5269	-5268	-5319	MG	0.00	0.00	500.00
3131	-5269	-5204	-5203	-5268	MG	0.00	0.00	500.00
3131	-5497	-5434	-5433	-5496	MG	0.00	0.00	500.00
3131	-5201	-5116	-5115	-5200	MG	0.00	0.00	500.00
3131	-5206	-5205	-5270	-5271	MG	0.00	0.00	500.00
3131	-5207	-5206	-5271	-5272	MG	0.00	0.00	500.00
3131	-5327	-5276	-5275	-5326	MG	0.00	0.00	500.00
3131	-5436	-5374	-5373	-5435	MG	0.00	0.00	500.00
3131	-5276	-5211	-5210	-5275	MG	0.00	0.00	500.00
3131	-5727	-5659	-5658	-5726	MG	0.00	0.00	500.00
3131	-5590	-5495	-5494	-5589	MG	0.00	0.00	500.00
3131	-5045	-5044	-5121	-5122	MG	0.00	0.00	500.00
3131	-5315	-5264	-5263	-5314	MG	0.00	0.00	500.00
3131	-5275	-5210	-5209	-5274	MG	0.00	0.00	500.00
3131	-5446	-5384	-5383	-5445	MG	0.00	0.00	500.00
3131	-5125	-5047	-5046	-5124	MG	0.00	0.00	500.00
3131	-5664	-5595	-5594	-5663	MG	0.00	0.00	500.00
3131	-5437	-5375	-5374	-5436	MG	0.00	0.00	500.00
3131	-5500	-5437	-5436	-5499	MG	0.00	0.00	500.00
3131	-5597	-5596	-5665	-5666	MG	0.00	0.00	500.00
3131	-5440	-5378	-5377	-5439	MG	0.00	0.00	500.00
3131	-5274	-5209	-5208	-5273	MG	0.00	0.00	500.00
3131	-5499	-5436	-5435	-5498	MG	0.00	0.00	500.00
3131	-5265	-5200	-5199	-5264	MG	0.00	0.00	500.00
3131	-5316	-5265	-5264	-5315	MG	0.00	0.00	500.00
3131	-5794	-5730	-5729	-5793	MG	0.00	0.00	500.00
3131	-5273	-5208	-5207	-5272	MG	0.00	0.00	500.00

3131	-5279	-5214	-5213	-5278	MG	0.00	0.00	500.00
3131	-5670	-5601	-5600	-5669	MG	0.00	0.00	500.00
3131	-5601	-5506	-5505	-5600	MG	0.00	0.00	500.00
3131	-5278	-5213	-5212	-5277	MG	0.00	0.00	500.00
3131	-5369	-5315	-5314	-5368	MG	0.00	0.00	500.00
3131	-5213	-5128	-5127	-5212	MG	0.00	0.00	500.00
3131	-5270	-5205	-5204	-5269	MG	0.00	0.00	500.00
3131	-5264	-5199	-5198	-5263	MG	0.00	0.00	500.00
3131	-5328	-5277	-5276	-5327	MG	0.00	0.00	500.00
3131	-5382	-5328	-5327	-5381	MG	0.00	0.00	500.00
3131	-5377	-5376	-5438	-5439	MG	0.00	0.00	500.00
3131	-5792	-5728	-5727	-5791	MG	0.00	0.00	500.00
3131	-5212	-5127	-5126	-5211	MG	0.00	0.00	500.00
3131	-5127	-5049	-5048	-5126	MG	0.00	0.00	500.00
3131	-5443	-5381	-5380	-5442	MG	0.00	0.00	500.00
3131	-5373	-5319	-5318	-5372	MG	0.00	0.00	500.00
3131	-5791	-5727	-5726	-5790	MG	0.00	0.00	500.00
3131	-5268	-5203	-5202	-5267	MG	0.00	0.00	500.00
3131	-5501	-5500	-5595	-5596	MG	0.00	0.00	500.00
3131	-5380	-5326	-5325	-5379	MG	0.00	0.00	500.00
3131	-5495	-5432	-5431	-5494	MG	0.00	0.00	500.00
3131	-5790	-5726	-5725	-5789	MG	0.00	0.00	500.00
3131	-5796	-5740	-5731	-5795	MG	0.00	0.00	500.00
3131	-5726	-5658	-5657	-5725	MG	0.00	0.00	500.00
3131	-5595	-5500	-5499	-5594	MG	0.00	0.00	500.00
3131	-5371	-5317	-5316	-5370	MG	0.00	0.00	500.00
3131	-5494	-5431	-5430	-5493	MG	0.00	0.00	500.00
3131	-5441	-5379	-5378	-5440	MG	0.00	0.00	500.00
3131	-5266	-5201	-5200	-5265	MG	0.00	0.00	500.00
3131	-5666	-5665	-5732	-5741	MG	0.00	0.00	500.00
3131	-5272	-5271	-5322	-5323	MG	0.00	0.00	500.00
3131	-5324	-5273	-5272	-5323	MG	0.00	0.00	500.00
3131	-5507	-5444	-5443	-5506	MG	0.00	0.00	500.00
3131	-5330	-5279	-5278	-5329	MG	0.00	0.00	500.00
3131	-5124	-5046	2902	-5123	MG	0.00	0.00	500.00
3131	-5502	-5501	-5596	-5597	MG	0.00	0.00	500.00
3131	-5732	-5740	-5796	-5797	MG	0.00	0.00	500.00
3131	-5383	-5329	-5328	-5382	MG	0.00	0.00	500.00
3131	-5329	-5278	-5277	-5328	MG	0.00	0.00	500.00
3131	-5205	-5120	-5119	-5204	MG	0.00	0.00	500.00
3131	-5506	-5443	-5442	-5505	MG	0.00	0.00	500.00
3131	-5321	-5270	-5269	-5320	MG	0.00	0.00	500.00
3131	-5374	-5320	-5319	-5373	MG	0.00	0.00	500.00
3131	-5199	-5114	-5113	-5198	MG	0.00	0.00	500.00
3131	-5669	-5600	-5599	-5668	MG	0.00	0.00	500.00
3131	-5376	-5375	-5437	-5438	MG	0.00	0.00	500.00
3131	-5600	-5505	-5504	-5599	MG	0.00	0.00	500.00
3131	-5326	-5275	-5274	-5325	MG	0.00	0.00	500.00
3131	-5271	-5270	-5321	-5322	MG	0.00	0.00	500.00
3131	-5599	-5504	-5503	-5598	MG	0.00	0.00	500.00
3131	-5381	-5327	-5326	-5380	MG	0.00	0.00	500.00
3131	-5211	-5126	-5125	-5210	MG	0.00	0.00	500.00
3131	-5659	-5590	-5589	-5658	MG	0.00	0.00	500.00
3131	-5673	-5604	-5603	-5672	MG	0.00	0.00	500.00
3131	-5442	-5380	-5379	-5441	MG	0.00	0.00	500.00
3131	-5317	-5266	-5265	-5316	MG	0.00	0.00	500.00
3131	-5503	-5440	-5439	-5502	MG	0.00	0.00	500.00
3131	-5509	-5446	-5445	-5508	MG	0.00	0.00	500.00
3131	-5740	-5664	-5663	-5731	MG	0.00	0.00	500.00
3131	-5202	-5117	-5116	-5201	MG	0.00	0.00	500.00
3131	-5589	-5494	-5493	-5588	MG	0.00	0.00	500.00
3131	-5433	-5371	-5370	-5432	MG	0.00	0.00	500.00
3131	-5603	-5508	-5507	-5602	MG	0.00	0.00	500.00
3131	-5596	-5595	-5664	-5665	MG	0.00	0.00	500.00
3131	-5208	-5123	-5122	-5207	MG	0.00	0.00	500.00
3131	-5602	-5507	-5506	-5601	MG	0.00	0.00	500.00
3131	-5323	-5322	-5376	-5377	MG	0.00	0.00	500.00
3131	-5378	-5324	-5323	-5377	MG	0.00	0.00	500.00
3131	-5319	-5268	-5267	-5318	MG	0.00	0.00	500.00
3131	-5742	-5668	-5667	-5733	MG	0.00	0.00	500.00
3131	-5504	-5441	-5440	-5503	MG	0.00	0.00	500.00
3131	-5114	-5038	-5037	-5113	MG	0.00	0.00	500.00
3131	-5672	-5603	-5602	-5671	MG	0.00	0.00	500.00
3131	-5431	-5369	-5368	-5430	MG	0.00	0.00	500.00
3131	-5729	-5661	-5660	-5728	MG	0.00	0.00	500.00
3131	-5793	-5729	-5728	-5792	MG	0.00	0.00	500.00
3131	-5438	-5437	-5500	-5501	MG	0.00	0.00	500.00
3131	-5267	-5202	-5201	-5266	MG	0.00	0.00	500.00
3131	-5658	-5589	-5588	-5657	MG	0.00	0.00	500.00

3131	-5209	-5124	-5123	-5208	MG	0.00	0.00	500.00
3131	-5126	-5048	-5047	-5125	MG	0.00	0.00	500.00
3131	-5118	-5042	-5041	-5117	MG	0.00	0.00	500.00
3131	-5372	-5318	-5317	-5371	MG	0.00	0.00	500.00
3131	-5122	-5121	-5206	-5207	MG	0.00	0.00	500.00
3131	-5121	-5120	-5205	-5206	MG	0.00	0.00	500.00
3131	-5668	-5599	-5598	-5667	MG	0.00	0.00	500.00
3131	-5604	-5509	-5508	-5603	MG	0.00	0.00	500.00
3131	-5598	-5503	-5502	-5597	MG	0.00	0.00	500.00
3131	-5322	-5321	-5375	-5376	MG	0.00	0.00	500.00
3131	-5117	-5041	-5040	-5116	MG	0.00	0.00	500.00
3131	-5115	-5039	-5038	-5114	MG	0.00	0.00	500.00
3131	-5733	-5667	-5666	-5741	MG	0.00	0.00	500.00
3131	-5804	-5736	-5743	-5803	MG	0.00	0.00	500.00
3131	-5318	-5267	-5266	-5317	MG	0.00	0.00	500.00
3131	-5044	-5043	-5120	-5121	MG	0.00	0.00	500.00
3131	-5667	-5598	-5597	-5666	MG	0.00	0.00	500.00
3131	-5498	-5435	-5434	-5497	MG	0.00	0.00	500.00
3131	-5593	-5498	-5497	-5592	MG	0.00	0.00	500.00
3131	-5736	-5672	-5671	-5743	MG	0.00	0.00	500.00
3131	-5384	-5330	-5329	-5383	MG	0.00	0.00	500.00
3131	-5662	-5593	-5592	-5661	MG	0.00	0.00	500.00
3131	-5444	-5382	-5381	-5443	MG	0.00	0.00	500.00
3131	-5375	-5321	-5320	-5374	MG	0.00	0.00	500.00
3131	-5434	-5372	-5371	-5433	MG	0.00	0.00	500.00
3131	-5800	-5742	-5733	-5799	MG	0.00	0.00	500.00
3131	-5799	-5733	-5741	-5798	MG	0.00	0.00	500.00
3131	-5123	2902	-5045	-5122	MG	0.00	0.00	500.00
3133	-7139	-3826	-3988	-7202	MG	0.00	0.00	500.00
3133	-6835	-3843	-3905	-6917	MG	0.00	0.00	500.00
3133	-6917	-3905	-3964	-7000	MG	0.00	0.00	500.00
3133	-7202	-3988	-4125	-7265	MG	0.00	0.00	500.00
3133	-6750	-3699	-3843	-6835	MG	0.00	0.00	500.00
3133	-7059	-3888	-3826	-7139	MG	0.00	0.00	500.00
3133	-7000	-3964	-3888	-7059	MG	0.00	0.00	500.00
3147	-5050	-4446	-5049	-5049	MG	0.00	0.00	500.00
3150	-4936	-4282	-5443	-5444	MG	0.00	0.00	500.00
3152	-3656	-3697	-6247	-6248	MG	0.00	0.00	500.00
3219	-4935	-5431	-5432	-5432	MG	0.00	0.00	500.00
3222	-5333	-5837	-5838	-4699	MG	0.00	0.00	500.00
3222	-5333	-5836	-5837	-5837	MG	0.00	0.00	500.00
3229	-6670	-3985	-3947	-6669	MG	0.00	0.00	500.00
3232	-3825	-3607	-7136	-7137	MG	0.00	0.00	500.00
3233	-7136	-4251	-4219	-7135	MG	0.00	0.00	500.00
3234	-5987	-5878	-5877	-5986	MG	0.00	0.00	500.00
3234	-5888	-5846	-5845	-5887	MG	0.00	0.00	500.00
3234	-6067	-6066	-6134	-6135	MG	0.00	0.00	500.00
3234	-6060	-5987	-5986	-6059	MG	0.00	0.00	500.00
3234	-6070	-5996	-5995	-6069	MG	0.00	0.00	500.00
3234	-6130	-6062	-6061	-6129	MG	0.00	0.00	500.00
3234	-5989	-5880	-5879	-5988	MG	0.00	0.00	500.00
3234	-6249	-6197	-6196	-6239	MG	0.00	0.00	500.00
3234	-6193	-6194	-6137	-6136	MG	0.00	0.00	500.00
3234	-6250	-6198	-6197	-6249	MG	0.00	0.00	500.00
3234	-6142	-6074	-6073	-6141	MG	0.00	0.00	500.00
3234	-6073	-5999	-5998	-6072	MG	0.00	0.00	500.00
3234	-5878	-5836	-5835	-5877	MG	0.00	0.00	500.00
3234	-6185	-6128	-6127	-6184	MG	0.00	0.00	500.00
3234	-5891	-5849	-5848	-5890	MG	0.00	0.00	500.00
3234	-6252	-6200	-6199	-6251	MG	0.00	0.00	500.00
3234	-6000	-5892	-5891	-5999	MG	0.00	0.00	500.00
3234	-5838	-5792	-5791	-5837	MG	0.00	0.00	500.00
3234	-6199	-6142	-6141	-6198	MG	0.00	0.00	500.00
3234	-6068	-6067	-6135	-6136	MG	0.00	0.00	500.00
3234	-5999	-5891	-5890	-5998	MG	0.00	0.00	500.00
3234	-6248	-6195	-6194	-6247	MG	0.00	0.00	500.00
3234	-6136	-6135	-6192	-6193	MG	0.00	0.00	500.00
3234	-6138	-6070	-6069	-6137	MG	0.00	0.00	500.00
3234	-6187	-6130	-6129	-6186	MG	0.00	0.00	500.00
3234	-6236	-6187	-6186	-6235	MG	0.00	0.00	500.00
3234	-5798	-5797	-5843	-5844	MG	0.00	0.00	500.00
3234	-5847	-5801	-5800	-5846	MG	0.00	0.00	500.00
3234	-6198	-6141	-6140	-6197	MG	0.00	0.00	500.00
3234	-6068	-6069	-5995	-6025	MG	0.00	0.00	500.00
3234	-6242	-6185	-6184	-6234	MG	0.00	0.00	500.00
3234	-6246	-6247	-6194	-6193	MG	0.00	0.00	500.00
3234	-5886	-5887	-5845	-5844	MG	0.00	0.00	500.00
3234	-6128	-6060	-6059	-6127	MG	0.00	0.00	500.00
3234	-6238	-6191	-6190	-6244	MG	0.00	0.00	500.00

3234	-6074	-6000	-5999	-6073	MG	0.00	0.00	500.00
3234	-5892	-5850	-5849	-5891	MG	0.00	0.00	500.00
3234	-5884	-5842	-5841	-5883	MG	0.00	0.00	500.00
3234	-5846	-5800	-5799	-5845	MG	0.00	0.00	500.00
3234	-5848	-5802	-5801	-5847	MG	0.00	0.00	500.00
3234	-5837	-5791	-5790	-5836	MG	0.00	0.00	500.00
3234	-5885	-5884	-5993	-5994	MG	0.00	0.00	500.00
3234	-5992	-5883	-5882	-5991	MG	0.00	0.00	500.00
3234	-6140	-6072	-6071	-6139	MG	0.00	0.00	500.00
3234	-5839	-5793	-5792	-5838	MG	0.00	0.00	500.00
3234	-6025	-5995	-5887	-5886	MG	0.00	0.00	500.00
3234	-5882	-5840	-5839	-5881	MG	0.00	0.00	500.00
3234	-5890	-5848	-5847	-5889	MG	0.00	0.00	500.00
3234	-5851	-5805	-5804	-5850	MG	0.00	0.00	500.00
3234	-6244	-6190	-6189	-6243	MG	0.00	0.00	500.00
3234	-6063	-5990	-5989	-6062	MG	0.00	0.00	500.00
3234	-5990	-5881	-5880	-5989	MG	0.00	0.00	500.00
3234	-6196	-6139	-6138	-6195	MG	0.00	0.00	500.00
3234	-5881	-5839	-5838	-5880	MG	0.00	0.00	500.00
3234	-5843	-5842	-5884	-5885	MG	0.00	0.00	500.00
3234	-5797	-5796	-5842	-5843	MG	0.00	0.00	500.00
3234	-5842	-5796	-5795	-5841	MG	0.00	0.00	500.00
3234	-6062	-5989	-5988	-6061	MG	0.00	0.00	500.00
3234	-5840	-5794	-5793	-5839	MG	0.00	0.00	500.00
3234	-5988	-5879	-5878	-5987	MG	0.00	0.00	500.00
3234	-5996	-5888	-5887	-5995	MG	0.00	0.00	500.00
3234	-5998	-5890	-5889	-5997	MG	0.00	0.00	500.00
3234	-6129	-6061	-6060	-6128	MG	0.00	0.00	500.00
3234	-5972	-5893	-5892	-6000	MG	0.00	0.00	500.00
3234	-5880	-5838	-5837	-5879	MG	0.00	0.00	500.00
3234	-6075	-5972	-6000	-6074	MG	0.00	0.00	500.00
3234	-5879	-5837	-5836	-5878	MG	0.00	0.00	500.00
3234	-5883	-5841	-5840	-5882	MG	0.00	0.00	500.00
3234	-6061	-5988	-5987	-6060	MG	0.00	0.00	500.00
3234	-6134	-6066	-6065	-6133	MG	0.00	0.00	500.00
3234	-6066	-5993	-5992	-6065	MG	0.00	0.00	500.00
3234	-5993	-5884	-5883	-5992	MG	0.00	0.00	500.00
3234	-5997	-5889	-5888	-5996	MG	0.00	0.00	500.00
3234	-6141	-6073	-6072	-6140	MG	0.00	0.00	500.00
3234	-6133	-6065	-6064	-6132	MG	0.00	0.00	500.00
3234	-6239	-6196	-6195	-6248	MG	0.00	0.00	500.00
3234	-6188	-6131	-6130	-6187	MG	0.00	0.00	500.00
3234	-6065	-5992	-5991	-6064	MG	0.00	0.00	500.00
3234	-5845	-5799	-5798	-5844	MG	0.00	0.00	500.00
3234	-6064	-5991	-5990	-6063	MG	0.00	0.00	500.00
3234	-5994	-5993	-6066	-6067	MG	0.00	0.00	500.00
3234	-5991	-5882	-5881	-5990	MG	0.00	0.00	500.00
3234	-5841	-5795	-5794	-5840	MG	0.00	0.00	500.00
3234	-6195	-6138	-6137	-6194	MG	0.00	0.00	500.00
3234	-5886	-5885	-5994	-6025	MG	0.00	0.00	500.00
3234	-6131	-6063	-6062	-6130	MG	0.00	0.00	500.00
3234	-6237	-6188	-6187	-6236	MG	0.00	0.00	500.00
3234	-6192	-6191	-6238	-6245	MG	0.00	0.00	500.00
3234	-6071	-5997	-5996	-6070	MG	0.00	0.00	500.00
3234	-6193	-6192	-6245	-6246	MG	0.00	0.00	500.00
3234	-5889	-5847	-5846	-5888	MG	0.00	0.00	500.00
3234	-5836	-5790	-5789	-5835	MG	0.00	0.00	500.00
3234	-6251	-6199	-6198	-6250	MG	0.00	0.00	500.00
3234	-5893	-5851	-5850	-5892	MG	0.00	0.00	500.00
3234	-6200	-6143	-6142	-6199	MG	0.00	0.00	500.00
3234	-5844	-5843	-5885	-5886	MG	0.00	0.00	500.00
3234	-6186	-6129	-6128	-6185	MG	0.00	0.00	500.00
3234	-6136	-6137	-6069	-6068	MG	0.00	0.00	500.00
3234	-6132	-6064	-6063	-6131	MG	0.00	0.00	500.00
3234	-5849	-5803	-5802	-5848	MG	0.00	0.00	500.00
3234	-6025	-5994	-6067	-6068	MG	0.00	0.00	500.00
3234	-6190	-6133	-6132	-6189	MG	0.00	0.00	500.00
3234	-6243	-6189	-6188	-6237	MG	0.00	0.00	500.00
3234	-5850	-5804	-5803	-5849	MG	0.00	0.00	500.00
3234	-6191	-6134	-6133	-6190	MG	0.00	0.00	500.00
3234	-6139	-6071	-6070	-6138	MG	0.00	0.00	500.00
3234	-6189	-6132	-6131	-6188	MG	0.00	0.00	500.00
3234	-6072	-5998	-5997	-6071	MG	0.00	0.00	500.00
3234	-6135	-6134	-6191	-6192	MG	0.00	0.00	500.00
3234	-6143	-6075	-6074	-6142	MG	0.00	0.00	500.00
3234	-6197	-6140	-6139	-6196	MG	0.00	0.00	500.00
3234	-6235	-6186	-6185	-6242	MG	0.00	0.00	500.00
3255	-5445	-4936	-5444	-5444	MG	0.00	0.00	500.00
3257	-5334	-4700	-5848	-5849	MG	0.00	0.00	500.00

3257	-5850	-5334	-5849	-5849	MG	0.00	0.00	500.00
3259	-3948	-3986	-6673	-6677	MG	0.00	0.00	500.00
3264	-4220	-4252	-7140	-7141	MG	0.00	0.00	500.00
3266	-3608	-3826	-7139	-7140	MG	0.00	0.00	500.00
3325	-5746	-6242	-6235	-6235	MG	0.00	0.00	500.00
3325	-5746	-6235	-6236	-5052	MG	0.00	0.00	500.00
3331	-6151	-6667	-6688	-5447	MG	0.00	0.00	500.00
3333	-6304	-6303	-6371	-6372	MG	0.00	0.00	500.00
3333	-6999	-6998	-7057	-7058	MG	0.00	0.00	500.00
3333	-6917	-6916	-6999	-7000	MG	0.00	0.00	500.00
3333	-6378	-6310	-6309	-6377	MG	0.00	0.00	500.00
3333	-6828	-6743	-6742	-6827	MG	0.00	0.00	500.00
3333	-6301	-6244	-6243	-6300	MG	0.00	0.00	500.00
3333	-6303	-6302	-6370	-6371	MG	0.00	0.00	500.00
3333	-6916	-6915	-6998	-6999	MG	0.00	0.00	500.00
3333	-7061	-7002	-7001	-7060	MG	0.00	0.00	500.00
3333	-6833	-6748	-6747	-6832	MG	0.00	0.00	500.00
3333	-7141	-7061	-7060	-7140	MG	0.00	0.00	500.00
3333	-6834	-6833	-6915	-6916	MG	0.00	0.00	500.00
3333	-6374	-6306	-6305	-6373	MG	0.00	0.00	500.00
3333	-6624	-6539	-6551	-6623	MG	0.00	0.00	500.00
3333	-6994	-6911	-6910	-6993	MG	0.00	0.00	500.00
3333	-7140	-7060	-7059	-7139	MG	0.00	0.00	500.00
3333	-6993	-6910	-6909	-6992	MG	0.00	0.00	500.00
3333	-6379	-6311	-6310	-6378	MG	0.00	0.00	500.00
3333	-6842	-6757	-6756	-6841	MG	0.00	0.00	500.00
3333	-6364	-6296	-6295	-6363	MG	0.00	0.00	500.00
3333	-7062	-7003	-7002	-7061	MG	0.00	0.00	500.00
3333	-7003	-6920	-6919	-7002	MG	0.00	0.00	500.00
3333	-6536	-6477	-6476	-6535	MG	0.00	0.00	500.00
3333	-6484	-6483	-6548	-6549	MG	0.00	0.00	500.00
3333	-7057	-6998	-6997	-7056	MG	0.00	0.00	500.00
3333	-6302	-6238	-6244	-6301	MG	0.00	0.00	500.00
3333	-6547	-6482	-6481	-6538	MG	0.00	0.00	500.00
3333	-6369	-6301	-6300	-6368	MG	0.00	0.00	500.00
3333	-6371	-6370	-6483	-6484	MG	0.00	0.00	500.00
3333	-6485	-6484	-6549	-6550	MG	0.00	0.00	500.00
3333	-7133	-7053	-7052	-7132	MG	0.00	0.00	500.00
3333	-7000	-6999	-7058	-7059	MG	0.00	0.00	500.00
3333	-6492	-6379	-6378	-6491	MG	0.00	0.00	500.00
3333	-6368	-6300	-6299	-6367	MG	0.00	0.00	500.00
3333	-7132	-7052	-7051	-7131	MG	0.00	0.00	500.00
3333	-7136	-7056	-7055	-7135	MG	0.00	0.00	500.00
3333	-6308	-6249	-6239	-6307	MG	0.00	0.00	500.00
3333	-6678	-6625	-6624	-6677	MG	0.00	0.00	500.00
3333	-6625	-6552	-6539	-6624	MG	0.00	0.00	500.00
3333	-6671	-6689	-6748	-6749	MG	0.00	0.00	500.00
3333	-6677	-6624	-6623	-6673	MG	0.00	0.00	500.00
3333	-7146	-7066	-7065	-7145	MG	0.00	0.00	500.00
3333	-7051	-6992	-6991	-7050	MG	0.00	0.00	500.00
3333	-6299	-6237	-6236	-6298	MG	0.00	0.00	500.00
3333	-6306	-6248	-6247	-6305	MG	0.00	0.00	500.00
3333	-6748	-6689	-6670	-6747	MG	0.00	0.00	500.00
3333	-6487	-6374	-6373	-6486	MG	0.00	0.00	500.00
3333	-7056	-6997	-6996	-7055	MG	0.00	0.00	500.00
3333	-6629	-6556	-6555	-6628	MG	0.00	0.00	500.00
3333	-6832	-6747	-6746	-6831	MG	0.00	0.00	500.00
3333	-7143	-7063	-7062	-7142	MG	0.00	0.00	500.00
3333	-7055	-6996	-6995	-7054	MG	0.00	0.00	500.00
3333	-6901	-6842	-6841	-6923	MG	0.00	0.00	500.00
3333	-6297	-6235	-6242	-6296	MG	0.00	0.00	500.00
3333	-6614	-6536	-6535	-6613	MG	0.00	0.00	500.00
3333	-6754	-6690	-6678	-6753	MG	0.00	0.00	500.00
3333	-6477	-6364	-6363	-6476	MG	0.00	0.00	500.00
3333	-6375	-6307	-6306	-6374	MG	0.00	0.00	500.00
3333	-6998	-6915	-6914	-6997	MG	0.00	0.00	500.00
3333	-6619	-6547	-6538	-6618	MG	0.00	0.00	500.00
3333	-6995	-6912	-6911	-6994	MG	0.00	0.00	500.00
3333	-6246	-6245	-6303	-6304	MG	0.00	0.00	500.00
3333	-6830	-6745	-6744	-6829	MG	0.00	0.00	500.00
3333	-6482	-6369	-6368	-6481	MG	0.00	0.00	500.00
3333	-7053	-6994	-6993	-7052	MG	0.00	0.00	500.00
3333	-6377	-6309	-6308	-6376	MG	0.00	0.00	500.00
3333	-6538	-6481	-6480	-6546	MG	0.00	0.00	500.00
3333	-6835	-6834	-6916	-6917	MG	0.00	0.00	500.00
3333	-6829	-6744	-6743	-6828	MG	0.00	0.00	500.00
3333	-6481	-6368	-6367	-6480	MG	0.00	0.00	500.00
3333	-7007	-6901	-6923	-7006	MG	0.00	0.00	500.00
3333	-6300	-6243	-6237	-6299	MG	0.00	0.00	500.00

3333	-6668	-6617	-6616	-6688	MG	0.00	0.00	500.00
3333	-6757	-6693	-6692	-6756	MG	0.00	0.00	500.00
3333	-6546	-6480	-6479	-6537	MG	0.00	0.00	500.00
3333	-6307	-6239	-6248	-6306	MG	0.00	0.00	500.00
3333	-6751	-6673	-6672	-6750	MG	0.00	0.00	500.00
3333	-7131	-7051	-7050	-7130	MG	0.00	0.00	500.00
3333	-6915	-6833	-6832	-6914	MG	0.00	0.00	500.00
3333	-6537	-6479	-6478	-6545	MG	0.00	0.00	500.00
3333	-7059	-7058	-7138	-7139	MG	0.00	0.00	500.00
3333	-6742	-6687	-6666	-6741	MG	0.00	0.00	500.00
3333	-6997	-6914	-6913	-6996	MG	0.00	0.00	500.00
3333	-6922	-6840	-6839	-6921	MG	0.00	0.00	500.00
3333	-6556	-6492	-6491	-6555	MG	0.00	0.00	500.00
3333	-6840	-6755	-6754	-6839	MG	0.00	0.00	500.00
3333	-6545	-6478	-6477	-6536	MG	0.00	0.00	500.00
3333	-6311	-6252	-6251	-6310	MG	0.00	0.00	500.00
3333	-6365	-6297	-6296	-6364	MG	0.00	0.00	500.00
3333	-6921	-6839	-6838	-6920	MG	0.00	0.00	500.00
3333	-6839	-6754	-6753	-6838	MG	0.00	0.00	500.00
3333	-6491	-6378	-6377	-6490	MG	0.00	0.00	500.00
3333	-7142	-7062	-7061	-7141	MG	0.00	0.00	500.00
3333	-7134	-7054	-7053	-7133	MG	0.00	0.00	500.00
3333	-6310	-6251	-6250	-6309	MG	0.00	0.00	500.00
3333	-6912	-6830	-6829	-6911	MG	0.00	0.00	500.00
3333	-6490	-6377	-6376	-6489	MG	0.00	0.00	500.00
3333	-6753	-6678	-6677	-6752	MG	0.00	0.00	500.00
3333	-6621	-6620	-6689	-6671	MG	0.00	0.00	500.00
3333	-6549	-6548	-6620	-6621	MG	0.00	0.00	500.00
3333	-6673	-6623	-6622	-6672	MG	0.00	0.00	500.00
3333	-6618	-6538	-6546	-6617	MG	0.00	0.00	500.00
3333	-6670	-6619	-6618	-6669	MG	0.00	0.00	500.00
3333	-6752	-6677	-6673	-6751	MG	0.00	0.00	500.00
3333	-7001	-6918	-6917	-7000	MG	0.00	0.00	500.00
3333	-6376	-6308	-6307	-6375	MG	0.00	0.00	500.00
3333	-6372	-6371	-6484	-6485	MG	0.00	0.00	500.00
3333	-6550	-6549	-6621	-6622	MG	0.00	0.00	500.00
3333	-6552	-6488	-6487	-6539	MG	0.00	0.00	500.00
3333	-6488	-6375	-6374	-6487	MG	0.00	0.00	500.00
3333	-6480	-6367	-6366	-6479	MG	0.00	0.00	500.00
3333	-7145	-7065	-7064	-7144	MG	0.00	0.00	500.00
3333	-6367	-6299	-6298	-6366	MG	0.00	0.00	500.00
3333	-6992	-6909	-6900	-6991	MG	0.00	0.00	500.00
3333	-6616	-6537	-6545	-6615	MG	0.00	0.00	500.00
3333	-6539	-6487	-6486	-6551	MG	0.00	0.00	500.00
3333	-6827	-6742	-6741	-6826	MG	0.00	0.00	500.00
3333	-7058	-7057	-7137	-7138	MG	0.00	0.00	500.00
3333	-6914	-6832	-6831	-6913	MG	0.00	0.00	500.00
3333	-6623	-6551	-6550	-6622	MG	0.00	0.00	500.00
3333	-7135	-7055	-7054	-7134	MG	0.00	0.00	500.00
3333	-6551	-6486	-6485	-6550	MG	0.00	0.00	500.00
3333	-6373	-6305	-6304	-6372	MG	0.00	0.00	500.00
3333	-6996	-6913	-6912	-6995	MG	0.00	0.00	500.00
3333	-6913	-6831	-6830	-6912	MG	0.00	0.00	500.00
3333	-7137	-7057	-7056	-7136	MG	0.00	0.00	500.00
3333	-6548	-6483	-6482	-6547	MG	0.00	0.00	500.00
3333	-6620	-6548	-6547	-6619	MG	0.00	0.00	500.00
3333	-6370	-6302	-6301	-6369	MG	0.00	0.00	500.00
3333	-7054	-6995	-6994	-7053	MG	0.00	0.00	500.00
3333	-6296	-6242	-6234	-6295	MG	0.00	0.00	500.00
3333	-6622	-6621	-6671	-6672	MG	0.00	0.00	500.00
3333	-6745	-6668	-6688	-6744	MG	0.00	0.00	500.00
3333	-6838	-6753	-6752	-6837	MG	0.00	0.00	500.00
3333	-6627	-6554	-6553	-6626	MG	0.00	0.00	500.00
3333	-6690	-6626	-6625	-6678	MG	0.00	0.00	500.00
3333	-6911	-6829	-6828	-6910	MG	0.00	0.00	500.00
3333	-6626	-6553	-6552	-6625	MG	0.00	0.00	500.00
3333	-6672	-6671	-6749	-6750	MG	0.00	0.00	500.00
3333	-7066	-7007	-7006	-7065	MG	0.00	0.00	500.00
3333	-7052	-6993	-6992	-7051	MG	0.00	0.00	500.00
3333	-6489	-6376	-6375	-6488	MG	0.00	0.00	500.00
3333	-6910	-6828	-6827	-6909	MG	0.00	0.00	500.00
3333	-6617	-6546	-6537	-6616	MG	0.00	0.00	500.00
3333	-6687	-6614	-6613	-6666	MG	0.00	0.00	500.00
3333	-6746	-6669	-6668	-6745	MG	0.00	0.00	500.00
3333	-7065	-7006	-7005	-7064	MG	0.00	0.00	500.00
3333	-6743	-6667	-6687	-6742	MG	0.00	0.00	500.00
3333	-6923	-6841	-6840	-6922	MG	0.00	0.00	500.00
3333	-7144	-7064	-7063	-7143	MG	0.00	0.00	500.00
3333	-6756	-6692	-6691	-6755	MG	0.00	0.00	500.00

3333	-6841	-6756	-6755	-6840	MG	0.00	0.00	500.00
3333	-7005	-6922	-6921	-7004	MG	0.00	0.00	500.00
3333	-6298	-6236	-6235	-6297	MG	0.00	0.00	500.00
3333	-6366	-6298	-6297	-6365	MG	0.00	0.00	500.00
3333	-6755	-6691	-6690	-6754	MG	0.00	0.00	500.00
3333	-6615	-6545	-6536	-6614	MG	0.00	0.00	500.00
3333	-7063	-7004	-7003	-7062	MG	0.00	0.00	500.00
3333	-6692	-6628	-6627	-6691	MG	0.00	0.00	500.00
3333	-6628	-6555	-6554	-6627	MG	0.00	0.00	500.00
3333	-6555	-6491	-6490	-6554	MG	0.00	0.00	500.00
3333	-6750	-6749	-6834	-6835	MG	0.00	0.00	500.00
3333	-6831	-6746	-6745	-6830	MG	0.00	0.00	500.00
3333	-6483	-6370	-6369	-6482	MG	0.00	0.00	500.00
3333	-6245	-6238	-6302	-6303	MG	0.00	0.00	500.00
3333	-6693	-6629	-6628	-6692	MG	0.00	0.00	500.00
3333	-6554	-6490	-6489	-6553	MG	0.00	0.00	500.00
3333	-6691	-6627	-6626	-6690	MG	0.00	0.00	500.00
3333	-6688	-6616	-6615	-6667	MG	0.00	0.00	500.00
3333	-6836	-6751	-6750	-6835	MG	0.00	0.00	500.00
3333	-6919	-6837	-6836	-6918	MG	0.00	0.00	500.00
3333	-6669	-6618	-6617	-6668	MG	0.00	0.00	500.00
3333	-6749	-6748	-6833	-6834	MG	0.00	0.00	500.00
3333	-6747	-6670	-6669	-6746	MG	0.00	0.00	500.00
3333	-7060	-7001	-7000	-7059	MG	0.00	0.00	500.00
3333	-6305	-6247	-6246	-6304	MG	0.00	0.00	500.00
3333	-6918	-6836	-6835	-6917	MG	0.00	0.00	500.00
3333	-6689	-6620	-6619	-6670	MG	0.00	0.00	500.00
3333	-6478	-6365	-6364	-6477	MG	0.00	0.00	500.00
3333	-6479	-6366	-6365	-6478	MG	0.00	0.00	500.00
3333	-7002	-6919	-6918	-7001	MG	0.00	0.00	500.00
3333	-7006	-6923	-6922	-7005	MG	0.00	0.00	500.00
3333	-6667	-6615	-6614	-6667	MG	0.00	0.00	500.00
3333	-6909	-6827	-6826	-6908	MG	0.00	0.00	500.00
3333	-6920	-6838	-6837	-6919	MG	0.00	0.00	500.00
3333	-6553	-6489	-6488	-6552	MG	0.00	0.00	500.00
3333	-7004	-6921	-6920	-7003	MG	0.00	0.00	500.00
3333	-6486	-6373	-6372	-6485	MG	0.00	0.00	500.00
3333	-6744	-6688	-6667	-6743	MG	0.00	0.00	500.00
3333	-6837	-6752	-6751	-6836	MG	0.00	0.00	500.00
3333	-6309	-6250	-6249	-6308	MG	0.00	0.00	500.00
3333	-7064	-7005	-7004	-7063	MG	0.00	0.00	500.00
3364	-5747	-5053	-6249	-6250	MG	0.00	0.00	500.00
3364	-6251	-5747	-6250	-6250	MG	0.00	0.00	500.00
3372	-6152	-5448	-6690	-6691	MG	0.00	0.00	500.00
3435	-6151	-6687	-6667	-6667	MG	0.00	0.00	500.00
3437	-7502	-7466	-7465	-7501	MG	0.00	0.00	500.00
3437	-7269	-7206	-7205	-7268	MG	0.00	0.00	500.00
3437	-7349	-7348	-7464	-7465	MG	0.00	0.00	500.00
3437	-7257	-7194	-7193	-7256	MG	0.00	0.00	500.00
3437	-7348	-7347	-7463	-7464	MG	0.00	0.00	500.00
3437	-7468	-7352	-7351	-7467	MG	0.00	0.00	500.00
3437	-7265	-7264	-7298	-7299	MG	0.00	0.00	500.00
3437	-7459	-7343	-7342	-7458	MG	0.00	0.00	500.00
3437	-7472	-7356	-7355	-7471	MG	0.00	0.00	500.00
3437	-7505	-7469	-7468	-7504	MG	0.00	0.00	500.00
3437	-7495	-7459	-7458	-7494	MG	0.00	0.00	500.00
3437	-7264	-7263	-7297	-7298	MG	0.00	0.00	500.00
3437	-7138	-7137	-7200	-7201	MG	0.00	0.00	500.00
3437	-7291	-7257	-7256	-7290	MG	0.00	0.00	500.00
3437	-7299	-7298	-7348	-7349	MG	0.00	0.00	500.00
3437	-7499	-7463	-7462	-7498	MG	0.00	0.00	500.00
3437	-7139	-7138	-7201	-7202	MG	0.00	0.00	500.00
3437	-7356	-7306	-7305	-7355	MG	0.00	0.00	500.00
3437	-7306	-7272	-7271	-7305	MG	0.00	0.00	500.00
3437	-7272	-7209	-7208	-7271	MG	0.00	0.00	500.00
3437	-7305	-7271	-7270	-7304	MG	0.00	0.00	500.00
3437	-7271	-7208	-7207	-7270	MG	0.00	0.00	500.00
3437	-7208	-7145	-7144	-7207	MG	0.00	0.00	500.00
3437	-7470	-7354	-7353	-7469	MG	0.00	0.00	500.00
3437	-7303	-7269	-7268	-7302	MG	0.00	0.00	500.00
3437	-7504	-7468	-7467	-7503	MG	0.00	0.00	500.00
3437	-7467	-7351	-7350	-7466	MG	0.00	0.00	500.00
3437	-7351	-7301	-7300	-7350	MG	0.00	0.00	500.00
3437	-7301	-7267	-7266	-7300	MG	0.00	0.00	500.00
3437	-7267	-7204	-7203	-7266	MG	0.00	0.00	500.00
3437	-7508	-7472	-7471	-7507	MG	0.00	0.00	500.00
3437	-7263	-7200	-7199	-7262	MG	0.00	0.00	500.00
3437	-7200	-7137	-7136	-7199	MG	0.00	0.00	500.00
3437	-7296	-7262	-7261	-7295	MG	0.00	0.00	500.00

3437	-7262	-7199	-7198	-7261	MG	0.00	0.00	500.00
3437	-7497	-7461	-7460	-7496	MG	0.00	0.00	500.00
3437	-7461	-7345	-7344	-7460	MG	0.00	0.00	500.00
3437	-7345	-7295	-7294	-7344	MG	0.00	0.00	500.00
3437	-7295	-7261	-7260	-7294	MG	0.00	0.00	500.00
3437	-7261	-7198	-7197	-7260	MG	0.00	0.00	500.00
3437	-7198	-7135	-7134	-7197	MG	0.00	0.00	500.00
3437	-7496	-7460	-7459	-7495	MG	0.00	0.00	500.00
3437	-7460	-7344	-7343	-7459	MG	0.00	0.00	500.00
3437	-7344	-7294	-7293	-7343	MG	0.00	0.00	500.00
3437	-7294	-7260	-7259	-7293	MG	0.00	0.00	500.00
3437	-7260	-7197	-7196	-7259	MG	0.00	0.00	500.00
3437	-7197	-7134	-7133	-7196	MG	0.00	0.00	500.00
3437	-6558	-7131	-7132	-7132	MG	0.00	0.00	500.00
3437	-6558	-7132	-7133	-5852	MG	0.00	0.00	500.00
3437	-7343	-7293	-7292	-7342	MG	0.00	0.00	500.00
3437	-7293	-7259	-7258	-7292	MG	0.00	0.00	500.00
3437	-7259	-7196	-7195	-7258	MG	0.00	0.00	500.00
3437	-7196	-7133	-7132	-7195	MG	0.00	0.00	500.00
3437	-7494	-7458	-7457	-7493	MG	0.00	0.00	500.00
3437	-7458	-7342	-7341	-7457	MG	0.00	0.00	500.00
3437	-7342	-7292	-7291	-7341	MG	0.00	0.00	500.00
3437	-7292	-7258	-7257	-7291	MG	0.00	0.00	500.00
3437	-7258	-7195	-7194	-7257	MG	0.00	0.00	500.00
3437	-7195	-7132	-7131	-7194	MG	0.00	0.00	500.00
3437	-7493	-7457	-7456	-7492	MG	0.00	0.00	500.00
3437	-7457	-7341	-7340	-7456	MG	0.00	0.00	500.00
3437	-7341	-7291	-7290	-7340	MG	0.00	0.00	500.00
3437	-7194	-7131	-7130	-7193	MG	0.00	0.00	500.00
3437	-7465	-7464	-7500	-7501	MG	0.00	0.00	500.00
3437	-7464	-7463	-7499	-7500	MG	0.00	0.00	500.00
3437	-7298	-7297	-7347	-7348	MG	0.00	0.00	500.00
3437	-7302	-7268	-7267	-7301	MG	0.00	0.00	500.00
3437	-7503	-7467	-7466	-7502	MG	0.00	0.00	500.00
3437	-7202	-7201	-7264	-7265	MG	0.00	0.00	500.00
3437	-7201	-7200	-7263	-7264	MG	0.00	0.00	500.00
3437	-7498	-7462	-7461	-7497	MG	0.00	0.00	500.00
3437	-7209	-7146	-7145	-7208	MG	0.00	0.00	500.00
3437	-7507	-7471	-7470	-7506	MG	0.00	0.00	500.00
3437	-7471	-7355	-7354	-7470	MG	0.00	0.00	500.00
3437	-7355	-7305	-7304	-7354	MG	0.00	0.00	500.00
3437	-7506	-7470	-7469	-7505	MG	0.00	0.00	500.00
3437	-7354	-7304	-7303	-7353	MG	0.00	0.00	500.00
3437	-7304	-7270	-7269	-7303	MG	0.00	0.00	500.00
3437	-7270	-7207	-7206	-7269	MG	0.00	0.00	500.00
3437	-7207	-7144	-7143	-7206	MG	0.00	0.00	500.00
3437	-7469	-7353	-7352	-7468	MG	0.00	0.00	500.00
3437	-7353	-7303	-7302	-7352	MG	0.00	0.00	500.00
3437	-7206	-7143	-7142	-7205	MG	0.00	0.00	500.00
3437	-7352	-7302	-7301	-7351	MG	0.00	0.00	500.00
3437	-7268	-7205	-7204	-7267	MG	0.00	0.00	500.00
3437	-7205	-7142	-7141	-7204	MG	0.00	0.00	500.00
3437	-7204	-7141	-7140	-7203	MG	0.00	0.00	500.00
3437	-7466	-7350	-7349	-7465	MG	0.00	0.00	500.00
3437	-7350	-7300	-7299	-7349	MG	0.00	0.00	500.00
3437	-7300	-7266	-7265	-7299	MG	0.00	0.00	500.00
3437	-7266	-7203	-7202	-7265	MG	0.00	0.00	500.00
3437	-7203	-7140	-7139	-7202	MG	0.00	0.00	500.00
3437	-7463	-7347	-7346	-7462	MG	0.00	0.00	500.00
3437	-7347	-7297	-7296	-7346	MG	0.00	0.00	500.00
3437	-7297	-7263	-7262	-7296	MG	0.00	0.00	500.00
3437	-7462	-7346	-7345	-7461	MG	0.00	0.00	500.00
3437	-7346	-7296	-7295	-7345	MG	0.00	0.00	500.00
3437	-7199	-7136	-7135	-7198	MG	0.00	0.00	500.00
3471	-6692	-6152	-6691	-6691	MG	0.00	0.00	500.00
3474	-7145	-6559	-7144	-7144	MG	0.00	0.00	500.00
3474	-6559	-5853	-7143	-7144	MG	0.00	0.00	500.00
3824	-4583	-4588	-4572	-4571	MG	0.00	0.00	500.00
3824	-4611	-4594	-4597	-4625	MG	0.00	0.00	500.00
3824	-4626	-4611	-4625	-4625	MG	0.00	0.00	500.00
3824	-4621	-4603	-4601	-4620	MG	0.00	0.00	500.00
3824	-4652	-4635	-4634	-4651	MG	0.00	0.00	500.00
3824	-4589	-4598	-4608	-4592	MG	0.00	0.00	500.00
3824	-4607	-4583	-4592	-4608	MG	0.00	0.00	500.00
3824	-4573	-4570	-4558	-4555	MG	0.00	0.00	500.00
3824	-4651	-4634	-4633	-4650	MG	0.00	0.00	500.00
3824	-4536	-4527	-4531	-4531	MG	0.00	0.00	500.00
3824	-4594	-4579	-4590	-4597	MG	0.00	0.00	500.00
3824	-4579	-4569	-4574	-4590	MG	0.00	0.00	500.00

3824	-4569	-4554	-4562	-4574	MG	0.00	0.00	500.00
3824	-4554	-4541	-4551	-4562	MG	0.00	0.00	500.00
3824	-4541	-4539	-4545	-4551	MG	0.00	0.00	500.00
3824	-4583	-4607	-4604	-4588	MG	0.00	0.00	500.00
3824	-4649	-4632	-4631	-4648	MG	0.00	0.00	500.00
3824	-4634	-4620	-4619	-4633	MG	0.00	0.00	500.00
3824	-4648	-4631	-4636	-4653	MG	0.00	0.00	500.00
3824	-4631	-4617	-4616	-4636	MG	0.00	0.00	500.00
3824	-4636	-4616	-4615	-4638	MG	0.00	0.00	500.00
3824	-4615	-4614	-4640	-4638	MG	0.00	0.00	500.00
3824	-4614	-4613	-4629	-4640	MG	0.00	0.00	500.00
3824	-4613	-4612	-4627	-4629	MG	0.00	0.00	500.00
3824	-4627	-4642	-4644	-4629	MG	0.00	0.00	500.00
3824	-4642	-4659	-4663	-4644	MG	0.00	0.00	500.00
3824	-4562	-4551	-4558	-4570	MG	0.00	0.00	500.00
3824	-4545	-4555	-4558	-4551	MG	0.00	0.00	500.00
3824	-4570	-4573	-4587	-4586	MG	0.00	0.00	500.00
3824	-4650	-4633	-4632	-4649	MG	0.00	0.00	500.00
3824	-4633	-4619	-4618	-4632	MG	0.00	0.00	500.00
3824	-4597	-4590	-4591	-4609	MG	0.00	0.00	500.00
3824	-4591	-4590	-4574	-4586	MG	0.00	0.00	500.00
3824	-4586	-4587	-4605	-4606	MG	0.00	0.00	500.00
3824	-4632	-4618	-4617	-4631	MG	0.00	0.00	500.00
3824	-4629	-4644	-4646	-4640	MG	0.00	0.00	500.00
3824	-4644	-4663	-4661	-4646	MG	0.00	0.00	500.00
3824	-4646	-4661	-4657	-4640	MG	0.00	0.00	500.00
3824	-4532	-4528	-4537	-4537	MG	0.00	0.00	500.00
3824	-4635	-4621	-4620	-4634	MG	0.00	0.00	500.00
3824	-4653	-4636	-4638	-4655	MG	0.00	0.00	500.00
3824	-4655	-4638	-4640	-4657	MG	0.00	0.00	500.00
3824	-4660	-4643	-4645	-4664	MG	0.00	0.00	500.00
3824	-4643	-4628	-4630	-4645	MG	0.00	0.00	500.00
3824	-4628	-4626	-4625	-4630	MG	0.00	0.00	500.00
3824	-4625	-4624	-4641	-4630	MG	0.00	0.00	500.00
3824	-4624	-4623	-4639	-4641	MG	0.00	0.00	500.00
3824	-4623	-4622	-4637	-4639	MG	0.00	0.00	500.00
3824	-4637	-4622	-4621	-4635	MG	0.00	0.00	500.00
3824	-4654	-4637	-4635	-4652	MG	0.00	0.00	500.00
3824	-4539	-4532	-4537	-4545	MG	0.00	0.00	500.00
3824	-4537	-4550	-4555	-4545	MG	0.00	0.00	500.00
3824	-4550	-4567	-4573	-4555	MG	0.00	0.00	500.00
3824	-4567	-4585	-4587	-4573	MG	0.00	0.00	500.00
3824	-4585	-4603	-4605	-4587	MG	0.00	0.00	500.00
3824	-4603	-4621	-4622	-4605	MG	0.00	0.00	500.00
3824	-4622	-4623	-4606	-4605	MG	0.00	0.00	500.00
3824	-4623	-4624	-4609	-4606	MG	0.00	0.00	500.00
3824	-4624	-4625	-4597	-4609	MG	0.00	0.00	500.00
3824	-4658	-4662	-4647	-4641	MG	0.00	0.00	500.00
3824	-4662	-4664	-4645	-4647	MG	0.00	0.00	500.00
3824	-4647	-4645	-4630	-4641	MG	0.00	0.00	500.00
3824	-4639	-4637	-4654	-4656	MG	0.00	0.00	500.00
3824	-4639	-4656	-4658	-4641	MG	0.00	0.00	500.00
3824	-4570	-4586	-4574	-4562	MG	0.00	0.00	500.00
3824	-4606	-4609	-4591	-4586	MG	0.00	0.00	500.00
3824	-4603	-4585	-4582	-4601	MG	0.00	0.00	500.00
3824	-4585	-4567	-4565	-4582	MG	0.00	0.00	500.00
3824	-4567	-4550	-4548	-4565	MG	0.00	0.00	500.00
3824	-4550	-4537	-4535	-4548	MG	0.00	0.00	500.00
3824	-4537	-4528	-4526	-4535	MG	0.00	0.00	500.00
3824	-4620	-4601	-4599	-4619	MG	0.00	0.00	500.00
3824	-4601	-4582	-4580	-4599	MG	0.00	0.00	500.00
3824	-4582	-4565	-4563	-4580	MG	0.00	0.00	500.00
3824	-4565	-4548	-4546	-4563	MG	0.00	0.00	500.00
3824	-4548	-4535	-4533	-4546	MG	0.00	0.00	500.00
3824	-4535	-4526	-4524	-4533	MG	0.00	0.00	500.00
3824	-4619	-4599	-4600	-4618	MG	0.00	0.00	500.00
3824	-4599	-4580	-4581	-4600	MG	0.00	0.00	500.00
3824	-4580	-4563	-4564	-4581	MG	0.00	0.00	500.00
3824	-4563	-4546	-4547	-4564	MG	0.00	0.00	500.00
3824	-4546	-4533	-4534	-4547	MG	0.00	0.00	500.00
3824	-4533	-4524	-4525	-4534	MG	0.00	0.00	500.00
3824	-4618	-4600	-4602	-4617	MG	0.00	0.00	500.00
3824	-4600	-4581	-4584	-4602	MG	0.00	0.00	500.00
3824	-4581	-4564	-4566	-4584	MG	0.00	0.00	500.00
3824	-4564	-4547	-4549	-4566	MG	0.00	0.00	500.00
3824	-4547	-4534	-4536	-4549	MG	0.00	0.00	500.00
3824	-4534	-4525	-4527	-4536	MG	0.00	0.00	500.00
3824	-4610	-4612	-4613	-4613	MG	0.00	0.00	500.00
3824	-4602	-4584	-4588	-4604	MG	0.00	0.00	500.00

3824	-4584	-4566	-4572	-4588	MG	0.00	0.00	500.00
3824	-4566	-4549	-4556	-4572	MG	0.00	0.00	500.00
3824	-4549	-4536	-4544	-4556	MG	0.00	0.00	500.00
3824	-4536	-4531	-4538	-4544	MG	0.00	0.00	500.00
3824	-4538	-4540	-4552	-4544	MG	0.00	0.00	500.00
3824	-4540	-4553	-4561	-4552	MG	0.00	0.00	500.00
3824	-4553	-4568	-4575	-4561	MG	0.00	0.00	500.00
3824	-4568	-4578	-4589	-4575	MG	0.00	0.00	500.00
3824	-4578	-4593	-4598	-4589	MG	0.00	0.00	500.00
3824	-4593	-4610	-4613	-4598	MG	0.00	0.00	500.00
3824	-4613	-4614	-4608	-4598	MG	0.00	0.00	500.00
3824	-4614	-4615	-4607	-4608	MG	0.00	0.00	500.00
3824	-4615	-4616	-4604	-4607	MG	0.00	0.00	500.00
3824	-4617	-4602	-4604	-4616	MG	0.00	0.00	500.00
3824	-4544	-4552	-4557	-4556	MG	0.00	0.00	500.00
3824	-4561	-4571	-4557	-4552	MG	0.00	0.00	500.00
3824	-4572	-4556	-4557	-4571	MG	0.00	0.00	500.00
3824	-4575	-4583	-4571	-4561	MG	0.00	0.00	500.00
3824	-4575	-4589	-4592	-4583	MG	0.00	0.00	500.00

Elenco carichi elementi bidimensionali

Condizione di carico n. 8: Variabili impalc. (caso 4)_tors

Carichi uniformi

Bid.	N1	N2	N3	N4	T/DC	Qx	Qy	Qz
						<daN/mq>	<daN/mq>	<daN/mq>
2718	-3859	-3858	-3909	-3910	MG	0.00	0.00	500.00
2718	-3665	-3676	-3719	-3720	MG	0.00	0.00	500.00
2718	-3572	-3571	-3610	-3611	MG	0.00	0.00	500.00
2718	-3720	-3719	-3769	-3765	MG	0.00	0.00	500.00
2718	-3765	-3769	-3811	-3812	MG	0.00	0.00	500.00
2718	-3812	-3811	-3858	-3859	MG	0.00	0.00	500.00
2718	-3525	-3524	-3571	-3572	MG	0.00	0.00	500.00
2718	-3611	-3610	-3676	-3665	MG	0.00	0.00	500.00
2843	-4149	-3749	-3656	-3656	MG	0.00	0.00	500.00
2847	-4404	-4039	-3948	-3948	MG	0.00	0.00	500.00
2848	-3659	-4296	-4220	-4220	MG	0.00	0.00	500.00
2935	-4864	-4809	-4808	-4863	MG	0.00	0.00	500.00
2935	-4671	-4654	-4652	-4669	MG	0.00	0.00	500.00
2935	-4697	-4680	-4677	-4696	MG	0.00	0.00	500.00
2935	-4669	-4652	-4651	-4668	MG	0.00	0.00	500.00
2935	-4754	-4695	-4694	-4753	MG	0.00	0.00	500.00
2935	-4755	-4696	-4695	-4754	MG	0.00	0.00	500.00
2935	-4813	-4756	-4755	-4812	MG	0.00	0.00	500.00
2935	-4656	-4673	-4675	-4658	MG	0.00	0.00	500.00
2935	-4812	-4755	-4754	-4811	MG	0.00	0.00	500.00
2935	-4867	-4812	-4811	-4866	MG	0.00	0.00	500.00
2935	-4694	-4695	-4675	-4673	MG	0.00	0.00	500.00
2935	-4698	-4681	-4680	-4697	MG	0.00	0.00	500.00
2935	-4752	-4693	-4692	-4751	MG	0.00	0.00	500.00
2935	-4809	-4752	-4751	-4808	MG	0.00	0.00	500.00
2935	-4751	-4692	-4691	-4750	MG	0.00	0.00	500.00
2935	-4807	-4806	-4861	-4862	MG	0.00	0.00	500.00
2935	-4692	-4669	-4668	-4691	MG	0.00	0.00	500.00
2935	-4810	-4753	-4752	-4809	MG	0.00	0.00	500.00
2935	-4668	-4651	-4650	-4667	MG	0.00	0.00	500.00
2935	-4669	-4692	-4693	-4671	MG	0.00	0.00	500.00
2935	-4696	-4677	-4675	-4695	MG	0.00	0.00	500.00
2935	-4756	-4697	-4696	-4755	MG	0.00	0.00	500.00
2935	-4677	-4680	-4664	-4662	MG	0.00	0.00	500.00
2935	-4681	-4660	-4664	-4680	MG	0.00	0.00	500.00
2935	-4753	-4694	-4693	-4752	MG	0.00	0.00	500.00
2935	-4656	-4654	-4671	-4673	MG	0.00	0.00	500.00
2935	-4750	-4749	-4806	-4807	MG	0.00	0.00	500.00
2935	-4868	-4813	-4812	-4867	MG	0.00	0.00	500.00
2935	-4808	-4751	-4750	-4807	MG	0.00	0.00	500.00
2935	-4866	-4811	-4810	-4865	MG	0.00	0.00	500.00
2935	-4691	-4668	-4667	-4690	MG	0.00	0.00	500.00
2935	-4694	-4673	-4671	-4693	MG	0.00	0.00	500.00
2935	-4691	-4690	-4749	-4750	MG	0.00	0.00	500.00
2935	-4865	-4810	-4809	-4864	MG	0.00	0.00	500.00
2935	-4814	-4757	-4756	-4813	MG	0.00	0.00	500.00
2935	-4869	-4814	-4813	-4868	MG	0.00	0.00	500.00
2935	-4811	-4754	-4753	-4810	MG	0.00	0.00	500.00
2935	-4757	-4698	-4697	-4756	MG	0.00	0.00	500.00
2935	-4677	-4662	-4658	-4675	MG	0.00	0.00	500.00
2935	-4863	-4808	-4807	-4862	MG	0.00	0.00	500.00
2937	-6372	-3559	-3606	-6485	MG	0.00	0.00	500.00
2939	-6105	-3572	-3611	-6173	MG	0.00	0.00	500.00

2939	-6037	-3525	-3572	-6105	MG	0.00	0.00	500.00
2939	-6002	-3720	-3765	-6222	MG	0.00	0.00	500.00
2939	-6173	-3611	-3665	-6103	MG	0.00	0.00	500.00
2939	-6103	-3665	-3720	-6002	MG	0.00	0.00	500.00
2945	-4697	-4199	-4696	-4696	MG	0.00	0.00	500.00
2945	-4199	-3733	-4695	-4696	MG	0.00	0.00	500.00
2953	-4871	-4296	-4220	-4220	MG	0.00	0.00	500.00
2954	-3949	-4712	-4460	-4460	MG	0.00	0.00	500.00
2955	-5353	-4463	-3767	-3767	MG	0.00	0.00	500.00
3034	-4932	-4866	-4865	-4931	MG	0.00	0.00	500.00
3034	-5048	-4995	-4979	-5047	MG	0.00	0.00	500.00
3034	-4994	-4930	-4929	-4978	MG	0.00	0.00	500.00
3034	-4929	-4863	-4862	-4928	MG	0.00	0.00	500.00
3034	-4978	-4929	-4928	-4970	MG	0.00	0.00	500.00
3034	-4995	-4932	-4931	-4979	MG	0.00	0.00	500.00
3034	-5046	-4994	-4978	2902	MG	0.00	0.00	500.00
3034	-5051	-4997	-4980	-5050	MG	0.00	0.00	500.00
3034	2902	-4978	-4970	-5045	MG	0.00	0.00	500.00
3034	-4920	-4867	-4866	-4932	MG	0.00	0.00	500.00
3034	-4996	-4920	-4932	-4995	MG	0.00	0.00	500.00
3034	-4930	-4864	-4863	-4929	MG	0.00	0.00	500.00
3034	-4997	-4934	-4933	-4980	MG	0.00	0.00	500.00
3034	-4931	-4865	-4864	-4930	MG	0.00	0.00	500.00
3034	-4862	-4861	-4927	-4928	MG	0.00	0.00	500.00
3034	-4970	-4993	-5044	-5045	MG	0.00	0.00	500.00
3034	-4934	-4869	-4868	-4933	MG	0.00	0.00	500.00
3034	-5050	-4980	-4996	-5049	MG	0.00	0.00	500.00
3034	-5047	-4979	-4994	-5046	MG	0.00	0.00	500.00
3034	-4928	-4927	-4993	-4970	MG	0.00	0.00	500.00
3034	-4979	-4931	-4930	-4994	MG	0.00	0.00	500.00
3034	-5049	-4996	-4995	-5048	MG	0.00	0.00	500.00
3034	-4933	-4868	-4867	-4920	MG	0.00	0.00	500.00
3034	-4980	-4933	-4920	-4996	MG	0.00	0.00	500.00
3036	-6485	-3606	-3658	-6550	MG	0.00	0.00	500.00
3036	-6550	-3658	-3591	-6622	MG	0.00	0.00	500.00
3036	-6672	-3537	-3699	-6750	MG	0.00	0.00	500.00
3036	-6622	-3591	-3537	-6672	MG	0.00	0.00	500.00
3039	-6438	-3812	-3859	-6505	MG	0.00	0.00	500.00
3039	-6222	-3765	-3812	-6438	MG	0.00	0.00	500.00
3052	-4446	-4020	-5048	-5049	MG	0.00	0.00	500.00
3060	-4252	-3608	-7140	-7140	MG	0.00	0.00	500.00
3061	-5285	-4712	-4460	-4460	MG	0.00	0.00	500.00
3062	-4224	-5066	-4951	-4951	MG	0.00	0.00	500.00
3131	-5671	-5602	-5601	-5670	MG	0.00	0.00	500.00
3131	-5741	-5732	-5797	-5798	MG	0.00	0.00	500.00
3131	-5129	-5051	-5050	-5128	MG	0.00	0.00	500.00
3131	-5325	-5274	-5273	-5324	MG	0.00	0.00	500.00
3131	-5277	-5212	-5211	-5276	MG	0.00	0.00	500.00
3131	-5805	-5744	-5736	-5804	MG	0.00	0.00	500.00
3131	-5735	-5670	-5669	-5734	MG	0.00	0.00	500.00
3131	-5505	-5442	-5441	-5504	MG	0.00	0.00	500.00
3131	-5445	-5383	-5382	-5444	MG	0.00	0.00	500.00
3131	-5744	-5673	-5672	-5736	MG	0.00	0.00	500.00
3131	-5379	-5325	-5324	-5378	MG	0.00	0.00	500.00
3131	-5439	-5438	-5501	-5502	MG	0.00	0.00	500.00
3131	-5508	-5445	-5444	-5507	MG	0.00	0.00	500.00
3131	-5802	-5735	-5734	-5801	MG	0.00	0.00	500.00
3131	-5214	-5129	-5128	-5213	MG	0.00	0.00	500.00
3131	-5803	-5743	-5735	-5802	MG	0.00	0.00	500.00
3131	-5743	-5671	-5670	-5735	MG	0.00	0.00	500.00
3131	-5210	-5125	-5124	-5209	MG	0.00	0.00	500.00
3131	-5128	-5050	-5049	-5127	MG	0.00	0.00	500.00
3131	-5801	-5734	-5742	-5800	MG	0.00	0.00	500.00
3131	-5734	-5669	-5668	-5742	MG	0.00	0.00	500.00
3131	-5207	-5206	-5271	-5272	MG	0.00	0.00	500.00
3131	-5327	-5276	-5275	-5326	MG	0.00	0.00	500.00
3131	-5276	-5211	-5210	-5275	MG	0.00	0.00	500.00
3131	-5045	-5044	-5121	-5122	MG	0.00	0.00	500.00
3131	-5275	-5210	-5209	-5274	MG	0.00	0.00	500.00
3131	-5446	-5384	-5383	-5445	MG	0.00	0.00	500.00
3131	-5125	-5047	-5046	-5124	MG	0.00	0.00	500.00
3131	-5597	-5596	-5665	-5666	MG	0.00	0.00	500.00
3131	-5440	-5378	-5377	-5439	MG	0.00	0.00	500.00
3131	-5274	-5209	-5208	-5273	MG	0.00	0.00	500.00
3131	-5273	-5208	-5207	-5272	MG	0.00	0.00	500.00
3131	-5279	-5214	-5213	-5278	MG	0.00	0.00	500.00
3131	-5670	-5601	-5600	-5669	MG	0.00	0.00	500.00
3131	-5601	-5506	-5505	-5600	MG	0.00	0.00	500.00
3131	-5278	-5213	-5212	-5277	MG	0.00	0.00	500.00

3131	-5213	-5128	-5127	-5212	MG	0.00	0.00	500.00
3131	-5328	-5277	-5276	-5327	MG	0.00	0.00	500.00
3131	-5382	-5328	-5327	-5381	MG	0.00	0.00	500.00
3131	-5377	-5376	-5438	-5439	MG	0.00	0.00	500.00
3131	-5212	-5127	-5126	-5211	MG	0.00	0.00	500.00
3131	-5127	-5049	-5048	-5126	MG	0.00	0.00	500.00
3131	-5443	-5381	-5380	-5442	MG	0.00	0.00	500.00
3131	-5380	-5326	-5325	-5379	MG	0.00	0.00	500.00
3131	-5441	-5379	-5378	-5440	MG	0.00	0.00	500.00
3131	-5666	-5665	-5732	-5741	MG	0.00	0.00	500.00
3131	-5272	-5271	-5322	-5323	MG	0.00	0.00	500.00
3131	-5324	-5273	-5272	-5323	MG	0.00	0.00	500.00
3131	-5507	-5444	-5443	-5506	MG	0.00	0.00	500.00
3131	-5330	-5279	-5278	-5329	MG	0.00	0.00	500.00
3131	-5124	-5046	2902	-5123	MG	0.00	0.00	500.00
3131	-5502	-5501	-5596	-5597	MG	0.00	0.00	500.00
3131	-5383	-5329	-5328	-5382	MG	0.00	0.00	500.00
3131	-5329	-5278	-5277	-5328	MG	0.00	0.00	500.00
3131	-5506	-5443	-5442	-5505	MG	0.00	0.00	500.00
3131	-5669	-5600	-5599	-5668	MG	0.00	0.00	500.00
3131	-5600	-5505	-5504	-5599	MG	0.00	0.00	500.00
3131	-5326	-5275	-5274	-5325	MG	0.00	0.00	500.00
3131	-5599	-5504	-5503	-5598	MG	0.00	0.00	500.00
3131	-5381	-5327	-5326	-5380	MG	0.00	0.00	500.00
3131	-5211	-5126	-5125	-5210	MG	0.00	0.00	500.00
3131	-5673	-5604	-5603	-5672	MG	0.00	0.00	500.00
3131	-5442	-5380	-5379	-5441	MG	0.00	0.00	500.00
3131	-5503	-5440	-5439	-5502	MG	0.00	0.00	500.00
3131	-5509	-5446	-5445	-5508	MG	0.00	0.00	500.00
3131	-5603	-5508	-5507	-5602	MG	0.00	0.00	500.00
3131	-5208	-5123	-5122	-5207	MG	0.00	0.00	500.00
3131	-5602	-5507	-5506	-5601	MG	0.00	0.00	500.00
3131	-5323	-5322	-5376	-5377	MG	0.00	0.00	500.00
3131	-5378	-5324	-5323	-5377	MG	0.00	0.00	500.00
3131	-5742	-5668	-5667	-5733	MG	0.00	0.00	500.00
3131	-5504	-5441	-5440	-5503	MG	0.00	0.00	500.00
3131	-5672	-5603	-5602	-5671	MG	0.00	0.00	500.00
3131	-5209	-5124	-5123	-5208	MG	0.00	0.00	500.00
3131	-5126	-5048	-5047	-5125	MG	0.00	0.00	500.00
3131	-5122	-5121	-5206	-5207	MG	0.00	0.00	500.00
3131	-5668	-5599	-5598	-5667	MG	0.00	0.00	500.00
3131	-5604	-5509	-5508	-5603	MG	0.00	0.00	500.00
3131	-5598	-5503	-5502	-5597	MG	0.00	0.00	500.00
3131	-5733	-5667	-5666	-5741	MG	0.00	0.00	500.00
3131	-5804	-5736	-5743	-5803	MG	0.00	0.00	500.00
3131	-5667	-5598	-5597	-5666	MG	0.00	0.00	500.00
3131	-5736	-5672	-5671	-5743	MG	0.00	0.00	500.00
3131	-5384	-5330	-5329	-5383	MG	0.00	0.00	500.00
3131	-5444	-5382	-5381	-5443	MG	0.00	0.00	500.00
3131	-5800	-5742	-5733	-5799	MG	0.00	0.00	500.00
3131	-5799	-5733	-5741	-5798	MG	0.00	0.00	500.00
3131	-5123	2902	-5045	-5122	MG	0.00	0.00	500.00
3132	-6505	-3859	-3910	-6598	MG	0.00	0.00	500.00
3133	-7139	-3826	-3988	-7202	MG	0.00	0.00	500.00
3133	-7465	-4165	-4105	-7501	MG	0.00	0.00	500.00
3133	-6835	-3843	-3905	-6917	MG	0.00	0.00	500.00
3133	-6917	-3905	-3964	-7000	MG	0.00	0.00	500.00
3133	-7202	-3988	-4125	-7265	MG	0.00	0.00	500.00
3133	-6750	-3699	-3843	-6835	MG	0.00	0.00	500.00
3133	-7059	-3888	-3826	-7139	MG	0.00	0.00	500.00
3133	-7299	-4168	-4222	-7349	MG	0.00	0.00	500.00
3133	-7349	-4222	-4165	-7465	MG	0.00	0.00	500.00
3133	-7000	-3964	-3888	-7059	MG	0.00	0.00	500.00
3133	-7501	-4105	-4254	-7579	MG	0.00	0.00	500.00
3133	-7265	-4125	-4168	-7299	MG	0.00	0.00	500.00
3147	-5050	-4446	-5049	-5049	MG	0.00	0.00	500.00
3150	-4936	-4282	-5443	-5444	MG	0.00	0.00	500.00
3152	-3656	-3697	-6247	-6248	MG	0.00	0.00	500.00
3156	-5773	-4965	-4066	-4066	MG	0.00	0.00	500.00
3157	-3675	-5307	-6230	-6230	MG	0.00	0.00	500.00
3234	-5888	-5846	-5845	-5887	MG	0.00	0.00	500.00
3234	-6070	-5996	-5995	-6069	MG	0.00	0.00	500.00
3234	-6249	-6197	-6196	-6239	MG	0.00	0.00	500.00
3234	-6193	-6194	-6137	-6136	MG	0.00	0.00	500.00
3234	-6250	-6198	-6197	-6249	MG	0.00	0.00	500.00
3234	-6142	-6074	-6073	-6141	MG	0.00	0.00	500.00
3234	-6073	-5999	-5998	-6072	MG	0.00	0.00	500.00
3234	-5891	-5849	-5848	-5890	MG	0.00	0.00	500.00
3234	-6252	-6200	-6199	-6251	MG	0.00	0.00	500.00

3234	-6000	-5892	-5891	-5999	MG	0.00	0.00	500.00
3234	-6199	-6142	-6141	-6198	MG	0.00	0.00	500.00
3234	-6068	-6067	-6135	-6136	MG	0.00	0.00	500.00
3234	-5999	-5891	-5890	-5998	MG	0.00	0.00	500.00
3234	-6248	-6195	-6194	-6247	MG	0.00	0.00	500.00
3234	-6136	-6135	-6192	-6193	MG	0.00	0.00	500.00
3234	-6138	-6070	-6069	-6137	MG	0.00	0.00	500.00
3234	-5798	-5797	-5843	-5844	MG	0.00	0.00	500.00
3234	-5847	-5801	-5800	-5846	MG	0.00	0.00	500.00
3234	-6198	-6141	-6140	-6197	MG	0.00	0.00	500.00
3234	-6068	-6069	-5995	-6025	MG	0.00	0.00	500.00
3234	-6246	-6247	-6194	-6193	MG	0.00	0.00	500.00
3234	-5886	-5887	-5845	-5844	MG	0.00	0.00	500.00
3234	-6074	-6000	-5999	-6073	MG	0.00	0.00	500.00
3234	-5892	-5850	-5849	-5891	MG	0.00	0.00	500.00
3234	-5846	-5800	-5799	-5845	MG	0.00	0.00	500.00
3234	-5848	-5802	-5801	-5847	MG	0.00	0.00	500.00
3234	-6140	-6072	-6071	-6139	MG	0.00	0.00	500.00
3234	-6025	-5995	-5887	-5886	MG	0.00	0.00	500.00
3234	-5890	-5848	-5847	-5889	MG	0.00	0.00	500.00
3234	-5851	-5805	-5804	-5850	MG	0.00	0.00	500.00
3234	-6196	-6139	-6138	-6195	MG	0.00	0.00	500.00
3234	-5996	-5888	-5887	-5995	MG	0.00	0.00	500.00
3234	-5998	-5890	-5889	-5997	MG	0.00	0.00	500.00
3234	-5972	-5893	-5892	-6000	MG	0.00	0.00	500.00
3234	-6075	-5972	-6000	-6074	MG	0.00	0.00	500.00
3234	-5997	-5889	-5888	-5996	MG	0.00	0.00	500.00
3234	-6141	-6073	-6072	-6140	MG	0.00	0.00	500.00
3234	-6239	-6196	-6195	-6248	MG	0.00	0.00	500.00
3234	-5845	-5799	-5798	-5844	MG	0.00	0.00	500.00
3234	-6195	-6138	-6137	-6194	MG	0.00	0.00	500.00
3234	-5886	-5885	-5994	-6025	MG	0.00	0.00	500.00
3234	-6071	-5997	-5996	-6070	MG	0.00	0.00	500.00
3234	-6193	-6192	-6245	-6246	MG	0.00	0.00	500.00
3234	-5889	-5847	-5846	-5888	MG	0.00	0.00	500.00
3234	-6251	-6199	-6198	-6250	MG	0.00	0.00	500.00
3234	-5893	-5851	-5850	-5892	MG	0.00	0.00	500.00
3234	-6200	-6143	-6142	-6199	MG	0.00	0.00	500.00
3234	-5844	-5843	-5885	-5886	MG	0.00	0.00	500.00
3234	-6136	-6137	-6069	-6068	MG	0.00	0.00	500.00
3234	-5849	-5803	-5802	-5848	MG	0.00	0.00	500.00
3234	-6025	-5994	-6067	-6068	MG	0.00	0.00	500.00
3234	-5850	-5804	-5803	-5849	MG	0.00	0.00	500.00
3234	-6139	-6071	-6070	-6138	MG	0.00	0.00	500.00
3234	-6072	-5998	-5997	-6071	MG	0.00	0.00	500.00
3234	-6143	-6075	-6074	-6142	MG	0.00	0.00	500.00
3234	-6197	-6140	-6139	-6196	MG	0.00	0.00	500.00
3235	-7579	-4254	-4379	-7666	MG	0.00	0.00	500.00
3235	-7666	-4379	-4420	-7712	MG	0.00	0.00	500.00
3235	-7976	-4363	-4503	-8030	MG	0.00	0.00	500.00
3235	-7930	-4418	-4363	-7976	MG	0.00	0.00	500.00
3235	-7807	-4462	-4418	-7930	MG	0.00	0.00	500.00
3235	-7712	-4420	-4462	-7807	MG	0.00	0.00	500.00
3255	-5445	-4936	-5444	-5444	MG	0.00	0.00	500.00
3257	-5334	-4700	-5848	-5849	MG	0.00	0.00	500.00
3257	-5850	-5334	-5849	-5849	MG	0.00	0.00	500.00
3259	-3948	-3986	-6673	-6677	MG	0.00	0.00	500.00
3264	-4220	-4252	-7140	-7141	MG	0.00	0.00	500.00
3266	-3608	-3826	-7139	-7140	MG	0.00	0.00	500.00
3267	-4493	-3907	-7502	-7502	MG	0.00	0.00	500.00
3267	-3907	-4105	-7501	-7502	MG	0.00	0.00	500.00
3268	-5681	-5066	-4951	-4951	MG	0.00	0.00	500.00
3269	-5014	-4170	-7977	-7977	MG	0.00	0.00	500.00
3270	-4463	-5459	-5353	-5353	MG	0.00	0.00	500.00
3270	-6101	-5459	-5353	-5353	MG	0.00	0.00	500.00
3271	-4965	-5855	-5773	-5773	MG	0.00	0.00	500.00
3272	-4323	-3675	-6230	-6171	MG	0.00	0.00	500.00
3272	-6171	-5357	-4323	-4323	MG	0.00	0.00	500.00
3274	-4759	-3969	-6660	-6579	MG	0.00	0.00	500.00
3274	-6579	-5766	-4759	-4759	MG	0.00	0.00	500.00
3274	-3969	-5692	-6660	-6660	MG	0.00	0.00	500.00
3333	-6304	-6303	-6371	-6372	MG	0.00	0.00	500.00
3333	-6917	-6916	-6999	-7000	MG	0.00	0.00	500.00
3333	-6378	-6310	-6309	-6377	MG	0.00	0.00	500.00
3333	-7061	-7002	-7001	-7060	MG	0.00	0.00	500.00
3333	-7141	-7061	-7060	-7140	MG	0.00	0.00	500.00
3333	-6374	-6306	-6305	-6373	MG	0.00	0.00	500.00
3333	-6624	-6539	-6551	-6623	MG	0.00	0.00	500.00
3333	-7140	-7060	-7059	-7139	MG	0.00	0.00	500.00

3333	-6379	-6311	-6310	-6378	MG	0.00	0.00	500.00
3333	-6842	-6757	-6756	-6841	MG	0.00	0.00	500.00
3333	-7062	-7003	-7002	-7061	MG	0.00	0.00	500.00
3333	-7003	-6920	-6919	-7002	MG	0.00	0.00	500.00
3333	-6485	-6484	-6549	-6550	MG	0.00	0.00	500.00
3333	-7000	-6999	-7058	-7059	MG	0.00	0.00	500.00
3333	-6492	-6379	-6378	-6491	MG	0.00	0.00	500.00
3333	-6308	-6249	-6239	-6307	MG	0.00	0.00	500.00
3333	-6678	-6625	-6624	-6677	MG	0.00	0.00	500.00
3333	-6625	-6552	-6539	-6624	MG	0.00	0.00	500.00
3333	-6677	-6624	-6623	-6673	MG	0.00	0.00	500.00
3333	-7146	-7066	-7065	-7145	MG	0.00	0.00	500.00
3333	-6306	-6248	-6247	-6305	MG	0.00	0.00	500.00
3333	-6487	-6374	-6373	-6486	MG	0.00	0.00	500.00
3333	-6629	-6556	-6555	-6628	MG	0.00	0.00	500.00
3333	-7143	-7063	-7062	-7142	MG	0.00	0.00	500.00
3333	-6901	-6842	-6841	-6923	MG	0.00	0.00	500.00
3333	-6754	-6690	-6678	-6753	MG	0.00	0.00	500.00
3333	-6375	-6307	-6306	-6374	MG	0.00	0.00	500.00
3333	-6246	-6245	-6303	-6304	MG	0.00	0.00	500.00
3333	-6377	-6309	-6308	-6376	MG	0.00	0.00	500.00
3333	-6835	-6834	-6916	-6917	MG	0.00	0.00	500.00
3333	-7007	-6901	-6923	-7006	MG	0.00	0.00	500.00
3333	-6757	-6693	-6692	-6756	MG	0.00	0.00	500.00
3333	-6307	-6239	-6248	-6306	MG	0.00	0.00	500.00
3333	-6751	-6673	-6672	-6750	MG	0.00	0.00	500.00
3333	-7059	-7058	-7138	-7139	MG	0.00	0.00	500.00
3333	-6922	-6840	-6839	-6921	MG	0.00	0.00	500.00
3333	-6556	-6492	-6491	-6555	MG	0.00	0.00	500.00
3333	-6840	-6755	-6754	-6839	MG	0.00	0.00	500.00
3333	-6311	-6252	-6251	-6310	MG	0.00	0.00	500.00
3333	-6921	-6839	-6838	-6920	MG	0.00	0.00	500.00
3333	-6839	-6754	-6753	-6838	MG	0.00	0.00	500.00
3333	-6491	-6378	-6377	-6490	MG	0.00	0.00	500.00
3333	-7142	-7062	-7061	-7141	MG	0.00	0.00	500.00
3333	-6310	-6251	-6250	-6309	MG	0.00	0.00	500.00
3333	-6490	-6377	-6376	-6489	MG	0.00	0.00	500.00
3333	-6753	-6678	-6677	-6752	MG	0.00	0.00	500.00
3333	-6673	-6623	-6622	-6672	MG	0.00	0.00	500.00
3333	-6752	-6677	-6673	-6751	MG	0.00	0.00	500.00
3333	-7001	-6918	-6917	-7000	MG	0.00	0.00	500.00
3333	-6376	-6308	-6307	-6375	MG	0.00	0.00	500.00
3333	-6372	-6371	-6484	-6485	MG	0.00	0.00	500.00
3333	-6550	-6549	-6621	-6622	MG	0.00	0.00	500.00
3333	-6552	-6488	-6487	-6539	MG	0.00	0.00	500.00
3333	-6488	-6375	-6374	-6487	MG	0.00	0.00	500.00
3333	-7145	-7065	-7064	-7144	MG	0.00	0.00	500.00
3333	-6539	-6487	-6486	-6551	MG	0.00	0.00	500.00
3333	-6623	-6551	-6550	-6622	MG	0.00	0.00	500.00
3333	-6551	-6486	-6485	-6550	MG	0.00	0.00	500.00
3333	-6373	-6305	-6304	-6372	MG	0.00	0.00	500.00
3333	-6622	-6621	-6671	-6672	MG	0.00	0.00	500.00
3333	-6838	-6753	-6752	-6837	MG	0.00	0.00	500.00
3333	-6627	-6554	-6553	-6626	MG	0.00	0.00	500.00
3333	-6690	-6626	-6625	-6678	MG	0.00	0.00	500.00
3333	-6626	-6553	-6552	-6625	MG	0.00	0.00	500.00
3333	-6672	-6671	-6749	-6750	MG	0.00	0.00	500.00
3333	-7066	-7007	-7006	-7065	MG	0.00	0.00	500.00
3333	-6489	-6376	-6375	-6488	MG	0.00	0.00	500.00
3333	-7065	-7006	-7005	-7064	MG	0.00	0.00	500.00
3333	-6923	-6841	-6840	-6922	MG	0.00	0.00	500.00
3333	-7144	-7064	-7063	-7143	MG	0.00	0.00	500.00
3333	-6756	-6692	-6691	-6755	MG	0.00	0.00	500.00
3333	-6841	-6756	-6755	-6840	MG	0.00	0.00	500.00
3333	-7005	-6922	-6921	-7004	MG	0.00	0.00	500.00
3333	-6755	-6691	-6690	-6754	MG	0.00	0.00	500.00
3333	-7063	-7004	-7003	-7062	MG	0.00	0.00	500.00
3333	-6692	-6628	-6627	-6691	MG	0.00	0.00	500.00
3333	-6628	-6555	-6554	-6627	MG	0.00	0.00	500.00
3333	-6555	-6491	-6490	-6554	MG	0.00	0.00	500.00
3333	-6750	-6749	-6834	-6835	MG	0.00	0.00	500.00
3333	-6693	-6629	-6628	-6692	MG	0.00	0.00	500.00
3333	-6554	-6490	-6489	-6553	MG	0.00	0.00	500.00
3333	-6691	-6627	-6626	-6690	MG	0.00	0.00	500.00
3333	-6836	-6751	-6750	-6835	MG	0.00	0.00	500.00
3333	-6919	-6837	-6836	-6918	MG	0.00	0.00	500.00
3333	-7060	-7001	-7000	-7059	MG	0.00	0.00	500.00
3333	-6305	-6247	-6246	-6304	MG	0.00	0.00	500.00
3333	-6918	-6836	-6835	-6917	MG	0.00	0.00	500.00

3333	-7002	-6919	-6918	-7001	MG	0.00	0.00	500.00
3333	-7006	-6923	-6922	-7005	MG	0.00	0.00	500.00
3333	-6920	-6838	-6837	-6919	MG	0.00	0.00	500.00
3333	-6553	-6489	-6488	-6552	MG	0.00	0.00	500.00
3333	-7004	-6921	-6920	-7003	MG	0.00	0.00	500.00
3333	-6486	-6373	-6372	-6485	MG	0.00	0.00	500.00
3333	-6837	-6752	-6751	-6836	MG	0.00	0.00	500.00
3333	-6309	-6250	-6249	-6308	MG	0.00	0.00	500.00
3333	-7064	-7005	-7004	-7063	MG	0.00	0.00	500.00
3334	-8230	-4887	-4953	-8318	MG	0.00	0.00	500.00
3334	-8481	-5002	-5255	-8539	MG	0.00	0.00	500.00
3334	-8318	-4953	-4885	-8379	MG	0.00	0.00	500.00
3334	-8030	-4503	-4842	-8156	MG	0.00	0.00	500.00
3334	-8721	-5355	-5287	-8841	MG	0.00	0.00	500.00
3334	-8156	-4842	-4887	-8230	MG	0.00	0.00	500.00
3334	-8379	-4885	-4816	-8426	MG	0.00	0.00	500.00
3334	-8426	-4816	-5002	-8481	MG	0.00	0.00	500.00
3334	-8841	-5287	-5216	-8910	MG	0.00	0.00	500.00
3334	-8629	-5305	-5355	-8721	MG	0.00	0.00	500.00
3334	-8910	-5216	-5398	-8984	MG	0.00	0.00	500.00
3334	-8539	-5255	-5305	-8629	MG	0.00	0.00	500.00
3364	-5747	-5053	-6249	-6250	MG	0.00	0.00	500.00
3364	-6251	-5747	-6250	-6250	MG	0.00	0.00	500.00
3372	-6152	-5448	-6690	-6691	MG	0.00	0.00	500.00
3380	-4460	-4493	-7502	-7503	MG	0.00	0.00	500.00
3384	-4170	-4363	-7976	-7977	MG	0.00	0.00	500.00
3386	-5397	-4422	-8427	-8427	MG	0.00	0.00	500.00
3388	-6494	-5855	-5773	-5773	MG	0.00	0.00	500.00
3390	-5357	-6269	-6171	-6171	MG	0.00	0.00	500.00
3437	-10199	-10133	-10132	-10198	MG	0.00	0.00	500.00
3437	-10257	-10201	-10200	-10256	MG	0.00	0.00	500.00
3437	-8427	-8380	-8379	-8426	MG	0.00	0.00	500.00
3437	-10038	-9946	-9962	-10037	MG	0.00	0.00	500.00
3437	-7502	-7466	-7465	-7501	MG	0.00	0.00	500.00
3437	-10129	-10037	-10036	-10128	MG	0.00	0.00	500.00
3437	-8911	-8808	-8841	-8910	MG	0.00	0.00	500.00
3437	-10255	-10199	-10198	-10254	MG	0.00	0.00	500.00
3437	-10041	-9972	-9971	-10040	MG	0.00	0.00	500.00
3437	-10036	-10035	-10127	-10128	MG	0.00	0.00	500.00
3437	-9446	-9380	-9379	-9445	MG	0.00	0.00	500.00
3437	-10198	-10132	-10131	-10177	MG	0.00	0.00	500.00
3437	-7666	-7662	-7711	-7712	MG	0.00	0.00	500.00
3437	-10133	-10041	-10040	-10132	MG	0.00	0.00	500.00
3437	3302	-10176	-10196	-10251	MG	0.00	0.00	500.00
3437	-9972	-9849	-9848	-9971	MG	0.00	0.00	500.00
3437	-8984	-8983	-9095	-9074	MG	0.00	0.00	500.00
3437	-10132	-10040	-10039	-10131	MG	0.00	0.00	500.00
3437	-7269	-7206	-7205	-7268	MG	0.00	0.00	500.00
3437	-9557	-9505	-9493	-9556	MG	0.00	0.00	500.00
3437	-8230	-8229	-8317	-8318	MG	0.00	0.00	500.00
3437	-9447	-9381	-9380	-9446	MG	0.00	0.00	500.00
3437	-7349	-7348	-7464	-7465	MG	0.00	0.00	500.00
3437	-9493	-9446	-9445	-9488	MG	0.00	0.00	500.00
3437	-9600	-9599	-9641	-9642	MG	0.00	0.00	500.00
3437	-9962	-9857	-9847	-9970	MG	0.00	0.00	500.00
3437	-9857	-9741	-9740	-9847	MG	0.00	0.00	500.00
3437	-9974	-9863	-9840	-9973	MG	0.00	0.00	500.00
3437	-9445	-9379	-9378	-9444	MG	0.00	0.00	500.00
3437	-9742	-9644	-9643	-9741	MG	0.00	0.00	500.00
3437	-9644	-9602	-9601	-9643	MG	0.00	0.00	500.00
3437	-7468	-7352	-7351	-7467	MG	0.00	0.00	500.00
3437	-7265	-7264	-7298	-7299	MG	0.00	0.00	500.00
3437	-9444	-9378	-9377	-9443	MG	0.00	0.00	500.00
3437	-7501	-7500	-7572	-7579	MG	0.00	0.00	500.00
3437	-9648	-9606	-9605	-9647	MG	0.00	0.00	500.00
3437	-7472	-7356	-7355	-7471	MG	0.00	0.00	500.00
3437	-8917	-8809	-8827	-8916	MG	0.00	0.00	500.00
3437	-8433	-8386	-8385	-8432	MG	0.00	0.00	500.00
3437	-10134	-10042	-10041	-10133	MG	0.00	0.00	500.00
3437	-9747	-9649	-9648	-9746	MG	0.00	0.00	500.00
3437	-9744	-9646	-9645	-9743	MG	0.00	0.00	500.00
3437	-9646	-9604	-9603	-9645	MG	0.00	0.00	500.00
3437	-9604	-9556	-9555	-9603	MG	0.00	0.00	500.00
3437	-9740	-9728	-9856	-9847	MG	0.00	0.00	500.00
3437	-9743	-9645	-9644	-9742	MG	0.00	0.00	500.00
3437	-9645	-9603	-9602	-9644	MG	0.00	0.00	500.00
3437	-7505	-7469	-7468	-7504	MG	0.00	0.00	500.00
3437	-9555	-9488	-9504	-9554	MG	0.00	0.00	500.00
3437	-8426	-8425	-8480	-8481	MG	0.00	0.00	500.00

3437	-8539	-8538	-8621	-8629	MG	0.00	0.00	500.00
3437	-7813	-7723	-7722	-7812	MG	0.00	0.00	500.00
3437	-7723	-7671	-7670	-7722	MG	0.00	0.00	500.00
3437	-10196	-10195	-10250	-10251	MG	0.00	0.00	500.00
3437	-8910	-8909	-8983	-8984	MG	0.00	0.00	500.00
3437	-9074	-9095	-9150	-9151	MG	0.00	0.00	500.00
3437	-7812	-7722	-7716	-7811	MG	0.00	0.00	500.00
3437	-7722	-7670	-7669	-7716	MG	0.00	0.00	500.00
3437	-9377	-9286	-9285	-9376	MG	0.00	0.00	500.00
3437	-10254	-10198	-10177	-10253	MG	0.00	0.00	500.00
3437	-9847	-9856	-9969	-9970	MG	0.00	0.00	500.00
3437	-10040	-9971	-9963	-10039	MG	0.00	0.00	500.00
3437	-7807	-7806	-7929	-7930	MG	0.00	0.00	500.00
3437	-9506	-9448	-9447	-9505	MG	0.00	0.00	500.00
3437	-7715	-7668	-7643	-7721	MG	0.00	0.00	500.00
3437	-7668	-7583	-7582	-7643	MG	0.00	0.00	500.00
3437	-7583	-7505	-7504	-7582	MG	0.00	0.00	500.00
3437	-10197	-10130	-10129	-10176	MG	0.00	0.00	500.00
3437	-10130	-10038	-10037	-10129	MG	0.00	0.00	500.00
3437	-10200	-10134	-10133	-10199	MG	0.00	0.00	500.00
3437	-7643	-7582	-7581	-7667	MG	0.00	0.00	500.00
3437	-10176	-10129	-10128	-10196	MG	0.00	0.00	500.00
3437	-10256	-10200	-10199	-10255	MG	0.00	0.00	500.00
3437	-10037	-9962	-9970	-10036	MG	0.00	0.00	500.00
3437	-7299	-7298	-7348	-7349	MG	0.00	0.00	500.00
3437	-7714	-7667	-7663	-7713	MG	0.00	0.00	500.00
3437	-9863	-9747	-9746	-9840	MG	0.00	0.00	500.00
3437	-7581	-7503	-7502	-7580	MG	0.00	0.00	500.00
3437	-7931	-7808	-7807	-7930	MG	0.00	0.00	500.00
3437	-7808	-7713	-7712	-7807	MG	0.00	0.00	500.00
3437	-7663	-7580	-7579	-7666	MG	0.00	0.00	500.00
3437	-9554	-9504	-9487	-9553	MG	0.00	0.00	500.00
3437	-9504	-9444	-9443	-9487	MG	0.00	0.00	500.00
3437	-9643	-9601	-9600	-9642	MG	0.00	0.00	500.00
3437	-9849	-9745	-9744	-9848	MG	0.00	0.00	500.00
3437	-9487	-9443	-9442	-9486	MG	0.00	0.00	500.00
3437	-7935	-7811	-7810	-7934	MG	0.00	0.00	500.00
3437	-9383	-9292	-9291	-9382	MG	0.00	0.00	500.00
3437	-9209	-9208	-9284	-9285	MG	0.00	0.00	500.00
3437	-8721	-8720	-8825	-8841	MG	0.00	0.00	500.00
3437	-7671	-7586	-7585	-7670	MG	0.00	0.00	500.00
3437	-7139	-7138	-7201	-7202	MG	0.00	0.00	500.00
3437	-7930	-7929	-7975	-7976	MG	0.00	0.00	500.00
3437	-7712	-7711	-7806	-7807	MG	0.00	0.00	500.00
3437	-10042	-9973	-9972	-10041	MG	0.00	0.00	500.00
3437	-7356	-7306	-7305	-7355	MG	0.00	0.00	500.00
3437	-7306	-7272	-7271	-7305	MG	0.00	0.00	500.00
3437	-7272	-7209	-7208	-7271	MG	0.00	0.00	500.00
3437	-9741	-9643	-9642	-9740	MG	0.00	0.00	500.00
3437	-10043	-9974	-9973	-10042	MG	0.00	0.00	500.00
3437	-10135	-10043	-10042	-10134	MG	0.00	0.00	500.00
3437	-10201	-10135	-10134	-10200	MG	0.00	0.00	500.00
3437	-7305	-7271	-7270	-7304	MG	0.00	0.00	500.00
3437	-7271	-7208	-7207	-7270	MG	0.00	0.00	500.00
3437	-7208	-7145	-7144	-7207	MG	0.00	0.00	500.00
3437	-9556	-9493	-9488	-9555	MG	0.00	0.00	500.00
3437	-7470	-7354	-7353	-7469	MG	0.00	0.00	500.00
3437	-9970	-9969	-10035	-10036	MG	0.00	0.00	500.00
3437	-10128	-10127	-10195	-10196	MG	0.00	0.00	500.00
3437	-9603	-9555	-9554	-9602	MG	0.00	0.00	500.00
3437	-9488	-9445	-9444	-9504	MG	0.00	0.00	500.00
3437	-7303	-7269	-7268	-7302	MG	0.00	0.00	500.00
3437	-9602	-9554	-9553	-9601	MG	0.00	0.00	500.00
3437	-7504	-7468	-7467	-7503	MG	0.00	0.00	500.00
3437	-8809	-8728	-8727	-8827	MG	0.00	0.00	500.00
3437	-8728	-8635	-8634	-8727	MG	0.00	0.00	500.00
3437	-9601	-9553	-9552	-9600	MG	0.00	0.00	500.00
3437	-9553	-9487	-9486	-9552	MG	0.00	0.00	500.00
3437	-9443	-9377	-9376	-9442	MG	0.00	0.00	500.00
3437	-7467	-7351	-7350	-7466	MG	0.00	0.00	500.00
3437	-7351	-7301	-7300	-7350	MG	0.00	0.00	500.00
3437	-7301	-7267	-7266	-7300	MG	0.00	0.00	500.00
3437	-7267	-7204	-7203	-7266	MG	0.00	0.00	500.00
3437	-8485	-8432	-8431	-8484	MG	0.00	0.00	500.00
3437	-8915	-8826	-8843	-8914	MG	0.00	0.00	500.00
3437	-7508	-7472	-7471	-7507	MG	0.00	0.00	500.00
3437	-7983	-7937	-7936	-7982	MG	0.00	0.00	500.00
3437	-8379	-8378	-8425	-8426	MG	0.00	0.00	500.00
3437	-7465	-7464	-7500	-7501	MG	0.00	0.00	500.00

3437	-7580	-7502	-7501	-7579	MG	0.00	0.00	500.00
3437	-8030	-8029	-8155	-8156	MG	0.00	0.00	500.00
3437	-7302	-7268	-7267	-7301	MG	0.00	0.00	500.00
3437	-7503	-7467	-7466	-7502	MG	0.00	0.00	500.00
3437	-8841	-8825	-8909	-8910	MG	0.00	0.00	500.00
3437	-8237	-8163	-8162	-8236	MG	0.00	0.00	500.00
3437	-7977	-7931	-7930	-7976	MG	0.00	0.00	500.00
3437	-8037	-7983	-7982	-8036	MG	0.00	0.00	500.00
3437	-8432	-8385	-8384	-8431	MG	0.00	0.00	500.00
3437	-8236	-8162	-8161	-8235	MG	0.00	0.00	500.00
3437	-8431	-8384	-8383	-8430	MG	0.00	0.00	500.00
3437	-8384	-8323	-8322	-8383	MG	0.00	0.00	500.00
3437	-8323	-8235	-8234	-8322	MG	0.00	0.00	500.00
3437	-8235	-8161	-8160	-8234	MG	0.00	0.00	500.00
3437	-8161	-8035	-8034	-8160	MG	0.00	0.00	500.00
3437	-7202	-7201	-7264	-7265	MG	0.00	0.00	500.00
3437	-9649	-9607	-9606	-9648	MG	0.00	0.00	500.00
3437	-9607	-9559	-9558	-9606	MG	0.00	0.00	500.00
3437	-9559	-9507	-9506	-9558	MG	0.00	0.00	500.00
3437	-9507	-9449	-9448	-9506	MG	0.00	0.00	500.00
3437	-9449	-9383	-9382	-9448	MG	0.00	0.00	500.00
3437	-9746	-9648	-9647	-9745	MG	0.00	0.00	500.00
3437	-9376	-9375	-9441	-9442	MG	0.00	0.00	500.00
3437	-9606	-9558	-9557	-9605	MG	0.00	0.00	500.00
3437	-9558	-9506	-9505	-9557	MG	0.00	0.00	500.00
3437	-9486	-9485	-9551	-9552	MG	0.00	0.00	500.00
3437	-9448	-9382	-9381	-9447	MG	0.00	0.00	500.00
3437	-9745	-9647	-9646	-9744	MG	0.00	0.00	500.00
3437	-9647	-9605	-9604	-9646	MG	0.00	0.00	500.00
3437	-9605	-9557	-9556	-9604	MG	0.00	0.00	500.00
3437	-9505	-9447	-9446	-9493	MG	0.00	0.00	500.00
3437	-7976	-7975	-8029	-8030	MG	0.00	0.00	500.00
3437	-8156	-8155	-8229	-8230	MG	0.00	0.00	500.00
3437	-8318	-8317	-8378	-8379	MG	0.00	0.00	500.00
3437	-8545	-8485	-8484	-8544	MG	0.00	0.00	500.00
3437	-7579	-7572	-7662	-7666	MG	0.00	0.00	500.00
3437	-7937	-7813	-7812	-7936	MG	0.00	0.00	500.00
3437	-7586	-7508	-7507	-7585	MG	0.00	0.00	500.00
3437	-7982	-7936	-7935	-7981	MG	0.00	0.00	500.00
3437	-7936	-7812	-7811	-7935	MG	0.00	0.00	500.00
3437	-7670	-7585	-7584	-7669	MG	0.00	0.00	500.00
3437	-7585	-7507	-7506	-7584	MG	0.00	0.00	500.00
3437	-7981	-7935	-7934	-7980	MG	0.00	0.00	500.00
3437	-7811	-7716	-7715	-7810	MG	0.00	0.00	500.00
3437	-7716	-7669	-7668	-7715	MG	0.00	0.00	500.00
3437	-7669	-7584	-7583	-7668	MG	0.00	0.00	500.00
3437	-7584	-7506	-7505	-7583	MG	0.00	0.00	500.00
3437	-7980	-7934	-7933	-7979	MG	0.00	0.00	500.00
3437	-7934	-7810	-7809	-7933	MG	0.00	0.00	500.00
3437	-7810	-7715	-7721	-7809	MG	0.00	0.00	500.00
3437	-9642	-9641	-9728	-9740	MG	0.00	0.00	500.00
3437	-9552	-9551	-9599	-9600	MG	0.00	0.00	500.00
3437	-7979	-7933	-7932	-7978	MG	0.00	0.00	500.00
3437	-7933	-7809	-7781	-7932	MG	0.00	0.00	500.00
3437	-7809	-7721	-7714	-7781	MG	0.00	0.00	500.00
3437	-7721	-7643	-7667	-7714	MG	0.00	0.00	500.00
3437	-9100	-8991	-8990	-9099	MG	0.00	0.00	500.00
3437	-7582	-7504	-7503	-7581	MG	0.00	0.00	500.00
3437	-7978	-7932	-7931	-7977	MG	0.00	0.00	500.00
3437	-7932	-7781	-7808	-7931	MG	0.00	0.00	500.00
3437	-7781	-7714	-7713	-7808	MG	0.00	0.00	500.00
3437	-9157	-9099	-9098	-9156	MG	0.00	0.00	500.00
3437	-7667	-7581	-7580	-7663	MG	0.00	0.00	500.00
3437	-8990	-8916	-8915	-8989	MG	0.00	0.00	500.00
3437	-9381	-9290	-9289	-9380	MG	0.00	0.00	500.00
3437	-9290	-9214	-9213	-9289	MG	0.00	0.00	500.00
3437	-7713	-7663	-7666	-7712	MG	0.00	0.00	500.00
3437	-9156	-9098	-9097	-9155	MG	0.00	0.00	500.00
3437	-9098	-8989	-8988	-9097	MG	0.00	0.00	500.00
3437	-9380	-9289	-9288	-9379	MG	0.00	0.00	500.00
3437	-9213	-9155	-9154	-9212	MG	0.00	0.00	500.00
3437	-9155	-9097	-9096	-9154	MG	0.00	0.00	500.00
3437	-9076	-8986	-8985	-9075	MG	0.00	0.00	500.00
3437	-8986	-8912	-8911	-8985	MG	0.00	0.00	500.00
3437	-9075	-8985	-8984	-9074	MG	0.00	0.00	500.00
3437	-8985	-8911	-8910	-8984	MG	0.00	0.00	500.00
3437	-8033	-7979	-7978	-8032	MG	0.00	0.00	500.00
3437	-7209	-7146	-7145	-7208	MG	0.00	0.00	500.00
3437	-7507	-7471	-7470	-7506	MG	0.00	0.00	500.00

3437	-7471	-7355	-7354	-7470	MG	0.00	0.00	500.00
3437	-7355	-7305	-7304	-7354	MG	0.00	0.00	500.00
3437	-7506	-7470	-7469	-7505	MG	0.00	0.00	500.00
3437	-7354	-7304	-7303	-7353	MG	0.00	0.00	500.00
3437	-7304	-7270	-7269	-7303	MG	0.00	0.00	500.00
3437	-7270	-7207	-7206	-7269	MG	0.00	0.00	500.00
3437	-7207	-7144	-7143	-7206	MG	0.00	0.00	500.00
3437	-7469	-7353	-7352	-7468	MG	0.00	0.00	500.00
3437	-7353	-7303	-7302	-7352	MG	0.00	0.00	500.00
3437	-9285	-9284	-9375	-9376	MG	0.00	0.00	500.00
3437	-9214	-9156	-9155	-9213	MG	0.00	0.00	500.00
3437	-7206	-7143	-7142	-7205	MG	0.00	0.00	500.00
3437	-7352	-7302	-7301	-7351	MG	0.00	0.00	500.00
3437	-8635	-8546	-8545	-8634	MG	0.00	0.00	500.00
3437	-7268	-7205	-7204	-7267	MG	0.00	0.00	500.00
3437	-7205	-7142	-7141	-7204	MG	0.00	0.00	500.00
3437	-8916	-8827	-8826	-8915	MG	0.00	0.00	500.00
3437	-8827	-8727	-8726	-8826	MG	0.00	0.00	500.00
3437	-8727	-8634	-8633	-8726	MG	0.00	0.00	500.00
3437	-8634	-8545	-8544	-8633	MG	0.00	0.00	500.00
3437	-7204	-7141	-7140	-7203	MG	0.00	0.00	500.00
3437	-7466	-7350	-7349	-7465	MG	0.00	0.00	500.00
3437	-7350	-7300	-7299	-7349	MG	0.00	0.00	500.00
3437	-7300	-7266	-7265	-7299	MG	0.00	0.00	500.00
3437	-7266	-7203	-7202	-7265	MG	0.00	0.00	500.00
3437	-7203	-7140	-7139	-7202	MG	0.00	0.00	500.00
3437	-8484	-8431	-8430	-8483	MG	0.00	0.00	500.00
3437	-8543	-8483	-8474	-8542	MG	0.00	0.00	500.00
3437	-8483	-8430	-8429	-8474	MG	0.00	0.00	500.00
3437	-8724	-8631	-8630	-8723	MG	0.00	0.00	500.00
3437	-8631	-8542	-8541	-8630	MG	0.00	0.00	500.00
3437	-8474	-8429	-8428	-8473	MG	0.00	0.00	500.00
3437	-8912	-8787	-8808	-8911	MG	0.00	0.00	500.00
3437	-8787	-8723	-8722	-8808	MG	0.00	0.00	500.00
3437	-9973	-9840	-9849	-9972	MG	0.00	0.00	500.00
3437	-9840	-9746	-9745	-9849	MG	0.00	0.00	500.00
3437	-8541	-8473	-8482	-8540	MG	0.00	0.00	500.00
3437	-8473	-8428	-8427	-8482	MG	0.00	0.00	500.00
3437	-8808	-8722	-8721	-8841	MG	0.00	0.00	500.00
3437	-8722	-8622	-8629	-8721	MG	0.00	0.00	500.00
3437	-8622	-8540	-8539	-8629	MG	0.00	0.00	500.00
3437	-8540	-8482	-8481	-8539	MG	0.00	0.00	500.00
3437	-8482	-8427	-8426	-8481	MG	0.00	0.00	500.00
3437	-9971	-9848	-9862	-9963	MG	0.00	0.00	500.00
3437	-9848	-9744	-9743	-9862	MG	0.00	0.00	500.00
3437	-10253	-10177	-10197	-10252	MG	0.00	0.00	500.00
3437	-10177	-10131	-10130	-10197	MG	0.00	0.00	500.00
3437	-10131	-10039	-10038	-10130	MG	0.00	0.00	500.00
3437	-10039	-9963	-9946	-10038	MG	0.00	0.00	500.00
3437	-9963	-9862	-9858	-9946	MG	0.00	0.00	500.00
3437	-9862	-9743	-9742	-9858	MG	0.00	0.00	500.00
3437	-10252	-10197	-10176	3302	MG	0.00	0.00	500.00
3437	-9946	-9858	-9857	-9962	MG	0.00	0.00	500.00
3437	-9858	-9742	-9741	-9857	MG	0.00	0.00	500.00
3437	-9215	-9157	-9156	-9214	MG	0.00	0.00	500.00
3437	-8234	-8160	-8159	-8233	MG	0.00	0.00	500.00
3437	-8160	-8034	-8033	-8159	MG	0.00	0.00	500.00
3437	-9379	-9288	-9287	-9378	MG	0.00	0.00	500.00
3437	-8629	-8621	-8720	-8721	MG	0.00	0.00	500.00
3437	-9288	-9212	-9211	-9287	MG	0.00	0.00	500.00
3437	-8386	-8325	-8324	-8385	MG	0.00	0.00	500.00
3437	-8325	-8237	-8236	-8324	MG	0.00	0.00	500.00
3437	-9287	-9211	-9210	-9286	MG	0.00	0.00	500.00
3437	-9211	-9153	-9152	-9210	MG	0.00	0.00	500.00
3437	-8385	-8324	-8323	-8384	MG	0.00	0.00	500.00
3437	-8324	-8236	-8235	-8323	MG	0.00	0.00	500.00
3437	-8914	-8843	-8842	-8913	MG	0.00	0.00	500.00
3437	-8162	-8036	-8035	-8161	MG	0.00	0.00	500.00
3437	-8036	-7982	-7981	-8035	MG	0.00	0.00	500.00
3437	-9152	-9075	-9074	-9151	MG	0.00	0.00	500.00
3437	-9442	-9441	-9485	-9486	MG	0.00	0.00	500.00
3437	-8035	-7981	-7980	-8034	MG	0.00	0.00	500.00
3437	-8430	-8383	-8382	-8429	MG	0.00	0.00	500.00
3437	-8383	-8322	-8321	-8382	MG	0.00	0.00	500.00
3437	-8322	-8234	-8233	-8321	MG	0.00	0.00	500.00
3437	-8034	-7980	-7979	-8033	MG	0.00	0.00	500.00
3437	-8429	-8382	-8381	-8428	MG	0.00	0.00	500.00
3437	-8382	-8321	-8320	-8381	MG	0.00	0.00	500.00
3437	-8321	-8233	-8232	-8320	MG	0.00	0.00	500.00

3437	-8233	-8159	-8158	-8232	MG	0.00	0.00	500.00
3437	-8159	-8033	-8032	-8158	MG	0.00	0.00	500.00
3437	-9289	-9213	-9212	-9288	MG	0.00	0.00	500.00
3437	-8428	-8381	-8380	-8427	MG	0.00	0.00	500.00
3437	-8381	-8320	-8319	-8380	MG	0.00	0.00	500.00
3437	-8320	-8232	-8231	-8319	MG	0.00	0.00	500.00
3437	-8232	-8158	-8157	-8231	MG	0.00	0.00	500.00
3437	-8158	-8032	-8031	-8157	MG	0.00	0.00	500.00
3437	-8032	-7978	-7977	-8031	MG	0.00	0.00	500.00
3437	-8380	-8319	-8318	-8379	MG	0.00	0.00	500.00
3437	-8319	-8231	-8230	-8318	MG	0.00	0.00	500.00
3437	-8231	-8157	-8156	-8230	MG	0.00	0.00	500.00
3437	-8157	-8031	-8030	-8156	MG	0.00	0.00	500.00
3437	-8031	-7977	-7976	-8030	MG	0.00	0.00	500.00
3437	-8481	-8480	-8538	-8539	MG	0.00	0.00	500.00
3437	-8991	-8917	-8916	-8990	MG	0.00	0.00	500.00
3437	-9382	-9291	-9290	-9381	MG	0.00	0.00	500.00
3437	-9099	-8990	-8989	-9098	MG	0.00	0.00	500.00
3437	-8826	-8726	-8725	-8843	MG	0.00	0.00	500.00
3437	-8726	-8633	-8632	-8725	MG	0.00	0.00	500.00
3437	-8723	-8630	-8622	-8722	MG	0.00	0.00	500.00
3437	-9151	-9150	-9208	-9209	MG	0.00	0.00	500.00
3437	-8989	-8915	-8914	-8988	MG	0.00	0.00	500.00
3437	-8546	-8486	-8485	-8545	MG	0.00	0.00	500.00
3437	-8486	-8433	-8432	-8485	MG	0.00	0.00	500.00
3437	-9097	-8988	-8987	-9096	MG	0.00	0.00	500.00
3437	-8988	-8914	-8913	-8987	MG	0.00	0.00	500.00
3437	-9212	-9154	-9153	-9211	MG	0.00	0.00	500.00
3437	-9154	-9096	-9076	-9153	MG	0.00	0.00	500.00
3437	-9096	-8987	-8986	-9076	MG	0.00	0.00	500.00
3437	-8633	-8544	-8543	-8632	MG	0.00	0.00	500.00
3437	-8544	-8484	-8483	-8543	MG	0.00	0.00	500.00
3437	-9153	-9076	-9075	-9152	MG	0.00	0.00	500.00
3437	-8632	-8543	-8542	-8631	MG	0.00	0.00	500.00
3437	-8725	-8632	-8631	-8724	MG	0.00	0.00	500.00
3437	-8913	-8842	-8841	-8912	MG	0.00	0.00	500.00
3437	-8842	-8724	-8723	-8787	MG	0.00	0.00	500.00
3437	-8542	-8474	-8473	-8541	MG	0.00	0.00	500.00
3437	-8987	-8913	-8912	-8986	MG	0.00	0.00	500.00
3437	-8630	-8541	-8540	-8622	MG	0.00	0.00	500.00
3437	-9292	-9216	-9215	-9291	MG	0.00	0.00	500.00
3437	-9216	-9158	-9157	-9215	MG	0.00	0.00	500.00
3437	-9291	-9215	-9214	-9290	MG	0.00	0.00	500.00
3437	-9286	-9210	-9209	-9285	MG	0.00	0.00	500.00
3437	-9378	-9287	-9286	-9377	MG	0.00	0.00	500.00
3437	-9158	-9100	-9099	-9157	MG	0.00	0.00	500.00
3437	-8163	-8037	-8036	-8162	MG	0.00	0.00	500.00
3437	-8843	-8725	-8724	-8842	MG	0.00	0.00	500.00
3437	-9210	-9152	-9151	-9209	MG	0.00	0.00	500.00
3438	-10036	-6505	-6598	-10128	MG	0.00	0.00	500.00
3438	-9376	-5606	-5818	-9442	MG	0.00	0.00	500.00
3438	-9642	-6103	-6002	-9740	MG	0.00	0.00	500.00
3438	-8984	-5398	-5621	-9074	MG	0.00	0.00	500.00
3438	-9847	-6222	-6438	-9970	MG	0.00	0.00	500.00
3438	-9486	-6037	-6105	-9552	MG	0.00	0.00	500.00
3438	-9552	-6105	-6173	-9600	MG	0.00	0.00	500.00
3438	-9209	-5774	-5690	-9285	MG	0.00	0.00	500.00
3438	-9285	-5690	-5606	-9376	MG	0.00	0.00	500.00
3438	-9151	-5702	-5774	-9209	MG	0.00	0.00	500.00
3438	-9740	-6002	-6222	-9847	MG	0.00	0.00	500.00
3438	-9074	-5621	-5702	-9151	MG	0.00	0.00	500.00
3438	-9970	-6438	-6505	-10036	MG	0.00	0.00	500.00
3438	-9442	-5818	-6037	-9486	MG	0.00	0.00	500.00
3438	-9600	-6173	-6103	-9642	MG	0.00	0.00	500.00
3471	-6692	-6152	-6691	-6691	MG	0.00	0.00	500.00
3474	-7145	-6559	-7144	-7144	MG	0.00	0.00	500.00
3474	-6559	-5853	-7143	-7144	MG	0.00	0.00	500.00
3478	-7009	-6253	-7505	-7506	MG	0.00	0.00	500.00
3482	-4951	-5014	-7977	-7978	MG	0.00	0.00	500.00
3484	-5353	-5397	-8427	-8428	MG	0.00	0.00	500.00
3485	-4422	-4816	-8426	-8427	MG	0.00	0.00	500.00
3487	-5817	-4897	-8911	-8911	MG	0.00	0.00	500.00
3487	-4897	-5216	-8910	-8911	MG	0.00	0.00	500.00
3490	-6927	-6269	-6171	-6171	MG	0.00	0.00	500.00
3491	-6230	-5307	-9377	-9377	MG	0.00	0.00	500.00
3495	-5766	-6700	-6579	-6579	MG	0.00	0.00	500.00
3495	-7310	-6700	-6579	-6579	MG	0.00	0.00	500.00
3599	-7507	-7009	-7506	-7506	MG	0.00	0.00	500.00
3601	-7358	-6694	-7980	-7981	MG	0.00	0.00	500.00

3601	-7982	-7358	-7981	-7981	MG	0.00	0.00	500.00
3605	-8432	-7815	-8431	-8431	MG	0.00	0.00	500.00
3605	-7815	-7148	-8430	-8431	MG	0.00	0.00	500.00
3607	-5773	-5817	-8911	-8912	MG	0.00	0.00	500.00
3609	-8916	-8327	-8915	-8915	MG	0.00	0.00	500.00
3609	-8327	-7510	-8914	-8915	MG	0.00	0.00	500.00
3611	-6171	-6230	-9377	-9378	MG	0.00	0.00	500.00
3612	-5307	-5606	-9376	-9377	MG	0.00	0.00	500.00
3614	-9382	-8730	-9381	-9381	MG	0.00	0.00	500.00
3614	-8730	-7985	-9380	-9381	MG	0.00	0.00	500.00
3620	-5692	-6002	-9740	-9741	MG	0.00	0.00	500.00
3620	-6579	-6660	-9741	-9742	MG	0.00	0.00	500.00
3620	-6660	-5692	-9741	-9741	MG	0.00	0.00	500.00
3622	-9746	-9218	-9745	-9745	MG	0.00	0.00	500.00
3622	-9218	-8435	-9744	-9745	MG	0.00	0.00	500.00
3627	-9608	-10244	-10245	-10245	MG	0.00	0.00	500.00
3627	-9608	-10245	-10246	-8918	MG	0.00	0.00	500.00
3824	-4611	-4594	-4597	-4625	MG	0.00	0.00	500.00
3824	-4626	-4611	-4625	-4625	MG	0.00	0.00	500.00
3824	-4621	-4603	-4601	-4620	MG	0.00	0.00	500.00
3824	-4652	-4635	-4634	-4651	MG	0.00	0.00	500.00
3824	-4573	-4570	-4558	-4555	MG	0.00	0.00	500.00
3824	-4651	-4634	-4633	-4650	MG	0.00	0.00	500.00
3824	-4594	-4579	-4590	-4597	MG	0.00	0.00	500.00
3824	-4579	-4569	-4574	-4590	MG	0.00	0.00	500.00
3824	-4569	-4554	-4562	-4574	MG	0.00	0.00	500.00
3824	-4554	-4541	-4551	-4562	MG	0.00	0.00	500.00
3824	-4541	-4539	-4545	-4551	MG	0.00	0.00	500.00
3824	-4634	-4620	-4619	-4633	MG	0.00	0.00	500.00
3824	-4562	-4551	-4558	-4570	MG	0.00	0.00	500.00
3824	-4545	-4555	-4558	-4551	MG	0.00	0.00	500.00
3824	-4570	-4573	-4587	-4586	MG	0.00	0.00	500.00
3824	-4597	-4590	-4591	-4609	MG	0.00	0.00	500.00
3824	-4591	-4590	-4574	-4586	MG	0.00	0.00	500.00
3824	-4586	-4587	-4605	-4606	MG	0.00	0.00	500.00
3824	-4532	-4528	-4537	-4537	MG	0.00	0.00	500.00
3824	-4635	-4621	-4620	-4634	MG	0.00	0.00	500.00
3824	-4660	-4643	-4645	-4664	MG	0.00	0.00	500.00
3824	-4643	-4628	-4630	-4645	MG	0.00	0.00	500.00
3824	-4628	-4626	-4625	-4630	MG	0.00	0.00	500.00
3824	-4625	-4624	-4641	-4630	MG	0.00	0.00	500.00
3824	-4624	-4623	-4639	-4641	MG	0.00	0.00	500.00
3824	-4623	-4622	-4637	-4639	MG	0.00	0.00	500.00
3824	-4637	-4622	-4621	-4635	MG	0.00	0.00	500.00
3824	-4654	-4637	-4635	-4652	MG	0.00	0.00	500.00
3824	-4539	-4532	-4537	-4545	MG	0.00	0.00	500.00
3824	-4537	-4550	-4555	-4545	MG	0.00	0.00	500.00
3824	-4550	-4567	-4573	-4555	MG	0.00	0.00	500.00
3824	-4567	-4585	-4587	-4573	MG	0.00	0.00	500.00
3824	-4585	-4603	-4605	-4587	MG	0.00	0.00	500.00
3824	-4603	-4621	-4622	-4605	MG	0.00	0.00	500.00
3824	-4622	-4623	-4606	-4605	MG	0.00	0.00	500.00
3824	-4623	-4624	-4609	-4606	MG	0.00	0.00	500.00
3824	-4624	-4625	-4597	-4609	MG	0.00	0.00	500.00
3824	-4658	-4662	-4647	-4641	MG	0.00	0.00	500.00
3824	-4662	-4664	-4645	-4647	MG	0.00	0.00	500.00
3824	-4647	-4645	-4630	-4641	MG	0.00	0.00	500.00
3824	-4639	-4637	-4654	-4656	MG	0.00	0.00	500.00
3824	-4639	-4656	-4658	-4641	MG	0.00	0.00	500.00
3824	-4570	-4586	-4574	-4562	MG	0.00	0.00	500.00
3824	-4606	-4609	-4591	-4586	MG	0.00	0.00	500.00
3824	-4603	-4585	-4582	-4601	MG	0.00	0.00	500.00
3824	-4585	-4567	-4565	-4582	MG	0.00	0.00	500.00
3824	-4567	-4550	-4548	-4565	MG	0.00	0.00	500.00
3824	-4550	-4537	-4535	-4548	MG	0.00	0.00	500.00
3824	-4537	-4528	-4526	-4535	MG	0.00	0.00	500.00
3824	-4620	-4601	-4599	-4619	MG	0.00	0.00	500.00
3824	-4601	-4582	-4580	-4599	MG	0.00	0.00	500.00
3824	-4582	-4565	-4563	-4580	MG	0.00	0.00	500.00
3824	-4565	-4548	-4546	-4563	MG	0.00	0.00	500.00
3824	-4548	-4535	-4533	-4546	MG	0.00	0.00	500.00
3824	-4535	-4526	-4524	-4533	MG	0.00	0.00	500.00

Elenco carichi elementi bidimensionali
Condizione di carico n. 9: Var. termiche
Carichi termici

Simbologia

Bid. = Numero del muro/elemento bidimensionale

N1 = Nodo1

N2 = Nodo2

N3 = Nodo3

N4 = Nodo4

DT = Incremento di temperatura

Gy = Gradiente termico in dir. Y

Bid.	N1	N2	N3	N4	DT <°C>	Gy <°C/m>	Bid.	N1	N2	N3	N4	DT <°C>	Gy <°C/m>
2935	-4670	-4653	-4655	-4672	25.00		2935	-4676	-4661	-4663	-4679	25.00	
2935	-4804	-4747	-4746	-4803	25.00		2935	-4746	-4687	-4686	-4745	25.00	
2935	-4858	-4803	-4802	-4857	25.00		2935	-4676	-4674	-4657	-4661	25.00	
2935	-4864	-4809	-4808	-4863	25.00		2935	-4671	-4654	-4652	-4669	25.00	
2935	-4747	-4688	-4687	-4746	25.00		2935	-4690	-4689	-4748	-4749	25.00	
2935	-4697	-4680	-4677	-4696	25.00		2935	-4672	-4655	-4657	-4674	25.00	
2935	-4855	-4800	-4799	-4854	25.00		2935	-4803	-4746	-4745	-4802	25.00	
2935	-4669	-4652	-4651	-4668	25.00		2935	-4754	-4695	-4694	-4753	25.00	
2935	-4859	-4804	-4803	-4858	25.00		2935	-4755	-4696	-4695	-4754	25.00	
2935	-4813	-4756	-4755	-4812	25.00		2935	-4802	-4745	-4744	-4801	25.00	
2935	-4656	-4673	-4675	-4658	25.00		2935	-4812	-4755	-4754	-4811	25.00	
2935	-4867	-4812	-4811	-4866	25.00		2935	-4748	-4689	-4688	-4747	25.00	
2935	-4666	-4649	-4648	-4665	25.00		2935	-4688	-4665	-4670	-4687	25.00	
2935	-4694	-4695	-4675	-4673	25.00		2935	-4698	-4681	-4680	-4697	25.00	
2935	-4749	-4748	-4805	-4806	25.00		2935	-4752	-4693	-4692	-4751	25.00	
2935	-4809	-4752	-4751	-4808	25.00		2935	-4751	-4692	-4691	-4750	25.00	
2935	-4807	-4806	-4861	-4862	25.00		2935	-4745	-4686	-4685	-4744	25.00	
2935	-4692	-4669	-4668	-4691	25.00		2935	-4857	-4802	-4801	-4856	25.00	
2935	-4667	-4650	-4649	-4666	25.00		2935	-4689	-4666	-4665	-4688	25.00	
2935	-4810	-4753	-4752	-4809	25.00		2935	-4686	-4687	-4670	-4672	25.00	
2935	-4856	-4801	-4800	-4855	25.00		2935	-4668	-4651	-4650	-4667	25.00	
2935	-4669	-4692	-4693	-4671	25.00		2935	-4665	-4648	-4653	-4670	25.00	
2935	-4696	-4677	-4675	-4695	25.00		2935	-4744	-4685	-4684	-4743	25.00	
2935	-4805	-4748	-4747	-4804	25.00		2935	-4756	-4697	-4696	-4755	25.00	
2935	-4677	-4680	-4664	-4662	25.00		2935	-4686	-4672	-4674	-4685	25.00	
2935	-4681	-4660	-4664	-4680	25.00		2935	-4753	-4694	-4693	-4752	25.00	
2935	-4684	-4685	-4674	-4676	25.00		2935	-4656	-4654	-4671	-4673	25.00	
2935	-4750	-4749	-4806	-4807	25.00		2935	-4690	-4667	-4666	-4689	25.00	
2935	-4742	-4683	-4682	-4741	25.00		2935	-4868	-4813	-4812	-4867	25.00	
2935	-4808	-4751	-4750	-4807	25.00		2935	-4866	-4811	-4810	-4865	25.00	
2935	-4691	-4668	-4667	-4690	25.00		2935	-4694	-4673	-4671	-4693	25.00	
2935	-4691	-4690	-4749	-4750	25.00		2935	-4801	-4744	-4743	-4800	25.00	
2935	-4865	-4810	-4809	-4864	25.00		2935	-4814	-4757	-4756	-4813	25.00	
2935	-4659	-4678	-4679	-4663	25.00		2935	-4869	-4814	-4813	-4868	25.00	
2935	-4811	-4754	-4753	-4810	25.00		2935	-4799	-4742	-4741	-4798	25.00	
2935	-4854	-4799	-4798	-4853	25.00		2935	-4684	-4676	-4679	-4683	25.00	
2935	-4683	-4679	-4678	-4682	25.00		2935	-4757	-4698	-4697	-4756	25.00	
2935	-4743	-4684	-4683	-4742	25.00		2935	-4677	-4662	-4658	-4675	25.00	
2935	-4860	-4805	-4804	-4859	25.00		2935	-4806	-4805	-4860	-4861	25.00	
2935	-4800	-4743	-4742	-4799	25.00		2935	-4863	-4808	-4807	-4862	25.00	
3034	-5041	-4976	-4992	-5040	25.00		3034	-4918	-4855	-4854	-4917	25.00	
3034	-5042	-4968	-4976	-5041	25.00		3034	-4932	-4866	-4865	-4931	25.00	
3034	-4967	-4918	-4917	-4966	25.00		3034	-5048	-4995	-4979	-5047	25.00	
3034	-4926	-4860	-4859	-4925	25.00		3034	-4861	-4860	-4926	-4927	25.00	
3034	-4994	-4930	-4929	-4978	25.00		3034	-4929	-4863	-4862	-4928	25.00	
3034	-4924	-4858	-4857	-4919	25.00		3034	-4978	-4929	-4928	-4970	25.00	
3034	-4927	-4926	-4969	-4993	25.00		3034	-4925	-4859	-4858	-4924	25.00	
3034	-4976	-4919	-4923	-4992	25.00		3034	-4995	-4932	-4931	-4979	25.00	
3034	-5046	-4994	-4978	2902	25.00		3034	-4969	-4926	-4925	-4977	25.00	
3034	-4919	-4857	-4856	-4923	25.00		3034	-5051	-4997	-4980	-5050	25.00	
3034	2902	-4978	-4970	-5045	25.00		3034	-5043	-4969	-4977	2901	25.00	
3034	-4920	-4867	-4866	-4932	25.00		3034	-4992	-4923	-4918	-4967	25.00	
3034	-4996	-4920	-4932	-4995	25.00		3034	-4923	-4856	-4855	-4918	25.00	
3034	-4930	-4864	-4863	-4929	25.00		3034	-4997	-4934	-4933	-4980	25.00	
3034	-5039	-4967	-4966	-5038	25.00		3034	2901	-4977	-4968	-5042	25.00	
3034	-4993	-4969	-5043	-5044	25.00		3034	-4931	-4865	-4864	-4930	25.00	
3034	-4862	-4861	-4927	-4928	25.00		3034	-5040	-4992	-4967	-5039	25.00	
3034	-4970	-4993	-5044	-5045	25.00		3034	-4934	-4869	-4868	-4933	25.00	
3034	-4968	-4924	-4919	-4976	25.00		3034	-4917	-4854	-4853	-4916	25.00	
3034	-5050	-4980	-4996	-5049	25.00		3034	-5047	-4979	-4994	-5046	25.00	
3034	-4928	-4927	-4993	-4970	25.00		3034	-4979	-4931	-4930	-4994	25.00	
3034	-5049	-4996	-4995	-5048	25.00		3034	-4977	-4925	-4924	-4968	25.00	
3034	-4933	-4868	-4867	-4920	25.00		3034	-5038	-4966	-4991	-5037	25.00	
3034	-4966	-4917	-4916	-4991	25.00		3034	-4980	-4933	-4920	-4996	25.00	
3131	-5116	-5040	-5039	-5115	25.00		3131	-5671	-5602	-5601	-5670	25.00	
3131	-5663	-5594	-5593	-5662	25.00		3131	-5435	-5373	-5372	-5434	25.00	
3131	-5741	-5732	-5797	-5798	25.00		3131	-5119	2901	-5042	-5118	25.00	
3131	-5129	-5051	-5050	-5128	25.00		3131	-5200	-5115	-5114	-5199	25.00	
3131	-5325	-5274	-5273	-5324	25.00		3131	-5795	-5731	-5730	-5794	25.00	

3131	-5594	-5499	-5498	-5593	25.00		3131	-5592	-5497	-5496	-5591	25.00	
3131	-5204	-5119	-5118	-5203	25.00		3131	-5277	-5212	-5211	-5276	25.00	
3131	-5591	-5496	-5495	-5590	25.00		3131	-5203	-5118	-5117	-5202	25.00	
3131	-5805	-5744	-5736	-5804	25.00		3131	-5735	-5670	-5669	-5734	25.00	
3131	-5505	-5442	-5441	-5504	25.00		3131	-5432	-5370	-5369	-5431	25.00	
3131	-5445	-5383	-5382	-5444	25.00		3131	-5744	-5673	-5672	-5736	25.00	
3131	-5120	-5043	2901	-5119	25.00		3131	-5379	-5325	-5324	-5378	25.00	
3131	-5439	-5438	-5501	-5502	25.00		3131	-5731	-5663	-5662	-5730	25.00	
3131	-5508	-5445	-5444	-5507	25.00		3131	-5728	-5660	-5659	-5727	25.00	
3131	-5660	-5591	-5590	-5659	25.00		3131	-5496	-5433	-5432	-5495	25.00	
3131	-5665	-5664	-5740	-5732	25.00		3131	-5802	-5735	-5734	-5801	25.00	
3131	-5730	-5662	-5661	-5729	25.00		3131	-5370	-5316	-5315	-5369	25.00	
3131	-5214	-5129	-5128	-5213	25.00		3131	-5803	-5743	-5735	-5802	25.00	
3131	-5743	-5671	-5670	-5735	25.00		3131	-5210	-5125	-5124	-5209	25.00	
3131	-5128	-5050	-5049	-5127	25.00		3131	-5801	-5734	-5742	-5800	25.00	
3131	-5661	-5592	-5591	-5660	25.00		3131	-5734	-5669	-5668	-5742	25.00	
3131	-5320	-5269	-5268	-5319	25.00		3131	-5269	-5204	-5203	-5268	25.00	
3131	-5497	-5434	-5433	-5496	25.00		3131	-5201	-5116	-5115	-5200	25.00	
3131	-5206	-5205	-5270	-5271	25.00		3131	-5207	-5206	-5271	-5272	25.00	
3131	-5327	-5276	-5275	-5326	25.00		3131	-5436	-5374	-5373	-5435	25.00	
3131	-5276	-5211	-5210	-5275	25.00		3131	-5727	-5659	-5658	-5726	25.00	
3131	-5590	-5495	-5494	-5589	25.00		3131	-5045	-5044	-5121	-5122	25.00	
3131	-5315	-5264	-5263	-5314	25.00		3131	-5275	-5210	-5209	-5274	25.00	
3131	-5446	-5384	-5383	-5445	25.00		3131	-5125	-5047	-5046	-5124	25.00	
3131	-5664	-5595	-5594	-5663	25.00		3131	-5437	-5375	-5374	-5436	25.00	
3131	-5500	-5437	-5436	-5499	25.00		3131	-5597	-5596	-5665	-5666	25.00	
3131	-5440	-5378	-5377	-5439	25.00		3131	-5274	-5209	-5208	-5273	25.00	
3131	-5499	-5436	-5435	-5498	25.00		3131	-5265	-5200	-5199	-5264	25.00	
3131	-5316	-5265	-5264	-5315	25.00		3131	-5794	-5730	-5729	-5793	25.00	
3131	-5273	-5208	-5207	-5272	25.00		3131	-5279	-5214	-5213	-5278	25.00	
3131	-5670	-5601	-5600	-5669	25.00		3131	-5601	-5506	-5505	-5600	25.00	
3131	-5278	-5213	-5212	-5277	25.00		3131	-5369	-5315	-5314	-5368	25.00	
3131	-5213	-5128	-5127	-5212	25.00		3131	-5270	-5205	-5204	-5269	25.00	
3131	-5264	-5199	-5198	-5263	25.00		3131	-5328	-5277	-5276	-5327	25.00	
3131	-5382	-5328	-5327	-5381	25.00		3131	-5377	-5376	-5438	-5439	25.00	
3131	-5792	-5728	-5727	-5791	25.00		3131	-5212	-5127	-5126	-5211	25.00	
3131	-5127	-5049	-5048	-5126	25.00		3131	-5443	-5381	-5380	-5442	25.00	
3131	-5373	-5319	-5318	-5372	25.00		3131	-5791	-5727	-5726	-5790	25.00	
3131	-5268	-5203	-5202	-5267	25.00		3131	-5501	-5500	-5595	-5596	25.00	
3131	-5380	-5326	-5325	-5379	25.00		3131	-5495	-5432	-5431	-5494	25.00	
3131	-5790	-5726	-5725	-5789	25.00		3131	-5796	-5740	-5731	-5795	25.00	
3131	-5726	-5658	-5657	-5725	25.00		3131	-5595	-5500	-5499	-5594	25.00	
3131	-5371	-5317	-5316	-5370	25.00		3131	-5494	-5431	-5430	-5493	25.00	
3131	-5441	-5379	-5378	-5440	25.00		3131	-5266	-5201	-5200	-5265	25.00	
3131	-5666	-5665	-5732	-5741	25.00		3131	-5272	-5271	-5322	-5323	25.00	
3131	-5324	-5273	-5272	-5323	25.00		3131	-5507	-5444	-5443	-5506	25.00	
3131	-5330	-5279	-5278	-5329	25.00		3131	-5124	-5046	2902	-5123	25.00	
3131	-5502	-5501	-5596	-5597	25.00		3131	-5732	-5740	-5796	-5797	25.00	
3131	-5383	-5329	-5328	-5382	25.00		3131	-5329	-5278	-5277	-5328	25.00	
3131	-5205	-5120	-5119	-5204	25.00		3131	-5506	-5443	-5442	-5505	25.00	
3131	-5321	-5270	-5269	-5320	25.00		3131	-5374	-5320	-5319	-5373	25.00	
3131	-5199	-5114	-5113	-5198	25.00		3131	-5669	-5600	-5599	-5668	25.00	
3131	-5376	-5375	-5437	-5438	25.00		3131	-5600	-5505	-5504	-5599	25.00	
3131	-5326	-5275	-5274	-5325	25.00		3131	-5271	-5270	-5321	-5322	25.00	
3131	-5599	-5504	-5503	-5598	25.00		3131	-5381	-5327	-5326	-5380	25.00	
3131	-5211	-5126	-5125	-5210	25.00		3131	-5659	-5590	-5589	-5658	25.00	
3131	-5673	-5604	-5603	-5672	25.00		3131	-5442	-5380	-5379	-5441	25.00	
3131	-5317	-5266	-5265	-5316	25.00		3131	-5503	-5440	-5439	-5502	25.00	
3131	-5509	-5446	-5445	-5508	25.00		3131	-5740	-5664	-5663	-5731	25.00	
3131	-5202	-5117	-5116	-5201	25.00		3131	-5589	-5494	-5493	-5588	25.00	
3131	-5433	-5371	-5370	-5432	25.00		3131	-5603	-5508	-5507	-5602	25.00	
3131	-5596	-5595	-5664	-5665	25.00		3131	-5208	-5123	-5122	-5207	25.00	
3131	-5602	-5507	-5506	-5601	25.00		3131	-5323	-5322	-5376	-5377	25.00	
3131	-5378	-5324	-5323	-5377	25.00		3131	-5319	-5268	-5267	-5318	25.00	
3131	-5742	-5668	-5667	-5733	25.00		3131	-5504	-5441	-5440	-5503	25.00	
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3437	-9071	-8980	-8979	-9094	25.00		3437	-8619	-8535	-8534	-8618	25.00	
3437	-8627	-8531	-8530	-8615	25.00		3437	-9280	-9204	-9203	-9279	25.00	
3437	-8163	-8037	-8036	-8162	25.00		3437	-8978	-8904	-8903	-8977	25.00	
3437	-8843	-8725	-8724	-8842	25.00		3437	-8807	-8717	-8716	-8806	25.00	
3437	-8717	-8619	-8618	-8716	25.00		3437	-9072	-8981	-8980	-9071	25.00	
3437	-8713	-8627	-8615	-8712	25.00		3437	-9210	-9152	-9151	-9209	25.00	
3824	-4583	-4588	-4572	-4571	25.00		3824	-4611	-4594	-4597	-4625	25.00	
3824	-4626	-4611	-4625	-4625	25.00		3824	-4621	-4603	-4601	-4620	25.00	
3824	-4652	-4635	-4634	-4651	25.00		3824	-4589	-4598	-4608	-4592	25.00	
3824	-4607	-4583	-4592	-4608	25.00		3824	-4573	-4570	-4558	-4555	25.00	
3824	-4651	-4634	-4633	-4650	25.00		3824	-4536	-4527	-4531	-4531	25.00	
3824	-4594	-4579	-4590	-4597	25.00		3824	-4579	-4569	-4574	-4590	25.00	
3824	-4569	-4554	-4562	-4574	25.00		3824	-4554	-4541	-4551	-4562	25.00	
3824	-4541	-4539	-4545	-4551	25.00		3824	-4583	-4607	-4604	-4588	25.00	
3824	-4649	-4632	-4631	-4648	25.00		3824	-4634	-4620	-4619	-4633	25.00	
3824	-4648	-4631	-4636	-4653	25.00		3824	-4631	-4617	-4616	-4636	25.00	
3824	-4636	-4616	-4615	-4638	25.00		3824	-4615	-4614	-4640	-4638	25.00	
3824	-4614	-4613	-4629	-4640	25.00		3824	-4613	-4612	-4627	-4629	25.00	
3824	-4627	-4642	-4644	-4629	25.00		3824	-4642	-4659	-4663	-4644	25.00	
3824	-4562	-4551	-4558	-4570	25.00		3824	-4545	-4555	-4558	-4551	25.00	
3824	-4570	-4573	-4587	-4586	25.00		3824	-4650	-4633	-4632	-4649	25.00	
3824	-4633	-4619	-4618	-4632	25.00		3824	-4597	-4590	-4591	-4609	25.00	
3824	-4591	-4590	-4574	-4586	25.00		3824	-4586	-4587	-4605	-4606	25.00	
3824	-4632	-4618	-4617	-4631	25.00		3824	-4629	-4644	-4646	-4640	25.00	
3824	-4644	-4663	-4661	-4646	25.00		3824	-4646	-4661	-4657	-4640	25.00	
3824	-4532	-4528	-4537	-4537	25.00		3824	-4635	-4621	-4620	-4634	25.00	
3824	-4653	-4636	-4638	-4655	25.00		3824	-4655	-4638	-4640	-4657	25.00	
3824	-4660	-4643	-4645	-4664	25.00		3824	-4643	-4628	-4630	-4645	25.00	
3824	-4628	-4626	-4625	-4630	25.00		3824	-4625	-4624	-4641	-4630	25.00	
3824	-4624	-4623	-4639	-4641	25.00		3824	-4623	-4622	-4637	-4639	25.00	
3824	-4637	-4622	-4621	-4635	25.00		3824	-4654	-4637	-4635	-4652	25.00	
3824	-4539	-4532	-4537	-4545	25.00		3824	-4537	-4550	-4555	-4545	25.00	
3824	-4550	-4567	-4573	-4555	25.00		3824	-4567	-4585	-4587	-4573	25.00	
3824	-4585	-4603	-4605	-4587	25.00		3824	-4603	-4621	-4622	-4605	25.00	
3824	-4622	-4623	-4606	-4605	25.00		3824	-4623	-4624	-4609	-4606	25.00	
3824	-4624	-4625	-4597	-4609	25.00		3824	-4658	-4662	-4647	-4641	25.00	
3824	-4662	-4664	-4645	-4647	25.00		3824	-4647	-4645	-4630	-4641	25.00	
3824	-4639	-4637	-4654	-4656	25.00		3824	-4639	-4656	-4658	-4641	25.00	
3824	-4570	-4586	-4574	-4562	25.00		3824	-4606	-4609	-4591	-4586	25.00	
3824	-4603	-4585	-4582	-4601	25.00		3824	-4585	-4567	-4565	-4582	25.00	
3824	-4567	-4550	-4548	-4565	25.00		3824	-4550	-4537	-4535	-4548	25.00	
3824	-4537	-4528	-4526	-4535	25.00		3824	-4620	-4601	-4599	-4619	25.00	
3824	-4601	-4582	-4580	-4599	25.00		3824	-4582	-4565	-4563	-4580	25.00	
3824	-4565	-4548	-4546	-4563	25.00		3824	-4548	-4535	-4533	-4546	25.00	
3824	-4535	-4526	-4524	-4533	25.00		3824	-4619	-4599	-4600	-4618	25.00	
3824	-4599	-4580	-4581	-4600	25.00		3824	-4580	-4563	-4564	-4581	25.00	
3824	-4563	-4546	-4547	-4564	25.00		3824	-4546	-4533	-4534	-4547	25.00	
3824	-4533	-4524	-4525	-4534	25.00		3824	-4618	-4600	-4602	-4617	25.00	
3824	-4600	-4581	-4584	-4602	25.00		3824	-4581	-4564	-4566	-4584	25.00	
3824	-4564	-4547	-4549	-4566	25.00		3824	-4547	-4534	-4536	-4549	25.00	
3824	-4534	-4525	-4527	-4536	25.00		3824	-4610	-4612	-4613	-4613	25.00	
3824	-4602	-4584	-4588	-4604	25.00		3824	-4584	-4566	-4572	-4588	25.00	
3824	-4566	-4549	-4556	-4572	25.00		3824	-4549	-4536	-4544	-4556	25.00	
3824	-4536	-4531	-4538	-4544	25.00		3824	-4538	-4540	-4552	-4544	25.00	
3824	-4540	-4553	-4561	-4552	25.00		3824	-4553	-4568	-4575	-4561	25.00	
3824	-4568	-4578	-4589	-4575	25.00		3824	-4578	-4593	-4598	-4589	25.00	
3824	-4593	-4610	-4613	-4598	25.00		3824	-4613	-4614	-4608	-4598	25.00	
3824	-4614	-4615	-4607	-4608	25.00		3824	-4615	-4616	-4604	-4607	25.00	
3824	-4617	-4602	-4604	-4616	25.00		3824	-4544	-4552	-4557	-4556	25.00	
3824	-4561	-4571	-4557	-4552	25.00		3824	-4572	-4556	-4557	-4571	25.00	
3824	-4575	-4583	-4571	-4561	25.00		3824	-4575	-4589	-4592	-4583	25.00	

Impalcato “A” – Verifiche acciaio

Simbologia

Sez.		=Numero della sezione
Cod.		=Codice
Tipo		=Tipologia
		2C = Doppia C lato labbri
		2Cdx = Doppia C lato costola
		2I = Doppia I
		2L = Doppia L lato labbri
		2Ldx = Doppia L lato costole
		C = Sezione a C
		Cdx = C destra
		Cir. = Circolare
		Cir.c = Circolare cava
		I = Sezione a I
		L = Sezione a L
		Ldx = L destra
		Om. = Omega
		Pg = Pi greco
		Pr = Poligono regolare
		Prc = Poligono regolare cavo
		Pc = Per coordinate
		Ia = Inerzie assegnate
		R = Rettangolare
		Rc = Rettangolare cava
		T = Sezione a T
		U = Sezione a U
		Ur = U rovescia
		V = Sezione a V
		Vr = V rovescia
		Z = Sezione a Z
		Zdx = Z destra
		Ts = T stondata
		Ls = L stondata
		Cs = C stondata
		Is = I stondata
		Dis. = Disegnata
D	<cm>	=Distanza
Area	<cmq>	=Area
Anet	<cmq>	=Area netta per compressione
Aeff	<cmq>	=Area effettiva per trazione
Jy	<cm4>	=Momento d'inerzia rispetto all'asse Y
Jz	<cm4>	=Momento d'inerzia rispetto all'asse Z
Iy	<cm>	=Raggio giratorio d'inerzia rispetto all'asse Y
Iz	<cm>	=Raggio giratorio d'inerzia rispetto all'asse Z
Wymin	<cmc>	=Modulo di resistenza minimo rispetto all'asse Y
Wzmin	<cmc>	=Modulo di resistenza minimo rispetto all'asse Z
Tp		=Tipo di acciaio
Fyk	<daN/cmq>	=Tensione caratteristica di snervamento dell'acciaio
Fyt	<daN/cmq>	=Tensione caratteristica di rottura
Wy,plas	<cmc>	=Modulo di resistenza plastico intorno all'asse Y
Wz,plas	<cmc>	=Modulo di resistenza plastico intorno all'asse Z
Atag,y	<cmq>	=Area resistente a taglio in dir. Y
Atag,z	<cmq>	=Area resistente a taglio in dir. Z
Jø	<cm6>	=Costante di ingobbamento
CC		=Numero della combinazione delle condizioni di carico elementari
N,Ed	<daN>	=Forza assiale di calcolo
M,Ed	<daNm>	=Momento flettente di calcolo
Nc,Rd	<daN>	=Resistenza a compressione
My,c,Rd	<daNm>	=Resistenza di calcolo a flessione intorno all'asse Y
L	<cm>	=Lunghezza dell'asta
λ		=Snellezza per inflessione
Ncr	<daN>	=Sforzo normale critico euleriano
λ'		=Snellezza adimensionale
Curva		=Curva di instabilità adottata
Φ		=Coefficiente Φ
χ,min		=Coefficiente χ di riduzione per instabilità
Xl	<m>	=Coordinata progressiva (dal nodo iniziale dell'asta) in cui viene effettuato il progetto/verifica
N	<daN>	=Sforzo normale
T	<daN>	=Taglio agente
Mx	<daNm>	=Momento torcente intorno all'asse X
V,Ed	<daN>	=Forza di taglio di calcolo
Vc,Rd,Red	<daN>	=Resistenza a taglio ridotta
M	<daNm>	=Momento agente
σ _N	<daN/cmq>	=Tensione normale per sforzo normale
σ _M	<daN/cmq>	=Tensione normale per momento flettente
τ	<daN/cmq>	=Tensione tangenziale per taglio e/o torsione
σ _{Id,max}	<daN/cmq>	=Tensione ideale massima
M,c,Rd	<daNm>	=Resistenza di calcolo a flessione
MN,c,Rd	<daNm>	=Resistenza di calcolo a pressoflessione
My,Ed	<daNm>	=Momento flettente di calcolo intorno all'asse Y
Mz,Ed	<daNm>	=Momento flettente di calcolo intorno all'asse Z
Mz,c,Rd	<daNm>	=Resistenza di calcolo a flessione intorno all'asse Z
α _{my} , α _{mz} , α _{LT}		=Coefficienti correttivi per il momento flettente
λ _y		=Snellezza per inflessione intorno all'asse y(c)
Ncr,y	<daN>	=Sforzo normale critico euleriano per inflessione intorno all'asse y(c)
λ' _y		=Snellezza adimensionale per inflessione intorno all'asse y(c)
Φ _y		=Coefficiente Φ per inflessione intorno all'asse y(c)
χ _y		=Coefficiente χ di riduzione per instabilità intorno all'asse y(c)
λ _z		=Snellezza per inflessione intorno all'asse z(e)
Ncr,z	<daN>	=Sforzo normale critico euleriano per inflessione intorno all'asse z(e)
λ' _z		=Snellezza adimensionale per inflessione intorno all'asse z(e)
Φ _z		=Coefficiente Φ per inflessione intorno all'asse z(e)
χ _z		=Coefficiente χ di riduzione per instabilità intorno all'asse z(e)
K _{yy} , K _{yz} , K _{zy} , K _{zz}		=Coefficienti di interazione
Tz	<daN>	=Taglio in dir. Z
My	<daNm>	=Momento flettente intorno all'asse Y
Ty	<daN>	=Taglio in dir. Y
Mz	<daNm>	=Momento flettente intorno all'asse Z

MNy, c, Rd	<daNm>	= Resistenza di calcolo a pressoflessione intorno all'asse Y
Vc, Rd	<daN>	= Resistenza a taglio
Npl, Rd	<daN>	= Resistenza plastica a trazione per sezione lorda
Nu, Rd	<daN>	= Resistenza a rottura di trazione per sezione netta
Nt, Rd	<daN>	= Resistenza a trazione ultima
Nb, Rd	<daN>	= Resistenza all'instabilità
f _{z,l}	<cm>	= Freccia in direzione Z locale
f _{z,g}	<cm>	= Freccia in direzione Z globale

Caratteristiche profilati utilizzati

Sez.	Cod.	Tipo	D <cm>	Area <cmq>	Anet <cmq>	Aeff <cmq>	Jy <cm4>	Jz <cm4>	Iy <cm>	Iz <cm>	Wymin <cm>	Wzmin <cm>	Tp	Fyk <daN/cmq>	Fyt <daN/cmq>
31	Tube circolare d=114.3x6 mm - S355	Cir.c	--	20.41	20.41	20.41	300.21	300.21	3.83	3.83	52.53	52.53	S355H UNI EN 10210-1	3550.00	5100.00
32	Tube 60x80x5 mm - S355	Rc	--	13.00	13.00	13.00	113.08	71.08	2.95	2.34	28.27	23.69	S355H UNI EN 10210-1	3550.00	5100.00
33	Tube 60x100x5 mm - S355	Rc	--	15.00	15.00	15.00	196.25	86.25	3.62	2.40	39.25	28.75	S355H UNI EN 10210-1	3550.00	5100.00
34	Tube 80x120x5 mm - S355	Rc	--	19.00	19.00	19.00	375.58	197.58	4.45	3.22	62.60	49.40	S355H UNI EN 10210-1	3550.00	5100.00
39	Tube circolare d=70x4 mm - S355	Cir.c	--	8.29	8.29	8.29	45.33	45.33	2.34	2.34	12.95	12.95	S355H UNI EN 10210-1	3550.00	5100.00
48	Tube circolare d=101.6x6 mm - S355	Cir.c	--	18.02	18.02	18.02	206.68	206.68	3.39	3.39	40.68	40.68	S355H UNI EN 10210-1	3550.00	5100.00
50	Tube circolare d=90x4 mm - S355	Cir.c	--	10.81	10.81	10.81	100.13	100.13	3.04	3.04	22.25	22.25	S355H UNI EN 10210-1	3550.00	5100.00
53	Tube 60x60x4 mm - S235	Rc	--	8.96	8.96	8.96	47.07	47.07	2.29	2.29	15.69	15.69	S235H UNI EN 10210-1	2350.00	3600.00
61	Tube 60x120x4 mm - S235	Rc	--	13.76	13.76	13.76	255.20	84.77	4.31	2.48	42.53	28.26	S235H UNI EN 10210-1	2350.00	3600.00
68	Tube 80x100x(2x5+6) mm - S355 (32)	Rc	--	26.24	26.24	26.24	350.56	243.17	3.66	3.04	70.11	60.79	S355H UNI EN 10210-1	3550.00	5100.00

Caratteristiche profilati utilizzati

Sez.	Cod.	Wy, plas <cmq>	Wz, plas <cmq>	Atag, y <cmq>	Atag, z <cmq>	J ₀ <cm6>
31	Tube circolare d=114.3x6 mm - S355	68.72	68.72	13.00	13.00	
32	Tube 60x80x5 mm - S355	34.75	28.25	5.57	7.43	
33	Tube 60x100x5 mm - S355	48.75	33.75	5.63	9.38	
34	Tube 80x120x5 mm - S355	76.25	57.25	7.60	11.40	
39	Tube circolare d=70x4 mm - S355	17.02	17.02	5.28	5.28	
48	Tube circolare d=101.6x6 mm - S355	53.56	53.56	11.47	11.47	
50	Tube circolare d=90x4 mm - S355	28.88	28.88	6.88	6.88	
53	Tube 60x60x4 mm - S235	18.85	18.85	4.48	4.48	
61	Tube 60x120x4 mm - S235	52.93	32.29	4.59	9.17	
68	Tube 80x100x(2x5+6) mm - S355 (32)	87.10	73.98	11.66	14.58	

Asta n. 2003 (1902 -4691) Tube circolare d=70x4 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 1

Sollecitazioni: N,Ed=-4913.02 M,Ed=1.27
 Resistenze: Nc,Rd=28041.00 M,c,Rd=575.38 L=134.54
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, \text{----}, \text{----}$
 $\lambda=57.55 \text{ Ncr}=51897.20 \lambda^*=0.75$
 Curva a: $\Phi=0.84 \chi, \text{min}=0.82$
 Kyy, Kyz, Kzy, Kzz=1.06, ----, ----, ----
 Verifica: $0.21+0.00=0.22$

- Verifica Freccia massima per soli carichi accidentali - CC 69

f_{z,l}=0.01 (L/14585) f_{z,g}=0.01 (L/16931)

- Verifica Freccia massima carichi totali - CC 69

f_{z,l}=0.01 (L/14117) f_{z,g}=0.01 (L/16470)

- Verifica a compressione [4.2.9] - CC 45 SLU Xl=0.19 - Classe 1

Sollecitazioni: N=-4913.02 T=4.39 M_x=6.03
 N,Ed=-4913.02 Nc,Rd=-28041.00 N,Ed/Nc,Rd=0.18

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 54 SLU Xl=1.35

Sollecitazioni: N=-817.76 T=4.39 M_x=13.75
 V,Ed=4.39 Vc,Rd,Red=10026.60 V,Ed/Vc,Rd,Red=0.00

- Verifica a compressione [4.2.9] - CC 1 SND Xl=0.19 - Classe 3

Sollecitazioni: N=-2131.85 T=3.25 M_x=20.10
 N,Ed=-2131.85 Nc,Rd=-28041.00 N,Ed/Nc,Rd=0.08

Asta n. 2004 (1901 -4689) Tube circolare d=70x4 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 1

Sollecitazioni: N,Ed=-4824.66 M,Ed=1.27
 Resistenze: Nc,Rd=28041.00 M,c,Rd=575.38 L=134.54
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, \text{----}, \text{----}$
 $\lambda=57.55 \text{ Ncr}=51897.20 \lambda^*=0.75$
 Curva a: $\Phi=0.84 \chi, \text{min}=0.82$
 Kyy, Kyz, Kzy, Kzz=1.06, ----, ----, ----
 Verifica: $0.21+0.00=0.21$

- Verifica Freccia massima per soli carichi accidentali - CC 62

f_{z,l}=0.01 (L/13665) f_{z,g}=0.01 (L/15706)

- Verifica Freccia massima carichi totali - CC 62

$f_{z,L}=0.01$ (L/13550) $f_{z,G}=0.01$ (L/15455)

- Verifica a compressione [4.2.9] - CC 45 SLU $X_l=0.19$ - Classe 1
Sollecitazioni: $N=-4824.66$ $T=4.39$ $M_x=-5.28$
 $N,Ed=-4824.66$ $Nc,Rd=-28041.00$ $N,Ed/Nc,Rd=0.17$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 68 SLU $X_l=1.34$
Sollecitazioni: $N=470.52$ $T=4.39$ $M_x=-14.42$
 $V,Ed=4.39$ $Vc,Rd,Red=10012.80$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica a compressione [4.2.9] - CC 1 SND $X_l=0.19$ - Classe 3
Sollecitazioni: $N=-2988.12$ $T=3.25$ $M_x=-10.21$
 $N,Ed=-2988.12$ $Nc,Rd=-28041.00$ $N,Ed/Nc,Rd=0.11$

Asta n. 2024 (1902 -5439) Tubo circolare $d=90 \times 4$ mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 54 SLU - Classe 1
Sollecitazioni: $N,Ed=-8182.46$ $M,Ed=2.06$
Resistenze: $Nc,Rd=36538.20$ $M,c,Rd=976.45$ $L=134.54$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, \text{----}, \text{----}$
 $\lambda=44.20$ $Ncr=114642.00$ $\lambda^*=0.58$
Curva a: $\Phi=0.71$ $\chi_{,min}=0.90$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=1.04, \text{----}, \text{----}, \text{----}$
Verifica: $0.25+0.00=0.25$
- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,G}=0.02$ (L/7533) $f_{z,L}=0.00$ (L/36080)
- Verifica Freccia massima carichi totali - CC 26
 $f_{z,G}=0.02$ (L/7681) $f_{z,L}=0.01$ (L/8845)

- Verifica a compressione [4.2.9] - CC 54 SLU $X_l=0.04$ - Classe 1
Sollecitazioni: $N=-8182.46$ $T=6.30$ $M_x=7.80$
 $N,Ed=-8182.46$ $Nc,Rd=-36538.20$ $N,Ed/Nc,Rd=0.22$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 89 SLU $X_l=0.04$
Sollecitazioni: $N=-6365.06$ $T=6.30$ $M_x=40.81$
 $V,Ed=6.30$ $Vc,Rd,Red=12799.10$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.69$ - Classe 3
Sollecitazioni: $N=-5388.46$ $M=1.53$ $M_x=34.29$
Tensioni: $\sigma_N=-498.61$ $\sigma_M=-6.86$ $\tau=77.06$ $\sigma_{max}=-505.46$
Tensioni: $\sigma_N=-498.61$ $\sigma_M=5.94$ $\tau=77.06$ $\tau_{max}=77.06$
Tensioni: $\sigma_N=-498.61$ $\sigma_M=-6.86$ $\tau=77.06$ $\sigma_{ID,max}=522.79$

Asta n. 2025 (1901 -5437) Tubo circolare $d=90 \times 4$ mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 75 SLU - Classe 1
Sollecitazioni: $N,Ed=-8535.82$ $M,Ed=2.06$
Resistenze: $Nc,Rd=36538.20$ $M,c,Rd=976.45$ $L=134.54$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, \text{----}, \text{----}$
 $\lambda=44.20$ $Ncr=114642.00$ $\lambda^*=0.58$
Curva a: $\Phi=0.71$ $\chi_{,min}=0.90$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=1.04, \text{----}, \text{----}, \text{----}$
Verifica: $0.26+0.00=0.26$
- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,G}=0.02$ (L/7595) $f_{z,L}=0.00$ (L/35155)
- Verifica Freccia massima carichi totali - CC 77
 $f_{z,G}=0.02$ (L/7391) $f_{z,L}=0.01$ (L/9793)
- Verifica a compressione [4.2.9] - CC 75 SLU $X_l=0.04$ - Classe 1
Sollecitazioni: $N=-8535.82$ $T=6.30$ $M_x=-14.75$
 $N,Ed=-8535.82$ $Nc,Rd=-36538.20$ $N,Ed/Nc,Rd=0.23$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 54 SLU $X_l=0.04$
Sollecitazioni: $N=-7973.41$ $T=6.30$ $M_x=-16.67$
 $V,Ed=6.30$ $Vc,Rd,Red=13172.40$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.69$ - Classe 3
Sollecitazioni: $N=-4730.83$ $M=1.53$ $M_x=-20.61$
Tensioni: $\sigma_N=-437.75$ $\sigma_M=-6.86$ $\tau=46.31$ $\sigma_{max}=-444.61$
Tensioni: $\sigma_N=-437.75$ $\sigma_M=6.76$ $\tau=46.31$ $\tau_{max}=46.31$
Tensioni: $\sigma_N=-437.75$ $\sigma_M=-6.86$ $\tau=46.31$ $\sigma_{ID,max}=451.79$

Asta n. 2040 (1901 -5842) Tubo circolare d=90x4 mm - S355 Crit. 3

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 75 SLU - Classe 1
 Sollecitazioni: N,Ed=-6550.73 M,Ed=6.65
 Resistenze: Nc,Rd=36538.20 M,c,Rd=976.45 L=224.41
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, \text{----}, \text{----}$
 $\lambda=73.72 \text{ Ncr}=41210.70 \lambda^*=0.96$
 Curva a: $\Phi=1.05 \chi, \text{min}=0.69$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=1.14, \text{----}, \text{----}, \text{----}$
 Verifica: $0.26+0.01=0.27$
 - Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.02 \text{ (L/13621)} \quad f_{z,l}=0.00 \text{ (L/116461)}$
 - Verifica Freccia massima carichi totali - CC 77
 $f_{z,g}=0.02 \text{ (L/12940)} \quad f_{z,l}=0.01 \text{ (L/25595)}$
 - Verifica a compressione [4.2.9] - CC 75 SLU X1=0.02 - Classe 1
 Sollecitazioni: N=-6550.73 T=11.98 M_x=-23.86
 N,Ed=-6550.73 Nc,Rd=-36538.20 N,Ed/Nc,Rd=0.18
 - Verifica a taglio e torsione dir. Z [4.2.25] - CC 54 SLU X1=0.02
 Sollecitazioni: N=-6401.65 T=11.98 M_x=-31.19
 V,Ed=11.98 Vc,Rd,Red=12947.90 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 9 SND X1=1.13 - Classe 3
 Sollecitazioni: N=-3245.99 M=4.93 M_x=-21.41
 Tensioni: $\sigma_N=-300.36 \quad \sigma_M=-22.15 \quad \tau=48.11 \quad \sigma_{\text{max}}=-322.51$
 Tensioni: $\sigma_N=-300.36 \quad \sigma_M=21.82 \quad \tau=48.11 \quad \tau_{\text{max}}=48.11$
 Tensioni: $\sigma_N=-300.36 \quad \sigma_M=-22.15 \quad \tau=48.11 \quad \sigma_{ID,\text{max}}=333.10$

Asta n. 2041 (1902 -5844) Tubo circolare d=90x4 mm - S355 Crit. 3

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 1
 Sollecitazioni: N,Ed=-6406.51 M,Ed=6.65
 Resistenze: Nc,Rd=36538.20 M,c,Rd=976.45 L=224.41
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, \text{----}, \text{----}$
 $\lambda=73.72 \text{ Ncr}=41210.70 \lambda^*=0.96$
 Curva a: $\Phi=1.05 \chi, \text{min}=0.69$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=1.13, \text{----}, \text{----}, \text{----}$
 Verifica: $0.25+0.01=0.26$
 - Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.02 \text{ (L/13542)} \quad f_{z,l}=0.00 \text{ (L/119447)}$
 - Verifica Freccia massima carichi totali - CC 26
 $f_{z,g}=0.02 \text{ (L/13122)} \quad f_{z,l}=0.01 \text{ (L/26171)}$
 - Verifica a compressione [4.2.9] - CC 49 SLU X1=0.02 - Classe 1
 Sollecitazioni: N=-6406.51 T=11.98 M_x=25.42
 N,Ed=-6406.51 Nc,Rd=-36538.20 N,Ed/Nc,Rd=0.18
 - Verifica a taglio e torsione dir. Z [4.2.25] - CC 89 SLU X1=0.02
 Sollecitazioni: N=-5210.40 T=11.98 M_x=51.21
 V,Ed=11.98 Vc,Rd,Red=12638.40 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.13 - Classe 3
 Sollecitazioni: N=-3485.21 M=4.93 M_x=24.83
 Tensioni: $\sigma_N=-322.49 \quad \sigma_M=-22.15 \quad \tau=55.79 \quad \sigma_{\text{max}}=-344.65$
 Tensioni: $\sigma_N=-322.49 \quad \sigma_M=21.82 \quad \tau=55.79 \quad \tau_{\text{max}}=55.79$
 Tensioni: $\sigma_N=-322.49 \quad \sigma_M=-22.15 \quad \tau=55.79 \quad \sigma_{ID,\text{max}}=357.94$

Asta n. 2066 (-2477 1901) Tubo circolare d=101.6x6 mm - S355 Crit. 3

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-706.52 M,Ed=720.40
 Resistenze: Nc,Rd=60925.30 M,c,Rd=1375.52 L=104.09
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, \text{----}, \text{----}$
 $\lambda=30.74 \text{ Ncr}=395330.00 \lambda^*=0.40$
 Curva a: $\Phi=0.60 \chi, \text{min}=0.95$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, \text{----}, \text{----}, \text{----}$
 Verifica: $0.01+0.22=0.23$
 - Verifica a pressoflessione retta - CC 54 SLU X1=0.84 - Classe 1
 Sollecitazioni: N=-1316.51 T=899.64 M=616.78 M_x=-76.81
 M,Ed=616.78 M,c,Rd=1810.99

N,Ed=-1316.51 Nc,Rd=60925.30 n=N,Ed/Nc,Rd=0.02
 MN,c,Rd=1771.86 M,Ed/MN,c,Rd=0.35

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 54 SLU Xl=0.84
 Sollecitazioni: N=-1316.51 T=899.64 M=616.78 M_x=-76.81
 V,Ed=899.64 Vc,Rd,Red=21311.00 V,Ed/Vc,Rd,Red=0.04
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.84 - Classe 3
 Sollecitazioni: N=-706.52 T=1012.33 M=720.40 M_x=-123.56
 Tensioni: σ_N =-39.21 σ_M =-1770.71 τ =151.86 σ_{max} =-1809.92
 Tensioni: σ_N =-39.21 σ_M =-0.00 τ =263.92 τ_{max} =263.92
 Tensioni: σ_N =-39.21 σ_M =-1770.71 τ =151.86 $\sigma_{ID,max}$ =1828.93

Asta n. 2066 (1901 -2442) Tubo circolare d=101.6x6 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
 Sollecitazioni: N,Ed=-4761.85 M,Ed=554.13
 Resistenze: Nc,Rd=60925.30 M,c,Rd=1375.52 L=104.09
 α_{my} , α_{mz} , α_{LT} =0.95, ----, ----
 λ =30.74 Ncr=395326.00 λ^* =0.40
 Curva a: Φ =0.60 χ ,min=0.95
 Kyy, Kyz, Kzy, Kzz=0.97, ----, ----, ----
 Verifica: 0.08+0.35=0.43
- Verifica a pressoflessione retta - CC 54 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=8866.69 T=1251.88 M=1002.94 M_x=61.35
 M,Ed=1002.94 M,c,Rd=1810.99
 N,Ed=8866.69 Nc,Rd=60925.30 n=N,Ed/Nc,Rd=0.15
 MN,c,Rd=1547.43 M,Ed/MN,c,Rd=0.65

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 54 SLU Xl=0.00
 Sollecitazioni: N=8866.69 T=1251.88 M=1002.94 M_x=61.35
 V,Ed=1251.88 Vc,Rd,Red=21529.00 V,Ed/Vc,Rd,Red=0.06

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=10300.70 T=688.93 M=554.13 M_x=62.32
 Tensioni: σ_N =571.62 σ_M =1362.02 τ =76.59 σ_{max} =1933.64
 Tensioni: σ_N =571.62 σ_M =-0.00 τ =152.85 τ_{max} =152.85
 Tensioni: σ_N =571.62 σ_M =1362.02 τ =76.59 $\sigma_{ID,max}$ =1938.18

Asta n. 2066 (-2442 -2426) Tubo circolare d=101.6x6 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
 Sollecitazioni: N,Ed=-2818.47 M,Ed=82.50
 Resistenze: Nc,Rd=60925.30 M,c,Rd=1375.52 L=104.09
 α_{my} , α_{mz} , α_{LT} =0.95, ----, ----
 λ =30.74 Ncr=395327.00 λ^* =0.40
 Curva a: Φ =0.60 χ ,min=0.95
 Kyy, Kyz, Kzy, Kzz=0.96, ----, ----, ----
 Verifica: 0.05+0.05=0.10
- Verifica a pressoflessione retta - CC 54 SLU Xl=1.04 - Classe 1
 Sollecitazioni: N=15555.30 T=94.61 M=157.62 M_x=-124.80
 M,Ed=157.62 M,c,Rd=1810.99
 N,Ed=15555.30 Nc,Rd=60925.30 n=N,Ed/Nc,Rd=0.26
 MN,c,Rd=1348.61 M,Ed/MN,c,Rd=0.12

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 54 SLU Xl=0.00
 Sollecitazioni: N=15555.50 T=149.44 M=32.91 M_x=-124.80
 V,Ed=149.44 Vc,Rd,Red=20634.40 V,Ed/Vc,Rd,Red=0.01

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=1.04 - Classe 3
 Sollecitazioni: N=12398.40 T=70.96 M=82.50 M_x=-78.22
 Tensioni: σ_N =688.03 σ_M =202.79 τ =96.13 σ_{max} =890.81
 Tensioni: σ_N =688.03 σ_M =-0.00 τ =103.99 τ_{max} =103.99
 Tensioni: σ_N =688.03 σ_M =202.79 τ =96.13 $\sigma_{ID,max}$ =906.24

Asta n. 2066 (-2426 -2363) Tubo circolare d=101.6x6 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
 Sollecitazioni: N,Ed=-1526.50 M,Ed=72.52
 Resistenze: Nc,Rd=60925.30 M,c,Rd=1375.52 L=104.19
 α_{my} , α_{mz} , α_{LT} =0.95, ----, ----
 λ =30.76 Ncr=394643.00 λ^* =0.40
 Curva a: Φ =0.60 χ ,min=0.95
 Kyy, Kyz, Kzy, Kzz=0.96, ----, ----, ----

Verifica: $0.03+0.04=0.07$

- Verifica a pressoflessione retta - CC 54 SLU $X_l=1.04$ - Classe 1
 Sollecitazioni: $N=20258.30$ $T=116.01$ $M=122.14$ $M_x=-94.79$
 $M, Ed=122.14$ $M, c, Rd=1810.99$
 $N, Ed=20258.30$ $Nc, Rd=60925.30$ $n=N, Ed/Nc, Rd=0.33$
 $MN, c, Rd=1208.82$ $M, Ed/MN, c, Rd=0.10$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 75 SLU $X_l=0.00$
 Sollecitazioni: $N=20478.50$ $T=144.01$ $M=79.33$ $M_x=-68.20$
 $V, Ed=144.01$ $Vc, Rd, Red=21432.40$ $V, Ed/Vc, Rd, Red=0.01$
- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_l=1.04$ - Classe 3
 Sollecitazioni: $N=13922.00$ $T=59.54$ $M=70.03$ $M_x=-60.80$
 Tensioni: $\sigma_N=772.58$ $\sigma_M=172.14$ $\tau=74.72$ $\sigma_{max}=944.72$
 Tensioni: $\sigma_N=772.58$ $\sigma_M=-0.00$ $\tau=81.31$ $\tau_{max}=81.31$
 Tensioni: $\sigma_N=772.58$ $\sigma_M=172.14$ $\tau=74.72$ $\sigma_{ID, max}=953.54$

Asta n. 2066 (-2363 -2360) Tubo circolare $d=114.3 \times 6$ mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
 Sollecitazioni: $N, Ed=-543.10$ $M, Ed=92.28$
 Resistenze: $Nc, Rd=69019.00$ $M, c, Rd=1776.03$ $L=103.77$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, \text{----}, \text{----}$
 $\lambda=27.06$ $Ncr=577863.00$ $\lambda^*=0.35$
 Curva a: $\Phi=0.58$ $\chi, \text{min}=0.96$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, \text{----}, \text{----}, \text{----}$
 Verifica: $0.01+0.04=0.05$

- Verifica a pressoflessione retta - CC 54 SLU $X_l=1.04$ - Classe 1
 Sollecitazioni: $N=23853.30$ $T=131.41$ $M=146.85$ $M_x=-70.57$
 $M, Ed=146.85$ $M, c, Rd=2323.44$
 $N, Ed=23853.30$ $Nc, Rd=69019.00$ $n=N, Ed/Nc, Rd=0.35$
 $MN, c, Rd=1520.45$ $M, Ed/MN, c, Rd=0.10$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 75 SLU $X_l=0.00$
 Sollecitazioni: $N=24038.60$ $T=165.80$ $M=60.98$ $M_x=-53.16$
 $V, Ed=165.80$ $Vc, Rd, Red=24711.30$ $V, Ed/Vc, Rd, Red=0.01$
- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_l=1.04$ - Classe 3
 Sollecitazioni: $N=15074.20$ $T=69.57$ $M=88.25$ $M_x=-44.92$
 Tensioni: $\sigma_N=738.42$ $\sigma_M=168.00$ $\tau=42.75$ $\sigma_{max}=906.42$
 Tensioni: $\sigma_N=738.42$ $\sigma_M=-0.00$ $\tau=49.55$ $\tau_{max}=49.55$
 Tensioni: $\sigma_N=738.42$ $\sigma_M=168.00$ $\tau=42.75$ $\sigma_{ID, max}=909.44$

Asta n. 2066 (-2360 -2356) Tubo circolare $d=114.3 \times 6$ mm - S355 Crit. 3

- Verifica a pressoflessione retta - CC 54 SLU $X_l=1.04$ - Classe 1
 Sollecitazioni: $N=25708.20$ $T=54.53$ $M=97.08$ $M_x=-54.52$
 $M, Ed=97.08$ $M, c, Rd=2323.44$
 $N, Ed=25708.20$ $Nc, Rd=69019.00$ $n=N, Ed/Nc, Rd=0.37$
 $MN, c, Rd=1458.00$ $M, Ed/MN, c, Rd=0.07$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 74 SLU $X_l=0.00$
 Sollecitazioni: $N=20202.60$ $T=71.22$ $M=53.10$ $M_x=-33.97$
 $V, Ed=71.22$ $Vc, Rd, Red=24948.60$ $V, Ed/Vc, Rd, Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_l=1.04$ - Classe 3
 Sollecitazioni: $N=15345.20$ $T=32.66$ $M=71.89$ $M_x=-28.25$
 Tensioni: $\sigma_N=751.70$ $\sigma_M=136.85$ $\tau=26.89$ $\sigma_{max}=888.55$
 Tensioni: $\sigma_N=751.70$ $\sigma_M=-0.00$ $\tau=30.08$ $\tau_{max}=30.08$
 Tensioni: $\sigma_N=751.70$ $\sigma_M=136.85$ $\tau=26.89$ $\sigma_{ID, max}=889.77$

Asta n. 2066 (-2356 -2351) Tubo circolare $d=114.3 \times 6$ mm - S355 Crit. 3

- Verifica a pressoflessione retta - CC 37 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $N=16840.70$ $T=78.25$ $M=107.71$ $M_x=19.17$
 $M, Ed=107.71$ $M, c, Rd=2323.44$
 $N, Ed=16840.70$ $Nc, Rd=69019.00$ $n=N, Ed/Nc, Rd=0.24$
 $MN, c, Rd=1756.52$ $M, Ed/MN, c, Rd=0.06$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 37 SLU $X_l=1.04$
 Sollecitazioni: $N=16840.60$ $T=95.46$ $M=20.90$ $M_x=19.17$
 $V, Ed=95.46$ $Vc, Rd, Red=25131.80$ $V, Ed/Vc, Rd, Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_l=0.00$ - Classe 3

Sollecitazioni: $N=14975.80$ $T=48.06$ $M=69.34$ $M_x=-20.78$
 Tensioni: $\sigma_N=733.60$ $\sigma_M=131.99$ $\tau=19.78$ $\sigma_{max}=865.59$
 Tensioni: $\sigma_N=733.60$ $\sigma_M=-0.00$ $\tau=24.48$ $\tau_{max}=24.48$
 Tensioni: $\sigma_N=733.60$ $\sigma_M=131.99$ $\tau=19.78$ $\sigma_{ID,max}=866.27$

Asta n. 2535 (2401 -9374) Tubo circolare $d=90 \times 4$ mm - S355 Crit. 3

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 75 SLU - Classe 1
 Sollecitazioni: $N, Ed=-6992.12$ $M, Ed=5.56$
 Resistenze: $N_c, Rd=36538.20$ $M, c, Rd=976.45$ $L=224.40$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, \text{----}, \text{----}$
 $\lambda=73.72$ $N_{cr}=41210.70$ $\lambda^*=0.96$
 Curva a: $\Phi=1.05$ $\chi, \min=0.69$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=1.15, \text{----}, \text{----}, \text{----}$
 Verifica: $0.28+0.01=0.28$
 - Verifica Freccia massima per soli carichi accidentali - CC 26
 $f_{z,L}=0.04$ (L/4806) $f_{z,G}=0.04$ (L/5017)
 - Verifica Freccia massima carichi totali - CC 26
 $f_{z,L}=0.07$ (L/2764) $f_{z,G}=0.07$ (L/2885)
 - Verifica a compressione [4.2.9] - CC 75 SLU $X_1=0.23$ - Classe 1
 Sollecitazioni: $N=-6992.12$ $T=11.05$ $M_x=33.43$
 $N, Ed=-6992.12$ $N_c, Rd=-36538.20$ $N, Ed/N_c, Rd=0.19$
 - Verifica a taglio e torsione dir. Z [4.2.25] - CC 54 SLU $X_1=0.23$
 Sollecitazioni: $N=-6928.79$ $T=11.05$ $M_x=41.25$
 $V, Ed=11.05$ $V_c, Rd, Red=12792.40$ $V, Ed/V_c, Rd, Red=0.00$
 - Verifica in termini tensionali [4.2.4] - CC 9 SND $X_1=1.24$ - Classe 3
 Sollecitazioni: $N=-3525.31$ $M=4.12$ $M_x=22.32$
 Tensioni: $\sigma_N=-326.20$ $\sigma_M=-18.52$ $\tau=50.16$ $\sigma_{max}=-344.72$
 Tensioni: $\sigma_N=-326.20$ $\sigma_M=18.24$ $\tau=50.16$ $\tau_{max}=50.16$
 Tensioni: $\sigma_N=-326.20$ $\sigma_M=-18.52$ $\tau=50.16$ $\sigma_{ID,max}=355.50$

Asta n. 2536 (2402 -9376) Tubo circolare $d=90 \times 4$ mm - S355 Crit. 3

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 54 SLU - Classe 1
 Sollecitazioni: $N, Ed=-6953.42$ $M, Ed=5.56$
 Resistenze: $N_c, Rd=36538.20$ $M, c, Rd=976.45$ $L=224.40$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, \text{----}, \text{----}$
 $\lambda=73.72$ $N_{cr}=41210.70$ $\lambda^*=0.96$
 Curva a: $\Phi=1.05$ $\chi, \min=0.69$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=1.15, \text{----}, \text{----}, \text{----}$
 Verifica: $0.28+0.01=0.28$
 - Verifica Freccia massima per soli carichi accidentali - CC 26
 $f_{z,L}=0.04$ (L/4806) $f_{z,G}=0.04$ (L/5017)
 - Verifica Freccia massima carichi totali - CC 26
 $f_{z,L}=0.07$ (L/2763) $f_{z,G}=0.07$ (L/2884)
 - Verifica a compressione [4.2.9] - CC 54 SLU $X_1=0.23$ - Classe 1
 Sollecitazioni: $N=-6953.42$ $T=11.05$ $M_x=-26.79$
 $N, Ed=-6953.42$ $N_c, Rd=-36538.20$ $N, Ed/N_c, Rd=0.19$
 - Verifica a taglio e torsione dir. Z [4.2.25] - CC 89 SLU $X_1=0.23$
 Sollecitazioni: $N=-5204.43$ $T=11.05$ $M_x=-53.72$
 $V, Ed=11.05$ $V_c, Rd, Red=12599.60$ $V, Ed/V_c, Rd, Red=0.00$
 - Verifica in termini tensionali [4.2.4] - CC 9 SND $X_1=1.24$ - Classe 3
 Sollecitazioni: $N=-3749.15$ $M=4.12$ $M_x=-25.73$
 Tensioni: $\sigma_N=-346.92$ $\sigma_M=-18.52$ $\tau=57.82$ $\sigma_{max}=-365.44$
 Tensioni: $\sigma_N=-346.92$ $\sigma_M=-18.24$ $\tau=57.82$ $\tau_{max}=57.82$
 Tensioni: $\sigma_N=-346.92$ $\sigma_M=-18.52$ $\tau=57.82$ $\sigma_{ID,max}=378.91$

Asta n. 2541 (2401 -9727) Tubo circolare $d=90 \times 4$ mm - S355 Crit. 3

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 75 SLU - Classe 1
 Sollecitazioni: $N, Ed=-10440.40$ $M, Ed=1.55$
 Resistenze: $N_c, Rd=36538.20$ $M, c, Rd=976.45$ $L=134.54$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, \text{----}, \text{----}$
 $\lambda=44.20$ $N_{cr}=114643.00$ $\lambda^*=0.58$
 Curva a: $\Phi=0.71$ $\chi, \min=0.90$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=1.06, \text{----}, \text{----}, \text{----}$

Verifica: $0.32+0.00=0.32$

- Verifica Freccia massima per soli carichi accidentali - CC 26
 $f_{z,l}=0.04$ (L/2916) $f_{z,g}=0.03$ (L/3364)
- Verifica Freccia massima carichi totali - CC 26
 $f_{z,l}=0.07$ (L/1678) $f_{z,g}=0.06$ (L/1936)
- Verifica a compressione [4.2.9] - CC 75 SLU $Xl=0.23$ - Classe 1
 Sollecitazioni: $N=-10440.40$ $T=5.54$ $M_x=44.37$
 $N,Ed=-10440.40$ $Nc,Rd=-36538.20$ $N,Ed/Nc,Rd=0.29$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 54 SLU $Xl=0.23$
 Sollecitazioni: $N=-10127.80$ $T=5.54$ $M_x=51.45$
 $V,Ed=5.54$ $Vc,Rd,Red=12634.70$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 9 SND $Xl=0.79$ - Classe 3
 Sollecitazioni: $N=-5146.86$ $M=1.14$ $M_x=24.44$
 Tensioni: $\sigma_N=-476.25$ $\sigma_M=-5.15$ $\tau=54.93$ $\sigma_{max}=-481.39$
 Tensioni: $\sigma_N=-476.25$ $\sigma_M=3.94$ $\tau=54.93$ $\tau_{max}=54.93$
 Tensioni: $\sigma_N=-476.25$ $\sigma_M=-5.15$ $\tau=54.93$ $\sigma_{TD,max}=490.71$

Asta n. 2542 (2402 -9740) Tubo circolare $d=90 \times 4$ mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 54 SLU - Classe 1
 Sollecitazioni: $N,Ed=-10340.30$ $M,Ed=1.55$
 Resistenze: $Nc,Rd=36538.20$ $M,c,Rd=976.45$ $L=134.54$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, \text{----}, \text{----}$
 $\lambda=44.20$ $Ncr=114643.00$ $\lambda^*=0.58$
 Curva a: $\Phi=0.71$ $\chi_{,min}=0.90$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=1.06, \text{----}, \text{----}, \text{----}$
 Verifica: $0.32+0.00=0.32$

- Verifica Freccia massima per soli carichi accidentali - CC 26
 $f_{z,l}=0.04$ (L/2916) $f_{z,g}=0.03$ (L/3367)
- Verifica Freccia massima carichi totali - CC 26
 $f_{z,l}=0.07$ (L/1679) $f_{z,g}=0.06$ (L/1938)
- Verifica a compressione [4.2.9] - CC 54 SLU $Xl=0.23$ - Classe 1
 Sollecitazioni: $N=-10340.30$ $T=5.54$ $M_x=-36.63$
 $N,Ed=-10340.30$ $Nc,Rd=-36538.20$ $N,Ed/Nc,Rd=0.28$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 89 SLU $Xl=0.23$
 Sollecitazioni: $N=-7640.38$ $T=5.54$ $M_x=-53.61$
 $V,Ed=5.54$ $Vc,Rd,Red=12601.30$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 9 SND $Xl=0.79$ - Classe 3
 Sollecitazioni: $N=-5385.66$ $M=1.14$ $M_x=-27.35$
 Tensioni: $\sigma_N=-498.35$ $\sigma_M=-5.15$ $\tau=61.45$ $\sigma_{max}=-503.49$
 Tensioni: $\sigma_N=-498.35$ $\sigma_M=4.46$ $\tau=61.45$ $\tau_{max}=61.45$
 Tensioni: $\sigma_N=-498.35$ $\sigma_M=-5.15$ $\tau=61.45$ $\sigma_{TD,max}=514.62$

Asta n. 2590 (-2351 -2408) Tubo circolare $d=114.3 \times 6$ mm - S355 Crit. 3

- Verifica a pressoflessione retta - CC 54 SLU $Xl=1.04$ - Classe 1
 Sollecitazioni: $N=26094.60$ $T=18.80$ $M=98.09$ $M_x=4.85$
 $M,Ed=98.09$ $M,c,Rd=2323.44$
 $N,Ed=26094.60$ $Nc,Rd=69019.00$ $n=N,Ed/Nc,Rd=0.38$
 $MN,c,Rd=1445.00$ $M,Ed/MN,c,Rd=0.07$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 54 SLU $Xl=0.00$
 Sollecitazioni: $N=26093.00$ $T=77.06$ $M=53.41$ $M_x=4.85$
 $V,Ed=77.06$ $Vc,Rd,Red=25308.90$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 9 SND $Xl=1.04$ - Classe 3
 Sollecitazioni: $N=14955.10$ $T=28.19$ $M=46.81$ $M_x=21.64$
 Tensioni: $\sigma_N=732.59$ $\sigma_M=89.12$ $\tau=20.60$ $\sigma_{max}=821.71$
 Tensioni: $\sigma_N=732.59$ $\sigma_M=-0.00$ $\tau=23.36$ $\tau_{max}=23.36$
 Tensioni: $\sigma_N=732.59$ $\sigma_M=89.12$ $\tau=20.60$ $\sigma_{TD,max}=822.48$

Asta n. 2590 (-2408 -2437) Tubo circolare $d=114.3 \times 6$ mm - S355 Crit. 3

- Verifica a pressoflessione retta - CC 54 SLU $Xl=0.00$ - Classe 1
 Sollecitazioni: $N=26609.40$ $T=16.85$ $M=110.56$ $M_x=42.53$
 $M,Ed=110.56$ $M,c,Rd=2323.44$

N,Ed=26609.40 Nc,Rd=69019.00 n=N,Ed/Nc,Rd=0.39
MN,c,Rd=1427.67 M,Ed/MN,c,Rd=0.08

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 53 SLU Xl=1.04
Sollecitazioni: N=20423.40 T=69.81 M=57.52 M_x=40.71
V,Ed=69.81 Vc,Rd,Red=24865.30 V,Ed/Vc,Rd,Red=0.00
- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
Sollecitazioni: N=14829.10 T=30.60 M=61.68 M_x=35.31
Tensioni: $\sigma_N=726.42$ $\sigma_M=117.42$ $\tau=33.61$ $\sigma_{max}=843.84$
Tensioni: $\sigma_N=726.42$ $\sigma_M=-0.00$ $\tau=36.60$ $\tau_{max}=36.60$
Tensioni: $\sigma_N=726.42$ $\sigma_M=117.42$ $\tau=33.61$ $\sigma_{ID,max}=845.84$

Asta n. 2590 (-2437 -2463) Tubo circolare d=114.3x6 mm - S355 Crit. 3

- Verifica a pressoflessione retta - CC 54 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=25754.70 T=100.50 M=131.54 M_x=61.32
M,Ed=131.54 M,c,Rd=2323.44
N,Ed=25754.70 Nc,Rd=69019.00 n=N,Ed/Nc,Rd=0.37
MN,c,Rd=1456.44 M,Ed/MN,c,Rd=0.09
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 75 SLU Xl=1.04
Sollecitazioni: N=25935.90 T=134.85 M=39.77 M_x=45.07
V,Ed=134.85 Vc,Rd,Red=24811.40 V,Ed/Vc,Rd,Red=0.01
- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
Sollecitazioni: N=13905.90 T=61.13 M=68.01 M_x=43.37
Tensioni: $\sigma_N=681.19$ $\sigma_M=129.47$ $\tau=41.28$ $\sigma_{max}=810.66$
Tensioni: $\sigma_N=681.19$ $\sigma_M=-0.00$ $\tau=47.26$ $\tau_{max}=47.26$
Tensioni: $\sigma_N=681.19$ $\sigma_M=129.47$ $\tau=41.28$ $\sigma_{ID,max}=813.80$

Asta n. 2590 (-2463 -2486) Tubo circolare d=101.6x6 mm - S355 Crit. 3

- Verifica a pressoflessione retta - CC 54 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=23158.20 T=135.64 M=111.22 M_x=79.75
M,Ed=111.22 M,c,Rd=1810.99
N,Ed=23158.20 Nc,Rd=60925.30 n=N,Ed/Nc,Rd=0.38
MN,c,Rd=1122.62 M,Ed/MN,c,Rd=0.10
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 75 SLU Xl=1.04
Sollecitazioni: N=23394.70 T=163.96 M=81.65 M_x=58.97
V,Ed=163.96 Vc,Rd,Red=21562.60 V,Ed/Vc,Rd,Red=0.01
- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
Sollecitazioni: N=12155.70 T=72.16 M=54.12 M_x=48.38
Tensioni: $\sigma_N=674.56$ $\sigma_M=133.03$ $\tau=59.46$ $\sigma_{max}=807.60$
Tensioni: $\sigma_N=674.56$ $\sigma_M=-0.00$ $\tau=67.45$ $\tau_{max}=67.45$
Tensioni: $\sigma_N=674.56$ $\sigma_M=133.03$ $\tau=59.46$ $\sigma_{ID,max}=814.14$

Asta n. 2590 (-2486 -2541) Tubo circolare d=101.6x6 mm - S355 Crit. 3

- Verifica a pressoflessione retta - CC 75 SLU Xl=1.04 - Classe 1
Sollecitazioni: N=19685.70 T=90.48 M=139.43 M_x=82.48
M,Ed=139.43 M,c,Rd=1810.99
N,Ed=19685.70 Nc,Rd=60925.30 n=N,Ed/Nc,Rd=0.32
MN,c,Rd=1225.84 M,Ed/MN,c,Rd=0.11
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 75 SLU Xl=0.00
Sollecitazioni: N=19680.10 T=143.47 M=106.13 M_x=82.48
V,Ed=143.47 Vc,Rd,Red=21231.00 V,Ed/Vc,Rd,Red=0.01
- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=1.04 - Classe 3
Sollecitazioni: N=9932.25 T=61.05 M=74.04 M_x=60.50
Tensioni: $\sigma_N=551.17$ $\sigma_M=181.99$ $\tau=74.35$ $\sigma_{max}=733.16$
Tensioni: $\sigma_N=551.17$ $\sigma_M=-0.00$ $\tau=81.11$ $\tau_{max}=81.11$
Tensioni: $\sigma_N=551.17$ $\sigma_M=181.99$ $\tau=74.35$ $\sigma_{ID,max}=744.38$

Asta n. 2590 (-2541 2401) Tubo circolare d=101.6x6 mm - S355 Crit. 3

- Verifica a pressoflessione retta - CC 54 SLU Xl=0.84 - Classe 1
Sollecitazioni: N=13498.00 T=1789.25 M=1131.48 M_x=-4.35
M,Ed=1131.48 M,c,Rd=1810.99
N,Ed=13498.00 Nc,Rd=60925.30 n=N,Ed/Nc,Rd=0.22
MN,c,Rd=1409.76 M,Ed/MN,c,Rd=0.80
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 54 SLU Xl=0.84

Sollecitazioni: N=13498.00 T=1789.25 M=1131.48 $M_x=-4.35$
V,Ed=1789.25 Vc,Rd,Red=22332.60 V,Ed/Vc,Rd,Red=0.08

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_l=0.84$ - Classe 3
Sollecitazioni: N=6722.08 T=843.66 M=541.38 $M_x=-31.43$
Tensioni: $\sigma_N=373.03$ $\sigma_M=1330.69$ $\tau=38.63$ $\sigma_{max}=1703.72$
Tensioni: $\sigma_N=373.03$ $\sigma_M=-0.00$ $\tau=132.02$ $\tau_{max}=132.02$
Tensioni: $\sigma_N=373.03$ $\sigma_M=1330.69$ $\tau=38.63$ $\sigma_{ID,max}=1705.03$

Asta n. 2597 (-2352 -2409) Tubo circolare d=114.3x6 mm - S355 Crit. 3

- Verifica a pressoflessione retta - CC 75 SLU $X_l=1.04$ - Classe 1
Sollecitazioni: N=25772.60 T=35.93 M=95.86 $M_x=-1.69$
M,Ed=95.86 M,c,Rd=2323.44
N,Ed=25772.60 Nc,Rd=69019.00 n=N,Ed/Nc,Rd=0.37
MN,c,Rd=1455.84 M,Ed/MN,c,Rd=0.07
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 53 SLU $X_l=1.04$
Sollecitazioni: N=19560.60 T=83.29 M=69.53 $M_x=6.38$
V,Ed=83.29 Vc,Rd,Red=25289.90 V,Ed/Vc,Rd,Red=0.00
- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_l=1.04$ - Classe 3
Sollecitazioni: N=15696.00 T=29.72 M=49.21 $M_x=-26.33$
Tensioni: $\sigma_N=768.88$ $\sigma_M=93.67$ $\tau=25.06$ $\sigma_{max}=862.55$
Tensioni: $\sigma_N=768.88$ $\sigma_M=-0.00$ $\tau=27.97$ $\tau_{max}=27.97$
Tensioni: $\sigma_N=768.88$ $\sigma_M=93.67$ $\tau=25.06$ $\sigma_{ID,max}=863.64$

Asta n. 2597 (-2409 -2438) Tubo circolare d=114.3x6 mm - S355 Crit. 3

- Verifica a pressoflessione retta - CC 75 SLU $X_l=0.00$ - Classe 1
Sollecitazioni: N=26279.70 T=32.67 M=107.07 $M_x=-34.34$
M,Ed=107.07 M,c,Rd=2323.44
N,Ed=26279.70 Nc,Rd=69019.00 n=N,Ed/Nc,Rd=0.38
MN,c,Rd=1438.76 M,Ed/MN,c,Rd=0.07
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 115 SLU $X_l=1.04$
Sollecitazioni: N=9725.80 T=58.23 M=26.98 $M_x=-27.14$
V,Ed=58.23 Vc,Rd,Red=25033.20 V,Ed/Vc,Rd,Red=0.00
- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_l=0.00$ - Classe 3
Sollecitazioni: N=15633.70 T=31.81 M=67.51 $M_x=-44.57$
Tensioni: $\sigma_N=765.83$ $\sigma_M=128.51$ $\tau=42.42$ $\sigma_{max}=894.34$
Tensioni: $\sigma_N=765.83$ $\sigma_M=-0.00$ $\tau=45.53$ $\tau_{max}=45.53$
Tensioni: $\sigma_N=765.83$ $\sigma_M=128.51$ $\tau=42.42$ $\sigma_{ID,max}=897.36$

Asta n. 2597 (-2438 -2464) Tubo circolare d=114.3x6 mm - S355 Crit. 3

- Verifica a pressoflessione retta - CC 75 SLU $X_l=0.00$ - Classe 1
Sollecitazioni: N=25428.80 T=108.28 M=126.03 $M_x=-49.49$
M,Ed=126.03 M,c,Rd=2323.44
N,Ed=25428.80 Nc,Rd=69019.00 n=N,Ed/Nc,Rd=0.37
MN,c,Rd=1467.41 M,Ed/MN,c,Rd=0.09
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 25 SLU $X_l=1.04$
Sollecitazioni: N=24804.30 T=111.06 M=37.98 $M_x=-45.66$
V,Ed=111.06 Vc,Rd,Red=24804.10 V,Ed/Vc,Rd,Red=0.00
- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_l=0.00$ - Classe 3
Sollecitazioni: N=14660.20 T=68.44 M=75.80 $M_x=-52.39$
Tensioni: $\sigma_N=718.14$ $\sigma_M=144.31$ $\tau=49.87$ $\sigma_{max}=862.45$
Tensioni: $\sigma_N=718.14$ $\sigma_M=-0.00$ $\tau=56.56$ $\tau_{max}=56.56$
Tensioni: $\sigma_N=718.14$ $\sigma_M=144.31$ $\tau=49.87$ $\sigma_{ID,max}=866.76$

Asta n. 2597 (-2464 -2487) Tubo circolare d=101.6x6 mm - S355 Crit. 3

- Verifica a pressoflessione retta - CC 75 SLU $X_l=0.00$ - Classe 1
Sollecitazioni: N=22863.80 T=150.13 M=109.92 $M_x=-64.77$
M,Ed=109.92 M,c,Rd=1810.99
N,Ed=22863.80 Nc,Rd=60925.30 n=N,Ed/Nc,Rd=0.38
MN,c,Rd=1131.37 M,Ed/MN,c,Rd=0.10
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 75 SLU $X_l=0.00$
Sollecitazioni: N=22863.80 T=150.13 M=109.92 $M_x=-64.77$
V,Ed=150.13 Vc,Rd,Red=21480.80 V,Ed/Vc,Rd,Red=0.01
- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_l=0.00$ - Classe 3

Sollecitazioni: $N=12820.80$ $T=84.75$ $M=61.45$ $M_x=-55.97$
 Tensioni: $\sigma_N=711.47$ $\sigma_M=151.04$ $\tau=68.79$ $\sigma_{max}=862.51$
 Tensioni: $\sigma_N=711.47$ $\sigma_M=-0.00$ $\tau=78.17$ $\tau_{max}=78.17$
 Tensioni: $\sigma_N=711.47$ $\sigma_M=151.04$ $\tau=68.79$ $\sigma_{ID,max}=870.70$

Asta n. 2597 (-2487 -2539) Tubo circolare $d=101.6 \times 6$ mm - S355 Crit. 3

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- Verifica a pressoflessione retta - CC 54 SLU $X1=1.04$ - Classe 1
 Sollecitazioni: $N=19415.10$ $T=110.07$ $M=158.21$ $M_x=-63.63$
 $M,Ed=158.21$ $M,c,Rd=1810.99$
 $N,Ed=19415.10$ $Nc,Rd=60925.30$ $n=N,Ed/Nc,Rd=0.32$
 $MN,c,Rd=1233.88$ $M,Ed/MN,c,Rd=0.13$
 - Verifica a taglio e torsione dir. Z [4.2.25] - CC 75 SLU $X1=1.04$
 Sollecitazioni: $N=19148.30$ $T=145.32$ $M=151.24$ $M_x=-90.31$
 $V,Ed=145.32$ $Vc,Rd,Red=21120.70$ $V,Ed/Vc,Rd,Red=0.01$
 - Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=1.04$ - Classe 3
 Sollecitazioni: $N=10467.50$ $T=78.17$ $M=85.13$ $M_x=-66.79$
 Tensioni: $\sigma_N=580.87$ $\sigma_M=209.24$ $\tau=82.08$ $\sigma_{max}=790.12$
 Tensioni: $\sigma_N=580.87$ $\sigma_M=-0.00$ $\tau=90.73$ $\tau_{max}=90.73$
 Tensioni: $\sigma_N=580.87$ $\sigma_M=209.24$ $\tau=82.08$ $\sigma_{ID,max}=802.80$

Asta n. 2597 (-2539 2402) Tubo circolare $d=101.6 \times 6$ mm - S355 Crit. 3

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- Verifica a pressoflessione retta - CC 75 SLU $X1=0.84$ - Classe 1
 Sollecitazioni: $N=13270.00$ $T=1729.94$ $M=1077.21$ $M_x=5.23$
 $M,Ed=1077.21$ $M,c,Rd=1810.99$
 $N,Ed=13270.00$ $Nc,Rd=60925.30$ $n=N,Ed/Nc,Rd=0.22$
 $MN,c,Rd=1416.54$ $M,Ed/MN,c,Rd=0.76$
 - Verifica a taglio e torsione dir. Z [4.2.25] - CC 75 SLU $X1=0.84$
 Sollecitazioni: $N=13270.00$ $T=1729.94$ $M=1077.21$ $M_x=5.23$
 $V,Ed=1729.94$ $Vc,Rd,Red=22320.30$ $V,Ed/Vc,Rd,Red=0.08$
 - Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.84$ - Classe 3
 Sollecitazioni: $N=7033.25$ $T=952.98$ $M=602.35$ $M_x=20.42$
 Tensioni: $\sigma_N=390.30$ $\sigma_M=1480.54$ $\tau=25.09$ $\sigma_{max}=1870.84$
 Tensioni: $\sigma_N=390.30$ $\sigma_M=-0.00$ $\tau=130.58$ $\tau_{max}=130.58$
 Tensioni: $\sigma_N=390.30$ $\sigma_M=1480.54$ $\tau=25.09$ $\sigma_{ID,max}=1871.35$

Asta n. 2819 (1901 -2497) Tubo $80 \times 100 \times (2 \times 5 + 6)$ mm - S355 (32) Crit. 3

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N,Ed=-8453.39$ $M_y,Ed=3317.17$ $M_z,Ed=457.65$
 Resistenze: $Nc,Rd=88716.20$ $M_y,c,Rd=2370.44$ $M_z,c,Rd=2055.33$ $L=18.69$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=5.11$ $Ncr,y=20801700.00$ $\lambda^*_y=0.07$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.14$ $Ncr,z=14429200.00$ $\lambda^*_z=0.08$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.10+1.33+0.21=1.64$
 Verifica ZZ: $0.10+1.07+0.21=1.38$
 - Verifica in termini tensionali [4.2.4] - CC 54 SLU $X1=0.05$ - Classe 3
 Sollecitazioni: $N=-3320.41$ $T_x=7673.63$ $M_y=2876.37$ $T_y=-1364.15$ $M_z=710.88$ $M_x=-62.85$
 Tensioni: $\sigma_N=-126.54$ $\sigma_M=-5271.94$ $\tau=59.30$ $\sigma_{max}=-5398.48$
 Tensioni: $\sigma_N=-126.54$ $\sigma_M=-935.50$ $\tau=655.34$ $\tau_{max}=655.34$
 Tensioni: $\sigma_N=-126.54$ $\sigma_M=-5271.94$ $\tau=59.30$ $\sigma_{ID,max}=5399.45$
 - Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.05$ - Classe 3
 Sollecitazioni: $N=-8453.39$ $T_x=8782.01$ $M_y=3317.17$ $T_y=-942.93$ $M_z=457.65$ $M_x=-51.77$
 Tensioni: $\sigma_N=-322.16$ $\sigma_M=-5484.08$ $\tau=48.85$ $\sigma_{max}=-5806.24$
 Tensioni: $\sigma_N=-322.16$ $\sigma_M=-602.25$ $\tau=730.84$ $\tau_{max}=730.84$
 Tensioni: $\sigma_N=-322.16$ $\sigma_M=-5484.08$ $\tau=48.85$ $\sigma_{ID,max}=5806.86$

Asta n. 2819 (-2478 1902) Tubo circolare $d=101.6 \times 6$ mm - S355 Crit. 3

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N,Ed=-1166.72$ $M,Ed=370.42$
 Resistenze: $Nc,Rd=60925.30$ $M,c,Rd=1375.52$ $L=104.15$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, ---, ---$
 $\lambda=30.75$ $Ncr=394897.00$ $\lambda^*=0.40$
 Curva a: $\Phi=0.60$ $\chi_{min}=0.95$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, ---, ---, ---$
 Verifica: $0.02+0.19=0.21$

- Verifica a pressoflessione retta - CC 68 SLU $X_1=0.84$ - Classe 1
 Sollecitazioni: $N=-1606.62$ $T=699.52$ $M=486.36$ $M_x=31.92$
 $M, Ed=486.36$ $M, c, Rd=1810.99$
 $N, Ed=-1606.62$ $Nc, Rd=60925.30$ $n=N, Ed/Nc, Rd=0.03$
 $MN, c, Rd=1763.23$ $M, Ed/MN, c, Rd=0.28$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 68 SLU $X_1=0.00$
 Sollecitazioni: $N=-1604.99$ $T=731.85$ $M=124.33$ $M_x=31.92$
 $V, Ed=731.85$ $Vc, Rd, Red=21943.80$ $V, Ed/Vc, Rd, Red=0.03$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.84$ - Classe 3
 Sollecitazioni: $N=-1166.72$ $T=535.08$ $M=370.42$ $M_x=109.51$
 Tensioni: $\sigma_N=-64.75$ $\sigma_M=-910.46$ $\tau=134.58$ $\sigma_{max}=-975.21$
 Tensioni: $\sigma_N=-64.75$ $\sigma_M=-0.00$ $\tau=193.81$ $\tau_{max}=193.81$
 Tensioni: $\sigma_N=-64.75$ $\sigma_M=-910.46$ $\tau=134.58$ $\sigma_{ID, max}=1002.68$

Asta n. 2819 (1902 -2441) Tubo circolare $d=101.6 \times 6$ mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
 Sollecitazioni: $N, Ed=-5067.82$ $M, Ed=589.93$
 Resistenze: $Nc, Rd=60925.30$ $M, c, Rd=1375.52$ $L=104.11$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, \text{----}, \text{----}$
 $\lambda=30.74$ $Ncr=395194.00$ $\lambda^*=0.40$
 Curva a: $\Phi=0.60$ $\chi, \min=0.95$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.97, \text{----}, \text{----}, \text{----}$
 Verifica: $0.08+0.37=0.46$

- Verifica a pressoflessione retta - CC 75 SLU $X_1=0.00$ - Classe 1
 Sollecitazioni: $N=8817.24$ $T=1120.21$ $M=913.07$ $M_x=-59.68$
 $M, Ed=913.07$ $M, c, Rd=1810.99$
 $N, Ed=8817.24$ $Nc, Rd=60925.30$ $n=N, Ed/Nc, Rd=0.14$
 $MN, c, Rd=1548.90$ $M, Ed/MN, c, Rd=0.59$

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 75 SLU $X_1=0.00$
 Sollecitazioni: $N=8817.24$ $T=1120.21$ $M=913.07$ $M_x=-59.68$
 $V, Ed=1120.21$ $Vc, Rd, Red=21552.50$ $V, Ed/Vc, Rd, Red=0.05$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=10674.00$ $T=709.31$ $M=589.93$ $M_x=-66.30$
 Tensioni: $\sigma_N=592.34$ $\sigma_M=1450.01$ $\tau=81.48$ $\sigma_{max}=2042.34$
 Tensioni: $\sigma_N=592.34$ $\sigma_M=-0.00$ $\tau=160.00$ $\tau_{max}=160.00$
 Tensioni: $\sigma_N=592.34$ $\sigma_M=1450.01$ $\tau=81.48$ $\sigma_{ID, max}=2047.21$

Asta n. 2819 (-2441 -2427) Tubo circolare $d=101.6 \times 6$ mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
 Sollecitazioni: $N, Ed=-3398.79$ $M, Ed=86.98$
 Resistenze: $Nc, Rd=60925.30$ $M, c, Rd=1375.52$ $L=104.08$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, \text{----}, \text{----}$
 $\lambda=30.73$ $Ncr=395457.00$ $\lambda^*=0.40$
 Curva a: $\Phi=0.60$ $\chi, \min=0.95$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.96, \text{----}, \text{----}, \text{----}$
 Verifica: $0.06+0.05=0.11$

- Verifica a pressoflessione retta - CC 54 SLU $X_1=1.04$ - Classe 1
 Sollecitazioni: $N=15696.50$ $T=114.39$ $M=139.90$ $M_x=81.38$
 $M, Ed=139.90$ $M, c, Rd=1810.99$
 $N, Ed=15696.50$ $Nc, Rd=60925.30$ $n=N, Ed/Nc, Rd=0.26$
 $MN, c, Rd=1344.41$ $M, Ed/MN, c, Rd=0.10$

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 89 SLU $X_1=0.00$
 Sollecitazioni: $N=11502.40$ $T=131.41$ $M=19.94$ $M_x=152.37$
 $V, Ed=131.41$ $Vc, Rd, Red=20245.70$ $V, Ed/Vc, Rd, Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_1=1.04$ - Classe 3
 Sollecitazioni: $N=13013.10$ $T=84.87$ $M=86.98$ $M_x=84.86$
 Tensioni: $\sigma_N=722.14$ $\sigma_M=213.78$ $\tau=104.29$ $\sigma_{max}=935.92$
 Tensioni: $\sigma_N=722.14$ $\sigma_M=-0.00$ $\tau=113.69$ $\tau_{max}=113.69$
 Tensioni: $\sigma_N=722.14$ $\sigma_M=213.78$ $\tau=104.29$ $\sigma_{ID, max}=953.20$

Asta n. 2819 (-2427 -2405) Tubo circolare $d=101.6 \times 6$ mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
 Sollecitazioni: $N, Ed=-2253.61$ $M, Ed=84.98$
 Resistenze: $Nc, Rd=60925.30$ $M, c, Rd=1375.52$ $L=104.09$

α_{my} , α_{mz} , $\alpha_{LT}=0.95$, ----, ----
 $\lambda=30.74$ $N_{cr}=395322.00$ $\lambda^*=0.40$
 Curva a: $\Phi=0.60$ $\chi_{,min}=0.95$
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.96$, ----, ----
 Verifica: $0.04+0.05=0.09$

- Verifica a pressoflessione retta - CC 75 SLU $X_l=1.04$ - Classe 1
 Sollecitazioni: $N=19988.80$ $T=137.37$ $M=121.22$ $M_x=76.05$
 $M, Ed=121.22$ $M, c, Rd=1810.99$
 $N, Ed=19988.80$ $Nc, Rd=60925.30$ $n=N, Ed/Nc, Rd=0.33$
 $MN, c, Rd=1216.83$ $M, Ed/MN, c, Rd=0.10$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 75 SLU $X_l=1.04$
 Sollecitazioni: $N=19988.80$ $T=137.37$ $M=121.22$ $M_x=76.05$
 $V, Ed=137.37$ $Vc, Rd, Red=21321.80$ $V, Ed/Vc, Rd, Red=0.01$
- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_l=1.04$ - Classe 3
 Sollecitazioni: $N=14673.90$ $T=79.07$ $M=83.74$ $M_x=70.90$
 Tensioni: $\sigma_N=814.31$ $\sigma_M=205.84$ $\tau=87.14$ $\sigma_{max}=1020.14$
 Tensioni: $\sigma_N=814.31$ $\sigma_M=-0.00$ $\tau=95.89$ $\tau_{max}=95.89$
 Tensioni: $\sigma_N=814.31$ $\sigma_M=205.84$ $\tau=87.14$ $\sigma_{ID, max}=1031.25$

Asta n. 2819 (-2405 -2361) Tubo circolare $d=114.3 \times 6$ mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
 Sollecitazioni: $N, Ed=-1329.69$ $M, Ed=99.24$
 Resistenze: $Nc, Rd=69019.00$ $M, c, Rd=1776.03$ $L=103.81$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, ----, ----
 $\lambda=27.07$ $N_{cr}=577399.00$ $\lambda^*=0.35$
 Curva a: $\Phi=0.58$ $\chi_{,min}=0.96$
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, ----, ----
 Verifica: $0.02+0.05=0.07$

- Verifica a pressoflessione retta - CC 75 SLU $X_l=1.04$ - Classe 1
 Sollecitazioni: $N=23535.40$ $T=128.58$ $M=132.79$ $M_x=57.73$
 $M, Ed=132.79$ $M, c, Rd=2323.44$
 $N, Ed=23535.40$ $Nc, Rd=69019.00$ $n=N, Ed/Nc, Rd=0.34$
 $MN, c, Rd=1531.15$ $M, Ed/MN, c, Rd=0.09$

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 54 SLU $X_l=0.00$
 Sollecitazioni: $N=23781.80$ $T=133.60$ $M=64.34$ $M_x=49.30$
 $V, Ed=133.60$ $Vc, Rd, Red=24759.00$ $V, Ed/Vc, Rd, Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_l=1.04$ - Classe 3
 Sollecitazioni: $N=15864.80$ $T=71.36$ $M=96.52$ $M_x=56.27$
 Tensioni: $\sigma_N=777.15$ $\sigma_M=183.74$ $\tau=53.56$ $\sigma_{max}=960.89$
 Tensioni: $\sigma_N=777.15$ $\sigma_M=-0.00$ $\tau=60.54$ $\tau_{max}=60.54$
 Tensioni: $\sigma_N=777.15$ $\sigma_M=183.74$ $\tau=53.56$ $\sigma_{ID, max}=965.36$

Asta n. 2819 (-2361 -2357) Tubo circolare $d=114.3 \times 6$ mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
 Sollecitazioni: $N, Ed=-528.30$ $M, Ed=85.20$
 Resistenze: $Nc, Rd=69019.00$ $M, c, Rd=1776.03$ $L=103.81$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, ----, ----
 $\lambda=27.07$ $N_{cr}=577397.00$ $\lambda^*=0.35$
 Curva a: $\Phi=0.58$ $\chi_{,min}=0.96$
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, ----, ----
 Verifica: $0.01+0.04=0.05$

- Verifica a pressoflessione retta - CC 75 SLU $X_l=1.04$ - Classe 1
 Sollecitazioni: $N=25401.50$ $T=62.77$ $M=95.88$ $M_x=45.99$
 $M, Ed=95.88$ $M, c, Rd=2323.44$
 $N, Ed=25401.50$ $Nc, Rd=69019.00$ $n=N, Ed/Nc, Rd=0.37$
 $MN, c, Rd=1468.33$ $M, Ed/MN, c, Rd=0.07$

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 74 SLU $X_l=1.04$
 Sollecitazioni: $N=19434.30$ $T=69.94$ $M=75.57$ $M_x=35.47$
 $V, Ed=69.94$ $Vc, Rd, Red=24930.20$ $V, Ed/Vc, Rd, Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_l=1.04$ - Classe 3
 Sollecitazioni: $N=16146.50$ $T=35.46$ $M=85.20$ $M_x=34.94$
 Tensioni: $\sigma_N=790.95$ $\sigma_M=162.18$ $\tau=33.26$ $\sigma_{max}=953.13$
 Tensioni: $\sigma_N=790.95$ $\sigma_M=-0.00$ $\tau=36.73$ $\tau_{max}=36.73$
 Tensioni: $\sigma_N=790.95$ $\sigma_M=162.18$ $\tau=33.26$ $\sigma_{ID, max}=954.87$

Asta n. 2819 (-2357 -2352) Tubo circolare d=114.3x6 mm - S355 Crit. 3

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- Verifica a pressoflessione retta - CC 37 SLU $X_1=0.00$ - Classe 1
Sollecitazioni: $N=16851.70$ $T=78.50$ $M=107.80$ $M_x=-19.48$
 $M, Ed=107.80$ $M, c, Rd=2323.44$
 $N, Ed=16851.70$ $N_c, Rd=69019.00$ $n=N, Ed/N_c, Rd=0.24$
 $MN, c, Rd=1756.15$ $M, Ed/MN, c, Rd=0.06$
 - Verifica a taglio e torsione dir. Z [4.2.25] - CC 37 SLU $X_1=1.04$
Sollecitazioni: $N=16851.50$ $T=95.93$ $M=20.43$ $M_x=-19.48$
 $V, Ed=95.93$ $V_c, Rd, Red=25128.00$ $V, Ed/V_c, Rd, Red=0.00$
 - Verifica in termini tensionali [4.2.4] - CC 9 SND $X_1=0.00$ - Classe 3
Sollecitazioni: $N=15719.70$ $T=52.02$ $M=80.99$ $M_x=20.35$
Tensioni: $\sigma_N=770.04$ $\sigma_M=154.17$ $\tau=19.37$ $\sigma_{max}=924.21$
Tensioni: $\sigma_N=770.04$ $\sigma_M=-0.00$ $\tau=24.45$ $\tau_{max}=24.45$
Tensioni: $\sigma_N=770.04$ $\sigma_M=154.17$ $\tau=19.37$ $\sigma_{ID, max}=924.82$

Asta n. 2820 (-2644 -3199) Tubo 80x120x5 mm - S355 Crit. 3

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: $N, Ed=-2283.19$ $M_y, Ed=668.51$ $M_z, Ed=-119.08$
Resistenze: $N_c, Rd=64238.10$ $M_y, c, Rd=2116.38$ $M_z, c, Rd=1670.05$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ $N_{cr, y}=17091400.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ $N_{cr, z}=8991310.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.04+0.30+0.07=0.40$
Verifica ZZ: $0.04+0.24+0.07=0.34$
 - Verifica in termini tensionali [4.2.4] - CC 54 SLU $X_1=0.00$ - Classe 3
Sollecitazioni: $N=-1897.37$ $T_z=2705.67$ $M_y=451.94$ $T_y=751.13$ $M_z=-218.57$ $M_x=82.98$
Tensioni: $\sigma_N=-99.86$ $\sigma_M=-1164.46$ $\tau=96.21$ $\sigma_{max}=-1264.32$
Tensioni: $\sigma_N=-99.86$ $\sigma_M=-387.17$ $\tau=370.92$ $\tau_{max}=370.92$
Tensioni: $\sigma_N=-99.86$ $\sigma_M=-1104.30$ $\tau=261.90$ $\sigma_{ID, max}=1286.77$
 - Verifica a taglio e torsione dir. Y [4.2.25] - CC 37 SLU $X_1=0.14$
Sollecitazioni: $N=-1709.70$ $T_z=1848.77$ $T_y=487.12$ $M_z=-77.19$ $M_x=57.19$
 $V, Ed=487.12$ $V_c, Rd, Red=14331.70$ $V, Ed/V_c, Rd, Red=0.03$
 - Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed=1848.77$ $V_c, Rd, Red=21497.50$ $V, Ed/V_c, Rd, Red=0.09$
 - Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3
Sollecitazioni: $N=-2283.19$ $T_z=3026.53$ $M_y=668.51$ $T_y=388.79$ $M_z=-119.08$ $M_x=59.16$
Tensioni: $\sigma_N=-120.17$ $\sigma_M=-1309.02$ $\tau=68.59$ $\sigma_{max}=-1429.19$
Tensioni: $\sigma_N=-120.17$ $\sigma_M=-210.93$ $\tau=375.83$ $\tau_{max}=375.83$
Tensioni: $\sigma_N=-120.17$ $\sigma_M=-1309.02$ $\tau=68.59$ $\sigma_{ID, max}=1434.12$

Asta n. 2820 (-3199 2902) Tubo 80x120x5 mm - S355 Crit. 3

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
Sollecitazioni: $N, Ed=-6876.49$ $M_y, Ed=-142.00$ $M_z, Ed=121.30$
Resistenze: $N_c, Rd=64238.10$ $M_y, c, Rd=2116.38$ $M_z, c, Rd=1670.05$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ $N_{cr, y}=17091400.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ $N_{cr, z}=8991310.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
Verifica YY: $0.11+0.05+0.07=0.23$
Verifica ZZ: $0.11+0.04+0.07=0.22$
 - Verifica in termini tensionali [4.2.4] - CC 45 SLU $X_1=0.21$ - Classe 3
Sollecitazioni: $N=-7648.10$ $T_z=-447.29$ $M_y=-22.66$ $T_y=458.34$ $M_z=113.46$ $M_x=48.44$
Tensioni: $\sigma_N=-402.53$ $\sigma_M=-265.89$ $\tau=56.17$ $\sigma_{max}=-668.43$
Tensioni: $\sigma_N=-402.53$ $\sigma_M=33.19$ $\tau=122.62$ $\tau_{max}=122.62$
Tensioni: $\sigma_N=-402.53$ $\sigma_M=-262.88$ $\tau=83.56$ $\sigma_{ID, max}=680.97$
 - Verifica a taglio e torsione dir. Y [4.2.25] - CC 75 SLU $X_1=0.02$
Sollecitazioni: $N=-4320.08$ $T_z=-698.72$ $M_y=-134.63$ $T_y=565.84$ $M_x=76.18$
 $V, Ed=565.84$ $V_c, Rd, Red=14164.30$ $V, Ed/V_c, Rd, Red=0.04$
 - Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed=-698.72$ $V_c, Rd, Red=21246.50$ $V, Ed/V_c, Rd, Red=0.03$
 - Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3
Sollecitazioni: $N=-3607.93$ $T_z=-603.11$ $M_y=-134.69$ $T_y=375.60$ $M_z=-11.27$ $M_x=55.85$

Tensioni: $\sigma_N=-189.89$ $\sigma_M=-237.98$ $\tau=64.75$ $\sigma_{max}=-427.87$
 Tensioni: $\sigma_N=-189.89$ $\sigma_M=19.96$ $\tau=126.02$ $\tau_{max}=126.02$
 Tensioni: $\sigma_N=-189.89$ $\sigma_M=-237.98$ $\tau=64.75$ $\sigma_{ID,max}=442.32$

Asta n. 3457 (2401 -3082) Tubo 80x100x(2x5+6) mm - S355 (32) Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3

Sollecitazioni: N,Ed=-1233.65 My,Ed=568.00 Mz,Ed=-680.29
 Resistenze: Nc,Rd=88716.20 My,c,Rd=2370.44 Mz,c,Rd=2055.33 L=18.69
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=5.11$ Ncr,y=20801800.00 $\lambda^*_y=0.07$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.14$ Ncr,z=14429200.00 $\lambda^*_z=0.08$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.01+0.18+0.31=0.51
 Verifica ZZ: 0.01+0.15+0.31=0.48

- Verifica in termini tensionali [4.2.4] - CC 54 SLU Xl=0.09 - Classe 3

Sollecitazioni: N=1877.24 Tz=7182.21 My=706.66 Ty=765.66 Mz=-679.82 Mx=141.78
 Tensioni: $\sigma_N=71.54$ $\sigma_M=2126.19$ $\tau=133.77$ $\sigma_{max}=2197.73$
 Tensioni: $\sigma_N=71.54$ $\sigma_M=-894.63$ $\tau=691.51$ $\tau_{max}=691.51$
 Tensioni: $\sigma_N=71.54$ $\sigma_M=2126.19$ $\tau=133.77$ $\sigma_{ID,max}=2209.91$

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.09 - Classe 3

Sollecitazioni: N=-4287.32 Tz=5947.94 My=542.68 Ty=630.79 Mz=-326.20 Mx=116.85
 Tensioni: $\sigma_N=-163.39$ $\sigma_M=-1310.62$ $\tau=110.25$ $\sigma_{max}=-1474.01$
 Tensioni: $\sigma_N=-163.39$ $\sigma_M=-429.27$ $\tau=572.14$ $\tau_{max}=572.14$
 Tensioni: $\sigma_N=-163.39$ $\sigma_M=-1186.77$ $\tau=422.44$ $\sigma_{ID,max}=1535.68$

Asta n. 3457 (-3082 -3442) Tubo 80x100x(2x5+6) mm - S355 (32) Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3

Sollecitazioni: N,Ed=-4650.52 My,Ed=110.95 Mz,Ed=-580.93
 Resistenze: Nc,Rd=88716.20 My,c,Rd=2370.44 Mz,c,Rd=2055.33 L=8.90
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=2.44$ Ncr,y=91675200.00 $\lambda^*_y=0.03$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=2.92$ Ncr,z=63590900.00 $\lambda^*_z=0.04$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.05+0.04+0.27=0.36
 Verifica ZZ: 0.05+0.03+0.27=0.35

- Verifica in termini tensionali [4.2.4] - CC 49 SLU Xl=0.00 - Classe 3

Sollecitazioni: N=-4650.52 Tz=1931.72 My=110.95 Ty=916.95 Mz=-580.93 Mx=107.68
 Tensioni: $\sigma_N=-177.23$ $\sigma_M=-1113.86$ $\tau=101.60$ $\sigma_{max}=-1291.09$
 Tensioni: $\sigma_N=-177.23$ $\sigma_M=-764.49$ $\tau=251.83$ $\tau_{max}=251.83$
 Tensioni: $\sigma_N=-177.23$ $\sigma_M=-1088.54$ $\tau=202.99$ $\sigma_{ID,max}=1313.69$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU Xl=0.04

Sollecitazioni: N=-1053.62 Tz=1500.17 Ty=906.60 Mz=-567.40 Mx=128.79
 V,Ed=906.60 Vc,Rd,Red=21348.10 V,Ed/Vc,Rd,Red=0.04

- Verifica a taglio e torsione dir. Z [4.2.25]

V,Ed=1500.17 Vc,Rd,Red=26685.10 V,Ed/Vc,Rd,Red=0.06

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3

Sollecitazioni: N=-1744.02 Tz=699.09 My=32.60 Ty=525.44 Mz=-322.43 Mx=72.45
 Tensioni: $\sigma_N=-66.46$ $\sigma_M=-576.87$ $\tau=68.36$ $\sigma_{max}=-643.34$
 Tensioni: $\sigma_N=-66.46$ $\sigma_M=-424.31$ $\tau=122.80$ $\tau_{max}=122.80$
 Tensioni: $\sigma_N=-66.46$ $\sigma_M=-569.44$ $\tau=105.05$ $\sigma_{ID,max}=661.42$

Asta n. 3457 (-3442 -4235) Tubo 80x100x(2x5+6) mm - S355 (32) Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3

Sollecitazioni: N,Ed=-6174.26 My,Ed=-125.26 Mz,Ed=-482.50
 Resistenze: Nc,Rd=88716.20 My,c,Rd=2370.44 Mz,c,Rd=2055.33 L=8.90
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=2.44$ Ncr,y=91676200.00 $\lambda^*_y=0.03$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=2.92$ Ncr,z=63591500.00 $\lambda^*_z=0.04$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.07+0.04+0.22=0.33
 Verifica ZZ: 0.07+0.03+0.22=0.33

- Verifica in termini tensionali [4.2.4] - CC 49 SLU Xl=0.00 - Classe 3

Sollecitazioni: N=-6174.26 Tz=838.95 My=-50.62 Ty=989.05 Mz=-482.50 Mx=108.29
 Tensioni: $\sigma_N=-235.30$ $\sigma_M=-865.90$ $\tau=102.17$ $\sigma_{max}=-1101.20$

Tensioni: $\sigma_N=-235.30$ $\sigma_M=60.65$ $\tau=196.41$ $\tau_{max}=196.41$
 Tensioni: $\sigma_N=-235.30$ $\sigma_M=-854.35$ $\tau=146.21$ $\sigma_{TD,max}=1118.69$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU $X1=0.01$
 Sollecitazioni: $N=1045.74$ $T_z=251.11$ $T_y=727.53$ $M_z=-330.30$ $M_x=78.37$
 $V,Ed=727.53$ $Vc,Rd,Red=21902.90$ $V,Ed/Vc,Rd,Red=0.03$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=251.11$ $Vc,Rd,Red=27378.60$ $V,Ed/Vc,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=-1765.12$ $T_z=214.35$ $M_y=-43.15$ $T_y=556.02$ $M_z=-267.20$ $M_x=72.35$
 Tensioni: $\sigma_N=-67.27$ $\sigma_M=-501.07$ $\tau=68.26$ $\sigma_{max}=-568.34$
 Tensioni: $\sigma_N=-67.27$ $\sigma_M=51.70$ $\tau=121.15$ $\tau_{max}=121.15$
 Tensioni: $\sigma_N=-67.27$ $\sigma_M=-501.07$ $\tau=68.26$ $\sigma_{TD,max}=580.51$

Asta n. 3457 (-4235 -7091) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-9584.42$ $M_y,Ed=-114.28$ $M_z,Ed=-270.41$
 Resistenze: $Nc,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ $Ncr,y=17091400.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ $Ncr,z=8991280.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.96, 0.96, 0.76, 0.96$
 Verifica YY: $0.15+0.04+0.16=0.35$
 Verifica ZZ: $0.15+0.03+0.16=0.34$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X1=0.00$ - Classe 3
 Sollecitazioni: $N=-9584.42$ $T_z=-167.46$ $M_y=-114.28$ $T_y=724.87$ $M_z=-270.41$ $M_x=77.46$
 Tensioni: $\sigma_N=-504.44$ $\sigma_M=-730.01$ $\tau=89.81$ $\sigma_{max}=-1234.45$
 Tensioni: $\sigma_N=-504.44$ $\sigma_M=167.35$ $\tau=194.83$ $\tau_{max}=194.83$
 Tensioni: $\sigma_N=-504.44$ $\sigma_M=-730.01$ $\tau=89.81$ $\sigma_{TD,max}=1244.21$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 115 SLU $X1=0.00$
 Sollecitazioni: $N=-414.61$ $T_z=64.46$ $T_y=311.33$ $M_z=-130.41$ $M_x=33.68$
 $V,Ed=311.33$ $Vc,Rd,Red=14538.80$ $V,Ed/Vc,Rd,Red=0.02$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=64.46$ $Vc,Rd,Red=21808.20$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=-1241.21$ $T_z=-144.45$ $M_y=-48.48$ $T_y=474.10$ $M_z=-193.11$ $M_x=70.51$
 Tensioni: $\sigma_N=-65.33$ $\sigma_M=-468.39$ $\tau=81.74$ $\sigma_{max}=-533.72$
 Tensioni: $\sigma_N=-65.33$ $\sigma_M=70.99$ $\tau=150.44$ $\tau_{max}=150.44$
 Tensioni: $\sigma_N=-65.33$ $\sigma_M=-468.39$ $\tau=81.74$ $\sigma_{TD,max}=552.18$

Asta n. 3457 (-7091 3301) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-9902.63$ $M_y,Ed=-88.87$ $M_z,Ed=87.69$
 Resistenze: $Nc,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ $Ncr,y=17091500.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ $Ncr,z=8991320.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.96, 0.96, 0.76, 0.96$
 Verifica YY: $0.15+0.03+0.05=0.24$
 Verifica ZZ: $0.15+0.03+0.05=0.23$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X1=0.21$ - Classe 3
 Sollecitazioni: $N=-9898.89$ $T_z=-655.99$ $M_y=48.56$ $T_y=659.06$ $M_z=87.69$ $M_x=84.79$
 Tensioni: $\sigma_N=-520.99$ $\sigma_M=-255.10$ $\tau=98.30$ $\sigma_{max}=-776.09$
 Tensioni: $\sigma_N=-520.99$ $\sigma_M=-71.11$ $\tau=193.85$ $\tau_{max}=193.85$
 Tensioni: $\sigma_N=-520.99$ $\sigma_M=-232.91$ $\tau=173.35$ $\sigma_{TD,max}=811.50$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 45 SLU $X1=0.08$
 Sollecitazioni: $N=-9901.27$ $T_z=-654.73$ $M_y=-38.94$ $T_y=659.06$ $M_x=84.79$
 $V,Ed=659.06$ $Vc,Rd,Red=14088.50$ $V,Ed/Vc,Rd,Red=0.05$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-654.73$ $Vc,Rd,Red=21132.70$ $V,Ed/Vc,Rd,Red=0.03$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=576.90$ $T_z=-162.76$ $M_y=-27.24$ $T_y=317.00$ $M_z=-41.29$ $M_x=86.44$
 Tensioni: $\sigma_N=30.36$ $\sigma_M=127.12$ $\tau=100.22$ $\sigma_{max}=157.48$

Tensioni: $\sigma_N=30.36$ $\sigma_M=39.90$ $\tau=146.15$ $\tau_{max}=146.15$
 Tensioni: $\sigma_N=30.36$ $\sigma_M=116.67$ $\tau=136.32$ $\sigma_{ID,max}=278.15$

Asta n. 3458 (2402 -3090) Tubo 80x100x(2x5+6) mm - S355 (32) Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3

Sollecitazioni: N,Ed=-1157.20 My,Ed=573.00 Mz,Ed=744.91
 Resistenze: Nc,Rd=88716.20 My,c,Rd=2370.44 Mz,c,Rd=2055.33 L=18.69
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=5.11$ Ncr,y=20801700.00 $\lambda^*_y=0.07$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.14$ Ncr,z=14429200.00 $\lambda^*_z=0.08$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.01+0.18+0.34=0.54
 Verifica ZZ: 0.01+0.15+0.34=0.51

- Verifica in termini tensionali [4.2.4] - CC 54 SLU Xl=0.09 - Classe 3

Sollecitazioni: N=1318.14 Tz=6189.13 My=620.66 Ty=-990.62 Mz=767.00 Mx=-94.86
 Tensioni: $\sigma_N=50.23$ $\sigma_M=2146.94$ $\tau=89.50$ $\sigma_{max}=2197.17$
 Tensioni: $\sigma_N=50.23$ $\sigma_M=-1009.35$ $\tau=570.19$ $\tau_{max}=570.19$
 Tensioni: $\sigma_N=50.23$ $\sigma_M=2146.94$ $\tau=89.50$ $\sigma_{ID,max}=2202.63$

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.09 - Classe 3

Sollecitazioni: N=2160.82 Tz=3851.64 My=368.58 Ty=-665.12 Mz=470.61 Mx=-87.30
 Tensioni: $\sigma_N=82.35$ $\sigma_M=1299.84$ $\tau=82.37$ $\sigma_{max}=1382.19$
 Tensioni: $\sigma_N=82.35$ $\sigma_M=-619.31$ $\tau=381.52$ $\tau_{max}=381.52$
 Tensioni: $\sigma_N=82.35$ $\sigma_M=1299.84$ $\tau=82.37$ $\sigma_{ID,max}=1389.53$

Asta n. 3458 (-3090 -3448) Tubo 80x100x(2x5+6) mm - S355 (32) Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3

Sollecitazioni: N,Ed=-4624.27 My,Ed=110.02 Mz,Ed=626.82
 Resistenze: Nc,Rd=88716.20 My,c,Rd=2370.44 Mz,c,Rd=2055.33 L=8.90
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=2.44$ Ncr,y=91675700.00 $\lambda^*_y=0.03$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=2.92$ Ncr,z=63591200.00 $\lambda^*_z=0.04$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.05+0.04+0.29=0.38
 Verifica ZZ: 0.05+0.03+0.29=0.37

- Verifica in termini tensionali [4.2.4] - CC 49 SLU Xl=0.00 - Classe 3

Sollecitazioni: N=-4624.27 Tz=1928.02 My=110.02 Ty=-1011.68 Mz=626.82 Mx=-89.18
 Tensioni: $\sigma_N=-176.23$ $\sigma_M=-1188.01$ $\tau=84.14$ $\sigma_{max}=-1364.24$
 Tensioni: $\sigma_N=-176.23$ $\sigma_M=-824.87$ $\tau=234.16$ $\tau_{max}=234.16$
 Tensioni: $\sigma_N=-176.23$ $\sigma_M=-1162.90$ $\tau=185.34$ $\sigma_{ID,max}=1377.08$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 49 SLU Xl=0.06

Sollecitazioni: N=-4622.88 Tz=1927.28 Ty=-1011.68 Mz=569.50 Mx=-89.18
 V,Ed=-1011.68 Vc,Rd,Red=21783.90 V,Ed/Vc,Rd,Red=0.05

- Verifica a taglio e torsione dir. Z [4.2.25]

V,Ed=1927.28 Vc,Rd,Red=27229.90 V,Ed/Vc,Rd,Red=0.07

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3

Sollecitazioni: N=-2465.03 Tz=847.07 My=25.40 Ty=-646.07 Mz=389.76 Mx=-64.65
 Tensioni: $\sigma_N=-93.94$ $\sigma_M=-677.37$ $\tau=61.00$ $\sigma_{max}=-771.31$
 Tensioni: $\sigma_N=-93.94$ $\sigma_M=-512.91$ $\tau=127.00$ $\tau_{max}=127.00$
 Tensioni: $\sigma_N=-93.94$ $\sigma_M=-671.57$ $\tau=105.46$ $\sigma_{ID,max}=787.00$

Asta n. 3458 (-3448 -4236) Tubo 80x100x(2x5+6) mm - S355 (32) Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3

Sollecitazioni: N,Ed=-6155.20 My,Ed=-124.76 Mz,Ed=515.67
 Resistenze: Nc,Rd=88716.20 My,c,Rd=2370.44 Mz,c,Rd=2055.33 L=8.90
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=2.44$ Ncr,y=91675200.00 $\lambda^*_y=0.03$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=2.92$ Ncr,z=63590900.00 $\lambda^*_z=0.04$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.07+0.04+0.24=0.35
 Verifica ZZ: 0.07+0.03+0.24=0.34

- Verifica in termini tensionali [4.2.4] - CC 49 SLU Xl=0.00 - Classe 3

Sollecitazioni: N=-6155.20 Tz=825.94 My=-51.28 Ty=-992.81 Mz=515.67 Mx=-89.86
 Tensioni: $\sigma_N=-234.57$ $\sigma_M=-921.41$ $\tau=84.79$ $\sigma_{max}=-1155.99$
 Tensioni: $\sigma_N=-234.57$ $\sigma_M=61.44$ $\tau=179.39$ $\tau_{max}=179.39$

Tensioni: $\sigma_N=-234.57$ $\sigma_M=-909.71$ $\tau=128.14$ $\sigma_{ID,max}=1165.61$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3
Sollecitazioni: $N=-2825.39$ $T_z=384.64$ $M_y=-56.82$ $T_y=-621.92$ $M_z=319.73$ $M_x=-64.34$
Tensioni: $\sigma_N=-107.67$ $\sigma_M=-606.98$ $\tau=60.71$ $\sigma_{max}=-714.65$
Tensioni: $\sigma_N=-107.67$ $\sigma_M=68.07$ $\tau=119.91$ $\tau_{max}=119.91$
Tensioni: $\sigma_N=-107.67$ $\sigma_M=-606.98$ $\tau=60.71$ $\sigma_{ID,max}=722.35$

Asta n. 3458 (-4236 -7092) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
Sollecitazioni: $N,Ed=-9569.06$ $M_y,Ed=-113.54$ $M_z,Ed=296.09$
Resistenze: $N_c,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ $N_{cr,y}=17091500.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ $N_{cr,z}=8991320.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.96, 0.96, 0.76, 0.96$
Verifica YY: $0.15+0.04+0.17=0.36$
Verifica ZZ: $0.15+0.03+0.17=0.35$
- Verifica in termini tensionali [4.2.4] - CC 49 SLU $X1=0.00$ - Classe 3
Sollecitazioni: $N=-6443.68$ $T_z=-171.02$ $M_y=-108.25$ $T_y=-987.38$ $M_z=380.08$ $M_x=-88.96$
Tensioni: $\sigma_N=-339.14$ $\sigma_M=-942.39$ $\tau=103.14$ $\sigma_{max}=-1281.54$
Tensioni: $\sigma_N=-339.14$ $\sigma_M=158.53$ $\tau=246.19$ $\tau_{max}=246.19$
Tensioni: $\sigma_N=-339.14$ $\sigma_M=-942.39$ $\tau=103.14$ $\sigma_{ID,max}=1293.93$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 81 SLU $X1=0.17$
Sollecitazioni: $N=225.42$ $T_z=-28.88$ $T_y=-320.77$ $M_z=76.76$ $M_x=-41.85$
 $V,Ed=-320.77$ $V_c,Rd,Red=14466.80$ $V,Ed/V_c,Rd,Red=0.02$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-28.88$ $V_c,Rd,Red=21700.20$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3
Sollecitazioni: $N=-2184.91$ $T_z=-108.66$ $M_y=-79.06$ $T_y=-615.70$ $M_z=235.83$ $M_x=-63.17$
Tensioni: $\sigma_N=-115.00$ $\sigma_M=-603.74$ $\tau=73.24$ $\sigma_{max}=-718.74$
Tensioni: $\sigma_N=-115.00$ $\sigma_M=115.78$ $\tau=162.44$ $\tau_{max}=162.44$
Tensioni: $\sigma_N=-115.00$ $\sigma_M=-603.74$ $\tau=73.24$ $\sigma_{ID,max}=729.85$

Asta n. 3458 (-7092 3302) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
Sollecitazioni: $N,Ed=-9883.79$ $M_y,Ed=-88.34$ $M_z,Ed=-96.69$
Resistenze: $N_c,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ $N_{cr,y}=17091500.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ $N_{cr,z}=8991320.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.96, 0.96, 0.76, 0.96$
Verifica YY: $0.15+0.03+0.06=0.24$
Verifica ZZ: $0.15+0.03+0.06=0.24$
- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X1=0.21$ - Classe 3
Sollecitazioni: $N=-9880.05$ $T_z=-644.01$ $M_y=46.58$ $T_y=-744.35$ $M_z=-96.69$ $M_x=-71.83$
Tensioni: $\sigma_N=-520.00$ $\sigma_M=-270.17$ $\tau=83.28$ $\sigma_{max}=-790.17$
Tensioni: $\sigma_N=-520.00$ $\sigma_M=-68.21$ $\tau=191.18$ $\tau_{max}=191.18$
Tensioni: $\sigma_N=-520.00$ $\sigma_M=-245.70$ $\tau=168.04$ $\sigma_{ID,max}=819.15$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 49 SLU $X1=0.17$
Sollecitazioni: $N=-6417.36$ $T_z=-475.53$ $T_y=-871.03$ $M_z=-55.68$ $M_x=-95.93$
 $V,Ed=-871.03$ $V_c,Rd,Red=13990.30$ $V,Ed/V_c,Rd,Red=0.06$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-475.53$ $V_c,Rd,Red=20985.40$ $V,Ed/V_c,Rd,Red=0.02$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3
Sollecitazioni: $N=977.05$ $T_z=-370.24$ $M_y=-66.66$ $T_y=-518.20$ $M_z=56.55$ $M_x=-62.59$
Tensioni: $\sigma_N=51.42$ $\sigma_M=220.98$ $\tau=72.57$ $\sigma_{max}=272.41$
Tensioni: $\sigma_N=51.42$ $\sigma_M=97.62$ $\tau=147.67$ $\tau_{max}=147.67$
Tensioni: $\sigma_N=51.42$ $\sigma_M=206.67$ $\tau=131.58$ $\sigma_{ID,max}=344.32$

Asta n. 3556 (-4659 -4678) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: $N,Ed=-596.40$ $M_y,Ed=-97.54$ $M_z,Ed=1.77$
Resistenze: $N_c,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=16.14$

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=3.75$ Ncr,y=20316600.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.50$ Ncr,z=6748320.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.02+0.10+0.00=0.12
 Verifica ZZ: 0.02+0.08+0.00=0.10

- Verifica in termini tensionali [4.2.4] - CC 49 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-598.43 T_z=-163.74 M_y=-91.18 T_y=21.96 M_z=-3.11 M_x=44.03
 Tensioni: $\sigma_N=-43.49$ $\sigma_M=-225.38$ $\tau=84.72$ $\sigma_{max}=-268.87$
 Tensioni: $\sigma_N=-43.49$ $\sigma_M=9.54$ $\tau=105.95$ $\tau_{max}=105.95$
 Tensioni: $\sigma_N=-43.49$ $\sigma_M=-225.38$ $\tau=84.72$ $\sigma_{ID,max}=306.31$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU Xl=0.00
 Sollecitazioni: N=-134.88 T_z=-204.40 M_y=-121.61 T_y=6.62 M_x=58.52
 V,Ed=6.62 Vc,Rd,Red=5410.39 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=-204.40 Vc,Rd,Red=10820.80 V,Ed/Vc,Rd,Red=0.02

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-596.40 T_z=-191.09 M_y=-97.54 T_y=-20.70 M_z=1.75 M_x=62.52
 Tensioni: $\sigma_N=-43.34$ $\sigma_M=-235.51$ $\tau=120.30$ $\sigma_{max}=-278.86$
 Tensioni: $\sigma_N=-43.34$ $\sigma_M=-5.35$ $\tau=145.07$ $\tau_{max}=145.07$
 Tensioni: $\sigma_N=-43.34$ $\sigma_M=-234.69$ $\tau=124.41$ $\sigma_{ID,max}=351.76$

Asta n. 3556 (-4678 -4682) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-702.76 M_y,Ed=-57.74 M_z,Ed=2.94
 Resistenze: Nc,Rd=30796.20 M_y,c,Rd=951.93 M_z,c,Rd=632.38 L=16.14

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=3.75$ Ncr,y=20316600.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.50$ Ncr,z=6748320.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.02+0.06+0.00=0.08
 Verifica ZZ: 0.02+0.05+0.00=0.07

- Verifica in termini tensionali [4.2.4] - CC 49 SLU Xl=0.07 - Classe 3
 Sollecitazioni: N=-747.47 T_z=-181.21 M_y=-38.52 T_y=28.95 M_z=1.13 M_x=42.02
 Tensioni: $\sigma_N=-54.32$ $\sigma_M=-94.56$ $\tau=80.85$ $\sigma_{max}=-148.88$
 Tensioni: $\sigma_N=-54.32$ $\sigma_M=-3.46$ $\tau=104.34$ $\tau_{max}=104.34$
 Tensioni: $\sigma_N=-54.32$ $\sigma_M=-88.52$ $\tau=93.21$ $\sigma_{ID,max}=215.56$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU Xl=0.00
 Sollecitazioni: N=-155.21 T_z=-219.53 M_y=-73.09 T_y=4.63 M_x=56.20
 V,Ed=4.63 Vc,Rd,Red=5430.85 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=-219.53 Vc,Rd,Red=10861.70 V,Ed/Vc,Rd,Red=0.02

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-702.76 T_z=-201.50 M_y=-57.74 T_y=-13.04 M_z=1.07 M_x=61.11
 Tensioni: $\sigma_N=-51.07$ $\sigma_M=-139.53$ $\tau=117.59$ $\sigma_{max}=-190.61$
 Tensioni: $\sigma_N=-51.07$ $\sigma_M=-3.28$ $\tau=143.71$ $\tau_{max}=143.71$
 Tensioni: $\sigma_N=-51.07$ $\sigma_M=-130.49$ $\tau=131.33$ $\sigma_{ID,max}=291.04$

Asta n. 3556 (-4682 -4741) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-1336.49 M_y,Ed=52.69 M_z,Ed=-0.62
 Resistenze: Nc,Rd=30796.20 M_y,c,Rd=951.93 M_z,c,Rd=632.38 L=17.28

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17710400.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882650.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.04+0.04+0.00=0.09
 Verifica ZZ: 0.04+0.03+0.00=0.08

- Verifica a pressoflessione retta - CC 45 SLU Xl=0.17 - Classe 1
 Sollecitazioni: N=-1336.42 T_z=-263.49 M_y=52.69 T_y=-2.73 M_x=-2.13
 M_y,Ed=52.69 M_y,c,Rd=1184.58
 N,Ed=-1336.42 Nc,Rd=30796.20 n=N,Ed/Nc,Rd=0.04
 M_{Ny},c,Rd=1184.58 M_y,Ed/M_{Ny},c,Rd=0.04

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X_1=0.00$
 Sollecitazioni: $N=-199.38$ $T_z=-395.40$ $M_y=-19.04$ $T_y=9.65$ $M_x=-4.74$
 $V,Ed=9.65$ $Vc,Rd,Red=5885.08$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-395.40$ $Vc,Rd,Red=11770.20$ $V,Ed/Vc,Rd,Red=0.03$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.17$ - Classe 3
 Sollecitazioni: $N=-630.25$ $T_z=-385.30$ $M_y=63.84$ $T_y=6.18$ $M_x=-7.37$
 Tensioni: $\sigma_N=-45.80$ $\sigma_M=-150.09$ $\tau=14.19$ $\sigma_{max}=-195.89$
 Tensioni: $\sigma_N=-45.80$ $\sigma_M=-0.00$ $\tau=64.13$ $\tau_{max}=64.13$
 Tensioni: $\sigma_N=-45.80$ $\sigma_M=-140.08$ $\tau=40.46$ $\sigma_{ID,max}=198.66$

Asta n. 3556 (-4741 -4798) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N,Ed=-573.68$ $M_y,Ed=161.43$ $M_z,Ed=1.53$
 Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr,y}=17710600.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882720.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.02+0.16+0.00=0.18$
 Verifica ZZ: $0.02+0.13+0.00=0.15$

- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X_1=0.17$ - Classe 3
 Sollecitazioni: $N=-202.89$ $T_z=-414.19$ $M_y=152.71$ $T_y=-1.77$ $M_z=1.17$ $M_x=-9.80$
 Tensioni: $\sigma_N=-14.74$ $\sigma_M=-363.18$ $\tau=18.85$ $\sigma_{max}=-377.92$
 Tensioni: $\sigma_N=-14.74$ $\sigma_M=3.58$ $\tau=72.54$ $\tau_{max}=72.54$
 Tensioni: $\sigma_N=-14.74$ $\sigma_M=-363.18$ $\tau=18.85$ $\sigma_{ID,max}=379.33$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X_1=0.00$
 Sollecitazioni: $N=-202.88$ $T_z=-414.62$ $M_y=81.09$ $T_y=5.35$ $M_x=-9.80$
 $V,Ed=5.35$ $Vc,Rd,Red=5840.43$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-414.62$ $Vc,Rd,Red=11680.90$ $V,Ed/Vc,Rd,Red=0.04$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.17$ - Classe 3
 Sollecitazioni: $N=-573.63$ $T_z=-395.76$ $M_y=161.43$ $T_y=-3.67$ $M_x=-8.41$
 Tensioni: $\sigma_N=-41.69$ $\sigma_M=-379.53$ $\tau=16.18$ $\sigma_{max}=-421.22$
 Tensioni: $\sigma_N=-41.69$ $\sigma_M=-0.00$ $\tau=67.48$ $\tau_{max}=67.48$
 Tensioni: $\sigma_N=-41.69$ $\sigma_M=-379.53$ $\tau=17.05$ $\sigma_{ID,max}=422.25$

Asta n. 3556 (-4798 -4853) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N,Ed=-476.01$ $M_y,Ed=265.69$ $M_z,Ed=1.75$
 Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr,y}=17710600.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882720.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.02+0.27+0.00=0.28$
 Verifica ZZ: $0.02+0.21+0.00=0.23$

- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X_1=0.17$ - Classe 3
 Sollecitazioni: $N=-174.46$ $T_z=-483.34$ $M_y=272.14$ $T_y=-2.79$ $M_z=1.60$ $M_x=-21.20$
 Tensioni: $\sigma_N=-12.68$ $\sigma_M=-645.50$ $\tau=40.80$ $\sigma_{max}=-658.17$
 Tensioni: $\sigma_N=-12.68$ $\sigma_M=4.90$ $\tau=103.45$ $\tau_{max}=103.45$
 Tensioni: $\sigma_N=-12.68$ $\sigma_M=-645.50$ $\tau=40.80$ $\sigma_{ID,max}=661.96$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 49 SLU $X_1=0.11$
 Sollecitazioni: $N=-960.07$ $T_z=-407.86$ $M_y=210.08$ $T_y=5.43$ $M_x=-17.85$
 $V,Ed=5.43$ $Vc,Rd,Red=5769.35$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-407.86$ $Vc,Rd,Red=11538.70$ $V,Ed/Vc,Rd,Red=0.04$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.17$ - Classe 3
 Sollecitazioni: $N=-475.96$ $T_z=-419.25$ $M_y=265.69$ $T_y=5.12$ $M_z=1.03$ $M_x=-11.55$
 Tensioni: $\sigma_N=-34.59$ $\sigma_M=-628.31$ $\tau=22.23$ $\sigma_{max}=-662.90$
 Tensioni: $\sigma_N=-34.59$ $\sigma_M=3.17$ $\tau=76.57$ $\tau_{max}=76.57$
 Tensioni: $\sigma_N=-34.59$ $\sigma_M=-628.31$ $\tau=22.23$ $\sigma_{ID,max}=664.02$

Asta n. 3556 (-4853 -4916) Tubo 60x120x4 mm - S235 Crit. 2

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-342.65 My,Ed=372.20 Mz,Ed=1.72
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17710400.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882650.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.01+0.37+0.00=0.39
 Verifica ZZ: 0.01+0.30+0.00=0.31
 - Verifica in termini tensionali [4.2.4] - CC 54 SLU Xl=0.17 - Classe 3
 Sollecitazioni: N=-101.17 Tz=-518.50 My=402.75 Ty=-6.98 Mz=1.17 Mx=-31.31
 Tensioni: $\sigma_N=-7.35$ $\sigma_M=-951.04$ $\tau=60.24$ $\sigma_{max}=-958.39$
 Tensioni: $\sigma_N=-7.35$ $\sigma_M=3.58$ $\tau=127.46$ $\tau_{max}=127.46$
 Tensioni: $\sigma_N=-7.35$ $\sigma_M=-951.04$ $\tau=60.24$ $\sigma_{ID,max}=964.05$
 - Verifica a taglio e torsione dir. Y [4.2.25] - CC 53 SLU Xl=0.17
 Sollecitazioni: N=-133.35 Tz=-451.88 My=364.04 Ty=-9.35 Mx=-26.24
 V,Ed=-9.35 Vc,Rd,Red=5695.30 V,Ed/Vc,Rd,Red=0.00
 - Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=-451.88 Vc,Rd,Red=11390.60 V,Ed/Vc,Rd,Red=0.04
 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3
 Sollecitazioni: N=-342.60 Tz=-422.33 My=372.20 Ty=-7.71 Mx=-14.26
 Tensioni: $\sigma_N=-24.90$ $\sigma_M=-875.08$ $\tau=27.45$ $\sigma_{max}=-899.98$
 Tensioni: $\sigma_N=-24.90$ $\sigma_M=-0.00$ $\tau=82.19$ $\tau_{max}=82.19$
 Tensioni: $\sigma_N=-24.90$ $\sigma_M=-875.08$ $\tau=29.28$ $\sigma_{ID,max}=901.40$

Asta n. 3556 (-4916 -4991) Tubo 60x120x4 mm - S235 Crit. 2

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-143.88 My,Ed=484.98 Mz,Ed=2.27
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17710400.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882650.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.48+0.00=0.49
 Verifica ZZ: 0.00+0.39+0.00=0.40
 - Verifica in termini tensionali [4.2.4] - CC 54 SLU Xl=0.17 - Classe 3
 Sollecitazioni: N=92.97 Tz=-592.03 My=551.30 Ty=-26.70 Mz=-1.25 Mx=-42.47
 Tensioni: $\sigma_N=6.76$ $\sigma_M=1300.59$ $\tau=81.73$ $\sigma_{max}=1307.35$
 Tensioni: $\sigma_N=6.76$ $\sigma_M=-3.83$ $\tau=158.47$ $\tau_{max}=158.47$
 Tensioni: $\sigma_N=6.76$ $\sigma_M=1300.59$ $\tau=81.73$ $\sigma_{ID,max}=1314.99$
 - Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU Xl=0.09
 Sollecitazioni: N=92.98 Tz=-592.23 My=504.79 Ty=-23.47 Mx=-42.47
 V,Ed=-23.47 Vc,Rd,Red=5552.05 V,Ed/Vc,Rd,Red=0.00
 - Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=-592.23 Vc,Rd,Red=11104.10 V,Ed/Vc,Rd,Red=0.05
 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3
 Sollecitazioni: N=221.32 Tz=-449.32 My=484.98 Ty=-23.05 Mz=-1.73 Mx=-18.13
 Tensioni: $\sigma_N=16.08$ $\sigma_M=1146.37$ $\tau=34.89$ $\sigma_{max}=1162.46$
 Tensioni: $\sigma_N=16.08$ $\sigma_M=-5.32$ $\tau=93.13$ $\tau_{max}=93.13$
 Tensioni: $\sigma_N=16.08$ $\sigma_M=1146.37$ $\tau=34.89$ $\sigma_{ID,max}=1164.03$

Asta n. 3556 (-4991 -5037) Tubo 60x120x4 mm - S235 Crit. 2

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-126.52 My,Ed=593.96 Mz,Ed=-7.25
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17710600.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882720.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.59+0.01=0.61
 Verifica ZZ: 0.00+0.47+0.01=0.49
 - Verifica in termini tensionali [4.2.4] - CC 54 SLU Xl=0.17 - Classe 3

Sollecitazioni: $N=410.19$ $T_z=-566.69$ $M_y=697.45$ $T_y=-58.22$ $M_z=-7.96$ $M_x=-43.37$
 Tensioni: $\sigma_N=29.81$ $\sigma_M=1667.96$ $\tau=83.46$ $\sigma_{max}=1697.77$
 Tensioni: $\sigma_N=29.81$ $\sigma_M=-24.41$ $\tau=156.92$ $\tau_{max}=156.92$
 Tensioni: $\sigma_N=29.81$ $\sigma_M=1667.96$ $\tau=83.46$ $\sigma_{ID,max}=1703.91$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X1=0.02$
 Sollecitazioni: $N=410.20$ $T_z=-567.08$ $M_y=608.39$ $T_y=-51.75$ $M_z=-43.37$
 $V,Ed=-51.75$ $Vc,Rd,Red=5544.10$ $V,Ed/Vc,Rd,Red=0.01$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-567.08$ $Vc,Rd,Red=11088.20$ $V,Ed/Vc,Rd,Red=0.05$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.17$ - Classe 3
 Sollecitazioni: $N=371.93$ $T_z=-426.05$ $M_y=593.96$ $T_y=-48.05$ $M_z=-7.25$ $M_x=-17.98$
 Tensioni: $\sigma_N=27.03$ $\sigma_M=1422.13$ $\tau=34.59$ $\sigma_{max}=1449.16$
 Tensioni: $\sigma_N=27.03$ $\sigma_M=-22.24$ $\tau=89.82$ $\tau_{max}=89.82$
 Tensioni: $\sigma_N=27.03$ $\sigma_M=1422.13$ $\tau=34.59$ $\sigma_{ID,max}=1450.40$

Asta n. 3556 (-5037 -5113) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N,Ed=-169.52$ $M_y,Ed=594.20$ $M_z,Ed=-9.33$
 Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $Ncr,y=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $Ncr,z=5882520.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.01+0.59+0.01=0.61$
 Verifica ZZ: $0.01+0.47+0.01=0.49$

- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X1=0.00$ - Classe 3
 Sollecitazioni: $N=414.15$ $T_z=526.22$ $M_y=699.27$ $T_y=78.26$ $M_z=-11.01$ $M_x=27.32$
 Tensioni: $\sigma_N=30.10$ $\sigma_M=1683.02$ $\tau=52.57$ $\sigma_{max}=1713.12$
 Tensioni: $\sigma_N=30.10$ $\sigma_M=-33.77$ $\tau=120.78$ $\tau_{max}=120.78$
 Tensioni: $\sigma_N=30.10$ $\sigma_M=1683.02$ $\tau=52.57$ $\sigma_{ID,max}=1715.54$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X1=0.16$
 Sollecitazioni: $N=414.14$ $T_z=526.61$ $M_y=616.56$ $T_y=71.78$ $M_x=27.32$
 $V,Ed=71.78$ $Vc,Rd,Red=5685.80$ $V,Ed/Vc,Rd,Red=0.01$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=526.61$ $Vc,Rd,Red=11371.60$ $V,Ed/Vc,Rd,Red=0.05$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=414.99$ $T_z=422.02$ $M_y=594.20$ $T_y=58.70$ $M_z=-9.33$ $M_x=18.54$
 Tensioni: $\sigma_N=30.16$ $\sigma_M=1430.04$ $\tau=35.67$ $\sigma_{max}=1460.20$
 Tensioni: $\sigma_N=30.16$ $\sigma_M=-28.62$ $\tau=90.38$ $\tau_{max}=90.38$
 Tensioni: $\sigma_N=30.16$ $\sigma_M=1430.04$ $\tau=35.67$ $\sigma_{ID,max}=1461.50$

Asta n. 3556 (-5113 -5198) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N,Ed=-170.74$ $M_y,Ed=486.24$ $M_z,Ed=-2.15$
 Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $Ncr,y=17709900.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $Ncr,z=5882460.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.01+0.49+0.00=0.49$
 Verifica ZZ: $0.01+0.39+0.00=0.40$

- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X1=0.00$ - Classe 3
 Sollecitazioni: $N=24.38$ $T_z=548.60$ $M_y=563.53$ $T_y=33.79$ $M_z=-1.96$ $M_x=26.01$
 Tensioni: $\sigma_N=1.77$ $\sigma_M=1331.85$ $\tau=50.05$ $\sigma_{max}=1333.62$
 Tensioni: $\sigma_N=1.77$ $\sigma_M=-6.00$ $\tau=121.17$ $\tau_{max}=121.17$
 Tensioni: $\sigma_N=1.77$ $\sigma_M=1331.85$ $\tau=50.05$ $\sigma_{ID,max}=1336.44$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X1=0.08$
 Sollecitazioni: $N=24.37$ $T_z=548.79$ $M_y=520.43$ $T_y=30.55$ $M_x=26.01$
 $V,Ed=30.55$ $Vc,Rd,Red=5697.33$ $V,Ed/Vc,Rd,Red=0.01$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=548.79$ $Vc,Rd,Red=11394.70$ $V,Ed/Vc,Rd,Red=0.05$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3

Sollecitazioni: $N=204.65$ $T_z=444.23$ $M_y=486.24$ $T_y=24.52$ $M_z=-2.15$ $M_x=18.63$
 Tensioni: $\sigma_N=14.87$ $\sigma_M=1150.79$ $\tau=35.85$ $\sigma_{max}=1165.67$
 Tensioni: $\sigma_N=14.87$ $\sigma_M=-6.58$ $\tau=93.43$ $\tau_{max}=93.43$
 Tensioni: $\sigma_N=14.87$ $\sigma_M=1150.79$ $\tau=35.85$ $\sigma_{ID,max}=1167.32$

Asta n. 3556 (-5198 -5263) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3

Sollecitazioni: $N, Ed=-328.05$ $M_y, Ed=374.70$ $M_z, Ed=1.27$
 Resistenze: $N_c, Rd=30796.20$ $M_y, c, Rd=951.93$ $M_z, c, Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr,y}=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882520.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.01+0.37+0.00=0.39$
 Verifica ZZ: $0.01+0.30+0.00=0.31$

- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X1=0.02$ - Classe 3

Sollecitazioni: $N=-232.11$ $T_z=475.70$ $M_y=418.69$ $T_y=10.04$ $M_z=1.00$ $M_x=14.63$
 Tensioni: $\sigma_N=-16.87$ $\sigma_M=-987.96$ $\tau=28.15$ $\sigma_{max}=-1004.82$
 Tensioni: $\sigma_N=-16.87$ $\sigma_M=3.08$ $\tau=89.81$ $\tau_{max}=89.81$
 Tensioni: $\sigma_N=-16.87$ $\sigma_M=-987.96$ $\tau=28.15$ $\sigma_{ID,max}=1006.01$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X1=0.00$

Sollecitazioni: $N=-232.11$ $T_z=475.66$ $M_y=426.17$ $T_y=10.69$ $M_x=14.63$
 $V, Ed=10.69$ $V_c, Rd, Red=5797.78$ $V, Ed/V_c, Rd, Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]

$V, Ed=475.66$ $V_c, Rd, Red=11595.60$ $V, Ed/V_c, Rd, Red=0.04$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3

Sollecitazioni: $N=-328.05$ $T_z=417.91$ $M_y=374.70$ $T_y=7.23$ $M_x=14.65$
 Tensioni: $\sigma_N=-23.84$ $\sigma_M=-880.95$ $\tau=28.19$ $\sigma_{max}=-904.79$
 Tensioni: $\sigma_N=-23.84$ $\sigma_M=-0.00$ $\tau=82.36$ $\tau_{max}=82.36$
 Tensioni: $\sigma_N=-23.84$ $\sigma_M=-880.95$ $\tau=29.91$ $\sigma_{ID,max}=906.28$

Asta n. 3556 (-5263 -5314) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3

Sollecitazioni: $N, Ed=-456.15$ $M_y, Ed=269.11$ $M_z, Ed=1.19$
 Resistenze: $N_c, Rd=30796.20$ $M_y, c, Rd=951.93$ $M_z, c, Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr,y}=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882520.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.01+0.27+0.00=0.29$
 Verifica ZZ: $0.01+0.21+0.00=0.23$

- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X1=0.00$ - Classe 3

Sollecitazioni: $N=-356.32$ $T_z=438.73$ $M_y=306.63$ $T_y=5.35$ $M_z=1.38$ $M_x=4.18$
 Tensioni: $\sigma_N=-25.90$ $\sigma_M=-725.80$ $\tau=8.05$ $\sigma_{max}=-751.70$
 Tensioni: $\sigma_N=-25.90$ $\sigma_M=4.24$ $\tau=64.92$ $\tau_{max}=64.92$
 Tensioni: $\sigma_N=-25.90$ $\sigma_M=-725.80$ $\tau=8.05$ $\sigma_{ID,max}=751.83$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 49 SLU $X1=0.00$

Sollecitazioni: $N=-1470.08$ $T_z=370.65$ $M_y=264.39$ $T_y=2.47$ $M_x=5.36$
 $V, Ed=2.47$ $V_c, Rd, Red=5879.62$ $V, Ed/V_c, Rd, Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]

$V, Ed=370.65$ $V_c, Rd, Red=11759.20$ $V, Ed/V_c, Rd, Red=0.03$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3

Sollecitazioni: $N=-456.15$ $T_z=413.54$ $M_y=269.11$ $T_y=4.07$ $M_x=11.63$
 Tensioni: $\sigma_N=-33.15$ $\sigma_M=-632.71$ $\tau=22.38$ $\sigma_{max}=-665.86$
 Tensioni: $\sigma_N=-33.15$ $\sigma_M=-0.00$ $\tau=75.98$ $\tau_{max}=75.98$
 Tensioni: $\sigma_N=-33.15$ $\sigma_M=-632.71$ $\tau=23.35$ $\sigma_{ID,max}=667.09$

Asta n. 3556 (-5314 -5368) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3

Sollecitazioni: $N, Ed=-2322.77$ $M_y, Ed=148.60$ $M_z, Ed=-0.71$
 Resistenze: $N_c, Rd=30796.20$ $M_y, c, Rd=951.93$ $M_z, c, Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr,y}=17709900.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882460.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.08+0.12+0.00=0.20
 Verifica ZZ: 0.08+0.10+0.00=0.17

- Verifica in termini tensionali [4.2.4] - CC 54 SLU Xl=0.08 - Classe 3
 Sollecitazioni: N=-428.64 T_z=370.07 M_y=169.67 T_y=2.04 M_z=1.03 M_x=-7.29
 Tensioni: $\sigma_N=-31.15$ $\sigma_M=-402.56$ $\tau=14.03$ $\sigma_{max}=-433.71$
 Tensioni: $\sigma_N=-31.15$ $\sigma_M=-3.15$ $\tau=62.00$ $\tau_{max}=62.00$
 Tensioni: $\sigma_N=-31.15$ $\sigma_M=-402.56$ $\tau=14.03$ $\sigma_{ID,max}=434.39$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU Xl=0.06
 Sollecitazioni: N=-428.64 T_z=370.03 M_y=175.49 T_y=2.69 M_z=-7.29
 V,Ed=2.69 Vc,Rd,Red=5862.54 V,Ed/Vc,Rd,Red=0.00
- Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=370.03 Vc,Rd,Red=11725.10 V,Ed/Vc,Rd,Red=0.03
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-569.46 T_z=390.58 M_y=165.88 T_y=-7.23 M_z=-11.88
 Tensioni: $\sigma_N=-41.38$ $\sigma_M=-390.00$ $\tau=22.85$ $\sigma_{max}=-431.39$
 Tensioni: $\sigma_N=-41.38$ $\sigma_M=-0.00$ $\tau=73.48$ $\tau_{max}=73.48$
 Tensioni: $\sigma_N=-41.38$ $\sigma_M=-390.00$ $\tau=24.57$ $\sigma_{ID,max}=433.48$

Asta n. 3556 (-5368 -5430) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-2447.84 M_y,Ed=84.88 M_z,Ed=4.99
 Resistenze: Nc,Rd=30796.20 M_y,c,Rd=951.93 M_z,c,Rd=632.38 L=17.28
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=4.01$ Ncr,y=17710000.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882520.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.08+0.07+0.01=0.16
 Verifica ZZ: 0.08+0.05+0.01=0.14

- Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-2447.84 T_z=239.28 M_y=84.88 T_y=37.29 M_z=-1.45 M_x=-7.19
 Tensioni: $\sigma_N=-177.90$ $\sigma_M=-204.70$ $\tau=13.84$ $\sigma_{max}=-382.60$
 Tensioni: $\sigma_N=-177.90$ $\sigma_M=4.46$ $\tau=44.86$ $\tau_{max}=44.86$
 Tensioni: $\sigma_N=-177.90$ $\sigma_M=-204.70$ $\tau=13.84$ $\sigma_{ID,max}=383.35$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU Xl=0.05
 Sollecitazioni: N=-472.99 T_z=353.91 M_y=89.83 T_y=11.67 M_z=-12.02
 V,Ed=11.67 Vc,Rd,Red=5820.84 V,Ed/Vc,Rd,Red=0.00
- Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=353.91 Vc,Rd,Red=11641.70 V,Ed/Vc,Rd,Red=0.03
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-675.13 T_z=378.86 M_y=69.27 T_y=19.44 M_z=-11.96
 Tensioni: $\sigma_N=-49.06$ $\sigma_M=-162.86$ $\tau=23.01$ $\sigma_{max}=-211.92$
 Tensioni: $\sigma_N=-49.06$ $\sigma_M=-0.00$ $\tau=72.12$ $\tau_{max}=72.12$
 Tensioni: $\sigma_N=-49.06$ $\sigma_M=-152.00$ $\tau=48.84$ $\sigma_{ID,max}=218.13$

Asta n. 3556 (-5430 -5493) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-2835.50 M_y,Ed=29.13 M_z,Ed=3.14
 Resistenze: Nc,Rd=30796.20 M_y,c,Rd=951.93 M_z,c,Rd=632.38 L=17.28
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=4.01$ Ncr,y=17710000.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882520.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.09+0.02+0.00=0.12
 Verifica ZZ: 0.09+0.02+0.00=0.12
- Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-2835.50 T_z=189.48 M_y=29.13 T_y=-21.14 M_z=3.14 M_x=-33.93
 Tensioni: $\sigma_N=-206.07$ $\sigma_M=-79.62$ $\tau=65.29$ $\sigma_{max}=-285.69$
 Tensioni: $\sigma_N=-206.07$ $\sigma_M=-9.64$ $\tau=89.85$ $\tau_{max}=89.85$
 Tensioni: $\sigma_N=-206.07$ $\sigma_M=-75.05$ $\tau=78.21$ $\sigma_{ID,max}=312.06$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU Xl=0.05
 Sollecitazioni: N=-582.68 T_z=243.77 M_y=16.25 T_y=16.75 M_z=-52.28
 V,Ed=16.75 Vc,Rd,Red=5465.44 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]

V,Ed=243.77 Vc,Rd,Red=10930.90 V,Ed/Vc,Rd,Red=0.02

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3

Sollecitazioni: N=-906.45 T_z=142.46 M_y=-43.30 T_y=9.84 M_x=-58.08

Tensioni: σ_N =-65.88 σ_M =-101.81 τ =111.77 σ_{max} =-167.68

Tensioni: σ_N =-65.88 σ_M =0.00 τ =130.24 τ_{max} =130.24

Tensioni: σ_N =-65.88 σ_M =-95.02 τ =121.48 $\sigma_{ID,max}$ =264.88

Asta n. 3556 (-5493 -5588) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3

Sollecitazioni: N,Ed=-2792.76 M_y,Ed=-45.87 M_z,Ed=-0.86

Resistenze: Nc,Rd=30796.20 M_y,c,Rd=951.93 M_z,c,Rd=632.38 L=17.28

α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95

λ_y =4.01 Ncr,y=17709800.00 λ^*_y =0.04 Curva a: Φ_y =0.00 χ_y =1.00

λ_z =6.96 Ncr,z=5882460.00 λ^*_z =0.07 Curva a: Φ_z =0.00 χ_z =1.00

K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.09+0.04+0.00=0.13

Verifica ZZ: 0.09+0.03+0.00=0.12

- Verifica a pressoflessione retta - CC 54 SLU Xl=0.17 - Classe 1

Sollecitazioni: N=-681.80 T_z=226.45 M_y=-73.21 T_y=5.43 M_x=-54.77

M_y,Ed=-73.21 M_y,c,Rd=1184.58

N,Ed=-681.80 Nc,Rd=30796.20 n=N,Ed/Nc,Rd=0.02

MN_y,c,Rd=1184.58 M_y,Ed/MN_y,c,Rd=0.06

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU Xl=0.00

Sollecitazioni: N=-681.99 T_z=233.80 M_y=-33.44 T_y=12.56 M_x=-54.77

V,Ed=12.56 Vc,Rd,Red=5443.54 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]

V,Ed=233.80 Vc,Rd,Red=10887.10 V,Ed/Vc,Rd,Red=0.02

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3

Sollecitazioni: N=-965.70 T_z=131.03 M_y=-72.09 T_y=5.30 M_x=-59.46

Tensioni: σ_N =-70.18 σ_M =-169.50 τ =114.41 σ_{max} =-239.68

Tensioni: σ_N =-70.18 σ_M =0.00 τ =131.39 τ_{max} =131.39

Tensioni: σ_N =-70.18 σ_M =-158.20 τ =123.34 $\sigma_{ID,max}$ =312.73

Asta n. 3556 (-5588 -5657) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3

Sollecitazioni: N,Ed=-2825.55 M_y,Ed=-78.77 M_z,Ed=-0.86

Resistenze: Nc,Rd=30796.20 M_y,c,Rd=951.93 M_z,c,Rd=632.38 L=17.28

α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95

λ_y =4.01 Ncr,y=17710000.00 λ^*_y =0.04 Curva a: Φ_y =0.00 χ_y =1.00

λ_z =6.96 Ncr,z=5882520.00 λ^*_z =0.07 Curva a: Φ_z =0.00 χ_z =1.00

K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.09+0.06+0.00=0.16

Verifica ZZ: 0.09+0.05+0.00=0.14

- Verifica a pressoflessione retta - CC 54 SLU Xl=0.17 - Classe 1

Sollecitazioni: N=-783.22 T_z=161.61 M_y=-118.00 T_y=2.93 M_x=-63.41

M_y,Ed=-118.00 M_y,c,Rd=1184.58

N,Ed=-783.22 Nc,Rd=30796.20 n=N,Ed/Nc,Rd=0.03

MN_y,c,Rd=1184.58 M_y,Ed/MN_y,c,Rd=0.10

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU Xl=0.00

Sollecitazioni: N=-783.41 T_z=168.96 M_y=-89.44 T_y=10.05 M_x=-63.41

V,Ed=10.05 Vc,Rd,Red=5367.28 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]

V,Ed=168.96 Vc,Rd,Red=10734.60 V,Ed/Vc,Rd,Red=0.02

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3

Sollecitazioni: N=-1045.85 T_z=107.03 M_y=-98.61 T_y=5.46 M_x=-62.13

Tensioni: σ_N =-76.01 σ_M =-231.85 τ =119.54 σ_{max} =-307.86

Tensioni: σ_N =-76.01 σ_M =0.00 τ =133.42 τ_{max} =133.42

Tensioni: σ_N =-76.01 σ_M =-231.85 τ =120.84 $\sigma_{ID,max}$ =372.27

Asta n. 3556 (-5657 -5725) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3

Sollecitazioni: N,Ed=-2888.23 M_y,Ed=-99.59 M_z,Ed=-0.92

Resistenze: $N_c, R_d=30796.20$ $M_y, c, R_d=951.93$ $M_z, c, R_d=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr,y}=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882520.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.09+0.08+0.00=0.18$
 Verifica ZZ: $0.09+0.06+0.00=0.16$

- Verifica a pressoflessione retta - CC 54 SLU $X_l=0.17$ - Classe 1
 Sollecitazioni: $N=-881.82$ $T_z=113.12$ $M_y=-149.07$ $T_y=2.24$ $M_x=-72.02$
 $M_y, Ed=-149.07$ $M_y, c, R_d=1184.58$
 $N, Ed=-881.82$ $N_c, R_d=30796.20$ $n=N, Ed/N_c, R_d=0.03$
 $MN_y, c, R_d=1184.58$ $M_y, Ed/MN_y, c, R_d=0.13$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X_l=0.00$
 Sollecitazioni: $N=-882.01$ $T_z=120.47$ $M_y=-128.88$ $T_y=9.36$ $M_x=-72.02$
 $V, Ed=9.36$ $V_c, R_d, Red=5291.30$ $V, Ed/V_c, R_d, Red=0.00$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed=120.47$ $V_c, R_d, Red=10582.60$ $V, Ed/V_c, R_d, Red=0.01$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.17$ - Classe 3
 Sollecitazioni: $N=-1140.56$ $T_z=85.65$ $M_y=-120.70$ $T_y=5.73$ $M_x=-64.88$
 Tensioni: $\sigma_N=-82.89$ $\sigma_M=-283.77$ $\tau=124.85$ $\sigma_{max}=-366.66$
 Tensioni: $\sigma_N=-82.89$ $\sigma_M=0.00$ $\tau=135.96$ $\tau_{max}=135.96$
 Tensioni: $\sigma_N=-82.89$ $\sigma_M=-283.77$ $\tau=126.22$ $\sigma_{ID, max}=426.89$

Asta n. 3556 (-5725 -5789) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N, Ed=-2965.16$ $M_y, Ed=-108.68$ $M_z, Ed=-1.37$
 Resistenze: $N_c, R_d=30796.20$ $M_y, c, R_d=951.93$ $M_z, c, R_d=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr,y}=17709800.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882460.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.10+0.09+0.00=0.19$
 Verifica ZZ: $0.10+0.07+0.00=0.17$
- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X_l=0.06$ - Classe 3
 Sollecitazioni: $N=-2965.06$ $T_z=34.08$ $M_y=-105.29$ $T_y=5.63$ $M_z=-1.02$ $M_x=-54.58$
 Tensioni: $\sigma_N=-215.48$ $\sigma_M=-251.16$ $\tau=105.03$ $\sigma_{max}=-466.65$
 Tensioni: $\sigma_N=-215.48$ $\sigma_M=3.13$ $\tau=109.45$ $\tau_{max}=109.45$
 Tensioni: $\sigma_N=-215.48$ $\sigma_M=-250.68$ $\tau=106.14$ $\sigma_{ID, max}=501.11$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 53 SLU $X_l=0.00$
 Sollecitazioni: $N=-931.87$ $T_z=59.39$ $M_y=-134.01$ $T_y=11.00$ $M_x=-72.57$
 $V, Ed=11.00$ $V_c, R_d, Red=5286.41$ $V, Ed/V_c, R_d, Red=0.00$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed=59.39$ $V_c, R_d, Red=10572.80$ $V, Ed/V_c, R_d, Red=0.01$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.17$ - Classe 3
 Sollecitazioni: $N=-1236.60$ $T_z=62.40$ $M_y=-136.87$ $T_y=6.26$ $M_x=-67.32$
 Tensioni: $\sigma_N=-89.87$ $\sigma_M=-321.80$ $\tau=129.54$ $\sigma_{max}=-411.67$
 Tensioni: $\sigma_N=-89.87$ $\sigma_M=0.00$ $\tau=137.63$ $\tau_{max}=137.63$
 Tensioni: $\sigma_N=-89.87$ $\sigma_M=-321.80$ $\tau=131.04$ $\sigma_{ID, max}=470.09$

Asta n. 3556 (-5789 -5835) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N, Ed=-1337.82$ $M_y, Ed=-149.95$ $M_z, Ed=2.56$
 Resistenze: $N_c, R_d=30796.20$ $M_y, c, R_d=951.93$ $M_z, c, R_d=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr,y}=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882520.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.04+0.15+0.00=0.20$
 Verifica ZZ: $0.04+0.12+0.00=0.17$
- Verifica in termini tensionali [4.2.4] - CC 49 SLU $X_l=0.17$ - Classe 3
 Sollecitazioni: $N=-2255.59$ $T_z=13.60$ $M_y=-141.07$ $T_y=26.07$ $M_z=2.66$ $M_x=-68.90$
 Tensioni: $\sigma_N=-163.92$ $\sigma_M=-341.09$ $\tau=132.59$ $\sigma_{max}=-505.01$
 Tensioni: $\sigma_N=-163.92$ $\sigma_M=-309.57$ $\tau=138.79$ $\tau_{max}=138.79$
 Tensioni: $\sigma_N=-163.92$ $\sigma_M=-339.83$ $\tau=137.76$ $\sigma_{ID, max}=557.41$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 45 SLU $X_1=0.05$
 Sollecitazioni: $N=-3088.24$ $T_z=15.60$ $M_y=-110.26$ $T_y=38.10$ $M_x=-56.44$
 $V,Ed=38.10$ $Vc,Rd,Red=5428.81$ $V,Ed/Vc,Rd,Red=0.01$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=15.60$ $Vc,Rd,Red=10857.60$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.17$ - Classe 3
 Sollecitazioni: $N=-1337.64$ $T_z=52.41$ $M_y=-149.95$ $T_y=18.89$ $M_z=2.56$ $M_x=-67.88$
 Tensioni: $\sigma_N=-97.21$ $\sigma_M=-361.60$ $\tau=130.62$ $\sigma_{max}=-458.81$
 Tensioni: $\sigma_N=-97.21$ $\sigma_M=-7.84$ $\tau=137.42$ $\tau_{max}=137.42$
 Tensioni: $\sigma_N=-97.21$ $\sigma_M=-360.39$ $\tau=134.37$ $\sigma_{ID,max}=513.39$

Asta n. 3556 (-5835 -5877) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-3616.21$ $M_y,Ed=-123.43$ $M_z,Ed=4.44$
 Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $Ncr,y=17709800.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $Ncr,z=5882460.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.12+0.10+0.01=0.22$
 Verifica ZZ: $0.12+0.08+0.01=0.20$

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $X_1=0.08$ - Classe 3
 Sollecitazioni: $N=-2741.69$ $T_z=60.50$ $M_y=-148.07$ $T_y=-11.56$ $M_z=1.05$ $M_x=-32.20$
 Tensioni: $\sigma_N=-199.25$ $\sigma_M=-351.86$ $\tau=61.95$ $\sigma_{max}=-551.12$
 Tensioni: $\sigma_N=-199.25$ $\sigma_M=-3.23$ $\tau=69.80$ $\tau_{max}=69.80$
 Tensioni: $\sigma_N=-199.25$ $\sigma_M=-351.86$ $\tau=61.95$ $\sigma_{ID,max}=561.47$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 37 SLU $X_1=0.03$
 Sollecitazioni: $N=-826.55$ $T_z=66.88$ $M_y=-132.33$ $T_y=12.51$ $M_x=-26.57$
 $V,Ed=12.51$ $Vc,Rd,Red=5692.42$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=66.88$ $Vc,Rd,Red=11384.80$ $V,Ed/Vc,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.17$ - Classe 3
 Sollecitazioni: $N=-1675.43$ $T_z=43.68$ $M_y=-148.62$ $T_y=8.28$ $M_z=1.06$ $M_x=-43.85$
 Tensioni: $\sigma_N=-121.76$ $\sigma_M=-353.18$ $\tau=84.37$ $\sigma_{max}=-474.94$
 Tensioni: $\sigma_N=-121.76$ $\sigma_M=-3.25$ $\tau=90.04$ $\tau_{max}=90.04$
 Tensioni: $\sigma_N=-121.76$ $\sigma_M=-352.68$ $\tau=86.01$ $\sigma_{ID,max}=497.28$

Asta n. 3556 (-5877 -5986) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: $N,Ed=-2764.57$ $M_y,Ed=-166.88$ $M_z,Ed=-1.21$
 Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $Ncr,y=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $Ncr,z=5882520.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.09+0.13+0.00=0.23$
 Verifica ZZ: $0.09+0.11+0.00=0.20$

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $X_1=0.02$ - Classe 3
 Sollecitazioni: $N=-2764.55$ $T_z=53.18$ $M_y=-159.26$ $T_y=7.74$ $M_z=-1.09$ $M_x=-33.36$
 Tensioni: $\sigma_N=-200.91$ $\sigma_M=-378.31$ $\tau=64.19$ $\sigma_{max}=-579.22$
 Tensioni: $\sigma_N=-200.91$ $\sigma_M=3.35$ $\tau=71.09$ $\tau_{max}=71.09$
 Tensioni: $\sigma_N=-200.91$ $\sigma_M=-377.79$ $\tau=65.73$ $\sigma_{ID,max}=589.79$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 37 SLU $X_1=0.00$
 Sollecitazioni: $N=-926.00$ $T_z=62.28$ $M_y=-146.63$ $T_y=8.98$ $M_x=-27.45$
 $V,Ed=8.98$ $Vc,Rd,Red=5684.60$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=62.28$ $Vc,Rd,Red=11369.20$ $V,Ed/Vc,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.17$ - Classe 3
 Sollecitazioni: $N=-1747.45$ $T_z=39.30$ $M_y=-149.94$ $T_y=8.09$ $M_z=1.09$ $M_x=-43.87$
 Tensioni: $\sigma_N=-127.00$ $\sigma_M=-356.38$ $\tau=84.42$ $\sigma_{max}=-483.38$
 Tensioni: $\sigma_N=-127.00$ $\sigma_M=-3.34$ $\tau=89.51$ $\tau_{max}=89.51$
 Tensioni: $\sigma_N=-127.00$ $\sigma_M=-355.87$ $\tau=86.02$ $\sigma_{ID,max}=505.33$

Asta n. 3556 (-5986 -6059) Tubo 60x120x4 mm - S235 Crit. 2

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: N,Ed=-2842.10 My,Ed=-168.84 Mz,Ed=-0.86
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17710000.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00 \chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882520.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00 \chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.09+0.14+0.00=0.23
 Verifica ZZ: 0.09+0.11+0.00=0.20

 - Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-3589.83 My=-135.81 Ty=5.67 Mz=-1.02 Mx=-33.20
 Tensioni: $\sigma_N=-260.89 \sigma_M=-322.89 \tau=63.88 \sigma_{max}=-583.78$
 Tensioni: $\sigma_N=-260.89 \sigma_M=-319.30 \tau=65.23 \tau_{max}=65.23$
 Tensioni: $\sigma_N=-260.89 \sigma_M=-322.89 \tau=63.88 \sigma_{ID,max}=594.18$

 - Verifica a taglio e torsione dir. Y [4.2.25] - CC 53 SLU Xl=0.00
 Sollecitazioni: N=-1547.61 Tz=-15.68 My=-169.46 Ty=13.33 Mx=-47.89
 V,Ed=13.33 Vc,Rd,Red=5504.19 V,Ed/Vc,Rd,Red=0.00

 - Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=-15.68 Vc,Rd,Red=11008.40 V,Ed/Vc,Rd,Red=0.00

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-1841.67 Tz=-27.40 My=-149.09 Ty=6.55 Mx=-46.50
 Tensioni: $\sigma_N=-133.84 \sigma_M=-350.52 \tau=89.48 \sigma_{max}=-484.36$
 Tensioni: $\sigma_N=-133.84 \sigma_M=0.00 \tau=93.03 \tau_{max}=93.03$
 Tensioni: $\sigma_N=-133.84 \sigma_M=-350.52 \tau=91.04 \sigma_{ID,max}=509.38$

Asta n. 3556 (-6059 -6127) Tubo 60x120x4 mm - S235 Crit. 2

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: N,Ed=-2927.26 My,Ed=-163.87 Mz,Ed=-0.74
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17709800.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00 \chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882460.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00 \chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.10+0.13+0.00=0.23
 Verifica ZZ: 0.10+0.11+0.00=0.20

 - Verifica a pressoflessione retta - CC 54 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=-1787.69 Tz=-59.36 My=-188.99 Ty=9.55 Mx=-58.68
 My,Ed=-188.99 My,c,Rd=1184.58
 N,Ed=-1787.69 Nc,Rd=30796.20 n=N,Ed/Nc,Rd=0.06
 MNy,c,Rd=1184.58 My,Ed/MNy,c,Rd=0.16

 - Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU Xl=0.17
 Sollecitazioni: N=-1787.51 Tz=-66.71 My=-178.10 Ty=2.43 Mx=-58.68
 V,Ed=2.43 Vc,Rd,Red=5409.00 V,Ed/Vc,Rd,Red=0.00

 - Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=-66.71 Vc,Rd,Red=10818.00 V,Ed/Vc,Rd,Red=0.01

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-1936.12 Tz=-44.74 My=-141.55 Ty=5.11 Mx=-49.24
 Tensioni: $\sigma_N=-140.71 \sigma_M=-332.81 \tau=94.75 \sigma_{max}=-473.51$
 Tensioni: $\sigma_N=-140.71 \sigma_M=0.00 \tau=100.55 \tau_{max}=100.55$
 Tensioni: $\sigma_N=-140.71 \sigma_M=-332.81 \tau=95.97 \sigma_{ID,max}=501.84$

Asta n. 3556 (-6127 -6184) Tubo 60x120x4 mm - S235 Crit. 2

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-3702.87 My,Ed=-117.31 Mz,Ed=-1.34
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17709900.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00 \chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882460.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00 \chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
 Verifica YY: 0.12+0.09+0.00=0.22
 Verifica ZZ: 0.12+0.08+0.00=0.20

 - Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.00 - Classe 3

Sollecitazioni: $N=-3702.87$ $T_z=-88.59$ $M_y=-117.31$ $T_y=2.12$ $M_z=-1.34$ $M_x=-44.86$
 Tensioni: $\sigma_N=-269.10$ $\sigma_M=-280.57$ $\tau=86.32$ $\sigma_{max}=-549.67$
 Tensioni: $\sigma_N=-269.10$ $\sigma_M=-4.12$ $\tau=97.80$ $\tau_{max}=97.80$
 Tensioni: $\sigma_N=-269.10$ $\sigma_M=-280.57$ $\tau=86.32$ $\sigma_{ID,max}=569.64$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X1=0.17$
 Sollecitazioni: $N=-1863.07$ $T_z=-133.21$ $M_y=-146.67$ $T_y=-2.10$ $M_x=-66.69$
 $V,Ed=-2.10$ $Vc,Rd,Red=5338.27$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-133.21$ $Vc,Rd,Red=10676.50$ $V,Ed/Vc,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=-2011.98$ $T_z=-75.29$ $M_y=-127.64$ $T_y=2.50$ $M_x=-52.13$
 Tensioni: $\sigma_N=-146.22$ $\sigma_M=-300.10$ $\tau=100.32$ $\sigma_{max}=-446.32$
 Tensioni: $\sigma_N=-146.22$ $\sigma_M=0.00$ $\tau=110.08$ $\tau_{max}=110.08$
 Tensioni: $\sigma_N=-146.22$ $\sigma_M=-300.10$ $\tau=100.91$ $\sigma_{ID,max}=479.32$

Asta n. 3556 (-6184 -6234) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-3800.11$ $M_y,Ed=-92.01$ $M_z,Ed=4.09$
 Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $Ncr,y=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $Ncr,z=5882520.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.12+0.07+0.01=0.20$
 Verifica ZZ: $0.12+0.06+0.01=0.19$

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $X1=0.00$ - Classe 3
 Sollecitazioni: $N=-3069.19$ $T_z=-123.89$ $M_y=-113.74$ $T_y=27.04$ $M_z=-2.16$ $M_x=-56.55$
 Tensioni: $\sigma_N=-223.05$ $\sigma_M=-275.04$ $\tau=108.81$ $\sigma_{max}=-498.09$
 Tensioni: $\sigma_N=-223.05$ $\sigma_M=-6.61$ $\tau=124.87$ $\tau_{max}=124.87$
 Tensioni: $\sigma_N=-223.05$ $\sigma_M=-274.02$ $\tau=114.17$ $\sigma_{ID,max}=534.97$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X1=0.17$
 Sollecitazioni: $N=-1912.56$ $T_z=-137.52$ $M_y=-111.50$ $T_y=7.33$ $M_x=-67.58$
 $V,Ed=7.33$ $Vc,Rd,Red=5330.48$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-137.52$ $Vc,Rd,Red=10661.00$ $V,Ed/Vc,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=-2082.31$ $T_z=-80.35$ $M_y=-106.87$ $T_y=19.57$ $M_x=-52.13$
 Tensioni: $\sigma_N=-151.33$ $\sigma_M=-251.26$ $\tau=100.31$ $\sigma_{max}=-402.59$
 Tensioni: $\sigma_N=-151.33$ $\sigma_M=0.00$ $\tau=110.72$ $\tau_{max}=110.72$
 Tensioni: $\sigma_N=-151.33$ $\sigma_M=-251.26$ $\tau=104.97$ $\sigma_{ID,max}=441.74$

Asta n. 3556 (-6234 -6295) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-4364.58$ $M_y,Ed=-86.12$ $M_z,Ed=5.48$
 Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $Ncr,y=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $Ncr,z=5882520.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.14+0.07+0.01=0.22$
 Verifica ZZ: $0.14+0.06+0.01=0.21$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X1=0.17$ - Classe 3
 Sollecitazioni: $N=-4364.31$ $T_z=51.00$ $M_y=-86.12$ $T_y=-38.91$ $M_z=-1.25$ $M_x=-3.64$
 Tensioni: $\sigma_N=-317.17$ $\sigma_M=-206.88$ $\tau=7.01$ $\sigma_{max}=-524.06$
 Tensioni: $\sigma_N=-317.17$ $\sigma_M=188.98$ $\tau=16.28$ $\tau_{max}=16.28$
 Tensioni: $\sigma_N=-317.17$ $\sigma_M=-206.88$ $\tau=7.01$ $\sigma_{ID,max}=524.20$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 37 SLU $X1=0.00$
 Sollecitazioni: $N=-1456.02$ $T_z=80.40$ $M_y=-90.42$ $T_y=6.36$ $M_x=2.42$
 $V,Ed=6.36$ $Vc,Rd,Red=5905.56$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=80.40$ $Vc,Rd,Red=11811.10$ $V,Ed/Vc,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.13$ - Classe 3

Sollecitazioni: $N=-2442.19$ $T_z=46.16$ $M_y=-93.80$ $T_y=11.04$ $M_z=1.05$ $M_x=-14.71$
 Tensioni: $\sigma_N=-177.49$ $\sigma_M=-224.26$ $\tau=28.31$ $\sigma_{max}=-401.75$
 Tensioni: $\sigma_N=-177.49$ $\sigma_M=-3.23$ $\tau=34.30$ $\tau_{max}=34.30$
 Tensioni: $\sigma_N=-177.49$ $\sigma_M=-224.26$ $\tau=28.31$ $\sigma_{ID,max}=404.73$

Asta n. 3556 (-6295 -6363) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-4281.68$ $M_y,Ed=-98.63$ $M_z,Ed=-1.39$
 Resistenze: $N_c,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr,y}=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882520.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.14+0.08+0.00=0.22$
 Verifica ZZ: $0.14+0.06+0.00=0.20$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X1=0.08$ - Classe 3
 Sollecitazioni: $N=-4281.56$ $T_z=45.63$ $M_y=-94.59$ $T_y=4.43$ $M_z=-1.04$ $M_x=-4.63$
 Tensioni: $\sigma_N=-311.16$ $\sigma_M=-226.09$ $\tau=8.91$ $\sigma_{max}=-537.25$
 Tensioni: $\sigma_N=-311.16$ $\sigma_M=3.20$ $\tau=14.82$ $\tau_{max}=14.82$
 Tensioni: $\sigma_N=-311.16$ $\sigma_M=-226.09$ $\tau=8.91$ $\sigma_{ID,max}=537.47$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 37 SLU $X1=0.00$
 Sollecitazioni: $N=-1536.89$ $T_z=76.92$ $M_y=-110.20$ $T_y=9.34$ $M_x=1.74$
 $V,Ed=9.34$ $V_c,Rd,Red=5911.59$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=76.92$ $V_c,Rd,Red=11823.20$ $V,Ed/V_c,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.17$ - Classe 3
 Sollecitazioni: $N=-2498.98$ $T_z=39.89$ $M_y=-100.59$ $T_y=9.43$ $M_z=1.28$ $M_x=-14.64$
 Tensioni: $\sigma_N=-181.61$ $\sigma_M=-241.02$ $\tau=28.17$ $\sigma_{max}=-422.63$
 Tensioni: $\sigma_N=-181.61$ $\sigma_M=-3.92$ $\tau=33.35$ $\tau_{max}=33.35$
 Tensioni: $\sigma_N=-181.61$ $\sigma_M=-241.02$ $\tau=28.17$ $\sigma_{ID,max}=425.44$

Asta n. 3556 (-6363 -6476) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-4289.40$ $M_y,Ed=-100.94$ $M_z,Ed=-0.93$
 Resistenze: $N_c,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr,y}=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882520.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.14+0.08+0.00=0.22$
 Verifica ZZ: $0.14+0.06+0.00=0.21$

- Verifica a pressoflessione retta - CC 54 SLU $X1=0.02$ - Classe 1
 Sollecitazioni: $N=-2575.66$ $M_y=-143.97$ $T_y=9.72$ $M_x=-16.38$
 $M_y,Ed=-143.97$ $M_y,c,Rd=1184.58$
 $N,Ed=-2575.66$ $N_c,Rd=30796.20$ $n=N,Ed/N_c,Rd=0.08$
 $M_{Ny,c,Rd}=1184.58$ $M_y,Ed/M_{Ny,c,Rd}=0.12$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 53 SLU $X1=0.00$
 Sollecitazioni: $N=-2325.88$ $T_z=-3.99$ $M_y=-122.57$ $T_y=11.71$ $M_x=-17.15$
 $V,Ed=11.71$ $V_c,Rd,Red=5775.58$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-3.99$ $V_c,Rd,Red=11551.20$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.11$ - Classe 3
 Sollecitazioni: $N=-2575.10$ $T_z=-22.34$ $M_y=-99.93$ $T_y=5.16$ $M_z=1.03$ $M_x=-17.79$
 Tensioni: $\sigma_N=-187.14$ $\sigma_M=-238.60$ $\tau=34.23$ $\sigma_{max}=-425.74$
 Tensioni: $\sigma_N=-187.14$ $\sigma_M=3.16$ $\tau=37.13$ $\tau_{max}=37.13$
 Tensioni: $\sigma_N=-187.14$ $\sigma_M=-238.60$ $\tau=34.23$ $\sigma_{ID,max}=429.85$

Asta n. 3556 (-6476 -6535) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: $N,Ed=-3717.17$ $M_y,Ed=-123.89$ $M_z,Ed=-0.56$
 Resistenze: $N_c,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr,y}=17709800.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882460.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$

Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
 Verifica YY: 0.12+0.10+0.00=0.22
 Verifica ZZ: 0.12+0.08+0.00=0.20

- Verifica a pressoflessione retta - CC 54 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=-2655.83 T_z=-42.77 M_y=-141.29 T_y=6.92 M_x=-24.34
 My,Ed=-141.29 My,c,Rd=1184.58
 N,Ed=-2655.83 Nc,Rd=30796.20 n=N,Ed/Nc,Rd=0.09
 MNy,c,Rd=1184.58 My,Ed/MNy,c,Rd=0.12
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 49 SLU Xl=0.17
 Sollecitazioni: N=-3716.90 T_z=-51.70 M_y=-115.84 T_y=2.37 M_x=-19.59
 V,Ed=2.37 Vc,Rd,Red=5754.00 V,Ed/Vc,Rd,Red=0.00
- Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=-51.70 Vc,Rd,Red=11508.00 V,Ed/Vc,Rd,Red=0.00
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-2638.86 T_z=-34.99 M_y=-96.89 T_y=3.00 M_x=-20.97
 Tensioni: σ_N=-191.78 σ_M=-227.81 τ=40.35 σ_{max}=-419.59
 Tensioni: σ_N=-191.78 σ_M=0.00 τ=44.88 τ_{max}=44.88
 Tensioni: σ_N=-191.78 σ_M=-227.81 τ=41.06 σ_{ID,max}=425.57

Asta n. 3556 (-6535 -6613) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-4345.61 My,Ed=-85.50 Mz,Ed=-1.50
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
 λ_y=4.01 Ncr,y=17710000.00 λ_y^{*}=0.04 Curva a: Φ_y=0.00 χ_y=1.00
 λ_z=6.96 Ncr,z=5882520.00 λ_z^{*}=0.07 Curva a: Φ_z=0.00 χ_z=1.00
 Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
 Verifica YY: 0.14+0.07+0.00=0.21
 Verifica ZZ: 0.14+0.06+0.00=0.20
- Verifica in termini tensionali [4.2.4] - CC 49 SLU Xl=0.03 - Classe 3
 Sollecitazioni: N=-3752.50 T_z=-104.98 M_y=-105.43 T_y=-1.52 M_z=-1.01 M_x=-27.26
 Tensioni: σ_N=-272.71 σ_M=-251.46 τ=52.45 σ_{max}=-524.17
 Tensioni: σ_N=-272.71 σ_M=-3.59 τ=66.06 τ_{max}=66.06
 Tensioni: σ_N=-272.71 σ_M=-251.46 τ=52.45 σ_{ID,max}=531.98
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU Xl=0.17
 Sollecitazioni: N=-2698.18 T_z=-118.14 M_y=-106.00 T_y=-5.74 M_x=-32.80
 V,Ed=-5.74 Vc,Rd,Red=5637.39 V,Ed/Vc,Rd,Red=0.00
- Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=-118.14 Vc,Rd,Red=11274.80 V,Ed/Vc,Rd,Red=0.01
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-2681.27 T_z=-69.20 M_y=-85.77 M_x=-24.56
 Tensioni: σ_N=-194.86 σ_M=-201.65 τ=47.26 σ_{max}=-396.51
 Tensioni: σ_N=-194.86 σ_M=0.00 τ=56.23 τ_{max}=56.23
 Tensioni: σ_N=-194.86 σ_M=-201.65 τ=47.26 σ_{ID,max}=404.87

Asta n. 3556 (-6613 -6666) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-4427.50 My,Ed=-61.57 Mz,Ed=4.81
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
 λ_y=4.01 Ncr,y=17710000.00 λ_y^{*}=0.04 Curva a: Φ_y=0.00 χ_y=1.00
 λ_z=6.96 Ncr,z=5882520.00 λ_z^{*}=0.07 Curva a: Φ_z=0.00 χ_z=1.00
 Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
 Verifica YY: 0.14+0.05+0.01=0.20
 Verifica ZZ: 0.14+0.04+0.01=0.19
- Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-4427.50 T_z=-96.77 M_y=-61.57 T_y=44.50 M_z=-2.88 M_x=-23.73
 Tensioni: σ_N=-321.77 σ_M=-154.94 τ=45.66 σ_{max}=-476.71
 Tensioni: σ_N=-321.77 σ_M=-8.83 τ=58.21 τ_{max}=58.21
 Tensioni: σ_N=-321.77 σ_M=-153.58 τ=54.48 σ_{ID,max}=484.62
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU Xl=0.13
 Sollecitazioni: N=-2728.86 T_z=-120.50 M_y=-80.63 T_y=16.47 M_x=-34.02
 V,Ed=16.47 Vc,Rd,Red=5626.65 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed = -120.50$ $Vc, Rd, Red = 11253.30$ $V, Ed/Vc, Rd, Red = 0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $Xl = 0.00$ - Classe 3
 Sollecitazioni: $N = -2725.46$ $T_z = -74.50$ $M_y = -66.86$ $T_y = 23.44$ $M_x = -24.88$
 Tensioni: $\sigma_N = -198.07$ $\sigma_M = -157.19$ $\tau = 47.87$ $\sigma_{max} = -355.26$
 Tensioni: $\sigma_N = -198.07$ $\sigma_M = 0.00$ $\tau = 57.53$ $\tau_{max} = 57.53$
 Tensioni: $\sigma_N = -198.07$ $\sigma_M = -157.19$ $\tau = 53.45$ $\sigma_{ID, max} = 367.13$

Asta n. 3556 (-6666 -6741) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N, Ed = -4972.97$ $M_y, Ed = -59.63$ $M_z, Ed = 6.88$
 Resistenze: $Nc, Rd = 30796.20$ $M_y, c, Rd = 951.93$ $M_z, c, Rd = 632.38$ $L = 17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 4.01$ $Ncr, y = 17709800.00$ $\lambda^*_y = 0.04$ Curva a: $\Phi_y = 0.00$ $\chi_y = 1.00$
 $\lambda_z = 6.96$ $Ncr, z = 5882460.00$ $\lambda^*_z = 0.07$ Curva a: $\Phi_z = 0.00$ $\chi_z = 1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.16 + 0.05 + 0.01 = 0.22$
 Verifica ZZ: $0.16 + 0.04 + 0.01 = 0.21$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $Xl = 0.17$ - Classe 3
 Sollecitazioni: $N = -4972.70$ $T_z = 52.08$ $M_y = -59.63$ $T_y = -50.45$ $M_z = -1.83$ $M_x = 5.95$
 Tensioni: $\sigma_N = -361.39$ $\sigma_M = -146.69$ $\tau = 11.45$ $\sigma_{max} = -508.08$
 Tensioni: $\sigma_N = -361.39$ $\sigma_M = -130.86$ $\tau = 23.46$ $\tau_{max} = 23.46$
 Tensioni: $\sigma_N = -361.39$ $\sigma_M = -145.83$ $\tau = 21.45$ $\sigma_{ID, max} = 508.57$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 45 SLU $Xl = 0.13$
 Sollecitazioni: $N = -4972.77$ $T_z = 54.88$ $M_y = -57.11$ $T_y = -50.45$ $M_x = 5.95$
 $V, Ed = -50.45$ $Vc, Rd, Red = 5874.39$ $V, Ed/Vc, Rd, Red = 0.01$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed = 54.88$ $Vc, Rd, Red = 11748.80$ $V, Ed/Vc, Rd, Red = 0.00$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $Xl = 0.17$ - Classe 3
 Sollecitazioni: $N = -3051.48$ $T_z = 40.30$ $M_y = -62.19$ $T_y = -18.15$ $M_x = 4.42$
 Tensioni: $\sigma_N = -221.76$ $\sigma_M = -146.22$ $\tau = 8.50$ $\sigma_{max} = -367.99$
 Tensioni: $\sigma_N = -221.76$ $\sigma_M = 0.00$ $\tau = 13.73$ $\tau_{max} = 13.73$
 Tensioni: $\sigma_N = -221.76$ $\sigma_M = -146.22$ $\tau = 12.82$ $\sigma_{ID, max} = 368.66$

Asta n. 3556 (-6741 -6826) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N, Ed = -4848.73$ $M_y, Ed = -72.20$ $M_z, Ed = -1.49$
 Resistenze: $Nc, Rd = 30796.20$ $M_y, c, Rd = 951.93$ $M_z, c, Rd = 632.38$ $L = 17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 4.01$ $Ncr, y = 17710000.00$ $\lambda^*_y = 0.04$ Curva a: $\Phi_y = 0.00$ $\chi_y = 1.00$
 $\lambda_z = 6.96$ $Ncr, z = 5882520.00$ $\lambda^*_z = 0.07$ Curva a: $\Phi_z = 0.00$ $\chi_z = 1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.16 + 0.06 + 0.00 = 0.22$
 Verifica ZZ: $0.16 + 0.05 + 0.00 = 0.21$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $Xl = 0.14$ - Classe 3
 Sollecitazioni: $N = -4848.52$ $T_z = 41.56$ $M_y = -70.92$ $T_y = 3.35$ $M_z = -1.01$ $M_x = 4.61$
 Tensioni: $\sigma_N = -352.36$ $\sigma_M = -170.33$ $\tau = 8.87$ $\sigma_{max} = -522.70$
 Tensioni: $\sigma_N = -352.36$ $\sigma_M = -3.11$ $\tau = 14.26$ $\tau_{max} = 14.26$
 Tensioni: $\sigma_N = -352.36$ $\sigma_M = -170.33$ $\tau = 8.87$ $\sigma_{ID, max} = 522.92$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 37 SLU $Xl = 0.00$
 Sollecitazioni: $N = -1960.55$ $T_z = 77.78$ $M_y = -95.44$ $T_y = 7.24$ $M_x = 18.91$
 $V, Ed = 7.24$ $Vc, Rd, Red = 5760.02$ $V, Ed/Vc, Rd, Red = 0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed = 77.78$ $Vc, Rd, Red = 11520.00$ $V, Ed/Vc, Rd, Red = 0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $Xl = 0.17$ - Classe 3
 Sollecitazioni: $N = -3058.66$ $T_z = 34.58$ $M_y = -71.19$ $T_y = 8.02$ $M_z = 1.15$ $M_x = 4.14$
 Tensioni: $\sigma_N = -222.29$ $\sigma_M = -171.43$ $\tau = 7.97$ $\sigma_{max} = -393.72$
 Tensioni: $\sigma_N = -222.29$ $\sigma_M = 3.53$ $\tau = 12.45$ $\tau_{max} = 12.45$
 Tensioni: $\sigma_N = -222.29$ $\sigma_M = -171.43$ $\tau = 7.97$ $\sigma_{ID, max} = 393.96$

Asta n. 3556 (-6826 -6900) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: $N, Ed = -4300.99$ $M_y, Ed = -96.36$ $M_z, Ed = -0.66$

Resistenze: $N_c, R_d=30796.20$ $M_y, c, R_d=951.93$ $M_z, c, R_d=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr, y}=17709900.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr, z}=5882490.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.14+0.08+0.00=0.22$
 Verifica ZZ: $0.14+0.06+0.00=0.20$

- Verifica a pressoflessione retta - CC 37 SLU $X_l=0.17$ - Classe 1
 Sollecitazioni: $N=-1996.69$ $T_x=2.90$ $M_y=-113.47$ $T_y=2.63$ $M_x=11.08$
 $M_y, Ed=-113.47$ $M_y, c, R_d=1184.58$
 $N, Ed=-1996.69$ $N_c, R_d=30796.20$ $n=N, Ed/N_c, R_d=0.06$
 $MN_y, c, R_d=1184.58$ $M_y, Ed/MN_y, c, R_d=0.10$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 53 SLU $X_l=0.00$
 Sollecitazioni: $N=-2918.02$ $T_x=-3.84$ $M_y=-92.14$ $T_y=10.05$ $M_x=-3.66$
 $V, Ed=10.05$ $V_c, R_d, Red=5894.56$ $V, Ed/V_c, R_d, Red=0.00$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed=-3.84$ $V_c, R_d, Red=11789.10$ $V, Ed/V_c, R_d, Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.11$ - Classe 3
 Sollecitazioni: $N=-3094.71$ $T_x=-12.33$ $M_y=-72.48$ $T_y=3.20$ $M_z=1.09$ $M_x=-3.68$
 Tensioni: $\sigma_N=-224.91$ $\sigma_M=-174.27$ $\tau=7.08$ $\sigma_{max}=-399.18$
 Tensioni: $\sigma_N=-224.91$ $\sigma_M=3.35$ $\tau=8.68$ $\tau_{max}=8.68$
 Tensioni: $\sigma_N=-224.91$ $\sigma_M=-174.27$ $\tau=7.08$ $\sigma_{ID, max}=399.37$

Asta n. 3556 (-6900 -6991) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: $N, Ed=-4322.83$ $M_y, Ed=-93.58$ $M_z, Ed=-0.47$
 Resistenze: $N_c, R_d=30796.20$ $M_y, c, R_d=951.93$ $M_z, c, R_d=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr, y}=17709900.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr, z}=5882490.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.14+0.08+0.00=0.22$
 Verifica ZZ: $0.14+0.06+0.00=0.20$
- Verifica a pressoflessione retta - CC 37 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $N=-2009.52$ $T_x=-30.32$ $M_y=-112.42$ $M_x=3.49$
 $M_y, Ed=-112.42$ $M_y, c, R_d=1184.58$
 $N, Ed=-2009.52$ $N_c, R_d=30796.20$ $n=N, Ed/N_c, R_d=0.07$
 $MN_y, c, R_d=1184.58$ $M_y, Ed/MN_y, c, R_d=0.09$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 49 SLU $X_l=0.17$
 Sollecitazioni: $N=-4322.57$ $T_x=-55.55$ $M_y=-84.87$ $M_x=-8.89$
 $V, Ed=-55.55$ $V_c, R_d, Red=11696.90$ $V, Ed/V_c, R_d, Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=-3120.24$ $T_x=-27.52$ $M_y=-70.77$ $T_y=1.07$ $M_x=-7.13$
 Tensioni: $\sigma_N=-226.76$ $\sigma_M=-166.38$ $\tau=13.72$ $\sigma_{max}=-393.15$
 Tensioni: $\sigma_N=-226.76$ $\sigma_M=0.00$ $\tau=17.29$ $\tau_{max}=17.29$
 Tensioni: $\sigma_N=-226.76$ $\sigma_M=-166.38$ $\tau=13.97$ $\sigma_{ID, max}=393.89$

Asta n. 3556 (-6991 -7050) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N, Ed=-4841.23$ $M_y, Ed=-58.65$ $M_z, Ed=-1.82$
 Resistenze: $N_c, R_d=30796.20$ $M_y, c, R_d=951.93$ $M_z, c, R_d=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr, y}=17709900.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr, z}=5882490.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.16+0.05+0.00=0.21$
 Verifica ZZ: $0.16+0.04+0.00=0.20$
- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=-4841.23$ $T_x=-85.54$ $M_y=-58.65$ $T_y=-2.94$ $M_z=-1.31$ $M_x=-13.85$
 Tensioni: $\sigma_N=-351.83$ $\sigma_M=-142.52$ $\tau=26.65$ $\sigma_{max}=-494.36$
 Tensioni: $\sigma_N=-351.83$ $\sigma_M=-4.01$ $\tau=37.73$ $\tau_{max}=37.73$
 Tensioni: $\sigma_N=-351.83$ $\sigma_M=-142.52$ $\tau=26.65$ $\sigma_{ID, max}=496.50$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X_l=0.16$
 Sollecitazioni: $N=-3322.30$ $T_x=-121.57$ $M_y=-72.75$ $T_y=-8.26$ $M_x=-19.25$
 $V, Ed=-8.26$ $V_c, R_d, Red=5757.04$ $V, Ed/V_c, R_d, Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]

V,Ed=-121.57 Vc,Rd,Red=11514.10 V,Ed/Vc,Rd,Red=0.01

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3

Sollecitazioni: N=-3127.35 T_z=-64.51 M_y=-61.51 T_y=1.92 M_x=-11.13

Tensioni: σ_N =-227.28 σ_M =-144.61 τ =21.42 σ_{max} =-371.89

Tensioni: σ_N =-227.28 σ_M =0.00 τ =29.78 τ_{max} =29.78

Tensioni: σ_N =-227.28 σ_M =-144.61 τ =21.87 $\sigma_{ID,max}$ =373.81

Asta n. 3556 (-7050 -7130) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3

Sollecitazioni: N,Ed=-4913.45 M_y,Ed=-34.36 M_z,Ed=5.46

Resistenze: N_c,Rd=30796.20 M_{y,c},Rd=951.93 M_{z,c},Rd=632.38 L=17.28

α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95

λ_y =4.01 Ncr,_y=17709900.00 λ^*_y =0.04 Curva a: Φ_y =0.00 χ_y =1.00

λ_z =6.96 Ncr,_z=5882490.00 λ^*_z =0.07 Curva a: Φ_z =0.00 χ_z =1.00

K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96

Verifica YY: 0.16+0.03+0.01=0.20

Verifica ZZ: 0.16+0.02+0.01=0.19

- Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.00 - Classe 3

Sollecitazioni: N=-4913.45 T_z=-98.45 M_y=-34.36 T_y=48.94 M_z=-3.00 M_x=-15.32

Tensioni: σ_N =-357.08 σ_M =-91.41 τ =29.49 σ_{max} =-448.49

Tensioni: σ_N =-357.08 σ_M =-9.21 τ =42.25 τ_{max} =42.25

Tensioni: σ_N =-357.08 σ_M =-89.99 τ =39.19 $\sigma_{ID,max}$ =452.20

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU Xl=0.11

Sollecitazioni: N=-3332.55 T_z=-123.99 M_y=-46.65 T_y=21.69 M_x=-20.65

V,Ed=21.69 Vc,Rd,Red=5744.68 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]

V,Ed=-123.99 Vc,Rd,Red=11489.40 V,Ed/Vc,Rd,Red=0.01

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3

Sollecitazioni: N=-3145.55 T_z=-70.45 M_y=-43.99 T_y=25.53 M_x=-11.69

Tensioni: σ_N =-228.60 σ_M =-103.44 τ =22.49 σ_{max} =-332.04

Tensioni: σ_N =-228.60 σ_M =0.00 τ =31.63 τ_{max} =31.63

Tensioni: σ_N =-228.60 σ_M =-103.44 τ =28.57 $\sigma_{ID,max}$ =335.70

Asta n. 3556 (-7130 -7193) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3

Sollecitazioni: N,Ed=-5431.41 M_y,Ed=-35.69 M_z,Ed=8.12

Resistenze: N_c,Rd=30796.20 M_{y,c},Rd=951.93 M_{z,c},Rd=632.38 L=17.28

α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95

λ_y =4.01 Ncr,_y=17709900.00 λ^*_y =0.04 Curva a: Φ_y =0.00 χ_y =1.00

λ_z =6.96 Ncr,_z=5882490.00 λ^*_z =0.07 Curva a: Φ_z =0.00 χ_z =1.00

K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96

Verifica YY: 0.18+0.03+0.01=0.22

Verifica ZZ: 0.18+0.02+0.01=0.21

- Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.17 - Classe 3

Sollecitazioni: N=-5431.15 T_z=66.07 M_y=-35.69 T_y=-59.70 M_z=-2.20 M_x=10.54

Tensioni: σ_N =-394.70 σ_M =-91.69 τ =20.29 σ_{max} =-486.39

Tensioni: σ_N =-394.70 σ_M =-78.31 τ =34.51 τ_{max} =34.51

Tensioni: σ_N =-394.70 σ_M =-90.65 τ =32.12 $\sigma_{ID,max}$ =488.53

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 45 SLU Xl=0.13

Sollecitazioni: N=-5431.22 T_z=68.88 M_y=-32.51 T_y=-59.70 M_x=10.54

V,Ed=-59.70 Vc,Rd,Red=5833.84 V,Ed/Vc,Rd,Red=0.01

- Verifica a taglio e torsione dir. Z [4.2.25]

V,Ed=68.88 Vc,Rd,Red=11667.70 V,Ed/Vc,Rd,Red=0.01

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3

Sollecitazioni: N=-3416.11 T_z=40.11 M_y=-42.17 T_y=-28.64 M_x=9.57

Tensioni: σ_N =-248.26 σ_M =-99.15 τ =18.42 σ_{max} =-347.41

Tensioni: σ_N =-248.26 σ_M =-92.54 τ =25.24 τ_{max} =25.24

Tensioni: σ_N =-248.26 σ_M =-99.15 τ =25.24 $\sigma_{ID,max}$ =350.15

Asta n. 3556 (-7193 -7256) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3

Sollecitazioni: $N, Ed = -5276.29$ $M_y, Ed = -51.81$ $M_z, Ed = -1.46$
 Resistenze: $N_c, Rd = 30796.20$ $M_y, c, Rd = 951.93$ $M_z, c, Rd = 632.38$ $L = 17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 4.01$ $N_{cr, y} = 17710000.00$ $\lambda^*_y = 0.04$ Curva a: $\Phi_y = 0.00$ $\chi_y = 1.00$
 $\lambda_z = 6.96$ $N_{cr, z} = 5882520.00$ $\lambda^*_z = 0.07$ Curva a: $\Phi_z = 0.00$ $\chi_z = 1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.17 + 0.04 + 0.00 = 0.22$
 Verifica ZZ: $0.17 + 0.03 + 0.00 = 0.21$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X_l = 0.17$ - Classe 3
 Sollecitazioni: $N = -5276.03$ $T_x = 53.54$ $M_y = -51.81$ $T_y = 2.50$ $M_z = -1.03$ $M_x = 9.07$
 Tensioni: $\sigma_N = -383.43$ $\sigma_M = -125.45$ $\tau = 17.44$ $\sigma_{max} = -508.88$
 Tensioni: $\sigma_N = -383.43$ $\sigma_M = -3.15$ $\tau = 24.38$ $\tau_{max} = 24.38$
 Tensioni: $\sigma_N = -383.43$ $\sigma_M = -125.45$ $\tau = 17.44$ $\sigma_{ID, max} = 509.77$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X_l = 0.03$
 Sollecitazioni: $N = -3712.88$ $T_x = 71.16$ $M_y = -66.52$ $T_y = 11.08$ $M_x = 11.83$
 $V, Ed = 11.08$ $V_c, Rd, Red = 5822.53$ $V, Ed/V_c, Rd, Red = 0.00$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed = 71.16$ $V_c, Rd, Red = 11645.10$ $V, Ed/V_c, Rd, Red = 0.01$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l = 0.17$ - Classe 3
 Sollecitazioni: $N = -3377.76$ $T_x = 33.63$ $M_y = -51.93$ $T_y = 6.21$ $M_x = 8.92$
 Tensioni: $\sigma_N = -245.48$ $\sigma_M = -122.10$ $\tau = 17.17$ $\sigma_{max} = -367.58$
 Tensioni: $\sigma_N = -245.48$ $\sigma_M = 0.00$ $\tau = 21.53$ $\tau_{max} = 21.53$
 Tensioni: $\sigma_N = -245.48$ $\sigma_M = -122.10$ $\tau = 17.17$ $\sigma_{ID, max} = 368.78$

Asta n. 3556 (-7256 -7290) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N, Ed = -5234.65$ $M_y, Ed = -57.31$ $M_z, Ed = -0.66$
 Resistenze: $N_c, Rd = 30796.20$ $M_y, c, Rd = 951.93$ $M_z, c, Rd = 632.38$ $L = 17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 4.01$ $N_{cr, y} = 17709900.00$ $\lambda^*_y = 0.04$ Curva a: $\Phi_y = 0.00$ $\chi_y = 1.00$
 $\lambda_z = 6.96$ $N_{cr, z} = 5882490.00$ $\lambda^*_z = 0.07$ Curva a: $\Phi_z = 0.00$ $\chi_z = 1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.17 + 0.05 + 0.00 = 0.22$
 Verifica ZZ: $0.17 + 0.04 + 0.00 = 0.21$
- Verifica a pressoflessione retta - CC 37 SLU $X_l = 0.00$ - Classe 1
 Sollecitazioni: $N = -2173.77$ $T_x = -9.40$ $M_y = -87.30$ $T_y = 1.01$ $M_x = 18.85$
 $M_y, Ed = -87.30$ $M_y, c, Rd = 1184.58$
 $N, Ed = -2173.77$ $N_c, Rd = 30796.20$ $n = N, Ed/N_c, Rd = 0.07$
 $MN_y, c, Rd = 1184.58$ $M_y, Ed/MN_y, c, Rd = 0.07$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 37 SLU $X_l = 0.17$
 Sollecitazioni: $N = -2173.51$ $T_x = -19.60$ $M_y = -84.79$ $T_y = 1.01$ $M_x = 18.85$
 $V, Ed = 1.01$ $V_c, Rd, Red = 5760.52$ $V, Ed/V_c, Rd, Red = 0.00$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed = -19.60$ $V_c, Rd, Red = 11521.00$ $V, Ed/V_c, Rd, Red = 0.00$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l = 0.08$ - Classe 3
 Sollecitazioni: $N = -3376.95$ $T_x = 6.04$ $M_y = -53.65$ $T_y = 1.52$ $M_z = 1.06$ $M_x = 4.75$
 Tensioni: $\sigma_N = -245.42$ $\sigma_M = -129.89$ $\tau = 9.14$ $\sigma_{max} = -375.31$
 Tensioni: $\sigma_N = -245.42$ $\sigma_M = 3.26$ $\tau = 9.92$ $\tau_{max} = 9.92$
 Tensioni: $\sigma_N = -245.42$ $\sigma_M = -129.89$ $\tau = 9.14$ $\sigma_{ID, max} = 375.64$

Asta n. 3556 (-7290 -7340) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N, Ed = -5222.47$ $M_y, Ed = -56.54$ $M_z, Ed = -0.60$
 Resistenze: $N_c, Rd = 30796.20$ $M_y, c, Rd = 951.93$ $M_z, c, Rd = 632.38$ $L = 17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 4.01$ $N_{cr, y} = 17709900.00$ $\lambda^*_y = 0.04$ Curva a: $\Phi_y = 0.00$ $\chi_y = 1.00$
 $\lambda_z = 6.96$ $N_{cr, z} = 5882490.00$ $\lambda^*_z = 0.07$ Curva a: $\Phi_z = 0.00$ $\chi_z = 1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.17 + 0.05 + 0.00 = 0.22$
 Verifica ZZ: $0.17 + 0.04 + 0.00 = 0.21$
- Verifica a pressoflessione retta - CC 37 SLU $X_l = 0.00$ - Classe 1
 Sollecitazioni: $N = -2162.15$ $T_x = -57.58$ $M_y = -81.85$ $T_y = -1.34$ $M_x = 10.43$
 $M_y, Ed = -81.85$ $M_y, c, Rd = 1184.58$
 $N, Ed = -2162.15$ $N_c, Rd = 30796.20$ $n = N, Ed/N_c, Rd = 0.07$
 $MN_y, c, Rd = 1184.58$ $M_y, Ed/MN_y, c, Rd = 0.07$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 37 SLU $X_1=0.17$
Sollecitazioni: $N=-2161.89$ $T_x=-67.78$ $M_y=-71.01$ $T_y=-1.34$ $M_x=10.43$
 $V,Ed=-1.34$ $V_c,Rd,Red=5834.86$ $V,Ed/V_c,Rd,Red=0.00$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-67.78$ $V_c,Rd,Red=11669.70$ $V,Ed/V_c,Rd,Red=0.01$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3
Sollecitazioni: $N=-3369.99$ $T_x=-26.19$ $M_y=-52.00$ $T_y=-1.18$ $M_z=1.12$ $M_x=-3.92$
Tensioni: $\sigma_N=-244.91$ $\sigma_M=-126.22$ $\tau=7.54$ $\sigma_{max}=-371.13$
Tensioni: $\sigma_N=-244.91$ $\sigma_M=3.44$ $\tau=10.93$ $\tau_{max}=10.93$
Tensioni: $\sigma_N=-244.91$ $\sigma_M=-126.22$ $\tau=7.54$ $\sigma_{ID,max}=371.36$

Asta n. 3556 (-7340 -7456) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
Sollecitazioni: $N,Ed=-5224.22$ $M_y,Ed=-46.21$ $M_z,Ed=-1.04$
Resistenze: $N_c,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr,y}=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882520.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
Verifica YY: $0.17+0.04+0.00=0.21$
Verifica ZZ: $0.17+0.03+0.00=0.20$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X_1=0.14$ - Classe 3
Sollecitazioni: $N=-5224.00$ $T_x=-80.61$ $M_y=-35.41$ $T_y=-1.15$ $M_z=-1.01$ $M_x=-9.65$
Tensioni: $\sigma_N=-379.65$ $\sigma_M=-86.82$ $\tau=18.57$ $\sigma_{max}=-466.47$
Tensioni: $\sigma_N=-379.65$ $\sigma_M=-3.09$ $\tau=29.02$ $\tau_{max}=29.02$
Tensioni: $\sigma_N=-379.65$ $\sigma_M=-86.82$ $\tau=18.57$ $\sigma_{ID,max}=467.58$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 37 SLU $X_1=0.17$
Sollecitazioni: $N=-2129.86$ $T_x=-131.45$ $M_y=-40.94$ $T_y=-5.32$ $M_x=1.90$
 $V,Ed=-5.32$ $V_c,Rd,Red=5910.10$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-131.45$ $V_c,Rd,Red=11820.20$ $V,Ed/V_c,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3
Sollecitazioni: $N=-3349.37$ $T_x=-64.54$ $M_y=-42.69$ $T_y=2.20$ $M_x=-6.14$
Tensioni: $\sigma_N=-243.41$ $\sigma_M=-100.36$ $\tau=11.82$ $\sigma_{max}=-343.77$
Tensioni: $\sigma_N=-243.41$ $\sigma_M=0.00$ $\tau=20.19$ $\tau_{max}=20.19$
Tensioni: $\sigma_N=-243.41$ $\sigma_M=-100.36$ $\tau=12.34$ $\sigma_{ID,max}=344.44$

Asta n. 3556 (-7456 -7492) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
Sollecitazioni: $N,Ed=-5291.27$ $M_y,Ed=-25.32$ $M_z,Ed=3.61$
Resistenze: $N_c,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr,y}=17709900.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882490.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
Verifica YY: $0.17+0.02+0.01=0.20$
Verifica ZZ: $0.17+0.02+0.01=0.19$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X_1=0.00$ - Classe 3
Sollecitazioni: $N=-5291.27$ $T_x=-85.35$ $M_y=-25.32$ $T_y=31.31$ $M_z=-1.80$ $M_x=-11.15$
Tensioni: $\sigma_N=-384.54$ $\sigma_M=-65.90$ $\tau=21.46$ $\sigma_{max}=-450.44$
Tensioni: $\sigma_N=-384.54$ $\sigma_M=-5.52$ $\tau=32.53$ $\tau_{max}=32.53$
Tensioni: $\sigma_N=-384.54$ $\sigma_M=-65.05$ $\tau=27.67$ $\sigma_{ID,max}=452.14$

- Verifica a taglio dir. Y [4.2.16] - CC 37 SLU $X_1=0.17$
Sollecitazioni: $N=-2098.65$ $T_x=-150.13$ $M_y=-4.07$ $T_y=1.98$
 $V,Ed=1.98$ $V_c,Rd=5926.90$ $V,Ed/V_c,Rd=0.00$

- Verifica a taglio dir. Z [4.2.16]
 $V,Ed=-150.13$ $V_c,Rd=11853.80$ $V,Ed/V_c,Rd=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3
Sollecitazioni: $N=-3344.36$ $T_x=-71.58$ $M_y=-24.99$ $T_y=15.98$ $M_x=-6.68$
Tensioni: $\sigma_N=-243.05$ $\sigma_M=-58.76$ $\tau=12.86$ $\sigma_{max}=-301.81$
Tensioni: $\sigma_N=-243.05$ $\sigma_M=0.00$ $\tau=22.14$ $\tau_{max}=22.14$
Tensioni: $\sigma_N=-243.05$ $\sigma_M=-58.76$ $\tau=16.67$ $\sigma_{ID,max}=303.19$

Asta n. 3556 (-7492 -7567) Tubo 60x120x4 mm - S235 Crit. 2

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-5316.88 My,Ed=-25.45 Mz,Ed=3.90
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17710000.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00 \chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882520.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00 \chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
 Verifica YY: 0.17+0.02+0.01=0.20
 Verifica ZZ: 0.17+0.02+0.01=0.19
 - Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.17 - Classe 3
 Sollecitazioni: N=-5316.61 Tz=86.62 My=-25.45 Ty=-31.71 Mz=-1.58 Mx=10.57
 Tensioni: $\sigma_N=-386.38 \sigma_M=-65.41 \tau=20.34 \sigma_{max}=-451.80$
 Tensioni: $\sigma_N=-386.38 \sigma_M=-4.84 \tau=31.57 \tau_{max}=31.57$
 Tensioni: $\sigma_N=-386.38 \sigma_M=-64.67 \tau=26.63 \sigma_{ID,max}=453.40$
 - Verifica a taglio e torsione dir. Y [4.2.25] - CC 75 SLU Xl=0.00
 Sollecitazioni: N=-2742.36 Tz=124.11 My=-4.27 Ty=-7.23 Mx=14.80
 V,Ed=-7.23 Vc,Rd,Red=5796.31 V,Ed/Vc,Rd,Red=0.00
 - Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=124.11 Vc,Rd,Red=11592.60 V,Ed/Vc,Rd,Red=0.01
 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3
 Sollecitazioni: N=-3326.56 Tz=51.77 My=-21.14 Ty=-17.68 Mx=12.03
 Tensioni: $\sigma_N=-241.76 \sigma_M=-49.69 \tau=23.16 \sigma_{max}=-291.45$
 Tensioni: $\sigma_N=-241.76 \sigma_M=0.00 \tau=29.87 \tau_{max}=29.87$
 Tensioni: $\sigma_N=-241.76 \sigma_M=-49.69 \tau=27.36 \sigma_{ID,max}=295.28$

Asta n. 3556 (-7567 -7654) Tubo 60x120x4 mm - S235 Crit. 2

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-5259.52 My,Ed=-46.66 Mz,Ed=-1.20
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17709900.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00 \chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882490.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00 \chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
 Verifica YY: 0.17+0.04+0.00=0.21
 Verifica ZZ: 0.17+0.03+0.00=0.20
 - Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.08 - Classe 3
 Sollecitazioni: N=-5259.40 Tz=79.12 My=-39.47 Ty=2.39 Mz=-1.02 Mx=9.08
 Tensioni: $\sigma_N=-382.22 \sigma_M=-96.39 \tau=17.48 \sigma_{max}=-478.62$
 Tensioni: $\sigma_N=-382.22 \sigma_M=-3.11 \tau=27.74 \tau_{max}=27.74$
 Tensioni: $\sigma_N=-382.22 \sigma_M=-96.39 \tau=17.48 \sigma_{ID,max}=479.57$
 - Verifica a taglio e torsione dir. Y [4.2.25] - CC 75 SLU Xl=0.05
 Sollecitazioni: N=-2784.21 Tz=118.19 My=-41.28 Ty=5.52 Mx=13.36
 V,Ed=5.52 Vc,Rd,Red=5809.01 V,Ed/Vc,Rd,Red=0.00
 - Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=118.19 Vc,Rd,Red=11618.00 V,Ed/Vc,Rd,Red=0.01
 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3
 Sollecitazioni: N=-3322.23 Tz=47.95 My=-34.20 Mx=11.72
 Tensioni: $\sigma_N=-241.44 \sigma_M=-80.40 \tau=22.56 \sigma_{max}=-321.84$
 Tensioni: $\sigma_N=-241.44 \sigma_M=0.00 \tau=28.77 \tau_{max}=28.77$
 Tensioni: $\sigma_N=-241.44 \sigma_M=-80.40 \tau=22.56 \sigma_{ID,max}=324.20$

Asta n. 3556 (-7654 -7697) Tubo 60x120x4 mm - S235 Crit. 2

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-5271.66 My,Ed=-57.36 Mz,Ed=-0.74
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17709900.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00 \chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882490.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00 \chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
 Verifica YY: 0.17+0.05+0.00=0.22
 Verifica ZZ: 0.17+0.04+0.00=0.21

- Verifica a pressoflessione retta - CC 54 SLU $X_1=0.17$ - Classe 1
 Sollecitazioni: $N=-3824.20$ $T_x=42.10$ $M_y=-79.05$ $T_y=-1.69$ $M_x=5.94$
 $M_y,Ed=-79.05$ $M_y,c,Rd=1184.58$
 $N,Ed=-3824.20$ $Nc,Rd=30796.20$ $n=N,Ed/Nc,Rd=0.12$
 $MN_y,c,Rd=1184.58$ $M_y,Ed/MN_y,c,Rd=0.07$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 75 SLU $X_1=0.00$
 Sollecitazioni: $N=-2827.29$ $T_x=51.60$ $M_y=-63.29$ $T_y=-1.66$ $M_x=4.48$
 $V,Ed=-1.66$ $Vc,Rd,Red=5887.35$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=51.60$ $Vc,Rd,Red=11774.70$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.17$ - Classe 3
 Sollecitazioni: $N=-3334.33$ $T_x=14.95$ $M_y=-40.07$ $T_y=1.12$ $M_z=1.07$ $M_x=8.16$
 Tensioni: $\sigma_N=-242.32$ $\sigma_M=-97.99$ $\tau=15.71$ $\sigma_{max}=-340.31$
 Tensioni: $\sigma_N=-242.32$ $\sigma_M=3.27$ $\tau=17.65$ $\tau_{max}=17.65$
 Tensioni: $\sigma_N=-242.32$ $\sigma_M=-97.99$ $\tau=15.71$ $\sigma_{ID,max}=341.40$

Asta n. 3556 (-7697 -7800) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-5300.49$ $M_y,Ed=-58.27$ $M_z,Ed=-0.57$
 Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $Ncr,y=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $Ncr,z=5882520.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.17+0.05+0.00=0.22$
 Verifica ZZ: $0.17+0.04+0.00=0.21$

- Verifica a pressoflessione retta - CC 54 SLU $X_1=0.14$ - Classe 1
 Sollecitazioni: $N=-3838.98$ $M_y=-81.38$ $T_y=-3.59$ $M_x=-2.50$
 $M_y,Ed=-81.38$ $M_y,c,Rd=1184.58$
 $N,Ed=-3838.98$ $Nc,Rd=30796.20$ $n=N,Ed/Nc,Rd=0.12$
 $MN_y,c,Rd=1184.58$ $M_y,Ed/MN_y,c,Rd=0.07$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 37 SLU $X_1=0.17$
 Sollecitazioni: $N=-2077.74$ $T_x=-18.36$ $M_y=-12.23$ $T_y=-1.90$ $M_x=14.78$
 $V,Ed=-1.90$ $Vc,Rd,Red=5796.46$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-18.36$ $Vc,Rd,Red=11592.90$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=-3333.95$ $T_x=9.93$ $M_y=-40.60$ $T_y=-1.71$ $M_z=1.14$ $M_x=-6.52$
 Tensioni: $\sigma_N=-242.29$ $\sigma_M=-99.48$ $\tau=12.54$ $\sigma_{max}=-341.77$
 Tensioni: $\sigma_N=-242.29$ $\sigma_M=-3.49$ $\tau=13.83$ $\tau_{max}=13.83$
 Tensioni: $\sigma_N=-242.29$ $\sigma_M=-99.48$ $\tau=12.54$ $\sigma_{ID,max}=342.46$

Asta n. 3556 (-7800 -7921) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-5361.46$ $M_y,Ed=-53.25$ $M_z,Ed=-1.36$
 Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $Ncr,y=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $Ncr,z=5882520.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.17+0.04+0.00=0.22$
 Verifica ZZ: $0.17+0.03+0.00=0.21$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=-5361.46$ $T_x=-51.56$ $M_y=-53.25$ $M_z=-1.20$ $M_x=-9.57$
 Tensioni: $\sigma_N=-389.64$ $\sigma_M=-129.44$ $\tau=18.41$ $\sigma_{max}=-519.08$
 Tensioni: $\sigma_N=-389.64$ $\sigma_M=-4.24$ $\tau=25.09$ $\tau_{max}=25.09$
 Tensioni: $\sigma_N=-389.64$ $\sigma_M=-129.44$ $\tau=18.41$ $\sigma_{ID,max}=520.06$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X_1=0.14$
 Sollecitazioni: $N=-3841.14$ $T_x=-69.02$ $M_y=-68.59$ $T_y=-9.08$ $M_x=-11.33$
 $V,Ed=-9.08$ $Vc,Rd,Red=5826.91$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-69.02$ $Vc,Rd,Red=11653.80$ $V,Ed/Vc,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3

Sollecitazioni: $N=-3329.19$ $T_z=-35.55$ $M_y=-37.73$ $T_y=2.09$ $M_x=-7.58$
 Tensioni: $\sigma_N=-241.95$ $\sigma_M=-88.71$ $\tau=14.58$ $\sigma_{max}=-330.65$
 Tensioni: $\sigma_N=-241.95$ $\sigma_M=0.00$ $\tau=19.18$ $\tau_{max}=19.18$
 Tensioni: $\sigma_N=-241.95$ $\sigma_M=-88.71$ $\tau=15.07$ $\sigma_{ID,max}=331.68$

Asta n. 3556 (-7921 -7967) Tubo 60x120x4 mm - S235 Crit. 2

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N_{Ed}=-5539.46$ $M_{y,Ed}=-37.60$ $M_{z,Ed}=8.42$
 Resistenze: $N_{c,Rd}=30796.20$ $M_{y,c,Rd}=951.93$ $M_{z,c,Rd}=632.38$ $L=17.28$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=4.01$ $N_{cr,y}=17709900.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882490.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.96 , 0.76 , 0.96
 Verifica YY: $0.18+0.03+0.01=0.22$
 Verifica ZZ: $0.18+0.02+0.01=0.22$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X1=0.00$ - Classe 3
 Sollecitazioni: $N=-5539.46$ $T_z=-64.81$ $M_y=-37.60$ $T_y=63.52$ $M_z=-2.56$ $M_x=-11.09$
 Tensioni: $\sigma_N=-402.58$ $\sigma_M=-97.45$ $\tau=21.34$ $\sigma_{max}=-500.02$
 Tensioni: $\sigma_N=-402.58$ $\sigma_M=-82.50$ $\tau=36.47$ $\tau_{max}=36.47$
 Tensioni: $\sigma_N=-402.58$ $\sigma_M=-96.24$ $\tau=33.93$ $\sigma_{ID,max}=502.27$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 45 SLU $X1=0.03$
 Sollecitazioni: $N=-5539.42$ $T_z=-66.68$ $M_y=-35.53$ $T_y=63.52$ $M_x=-11.09$
 $V_{Ed}=63.52$ $V_{c,Rd,Red}=5829.01$ $V_{Ed/V_{c,Rd,Red}}=0.01$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V_{Ed}=-66.68$ $V_{c,Rd,Red}=11658.00$ $V_{Ed/V_{c,Rd,Red}}=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=-3362.57$ $T_z=-40.57$ $M_y=-27.49$ $T_y=26.98$ $M_x=-7.73$
 Tensioni: $\sigma_N=-244.37$ $\sigma_M=-64.64$ $\tau=14.87$ $\sigma_{max}=-309.01$
 Tensioni: $\sigma_N=-244.37$ $\sigma_M=-60.33$ $\tau=21.30$ $\tau_{max}=21.30$
 Tensioni: $\sigma_N=-244.37$ $\sigma_M=-64.64$ $\tau=21.30$ $\sigma_{ID,max}=311.21$

Asta n. 3556 (-7967 -8021) Tubo 60x120x4 mm - S235 Crit. 2

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N_{Ed}=-5042.12$ $M_{y,Ed}=-35.14$ $M_{z,Ed}=5.90$
 Resistenze: $N_{c,Rd}=30796.20$ $M_{y,c,Rd}=951.93$ $M_{z,c,Rd}=632.38$ $L=17.28$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=4.01$ $N_{cr,y}=17709900.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882490.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.96 , 0.76 , 0.96
 Verifica YY: $0.16+0.03+0.01=0.20$
 Verifica ZZ: $0.16+0.02+0.01=0.20$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X1=0.17$ - Classe 3
 Sollecitazioni: $N=-5041.85$ $T_z=93.09$ $M_y=-35.14$ $T_y=-51.10$ $M_z=-2.93$ $M_x=13.44$
 Tensioni: $\sigma_N=-366.41$ $\sigma_M=-93.00$ $\tau=25.87$ $\sigma_{max}=-459.41$
 Tensioni: $\sigma_N=-366.41$ $\sigma_M=-77.12$ $\tau=38.04$ $\tau_{max}=38.04$
 Tensioni: $\sigma_N=-366.41$ $\sigma_M=-91.62$ $\tau=35.99$ $\sigma_{ID,max}=462.25$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 75 SLU $X1=0.03$
 Sollecitazioni: $N=-2590.96$ $T_z=117.41$ $M_y=-38.72$ $T_y=-19.31$ $M_x=15.84$
 $V_{Ed}=-19.31$ $V_{c,Rd,Red}=5787.10$ $V_{Ed/V_{c,Rd,Red}}=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V_{Ed}=117.41$ $V_{c,Rd,Red}=11574.20$ $V_{Ed/V_{c,Rd,Red}}=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.17$ - Classe 3
 Sollecitazioni: $N=-3082.88$ $T_z=54.68$ $M_y=-26.70$ $T_y=-26.92$ $M_x=15.07$
 Tensioni: $\sigma_N=-224.05$ $\sigma_M=-62.79$ $\tau=28.99$ $\sigma_{max}=-286.83$
 Tensioni: $\sigma_N=-224.05$ $\sigma_M=0.00$ $\tau=36.08$ $\tau_{max}=36.08$
 Tensioni: $\sigma_N=-224.05$ $\sigma_M=-62.79$ $\tau=35.40$ $\sigma_{ID,max}=293.31$

Asta n. 3556 (-8021 -8147) Tubo 60x120x4 mm - S235 Crit. 2

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: $N_{Ed}=-4516.26$ $M_{y,Ed}=-77.01$ $M_{z,Ed}=-1.95$
 Resistenze: $N_{c,Rd}=30796.20$ $M_{y,c,Rd}=951.93$ $M_{z,c,Rd}=632.38$ $L=17.28$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=4.01$ $N_{cr,y}=17709900.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882490.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$

Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
 Verifica YY: 0.15+0.06+0.00=0.21
 Verifica ZZ: 0.15+0.05+0.00=0.20

- Verifica in termini tensionali [4.2.4] - CC 49 SLU Xl=0.16 - Classe 3
 Sollecitazioni: N=-4516.02 T_x=101.61 M_y=-75.42 T_y=5.98 M_z=-1.01 M_x=14.50
 Tensioni: $\sigma_N=-328.20$ $\sigma_M=-180.89$ $\tau=27.91$ $\sigma_{max}=-509.09$
 Tensioni: $\sigma_N=-328.20$ $\sigma_M=-3.09$ $\tau=41.08$ $\tau_{max}=41.08$
 Tensioni: $\sigma_N=-328.20$ $\sigma_M=-180.89$ $\tau=27.91$ $\sigma_{ID,max}=511.38$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU Xl=0.05
 Sollecitazioni: N=-3532.69 T_x=112.29 M_y=-76.32 T_y=8.82 M_x=17.81
 V,Ed=8.82 Vc,Rd,Red=5769.73 V,Ed/Vc,Rd,Red=0.00
- Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=112.29 Vc,Rd,Red=11539.50 V,Ed/Vc,Rd,Red=0.01
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3
 Sollecitazioni: N=-3056.82 T_x=49.26 M_y=-40.41 M_x=14.59
 Tensioni: $\sigma_N=-222.15$ $\sigma_M=-95.01$ $\tau=28.08$ $\sigma_{max}=-317.16$
 Tensioni: $\sigma_N=-222.15$ $\sigma_M=0.00$ $\tau=34.46$ $\tau_{max}=34.46$
 Tensioni: $\sigma_N=-222.15$ $\sigma_M=-95.01$ $\tau=28.08$ $\sigma_{ID,max}=320.87$

Asta n. 3556 (-8147 -8221) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: N,Ed=-4526.34 M_y,Ed=-91.46 M_z,Ed=-0.55
 Resistenze: Nc,Rd=30796.20 M_y,c,Rd=951.93 M_z,c,Rd=632.38 L=17.28
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=4.01$ Ncr,y=17709900.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882490.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
 Verifica YY: 0.15+0.07+0.00=0.22
 Verifica ZZ: 0.15+0.06+0.00=0.21

- Verifica a pressoflessione retta - CC 54 SLU Xl=0.17 - Classe 1
 Sollecitazioni: N=-3543.58 T_x=38.81 M_y=-104.49 T_y=-3.38 M_x=9.08
 M_y,Ed=-104.49 M_y,c,Rd=1184.58
 N,Ed=-3543.58 Nc,Rd=30796.20 n=N,Ed/Nc,Rd=0.12
 MN_y,c,Rd=1184.58 M_y,Ed/MN_y,c,Rd=0.09
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 49 SLU Xl=0.00
 Sollecitazioni: N=-4526.34 T_x=49.10 M_y=-83.86 M_x=6.61
 V,Ed=49.10 Vc,Rd,Red=11737.20 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3
 Sollecitazioni: N=-3044.17 T_x=17.21 M_y=-47.11 T_y=-1.07 M_x=11.25
 Tensioni: $\sigma_N=-221.23$ $\sigma_M=-110.76$ $\tau=21.65$ $\sigma_{max}=-332.00$
 Tensioni: $\sigma_N=-221.23$ $\sigma_M=0.00$ $\tau=23.88$ $\tau_{max}=23.88$
 Tensioni: $\sigma_N=-221.23$ $\sigma_M=-110.76$ $\tau=21.90$ $\sigma_{ID,max}=334.16$

Asta n. 3556 (-8221 -8309) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: N,Ed=-4529.06 M_y,Ed=-93.11 M_z,Ed=-0.57
 Resistenze: Nc,Rd=30796.20 M_y,c,Rd=951.93 M_z,c,Rd=632.38 L=17.28
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=4.01$ Ncr,y=17710000.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882520.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
 Verifica YY: 0.15+0.07+0.00=0.22
 Verifica ZZ: 0.15+0.06+0.00=0.21

- Verifica a pressoflessione retta - CC 54 SLU Xl=0.05 - Classe 1
 Sollecitazioni: N=-3526.10 M_y=-106.22 T_y=-1.52
 M_y,Ed=-106.22 M_y,c,Rd=1184.58
 N,Ed=-3526.10 Nc,Rd=30796.20 n=N,Ed/Nc,Rd=0.11
 MN_y,c,Rd=1184.58 M_y,Ed/MN_y,c,Rd=0.09

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 53 SLU Xl=0.17
 Sollecitazioni: N=-3122.15 T_x=-3.39 M_y=-86.60 T_y=-8.67 M_x=3.24
 V,Ed=-8.67 Vc,Rd,Red=5898.30 V,Ed/Vc,Rd,Red=0.00
- Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=-3.39 Vc,Rd,Red=11796.60 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=-3016.67$ $T_z=6.13$ $M_y=-47.93$ $T_y=-3.10$ $M_z=1.15$ $M_x=-8.65$
 Tensioni: $\sigma_N=-219.24$ $\sigma_M=-116.76$ $\tau=16.64$ $\sigma_{max}=-335.99$
 Tensioni: $\sigma_N=-219.24$ $\sigma_M=-3.53$ $\tau=17.44$ $\tau_{max}=17.44$
 Tensioni: $\sigma_N=-219.24$ $\sigma_M=-116.76$ $\tau=16.64$ $\sigma_{ID,max}=337.23$

Asta n. 3556 (-8309 -8370) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: $N,Ed=-4538.86$ $M_y,Ed=-88.95$ $M_z,Ed=-1.42$
 Resistenze: $N_c,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=4.01$ $N_{cr,y}=17709900.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882490.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.96 , 0.76 , 0.96
 Verifica YY: $0.15+0.07+0.00=0.22$
 Verifica ZZ: $0.15+0.06+0.00=0.21$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=-5042.52$ $T_z=-45.17$ $M_y=-68.15$ $T_y=-1.74$ $M_z=-1.07$ $M_x=-6.57$
 Tensioni: $\sigma_N=-366.46$ $\sigma_M=-164.02$ $\tau=12.65$ $\sigma_{max}=-530.49$
 Tensioni: $\sigma_N=-366.46$ $\sigma_M=-3.29$ $\tau=18.51$ $\tau_{max}=18.51$
 Tensioni: $\sigma_N=-366.46$ $\sigma_M=-164.02$ $\tau=12.65$ $\sigma_{ID,max}=530.94$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 75 SLU $X_1=0.13$
 Sollecitazioni: $N=-2585.71$ $T_z=-72.26$ $M_y=-86.75$ $T_y=-5.44$ $M_x=-11.52$
 $V,Ed=-5.44$ $V_c,Rd,Red=5825.26$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-72.26$ $V_c,Rd,Red=11650.50$ $V,Ed/V_c,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=-2982.43$ $T_z=-30.17$ $M_y=-46.11$ $T_y=2.28$ $M_x=-9.89$
 Tensioni: $\sigma_N=-216.75$ $\sigma_M=-108.40$ $\tau=19.02$ $\sigma_{max}=-325.15$
 Tensioni: $\sigma_N=-216.75$ $\sigma_M=0.00$ $\tau=22.94$ $\tau_{max}=22.94$
 Tensioni: $\sigma_N=-216.75$ $\sigma_M=-108.40$ $\tau=19.57$ $\sigma_{ID,max}=326.91$

Asta n. 3556 (-8370 -8417) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-5192.48$ $M_y,Ed=-54.17$ $M_z,Ed=7.18$
 Resistenze: $N_c,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=4.01$ $N_{cr,y}=17709900.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882490.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.96 , 0.76 , 0.96
 Verifica YY: $0.17+0.04+0.01=0.22$
 Verifica ZZ: $0.17+0.03+0.01=0.21$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=-5192.48$ $T_z=-57.78$ $M_y=-54.17$ $T_y=54.21$ $M_z=-2.19$ $M_x=-7.99$
 Tensioni: $\sigma_N=-377.36$ $\sigma_M=-135.10$ $\tau=15.38$ $\sigma_{max}=-512.46$
 Tensioni: $\sigma_N=-377.36$ $\sigma_M=-118.87$ $\tau=28.29$ $\tau_{max}=28.29$
 Tensioni: $\sigma_N=-377.36$ $\sigma_M=-134.07$ $\tau=26.12$ $\sigma_{ID,max}=513.42$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 45 SLU $X_1=0.03$
 Sollecitazioni: $N=-5192.43$ $T_z=-59.65$ $M_y=-52.33$ $T_y=54.21$ $M_x=-7.99$
 $V,Ed=54.21$ $V_c,Rd,Red=5856.36$ $V,Ed/V_c,Rd,Red=0.01$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-59.65$ $V_c,Rd,Red=11712.70$ $V,Ed/V_c,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=-2979.32$ $T_z=-35.03$ $M_y=-37.34$ $T_y=17.76$ $M_x=-10.00$
 Tensioni: $\sigma_N=-216.52$ $\sigma_M=-87.80$ $\tau=19.23$ $\sigma_{max}=-304.32$
 Tensioni: $\sigma_N=-216.52$ $\sigma_M=0.00$ $\tau=23.78$ $\tau_{max}=23.78$
 Tensioni: $\sigma_N=-216.52$ $\sigma_M=-87.80$ $\tau=23.46$ $\sigma_{ID,max}=307.02$

Asta n. 3556 (-8417 -8468) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-4647.73$ $M_y,Ed=-52.28$ $M_z,Ed=5.56$
 Resistenze: $N_c,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=4.01$ $N_{cr,y}=17709900.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$

$\lambda_z=6.96$ Ncr,z=5882490.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
 Verifica YY: 0.15+0.04+0.01=0.20
 Verifica ZZ: 0.15+0.03+0.01=0.19

- Verifica in termini tensionali [4.2.4] - CC 49 SLU Xl=0.17 - Classe 3
 Sollecitazioni: N=-4110.87 T_z=101.42 M_y=-69.10 T_y=-38.97 M_z=-2.39 M_x=21.99
 Tensioni: $\sigma_N=-298.75$ $\sigma_M=-170.94$ $\tau=42.31$ $\sigma_{max}=-469.70$
 Tensioni: $\sigma_N=-298.75$ $\sigma_M=-7.34$ $\tau=55.46$ $\tau_{max}=55.46$
 Tensioni: $\sigma_N=-298.75$ $\sigma_M=-169.81$ $\tau=50.03$ $\sigma_{ID,max}=476.51$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 49 SLU Xl=0.09
 Sollecitazioni: N=-4110.99 T_z=106.10 M_y=-60.95 T_y=-38.97 M_z=21.99
 V,Ed=-38.97 Vc,Rd,Red=5732.86 V,Ed/Vc,Rd,Red=0.01
- Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=106.10 Vc,Rd,Red=11465.70 V,Ed/Vc,Rd,Red=0.01
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3
 Sollecitazioni: N=-2659.97 T_z=45.65 M_y=-36.50 T_y=-25.12 M_z=18.47
 Tensioni: $\sigma_N=-193.31$ $\sigma_M=-85.82$ $\tau=35.54$ $\sigma_{max}=-279.13$
 Tensioni: $\sigma_N=-193.31$ $\sigma_M=-80.10$ $\tau=41.52$ $\tau_{max}=41.52$
 Tensioni: $\sigma_N=-193.31$ $\sigma_M=-85.82$ $\tau=41.52$ $\sigma_{ID,max}=288.25$

Asta n. 3556 (-8468 -8530) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: N,Ed=-4056.56 M_y,Ed=-94.71 M_z,Ed=-1.52
 Resistenze: Nc,Rd=30796.20 M_y,c,Rd=951.93 M_z,c,Rd=632.38 L=17.28
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=4.01$ Ncr,y=17709900.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882490.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
 Verifica YY: 0.13+0.08+0.00=0.21
 Verifica ZZ: 0.13+0.06+0.00=0.19
- Verifica in termini tensionali [4.2.4] - CC 49 SLU Xl=0.17 - Classe 3
 Sollecitazioni: N=-4056.30 T_z=90.10 M_y=-94.71 T_y=2.91 M_z=-1.02 M_x=20.37
 Tensioni: $\sigma_N=-294.79$ $\sigma_M=-226.28$ $\tau=39.20$ $\sigma_{max}=-521.07$
 Tensioni: $\sigma_N=-294.79$ $\sigma_M=-3.13$ $\tau=50.87$ $\tau_{max}=50.87$
 Tensioni: $\sigma_N=-294.79$ $\sigma_M=-226.28$ $\tau=39.20$ $\sigma_{ID,max}=525.47$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU Xl=0.02
 Sollecitazioni: N=-3050.24 T_z=101.08 M_y=-92.94 T_y=6.79 M_z=25.61
 V,Ed=6.79 Vc,Rd,Red=5700.87 V,Ed/Vc,Rd,Red=0.00
- Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=101.08 Vc,Rd,Red=11401.70 V,Ed/Vc,Rd,Red=0.01
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3
 Sollecitazioni: N=-2613.01 T_z=39.97 M_y=-48.00 M_z=18.03
 Tensioni: $\sigma_N=-189.90$ $\sigma_M=-112.86$ $\tau=34.69$ $\sigma_{max}=-302.76$
 Tensioni: $\sigma_N=-189.90$ $\sigma_M=0.00$ $\tau=39.87$ $\tau_{max}=39.87$
 Tensioni: $\sigma_N=-189.90$ $\sigma_M=-112.86$ $\tau=34.69$ $\sigma_{ID,max}=308.66$

Asta n. 3556 (-8530 -8615) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: N,Ed=-4033.46 M_y,Ed=-106.57 M_z,Ed=-0.53
 Resistenze: Nc,Rd=30796.20 M_y,c,Rd=951.93 M_z,c,Rd=632.38 L=17.28
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=4.01$ Ncr,y=17709900.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882490.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
 Verifica YY: 0.13+0.09+0.00=0.22
 Verifica ZZ: 0.13+0.07+0.00=0.20
- Verifica a pressoflessione retta - CC 54 SLU Xl=0.17 - Classe 1
 Sollecitazioni: N=-3024.98 T_z=26.52 M_y=-119.62 T_y=-5.51 M_z=16.99
 M_y,Ed=-119.62 M_y,c,Rd=1184.58
 N,Ed=-3024.98 Nc,Rd=30796.20 n=N,Ed/Nc,Rd=0.10
 M_{Ny},c,Rd=1184.58 M_y,Ed/M_{Ny},c,Rd=0.10
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 49 SLU Xl=0.00
 Sollecitazioni: N=-4033.46 T_z=38.77 M_y=-100.75 T_y=-1.21 M_z=12.57

V,Ed=-1.21 Vc,Rd,Red=5815.95 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]
V,Ed=38.77 Vc,Rd,Red=11631.90 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3
Sollecitazioni: N=-2572.15 T_z=10.07 M_y=-52.83 T_y=-2.61 M_x=14.98
Tensioni: σ_N =-186.93 σ_M =-124.20 τ =28.83 σ_{max} =-311.13
Tensioni: σ_N =-186.93 σ_M =0.00 τ =30.13 τ_{max} =30.13
Tensioni: σ_N =-186.93 σ_M =-124.20 τ =29.45 $\sigma_{ID,max}$ =315.29

Asta n. 3556 (-8615 -8712) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
Sollecitazioni: N,Ed=-3997.71 M_y,Ed=-107.42 M_z,Ed=-0.70
Resistenze: Nc,Rd=30796.20 M_y,c,Rd=951.93 M_z,c,Rd=632.38 L=17.28
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 λ_y =4.01 Ncr,y=17709900.00 λ^*_y =0.04 Curva a: Φ_y =0.00 χ_y =1.00
 λ_z =6.96 Ncr,z=5882490.00 λ^*_z =0.07 Curva a: Φ_z =0.00 χ_z =1.00
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96
Verifica YY: 0.13+0.09+0.00=0.22
Verifica ZZ: 0.13+0.07+0.00=0.20

- Verifica a pressoflessione retta - CC 54 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=-2967.01 T_z=-10.25 M_y=-120.37 T_y=-1.74 M_x=8.77
M_y,Ed=-120.37 M_y,c,Rd=1184.58
N,Ed=-2967.01 Nc,Rd=30796.20 n=N,Ed/Nc,Rd=0.10
M_{Ny},c,Rd=1184.58 M_y,Ed/M_{Ny},c,Rd=0.10

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 111 SLU Xl=0.17
Sollecitazioni: N=-622.40 T_z=-21.50 M_y=-54.81 T_y=4.34 M_x=1.78
V,Ed=4.34 Vc,Rd,Red=5911.18 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]
V,Ed=-21.50 Vc,Rd,Red=11822.40 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-2515.19 T_z=-5.56 M_y=-53.13 T_y=-4.51 M_z=1.16 M_x=12.25
Tensioni: σ_N =-182.79 σ_M =-129.02 τ =23.58 σ_{max} =-311.81
Tensioni: σ_N =-182.79 σ_M =-116.59 τ =24.65 τ_{max} =24.65
Tensioni: σ_N =-182.79 σ_M =-129.02 τ =23.58 $\sigma_{ID,max}$ =314.47

Asta n. 3556 (-8712 -8801) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
Sollecitazioni: N,Ed=-4526.16 M_y,Ed=-79.66 M_z,Ed=-1.29
Resistenze: Nc,Rd=30796.20 M_y,c,Rd=951.93 M_z,c,Rd=632.38 L=17.28
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 λ_y =4.01 Ncr,y=17709900.00 λ^*_y =0.04 Curva a: Φ_y =0.00 χ_y =1.00
 λ_z =6.96 Ncr,z=5882490.00 λ^*_z =0.07 Curva a: Φ_z =0.00 χ_z =1.00
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96
Verifica YY: 0.15+0.06+0.00=0.21
Verifica ZZ: 0.15+0.05+0.00=0.20

- Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.09 - Classe 3
Sollecitazioni: N=-4526.02 T_z=-57.37 M_y=-74.52 T_y=-3.62 M_z=-1.00 M_x=-1.63
Tensioni: σ_N =-328.93 σ_M =-178.76 τ =3.13 σ_{max} =-507.69
Tensioni: σ_N =-328.93 σ_M =-3.08 τ =10.57 τ_{max} =10.57
Tensioni: σ_N =-328.93 σ_M =-178.76 τ =3.13 $\sigma_{ID,max}$ =507.72

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 75 SLU Xl=0.14
Sollecitazioni: N=-2119.87 T_z=-85.56 M_y=-92.76 T_y=-6.74 M_x=-5.29
V,Ed=-6.74 Vc,Rd,Red=5880.26 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]
V,Ed=-85.56 Vc,Rd,Red=11760.50 V,Ed/Vc,Rd,Red=0.01

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-2449.05 T_z=-34.83 M_y=-49.89 T_y=-8.48 M_z=1.10 M_x=-10.11
Tensioni: σ_N =-177.98 σ_M =-121.18 τ =19.46 σ_{max} =-299.17
Tensioni: σ_N =-177.98 σ_M =3.37 τ =23.98 τ_{max} =23.98
Tensioni: σ_N =-177.98 σ_M =-121.18 τ =19.46 $\sigma_{ID,max}$ =301.06

Asta n. 3556 (-8801 -8901) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3

Sollecitazioni: N,Ed=-4618.83 My,Ed=-64.08 Mz,Ed=5.08
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=4.01$ Ncr,y=17709900.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882490.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
 Verifica YY: 0.15+0.05+0.01=0.21
 Verifica ZZ: 0.15+0.04+0.01=0.20

- Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-4618.83 Tz=-63.84 My=-64.08 Ty=37.66 Mz=-1.43 Mx=-2.88
 Tensioni: $\sigma_N=-335.67$ $\sigma_M=-155.71$ $\tau=5.53$ $\sigma_{max}=-491.38$
 Tensioni: $\sigma_N=-335.67$ $\sigma_M=-140.62$ $\tau=14.51$ $\tau_{max}=14.51$
 Tensioni: $\sigma_N=-335.67$ $\sigma_M=-155.71$ $\tau=5.53$ $\sigma_{ID,max}=491.47$

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 75 SLU Xl=0.17
 Sollecitazioni: N=-2061.04 Tz=-90.03 My=-67.35 Mx=-6.41
 V,Ed=-90.03 Vc,Rd,Red=11740.60 V,Ed/Vc,Rd,Red=0.01

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-2403.90 Tz=-39.19 My=-40.21 Ty=6.67 Mx=-10.19
 Tensioni: $\sigma_N=-174.70$ $\sigma_M=-94.53$ $\tau=19.60$ $\sigma_{max}=-269.23$
 Tensioni: $\sigma_N=-174.70$ $\sigma_M=0.00$ $\tau=24.68$ $\tau_{max}=24.68$
 Tensioni: $\sigma_N=-174.70$ $\sigma_M=-94.53$ $\tau=21.19$ $\sigma_{ID,max}=271.72$

Asta n. 3556 (-8901 -8975) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-3995.09 My,Ed=-62.44 Mz,Ed=5.16
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=4.01$ Ncr,y=17709900.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882490.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
 Verifica YY: 0.13+0.05+0.01=0.19
 Verifica ZZ: 0.13+0.04+0.01=0.18

- Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.17 - Classe 3
 Sollecitazioni: N=-3994.83 Tz=86.30 My=-62.44 Ty=-44.90 Mz=-2.60 Mx=29.55
 Tensioni: $\sigma_N=-290.32$ $\sigma_M=-156.01$ $\tau=56.87$ $\sigma_{max}=-446.33$
 Tensioni: $\sigma_N=-290.32$ $\sigma_M=-7.98$ $\tau=68.05$ $\tau_{max}=68.05$
 Tensioni: $\sigma_N=-290.32$ $\sigma_M=-154.78$ $\tau=65.76$ $\sigma_{ID,max}=459.45$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 75 SLU Xl=0.00
 Sollecitazioni: N=-1682.65 Tz=111.57 My=-62.48 Ty=-14.48 Mx=36.30
 V,Ed=-14.48 Vc,Rd,Red=5606.50 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=111.57 Vc,Rd,Red=11213.00 V,Ed/Vc,Rd,Red=0.01

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3
 Sollecitazioni: N=-2059.61 Tz=40.88 My=-38.49 Ty=-21.24 Mx=24.50
 Tensioni: $\sigma_N=-149.68$ $\sigma_M=-90.49$ $\tau=47.14$ $\sigma_{max}=-240.17$
 Tensioni: $\sigma_N=-149.68$ $\sigma_M=0.00$ $\tau=52.44$ $\tau_{max}=52.44$
 Tensioni: $\sigma_N=-149.68$ $\sigma_M=-90.49$ $\tau=52.20$ $\sigma_{ID,max}=256.62$

Asta n. 3556 (-8975 -9068) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-3878.20 My,Ed=-83.66 Mz,Ed=-1.48
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=4.01$ Ncr,y=17709900.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882490.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
 Verifica YY: 0.13+0.07+0.00=0.20
 Verifica ZZ: 0.13+0.05+0.00=0.18

- Verifica in termini tensionali [4.2.4] - CC 49 SLU Xl=0.17 - Classe 3
 Sollecitazioni: N=-3316.45 Tz=92.68 My=-105.24 Ty=-1.56 Mz=-1.07 Mx=34.81
 Tensioni: $\sigma_N=-241.02$ $\sigma_M=-251.24$ $\tau=66.98$ $\sigma_{max}=-492.26$
 Tensioni: $\sigma_N=-241.02$ $\sigma_M=-3.29$ $\tau=79.00$ $\tau_{max}=79.00$
 Tensioni: $\sigma_N=-241.02$ $\sigma_M=-251.24$ $\tau=66.98$ $\sigma_{ID,max}=505.74$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 75 SLU Xl=0.00

Sollecitazioni: $N=-1666.39$ $T_z=106.30$ $M_y=-90.80$ $T_y=-2.66$ $M_x=34.94$
 $V,Ed=-2.66$ $Vc,Rd,Red=5618.53$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=106.30$ $Vc,Rd,Red=11237.10$ $V,Ed/Vc,Rd,Red=0.01$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.17$ - Classe 3
 Sollecitazioni: $N=-1995.53$ $T_z=36.00$ $M_y=-48.49$ $T_y=-1.67$ $M_x=24.12$
 Tensioni: $\sigma_N=-145.02$ $\sigma_M=-114.00$ $\tau=46.41$ $\sigma_{max}=-259.02$
 Tensioni: $\sigma_N=-145.02$ $\sigma_M=0.00$ $\tau=51.08$ $\tau_{max}=51.08$
 Tensioni: $\sigma_N=-145.02$ $\sigma_M=-114.00$ $\tau=46.81$ $\sigma_{ID,max}=271.41$

Asta n. 3556 (-9068 -9142) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: $N,Ed=-3242.60$ $M_y,Ed=-117.94$ $M_z,Ed=-0.75$
 Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $Ncr,y=17709900.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $Ncr,z=5882490.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.11+0.09+0.00=0.20$
 Verifica ZZ: $0.11+0.08+0.00=0.18$
- Verifica a pressoflessione retta - CC 54 SLU $X1=0.17$ - Classe 1
 Sollecitazioni: $N=-2248.67$ $T_z=29.85$ $M_y=-130.13$ $T_y=-8.24$ $M_x=33.76$
 $M_y,Ed=-130.13$ $M_y,c,Rd=1184.58$
 $N,Ed=-2248.67$ $Nc,Rd=30796.20$ $n=N,Ed/Nc,Rd=0.07$
 $MN_y,c,Rd=1184.58$ $M_y,Ed/MN_y,c,Rd=0.11$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 49 SLU $X1=0.00$
 Sollecitazioni: $N=-3242.60$ $T_z=41.63$ $M_y=-111.63$ $T_y=-4.57$ $M_x=27.13$
 $V,Ed=-4.57$ $Vc,Rd,Red=5687.49$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=41.63$ $Vc,Rd,Red=11375.00$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.17$ - Classe 3
 Sollecitazioni: $N=-1927.62$ $T_z=12.29$ $M_y=-52.35$ $T_y=-4.32$ $M_x=21.30$
 Tensioni: $\sigma_N=-140.09$ $\sigma_M=-123.08$ $\tau=40.99$ $\sigma_{max}=-263.17$
 Tensioni: $\sigma_N=-140.09$ $\sigma_M=0.00$ $\tau=42.59$ $\tau_{max}=42.59$
 Tensioni: $\sigma_N=-140.09$ $\sigma_M=-123.08$ $\tau=42.02$ $\sigma_{ID,max}=273.05$

Asta n. 3556 (-9142 -9200) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: $N,Ed=-3145.61$ $M_y,Ed=-119.13$ $M_z,Ed=-0.90$
 Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $Ncr,y=17709900.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $Ncr,z=5882490.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.10+0.10+0.00=0.20$
 Verifica ZZ: $0.10+0.08+0.00=0.18$
- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X1=0.16$ - Classe 3
 Sollecitazioni: $N=-3708.67$ $T_z=-15.15$ $M_y=-93.73$ $T_y=-6.90$ $M_z=-1.01$ $M_x=15.85$
 Tensioni: $\sigma_N=-269.52$ $\sigma_M=-223.94$ $\tau=30.50$ $\sigma_{max}=-493.47$
 Tensioni: $\sigma_N=-269.52$ $\sigma_M=3.10$ $\tau=32.47$ $\tau_{max}=32.47$
 Tensioni: $\sigma_N=-269.52$ $\sigma_M=-223.94$ $\tau=30.50$ $\sigma_{ID,max}=496.29$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 53 SLU $X1=0.17$
 Sollecitazioni: $N=-1920.83$ $T_z=-12.55$ $M_y=-105.71$ $T_y=-12.56$ $M_x=25.24$
 $V,Ed=-12.56$ $Vc,Rd,Red=5704.13$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-12.55$ $Vc,Rd,Red=11408.30$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=-1841.49$ $T_z=9.00$ $M_y=-52.48$ $T_y=-5.94$ $M_z=1.15$ $M_x=18.74$
 Tensioni: $\sigma_N=-133.83$ $\sigma_M=-127.45$ $\tau=36.06$ $\sigma_{max}=-261.28$
 Tensioni: $\sigma_N=-133.83$ $\sigma_M=-115.17$ $\tau=37.47$ $\tau_{max}=37.47$
 Tensioni: $\sigma_N=-133.83$ $\sigma_M=-127.45$ $\tau=36.06$ $\sigma_{ID,max}=268.64$

Asta n. 3556 (-9200 -9276) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N, Ed = -3632.36$ My, $Ed = -90.30$ Mz, $Ed = -1.18$
 Resistenze: $N_c, Rd = 30796.20$ My, $c, Rd = 951.93$ Mz, $c, Rd = 632.38$ L=17.28
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 4.01$ Ncr, $y = 17709900.00$ $\lambda^*_y = 0.04$ Curva a: $\Phi_y = 0.00$ $\chi_y = 1.00$
 $\lambda_z = 6.96$ Ncr, $z = 5882490.00$ $\lambda^*_z = 0.07$ Curva a: $\Phi_z = 0.00$ $\chi_z = 1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.12 + 0.07 + 0.00 = 0.19$
 Verifica ZZ: $0.12 + 0.06 + 0.00 = 0.18$

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $X1 = 0.16$ - Classe 3
 Sollecitazioni: $N = -3044.30$ $T_z = -76.54$ $M_y = -101.86$ $T_y = -9.51$ $M_z = -1.11$ $M_x = 11.52$
 Tensioni: $\sigma_N = -221.24$ $\sigma_M = -243.42$ $\tau = 22.17$ $\sigma_{max} = -464.66$
 Tensioni: $\sigma_N = -221.24$ $\sigma_M = 3.41$ $\tau = 32.09$ $\tau_{max} = 32.09$
 Tensioni: $\sigma_N = -221.24$ $\sigma_M = -243.42$ $\tau = 22.17$ $\sigma_{ID, max} = 466.24$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X1 = 0.16$
 Sollecitazioni: $N = -2024.25$ $T_z = -81.14$ $M_y = -112.88$ $T_y = -15.09$ $M_x = 17.08$
 $V, Ed = -15.09$ $V_c, Rd, Red = 5776.13$ $V, Ed/V_c, Rd, Red = 0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed = -81.14$ $V_c, Rd, Red = 11552.30$ $V, Ed/V_c, Rd, Red = 0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1 = 0.00$ - Classe 3
 Sollecitazioni: $N = -1746.81$ $T_z = -34.48$ $M_y = -48.90$ $T_y = -8.99$ $M_z = 1.14$ $M_x = 16.04$
 Tensioni: $\sigma_N = -126.95$ $\sigma_M = -119.00$ $\tau = 30.87$ $\sigma_{max} = -245.94$
 Tensioni: $\sigma_N = -126.95$ $\sigma_M = -3.48$ $\tau = 35.34$ $\tau_{max} = 35.34$
 Tensioni: $\sigma_N = -126.95$ $\sigma_M = -118.46$ $\tau = 32.65$ $\sigma_{ID, max} = 251.84$

Asta n. 3556 (-9276 -9367) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N, Ed = -3622.25$ My, $Ed = -74.85$ Mz, $Ed = 1.71$
 Resistenze: $N_c, Rd = 30796.20$ My, $c, Rd = 951.93$ Mz, $c, Rd = 632.38$ L=17.28
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 4.01$ Ncr, $y = 17709900.00$ $\lambda^*_y = 0.04$ Curva a: $\Phi_y = 0.00$ $\chi_y = 1.00$
 $\lambda_z = 6.96$ Ncr, $z = 5882490.00$ $\lambda^*_z = 0.07$ Curva a: $\Phi_z = 0.00$ $\chi_z = 1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.12 + 0.06 + 0.00 = 0.18$
 Verifica ZZ: $0.12 + 0.05 + 0.00 = 0.17$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X1 = 0.11$ - Classe 3
 Sollecitazioni: $N = -3622.08$ $T_z = -71.48$ $M_y = -67.34$ $T_y = 10.47$ $M_z = 1.05$ $M_x = 8.74$
 Tensioni: $\sigma_N = -263.23$ $\sigma_M = -162.04$ $\tau = 16.81$ $\sigma_{max} = -425.28$
 Tensioni: $\sigma_N = -263.23$ $\sigma_M = -3.21$ $\tau = 26.08$ $\tau_{max} = 26.08$
 Tensioni: $\sigma_N = -263.23$ $\sigma_M = -162.04$ $\tau = 16.81$ $\sigma_{ID, max} = 426.27$

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 49 SLU $X1 = 0.17$
 Sollecitazioni: $N = -2984.62$ $T_z = -88.69$ $M_y = -79.21$ $M_x = 10.01$
 $V, Ed = -88.69$ $V_c, Rd, Red = 11677.10$ $V, Ed/V_c, Rd, Red = 0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1 = 0.00$ - Classe 3
 Sollecitazioni: $N = -1663.77$ $T_z = -39.65$ $M_y = -39.52$ $T_y = -6.57$ $M_x = 15.65$
 Tensioni: $\sigma_N = -120.91$ $\sigma_M = -92.90$ $\tau = 30.12$ $\sigma_{max} = -213.82$
 Tensioni: $\sigma_N = -120.91$ $\sigma_M = 0.00$ $\tau = 35.26$ $\tau_{max} = 35.26$
 Tensioni: $\sigma_N = -120.91$ $\sigma_M = -92.90$ $\tau = 31.68$ $\sigma_{ID, max} = 220.75$

Asta n. 3556 (-9367 -9433) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N, Ed = -2845.68$ My, $Ed = -62.30$ Mz, $Ed = 4.98$
 Resistenze: $N_c, Rd = 30796.20$ My, $c, Rd = 951.93$ Mz, $c, Rd = 632.38$ L=17.28
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 4.01$ Ncr, $y = 17710000.00$ $\lambda^*_y = 0.04$ Curva a: $\Phi_y = 0.00$ $\chi_y = 1.00$
 $\lambda_z = 6.96$ Ncr, $z = 5882510.00$ $\lambda^*_z = 0.07$ Curva a: $\Phi_z = 0.00$ $\chi_z = 1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.09 + 0.05 + 0.01 = 0.15$
 Verifica ZZ: $0.09 + 0.04 + 0.01 = 0.14$

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $X1 = 0.17$ - Classe 3
 Sollecitazioni: $N = -2326.89$ $T_z = 26.37$ $M_y = -78.69$ $T_y = -31.76$ $M_z = -1.92$ $M_x = 38.15$
 Tensioni: $\sigma_N = -169.11$ $\sigma_M = -191.81$ $\tau = 73.42$ $\sigma_{max} = -360.91$
 Tensioni: $\sigma_N = -169.11$ $\sigma_M = -172.68$ $\tau = 80.98$ $\tau_{max} = 80.98$
 Tensioni: $\sigma_N = -169.11$ $\sigma_M = -190.90$ $\tau = 79.71$ $\sigma_{ID, max} = 385.57$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 45 SLU $X_1=0.10$
Sollecitazioni: $N=-2845.52$ $T_z=29.03$ $M_y=-60.44$ $T_y=-43.20$ $M_x=32.13$
 $V,Ed=-43.20$ $Vc,Rd,Red=5643.32$ $V,Ed/Vc,Rd,Red=0.01$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=29.03$ $Vc,Rd,Red=11286.60$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3
Sollecitazioni: $N=-1332.42$ $T_z=33.18$ $M_y=-30.62$ $T_y=-17.23$ $M_z=2.47$ $M_x=21.56$
Tensioni: $\sigma_N=-96.83$ $\sigma_M=-80.73$ $\tau=41.50$ $\sigma_{max}=-177.56$
Tensioni: $\sigma_N=-96.83$ $\sigma_M=7.56$ $\tau=45.80$ $\tau_{max}=45.80$
Tensioni: $\sigma_N=-96.83$ $\sigma_M=-79.56$ $\tau=44.91$ $\sigma_{ID,max}=192.79$

Asta n. 3556 (-9433 -9502) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
Sollecitazioni: $N,Ed=-2626.63$ $M_y,Ed=-67.23$ $M_z,Ed=-1.99$
Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr,y}=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882500.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.09+0.05+0.00=0.14$
Verifica ZZ: $0.09+0.04+0.00=0.13$

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $X_1=0.17$ - Classe 3
Sollecitazioni: $N=-2169.01$ $T_z=10.60$ $M_y=-84.43$ $T_y=-9.31$ $M_z=-1.34$ $M_x=36.08$
Tensioni: $\sigma_N=-157.63$ $\sigma_M=-203.26$ $\tau=69.43$ $\sigma_{max}=-360.89$
Tensioni: $\sigma_N=-157.63$ $\sigma_M=-185.28$ $\tau=71.65$ $\tau_{max}=71.65$
Tensioni: $\sigma_N=-157.63$ $\sigma_M=-202.62$ $\tau=71.28$ $\sigma_{ID,max}=380.82$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 111 SLU $X_1=0.00$
Sollecitazioni: $N=-234.20$ $T_z=36.84$ $M_y=-42.99$ $T_y=-4.60$ $M_x=16.27$
 $V,Ed=-4.60$ $Vc,Rd,Red=5783.35$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=36.84$ $Vc,Rd,Red=11566.70$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.17$ - Classe 3
Sollecitazioni: $N=-1247.88$ $T_z=21.75$ $M_y=-36.77$ $T_y=-4.50$ $M_x=20.92$
Tensioni: $\sigma_N=-90.69$ $\sigma_M=-86.46$ $\tau=40.25$ $\sigma_{max}=-177.15$
Tensioni: $\sigma_N=-90.69$ $\sigma_M=0.00$ $\tau=43.07$ $\tau_{max}=43.07$
Tensioni: $\sigma_N=-90.69$ $\sigma_M=-86.46$ $\tau=41.32$ $\sigma_{ID,max}=191.06$

Asta n. 3556 (-9502 -9543) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
Sollecitazioni: $N,Ed=-2408.03$ $M_y,Ed=-67.22$ $M_z,Ed=-1.64$
Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr,y}=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882500.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.08+0.05+0.00=0.13$
Verifica ZZ: $0.08+0.04+0.00=0.12$

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $X_1=0.17$ - Classe 3
Sollecitazioni: $N=-1999.60$ $T_z=-49.29$ $M_y=-76.58$ $T_y=-9.11$ $M_z=-1.05$ $M_x=28.29$
Tensioni: $\sigma_N=-145.32$ $\sigma_M=-183.76$ $\tau=54.44$ $\sigma_{max}=-329.08$
Tensioni: $\sigma_N=-145.32$ $\sigma_M=3.22$ $\tau=60.83$ $\tau_{max}=60.83$
Tensioni: $\sigma_N=-145.32$ $\sigma_M=-183.27$ $\tau=56.25$ $\sigma_{ID,max}=342.73$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X_1=0.17$
Sollecitazioni: $N=-1311.75$ $T_z=-63.36$ $M_y=-79.35$ $T_y=-9.23$ $M_x=33.23$
 $V,Ed=-9.23$ $Vc,Rd,Red=5633.61$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-63.36$ $Vc,Rd,Red=11267.20$ $V,Ed/Vc,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.17$ - Classe 3
Sollecitazioni: $N=-1152.94$ $T_z=-42.79$ $M_y=-38.33$ $T_y=-5.41$ $M_x=18.22$
Tensioni: $\sigma_N=-83.79$ $\sigma_M=-90.12$ $\tau=35.06$ $\sigma_{max}=-173.91$
Tensioni: $\sigma_N=-83.79$ $\sigma_M=0.00$ $\tau=40.61$ $\tau_{max}=40.61$
Tensioni: $\sigma_N=-83.79$ $\sigma_M=-90.12$ $\tau=36.35$ $\sigma_{ID,max}=184.96$

Asta n. 3556 (-9543 -9591) Tubo 60x120x4 mm - S235 Crit. 2

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-2164.16 My,Ed=-57.47 Mz,Ed=-2.03
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17710000.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882510.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.07+0.05+0.00=0.12
 Verifica ZZ: 0.07+0.04+0.00=0.11
 - Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.10 - Classe 3
 Sollecitazioni: N=-2164.00 Tz=-76.11 My=-49.90 Ty=-14.74 Mz=-1.02 Mx=17.84
 Tensioni: $\sigma_N=-157.27$ $\sigma_M=-120.91$ $\tau=34.32$ $\sigma_{max}=-278.18$
 Tensioni: $\sigma_N=-157.27$ $\sigma_M=3.12$ $\tau=44.19$ $\tau_{max}=44.19$
 Tensioni: $\sigma_N=-157.27$ $\sigma_M=-120.43$ $\tau=37.24$ $\sigma_{ID,max}=285.09$
 - Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU Xl=0.17
 Sollecitazioni: N=-1179.79 Tz=-109.95 My=-54.44 Ty=-12.13 Mx=24.70
 V,Ed=-12.13 Vc,Rd,Red=5708.90 V,Ed/Vc,Rd,Red=0.00
 - Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=-109.95 Vc,Rd,Red=11417.80 V,Ed/Vc,Rd,Red=0.01
 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-1039.28 Tz=-52.09 My=-38.14 Ty=-6.88 Mz=1.11 Mx=15.78
 Tensioni: $\sigma_N=-75.53$ $\sigma_M=-93.59$ $\tau=30.36$ $\sigma_{max}=-169.12$
 Tensioni: $\sigma_N=-75.53$ $\sigma_M=-3.40$ $\tau=37.11$ $\tau_{max}=37.11$
 Tensioni: $\sigma_N=-75.53$ $\sigma_M=-93.07$ $\tau=31.72$ $\sigma_{ID,max}=177.33$

Asta n. 3556 (-9591 -9633) Tubo 60x120x4 mm - S235 Crit. 2

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-1899.24 My,Ed=-36.12 Mz,Ed=-2.05
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17710000.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882510.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.06+0.03+0.00=0.09
 Verifica ZZ: 0.06+0.02+0.00=0.09
 - Verifica in termini tensionali [4.2.4] - CC 49 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-1562.24 Tz=-147.33 My=-44.51 Ty=-17.39 Mz=1.17 Mx=12.60
 Tensioni: $\sigma_N=-113.53$ $\sigma_M=-108.77$ $\tau=24.25$ $\sigma_{max}=-222.31$
 Tensioni: $\sigma_N=-113.53$ $\sigma_M=-3.58$ $\tau=43.35$ $\tau_{max}=43.35$
 Tensioni: $\sigma_N=-113.53$ $\sigma_M=-108.22$ $\tau=27.70$ $\sigma_{ID,max}=226.89$
 - Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU Xl=0.14
 Sollecitazioni: N=-1006.39 Tz=-173.18 My=-19.05 Ty=-18.29 Mx=16.35
 V,Ed=-18.29 Vc,Rd,Red=5782.58 V,Ed/Vc,Rd,Red=0.00
 - Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=-173.18 Vc,Rd,Red=11565.20 V,Ed/Vc,Rd,Red=0.01
 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-905.98 Tz=-76.24 My=-35.24 Ty=-11.15 Mz=1.26 Mx=13.27
 Tensioni: $\sigma_N=-65.84$ $\sigma_M=-87.31$ $\tau=25.54$ $\sigma_{max}=-153.15$
 Tensioni: $\sigma_N=-65.84$ $\sigma_M=-3.86$ $\tau=35.42$ $\tau_{max}=35.42$
 Tensioni: $\sigma_N=-65.84$ $\sigma_M=-86.71$ $\tau=27.75$ $\sigma_{ID,max}=159.95$

Asta n. 3556 (-9633 -9734) Tubo 60x120x4 mm - S235 Crit. 2

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-1645.45 My,Ed=17.88 Mz,Ed=-6.71
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17710000.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882500.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.05+0.01+0.01=0.08
 Verifica ZZ: 0.05+0.01+0.01=0.08
 - Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.17 - Classe 3

Sollecitazioni: $N=-1645.18$ $T_z=-135.65$ $M_y=17.88$ $T_y=-47.25$ $M_z=-6.71$ $M_x=11.03$
 Tensioni: $\sigma_N=-119.56$ $\sigma_M=-65.79$ $\tau=21.23$ $\sigma_{max}=-185.35$
 Tensioni: $\sigma_N=-119.56$ $\sigma_M=20.59$ $\tau=38.82$ $\tau_{max}=38.82$
 Tensioni: $\sigma_N=-119.56$ $\sigma_M=-65.79$ $\tau=21.23$ $\sigma_{ID,max}=188.96$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X_l=0.06$
 Sollecitazioni: $N=-802.68$ $T_z=-172.63$ $M_y=12.38$ $T_y=-31.19$ $M_x=15.25$
 $V,Ed=-31.19$ $V_c,Rd,Red=5792.29$ $V,Ed/V_c,Rd,Red=0.01$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-172.63$ $V_c,Rd,Red=11584.60$ $V,Ed/V_c,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.17$ - Classe 3
 Sollecitazioni: $N=-762.13$ $T_z=-85.59$ $M_y=39.54$ $T_y=-21.05$ $M_z=-2.55$ $M_x=13.07$
 Tensioni: $\sigma_N=-55.39$ $\sigma_M=-101.97$ $\tau=25.16$ $\sigma_{max}=-157.36$
 Tensioni: $\sigma_N=-55.39$ $\sigma_M=7.81$ $\tau=36.25$ $\tau_{max}=36.25$
 Tensioni: $\sigma_N=-55.39$ $\sigma_M=-101.97$ $\tau=25.16$ $\sigma_{ID,max}=163.28$

Asta n. 3556 (-9734 -9846) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N,Ed=-488.10$ $M_y,Ed=39.94$ $M_z,Ed=-1.34$
 Resistenze: $N_c,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr,y}=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882520.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.02+0.04+0.00=0.06$
 Verifica ZZ: $0.02+0.03+0.00=0.05$

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $X_l=0.11$ - Classe 3
 Sollecitazioni: $N=-606.44$ $T_z=129.75$ $M_y=11.11$ $T_y=-15.65$ $M_z=-1.19$ $M_x=56.84$
 Tensioni: $\sigma_N=-44.07$ $\sigma_M=-30.32$ $\tau=109.37$ $\sigma_{max}=-74.39$
 Tensioni: $\sigma_N=-44.07$ $\sigma_M=-3.64$ $\tau=126.19$ $\tau_{max}=126.19$
 Tensioni: $\sigma_N=-44.07$ $\sigma_M=-4.20$ $\tau=126.19$ $\sigma_{ID,max}=223.84$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X_l=0.00$
 Sollecitazioni: $N=-512.53$ $T_z=141.30$ $M_y=33.78$ $T_y=3.68$ $M_x=62.68$
 $V,Ed=3.68$ $V_c,Rd,Red=5373.72$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=141.30$ $V_c,Rd,Red=10747.40$ $V,Ed/V_c,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=-488.10$ $T_z=68.12$ $M_y=39.94$ $T_y=9.21$ $M_z=-1.34$ $M_x=27.84$
 Tensioni: $\sigma_N=-35.47$ $\sigma_M=-98.64$ $\tau=53.56$ $\sigma_{max}=-134.11$
 Tensioni: $\sigma_N=-35.47$ $\sigma_M=-4.10$ $\tau=62.40$ $\tau_{max}=62.40$
 Tensioni: $\sigma_N=-35.47$ $\sigma_M=-98.01$ $\tau=55.39$ $\sigma_{ID,max}=164.38$

Asta n. 3556 (-9846 -9941) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N,Ed=-426.49$ $M_y,Ed=-30.58$ $M_z,Ed=0.54$
 Resistenze: $N_c,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr,y}=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882520.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.01+0.03+0.00=0.05$
 Verifica ZZ: $0.01+0.02+0.00=0.04$

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $X_l=0.17$ - Classe 3
 Sollecitazioni: $N=-455.77$ $T_z=105.85$ $M_y=-27.26$ $T_y=-15.16$ $M_z=-2.21$ $M_x=54.21$
 Tensioni: $\sigma_N=-33.12$ $\sigma_M=-71.91$ $\tau=104.31$ $\sigma_{max}=-105.04$
 Tensioni: $\sigma_N=-33.12$ $\sigma_M=-6.78$ $\tau=118.03$ $\tau_{max}=118.03$
 Tensioni: $\sigma_N=-33.12$ $\sigma_M=-67.64$ $\tau=111.52$ $\sigma_{ID,max}=217.87$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X_l=0.00$
 Sollecitazioni: $N=-495.93$ $T_z=124.30$ $M_y=-1.93$ $T_y=2.72$ $M_x=59.94$
 $V,Ed=2.72$ $V_c,Rd,Red=5397.89$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=124.30$ $V_c,Rd,Red=10795.80$ $V,Ed/V_c,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.17$ - Classe 3

Sollecitazioni: $N=-426.31$ $T_z=54.28$ $M_y=-30.58$ $T_y=-4.39$ $M_x=27.15$
 Tensioni: $\sigma_N=-30.98$ $\sigma_M=-71.90$ $\tau=52.24$ $\sigma_{max}=-102.88$
 Tensioni: $\sigma_N=-30.98$ $\sigma_M=0.00$ $\tau=59.28$ $\tau_{max}=59.28$
 Tensioni: $\sigma_N=-30.98$ $\sigma_M=-71.90$ $\tau=53.29$ $\sigma_{ID,max}=138.22$

Asta n. 3556 (-9941 -10027) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 75 SLU - Classe 3

Sollecitazioni: $N,Ed=-322.93$ $M_y,Ed=-48.12$ $M_z,Ed=0.88$
 Resistenze: $N_c,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr,y}=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882510.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.01+0.04+0.00=0.05$
 Verifica ZZ: $0.01+0.03+0.00=0.04$

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $X1=0.17$ - Classe 3

Sollecitazioni: $N=-294.03$ $T_z=53.50$ $M_y=-45.48$ $T_y=-12.30$ $M_z=-2.20$ $M_x=46.25$
 Tensioni: $\sigma_N=-21.37$ $\sigma_M=-114.72$ $\tau=88.99$ $\sigma_{max}=-136.09$
 Tensioni: $\sigma_N=-21.37$ $\sigma_M=-6.75$ $\tau=95.93$ $\tau_{max}=95.93$
 Tensioni: $\sigma_N=-21.37$ $\sigma_M=-113.68$ $\tau=91.43$ $\sigma_{ID,max}=208.13$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X1=0.00$

Sollecitazioni: $N=-433.96$ $T_z=68.19$ $M_y=-31.58$ $T_y=-2.24$ $M_x=51.19$
 $V,Ed=-2.24$ $V_c,Rd,Red=5475.14$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]

$V,Ed=68.19$ $V_c,Rd,Red=10950.30$ $V,Ed/V_c,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.01$ - Classe 3

Sollecitazioni: $N=-341.45$ $T_z=42.03$ $M_y=-31.29$ $T_y=-6.06$ $M_x=24.71$
 Tensioni: $\sigma_N=-24.81$ $\sigma_M=-73.56$ $\tau=47.54$ $\sigma_{max}=-98.37$
 Tensioni: $\sigma_N=-24.81$ $\sigma_M=0.00$ $\tau=52.99$ $\tau_{max}=52.99$
 Tensioni: $\sigma_N=-24.81$ $\sigma_M=-73.56$ $\tau=48.99$ $\sigma_{ID,max}=129.91$

Asta n. 3556 (-10027 -10119) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 75 SLU - Classe 3

Sollecitazioni: $N,Ed=-255.93$ $M_y,Ed=-50.77$ $M_z,Ed=1.01$
 Resistenze: $N_c,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr,y}=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882520.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.01+0.04+0.00=0.05$
 Verifica ZZ: $0.01+0.03+0.00=0.04$

- Verifica in termini tensionali [4.2.4] - CC 75 SLU $X1=0.00$ - Classe 3

Sollecitazioni: $N=-255.93$ $T_z=-1.98$ $M_y=-50.77$ $T_y=-8.91$ $M_z=1.01$ $M_x=32.55$
 Tensioni: $\sigma_N=-18.60$ $\sigma_M=-122.94$ $\tau=62.63$ $\sigma_{max}=-141.54$
 Tensioni: $\sigma_N=-18.60$ $\sigma_M=-119.36$ $\tau=64.75$ $\tau_{max}=64.75$
 Tensioni: $\sigma_N=-18.60$ $\sigma_M=-122.46$ $\tau=64.39$ $\sigma_{ID,max}=179.83$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 53 SLU $X1=0.17$

Sollecitazioni: $N=-287.17$ $T_z=1.66$ $M_y=-33.17$ $T_y=-12.69$ $M_x=36.38$
 $V,Ed=-12.69$ $V_c,Rd,Red=5605.84$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]

$V,Ed=1.66$ $V_c,Rd,Red=11211.70$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3

Sollecitazioni: $N=-238.16$ $T_z=23.19$ $M_y=-29.85$ $T_y=-6.64$ $M_x=21.75$
 Tensioni: $\sigma_N=-17.31$ $\sigma_M=-70.18$ $\tau=41.86$ $\sigma_{max}=-87.48$
 Tensioni: $\sigma_N=-17.31$ $\sigma_M=0.00$ $\tau=44.86$ $\tau_{max}=44.86$
 Tensioni: $\sigma_N=-17.31$ $\sigma_M=-70.18$ $\tau=43.44$ $\sigma_{ID,max}=115.39$

Asta n. 3556 (-10119 -10188) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 75 SLU - Classe 3

Sollecitazioni: $N,Ed=-165.03$ $M_y,Ed=-46.66$ $M_z,Ed=0.98$
 Resistenze: $N_c,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr,y}=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882520.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.01+0.04+0.00=0.04
 Verifica ZZ: 0.01+0.03+0.00=0.04

- Verifica in termini tensionali [4.2.4] - CC 49 SLU Xl=0.14 - Classe 3
 Sollecitazioni: N=-49.97 T_z=-62.82 M_y=-36.29 T_y=-3.42 M_z=-1.02 M_x=26.40
 Tensioni: σ_N =-3.63 σ_M =-88.92 τ =50.79 σ_{max} =-92.56
 Tensioni: σ_N =-3.63 σ_M =3.13 τ =58.94 τ_{max} =58.94
 Tensioni: σ_N =-3.63 σ_M =-88.44 τ =51.47 $\sigma_{ID,max}$ =128.16
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 75 SLU Xl=0.17
 Sollecitazioni: N=-164.84 T_z=-67.04 M_y=-35.71 T_y=-4.10 M_x=22.48
 V,Ed=-4.10 Vc,Rd,Red=5728.54 V,Ed/Vc,Rd,Red=0.00
- Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=-67.04 Vc,Rd,Red=11457.10 V,Ed/Vc,Rd,Red=0.01
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-134.35 T_z=-36.12 M_y=-23.55 T_y=-7.11 M_x=19.01
 Tensioni: σ_N =-9.76 σ_M =-55.36 τ =36.58 σ_{max} =-65.12
 Tensioni: σ_N =-9.76 σ_M =0.00 τ =41.26 τ_{max} =41.26
 Tensioni: σ_N =-9.76 σ_M =-55.36 τ =38.28 $\sigma_{ID,max}$ =92.93

Asta n. 3556 (-10188 -10243) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 75 SLU - Classe 3
 Sollecitazioni: N,Ed=-63.88 M_y,Ed=-27.75 M_z,Ed=-1.21
 Resistenze: Nc,Rd=30796.20 M_y,c,Rd=951.93 M_z,c,Rd=632.38 L=17.28
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 λ_y =4.01 Ncr,y=17710000.00 λ^*_y =0.04 Curva a: Φ_y =0.00 χ_y =1.00
 λ_z =6.96 Ncr,z=5882520.00 λ^*_z =0.07 Curva a: Φ_z =0.00 χ_z =1.00
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.03
 Verifica ZZ: 0.00+0.02+0.00=0.02
- Verifica in termini tensionali [4.2.4] - CC 54 SLU Xl=0.17 - Classe 3
 Sollecitazioni: N=-74.61 T_z=-111.26 M_y=-7.57 T_y=-17.85 M_z=-1.77 M_x=22.88
 Tensioni: σ_N =-5.42 σ_M =-24.06 τ =44.02 σ_{max} =-29.48
 Tensioni: σ_N =-5.42 σ_M =5.42 τ =58.45 τ_{max} =58.45
 Tensioni: σ_N =-5.42 σ_M =6.26 τ =58.45 $\sigma_{ID,max}$ =101.24
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 75 SLU Xl=0.14
 Sollecitazioni: N=-63.73 T_z=-116.25 M_y=-11.73 T_y=-9.31 M_x=15.56
 V,Ed=-9.31 Vc,Rd,Red=5789.57 V,Ed/Vc,Rd,Red=0.00
- Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=-116.25 Vc,Rd,Red=11579.10 V,Ed/Vc,Rd,Red=0.01
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-42.23 T_z=-51.12 M_y=-12.67 T_y=-9.63 M_x=17.14
 Tensioni: σ_N =-3.07 σ_M =-29.78 τ =32.99 σ_{max} =-32.85
 Tensioni: σ_N =-3.07 σ_M =0.00 τ =39.61 τ_{max} =39.61
 Tensioni: σ_N =-3.07 σ_M =-27.79 τ =36.82 $\sigma_{ID,max}$ =70.85

Asta n. 3562 (-4660 -4681) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-720.19 M_y,Ed=-95.54 M_z,Ed=-2.60
 Resistenze: Nc,Rd=30796.20 M_y,c,Rd=951.93 M_z,c,Rd=632.38 L=16.14
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 λ_y =3.75 Ncr,y=20316600.00 λ^*_y =0.04 Curva a: Φ_y =0.00 χ_y =1.00
 λ_z =6.50 Ncr,z=6748320.00 λ^*_z =0.07 Curva a: Φ_z =0.00 χ_z =1.00
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.02+0.10+0.00=0.12
 Verifica ZZ: 0.02+0.08+0.00=0.10
- Verifica in termini tensionali [4.2.4] - CC 49 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-584.48 T_z=-150.21 M_y=-97.81 T_y=-21.74 M_z=3.08 M_x=-44.32
 Tensioni: σ_N =-42.48 σ_M =-240.85 τ =85.29 σ_{max} =-283.33
 Tensioni: σ_N =-42.48 σ_M =9.44 τ =104.76 τ_{max} =104.76
 Tensioni: σ_N =-42.48 σ_M =-240.85 τ =85.29 $\sigma_{ID,max}$ =319.52
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 68 SLU Xl=0.16
 Sollecitazioni: N=-55.09 T_z=-203.28 M_y=-67.87 T_y=-3.58 M_x=-52.48
 V,Ed=-3.58 Vc,Rd,Red=5463.72 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]
V,Ed=-203.28 Vc,Rd,Red=10927.40 V,Ed/Vc,Rd,Red=0.02
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-720.19 T_z=-125.56 M_y=-95.54 T_y=27.41 M_z=-2.60 M_x=-49.06
Tensioni: σ_N =-52.34 σ_M =-233.83 τ =94.41 σ_{max} =-286.17
Tensioni: σ_N =-52.34 σ_M =-7.99 τ =110.68 τ_{max} =110.68
Tensioni: σ_N =-52.34 σ_M =-232.60 τ =99.84 $\sigma_{ID,max}$ =333.31

Asta n. 3562 (-4681 -4698) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-887.52 M_y,Ed=-68.85 M_z,Ed=4.98
Resistenze: N_c,Rd=30796.20 M_y,c,Rd=951.93 M_z,c,Rd=632.38 L=16.14
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 λ_y =3.75 Ncr,y=20316600.00 λ^*_y =0.04 Curva a: Φ_y =0.00 χ_y =1.00
 λ_z =6.50 Ncr,z=6748320.00 λ^*_z =0.07 Curva a: Φ_z =0.00 χ_z =1.00
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.03+0.07+0.01=0.11
Verifica ZZ: 0.03+0.06+0.01=0.09

- Verifica in termini tensionali [4.2.4] - CC 49 SLU Xl=0.07 - Classe 3
Sollecitazioni: N=-734.24 T_z=-175.50 M_y=-47.86 T_y=-28.84 M_z=-1.12 M_x=-42.34
Tensioni: σ_N =-53.36 σ_M =-116.47 τ =81.47 σ_{max} =-169.83
Tensioni: σ_N =-53.36 σ_M =-3.42 τ =104.22 τ_{max} =104.22
Tensioni: σ_N =-53.36 σ_M =-108.97 τ =93.43 $\sigma_{ID,max}$ =229.21

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 68 SLU Xl=0.16
Sollecitazioni: N=-53.16 T_z=-218.49 M_y=-17.27 T_y=-1.83 M_x=-50.35
V,Ed=-1.83 Vc,Rd,Red=5482.50 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]
V,Ed=-218.49 Vc,Rd,Red=10965.00 V,Ed/Vc,Rd,Red=0.02

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-887.52 T_z=-137.52 M_y=-68.85 T_y=28.86 M_x=-47.93
Tensioni: σ_N =-64.50 σ_M =-161.88 τ =92.22 σ_{max} =-226.38
Tensioni: σ_N =-64.50 σ_M =0.00 τ =110.05 τ_{max} =110.05
Tensioni: σ_N =-64.50 σ_M =-161.88 τ =99.09 $\sigma_{ID,max}$ =284.09

Asta n. 3562 (-4698 -4757) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
Sollecitazioni: N,Ed=-1321.12 M_y,Ed=44.41 M_z,Ed=0.63
Resistenze: N_c,Rd=30796.20 M_y,c,Rd=951.93 M_z,c,Rd=632.38 L=17.28
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 λ_y =4.01 Ncr,y=17710400.00 λ^*_y =0.04 Curva a: Φ_y =0.00 χ_y =1.00
 λ_z =6.96 Ncr,z=5882650.00 λ^*_z =0.07 Curva a: Φ_z =0.00 χ_z =1.00
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.04+0.04+0.00=0.08
Verifica ZZ: 0.04+0.03+0.00=0.07

- Verifica a pressoflessione retta - CC 89 SLU Xl=0.17 - Classe 1
Sollecitazioni: N=84.86 T_z=-316.68 M_y=61.11 T_y=-5.95 M_x=4.60
M_y,Ed=61.11 M_y,c,Rd=1184.58
N,Ed=84.86 N_c,Rd=30796.20 n=N,Ed/N_c,Rd=0.00
M_{Ny},c,Rd=1184.58 M_y,Ed/M_{Ny},c,Rd=0.05

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU Xl=0.17
Sollecitazioni: N=-169.23 T_z=-341.96 M_y=24.95 T_y=-8.27 M_x=-1.17
V,Ed=-8.27 Vc,Rd,Red=5916.58 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]
V,Ed=-341.96 Vc,Rd,Red=11833.20 V,Ed/Vc,Rd,Red=0.03

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-915.88 T_z=-298.81 M_y=-38.15 T_y=-11.31 M_z=2.46 M_x=9.83
Tensioni: σ_N =-66.56 σ_M =-98.41 τ =18.91 σ_{max} =-164.97
Tensioni: σ_N =-66.56 σ_M =-7.56 τ =57.65 τ_{max} =57.65
Tensioni: σ_N =-66.56 σ_M =-92.43 τ =39.29 $\sigma_{ID,max}$ =172.94

Asta n. 3562 (-4757 -4814) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
Sollecitazioni: N,Ed=-1398.92 M_y,Ed=114.88 M_z,Ed=1.36

Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28

α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95

$\lambda_y=4.01$ Ncr,y=17710600.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$

$\lambda_z=6.96$ Ncr,z=5882720.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.05+0.09+0.00=0.14

Verifica ZZ: 0.05+0.07+0.00=0.12

- Verifica in termini tensionali [4.2.4] - CC 68 SLU Xl=0.17 - Classe 3
Sollecitazioni: N=-107.43 Tz=-359.40 My=147.60 Ty=-6.17 Mz=-1.22 Mx=6.18
Tensioni: $\sigma_N=-7.81$ $\sigma_M=-351.34$ $\tau=11.90$ $\sigma_{max}=-359.15$
Tensioni: $\sigma_N=-7.81$ $\sigma_M=3.73$ $\tau=58.48$ $\tau_{max}=58.48$
Tensioni: $\sigma_N=-7.81$ $\sigma_M=-351.34$ $\tau=11.90$ $\sigma_{ID,max}=359.74$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 54 SLU Xl=0.07
Sollecitazioni: N=-168.68 Tz=-362.24 My=77.52 Mx=3.67
V,Ed=-362.24 Vc,Rd,Red=11789.00 V,Ed/Vc,Rd,Red=0.03
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3
Sollecitazioni: N=-883.83 Tz=-318.72 My=104.04 Ty=-2.80 Mz=-1.22 Mx=10.58
Tensioni: $\sigma_N=-64.23$ $\sigma_M=-248.94$ $\tau=20.37$ $\sigma_{max}=-313.17$
Tensioni: $\sigma_N=-64.23$ $\sigma_M=3.74$ $\tau=61.68$ $\tau_{max}=61.68$
Tensioni: $\sigma_N=-64.23$ $\sigma_M=-248.94$ $\tau=20.37$ $\sigma_{ID,max}=315.15$

Asta n. 3562 (-4814 -4869) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-828.14 My,Ed=187.82 Mz,Ed=-1.70
Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=4.01$ Ncr,y=17710600.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882720.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.03+0.19+0.00=0.22
Verifica ZZ: 0.03+0.15+0.00=0.18
- Verifica in termini tensionali [4.2.4] - CC 49 SLU Xl=0.17 - Classe 3
Sollecitazioni: N=-934.90 Tz=-421.08 My=228.72 Ty=-5.33 Mz=-1.26 Mx=18.55
Tensioni: $\sigma_N=-67.94$ $\sigma_M=-542.22$ $\tau=35.69$ $\sigma_{max}=-610.17$
Tensioni: $\sigma_N=-67.94$ $\sigma_M=3.87$ $\tau=90.27$ $\tau_{max}=90.27$
Tensioni: $\sigma_N=-67.94$ $\sigma_M=-542.22$ $\tau=35.69$ $\sigma_{ID,max}=613.29$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 49 SLU Xl=0.11
Sollecitazioni: N=-934.99 Tz=-417.34 My=202.38 Ty=-5.33 Mx=18.55
V,Ed=-5.33 Vc,Rd,Red=5763.22 V,Ed/Vc,Rd,Red=0.00
- Verifica a taglio e torsione dir. Z [4.2.25]
V,Ed=-417.34 Vc,Rd,Red=11526.40 V,Ed/Vc,Rd,Red=0.04
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3
Sollecitazioni: N=-827.96 Tz=-341.40 My=187.82 Ty=-2.87 Mz=-1.40 Mx=13.03
Tensioni: $\sigma_N=-60.17$ $\sigma_M=-446.56$ $\tau=25.08$ $\sigma_{max}=-506.73$
Tensioni: $\sigma_N=-60.17$ $\sigma_M=4.31$ $\tau=69.33$ $\tau_{max}=69.33$
Tensioni: $\sigma_N=-60.17$ $\sigma_M=-446.56$ $\tau=25.08$ $\sigma_{ID,max}=508.59$

Asta n. 3562 (-4869 -4934) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
Sollecitazioni: N,Ed=-956.64 My,Ed=344.13 Mz,Ed=-0.92
Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=4.01$ Ncr,y=17710400.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882650.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.03+0.28+0.00=0.31
Verifica ZZ: 0.03+0.22+0.00=0.25
- Verifica in termini tensionali [4.2.4] - CC 68 SLU Xl=0.17 - Classe 3
Sollecitazioni: N=-29.02 Tz=-466.68 My=369.39 Mz=-1.27 Mx=27.55
Tensioni: $\sigma_N=-2.11$ $\sigma_M=-873.00$ $\tau=53.01$ $\sigma_{max}=-875.11$
Tensioni: $\sigma_N=-2.11$ $\sigma_M=3.91$ $\tau=113.51$ $\tau_{max}=113.51$
Tensioni: $\sigma_N=-2.11$ $\sigma_M=-873.00$ $\tau=53.01$ $\sigma_{ID,max}=879.91$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 49 SLU Xl=0.17
Sollecitazioni: N=-956.38 Tz=-465.62 My=344.13 Mx=28.14

V,Ed=-465.62 Vc,Rd,Red=11357.00 V,Ed/Vc,Rd,Red=0.04

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3
Sollecitazioni: N=-741.43 T_z=-350.00 M_y=274.91 T_y=4.79 M_z=-1.02 M_x=15.40
Tensioni: σ_N =-53.88 σ_M =-649.97 τ =29.64 σ_{max} =-703.85
Tensioni: σ_N =-53.88 σ_M =3.13 τ =75.01 τ_{max} =75.01
Tensioni: σ_N =-53.88 σ_M =-649.97 τ =29.64 $\sigma_{ID,max}$ =705.72

Asta n. 3562 (-4934 -4997) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
Sollecitazioni: N,Ed=-880.64 My,Ed=477.19 Mz,Ed=-1.46
Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 λ_y =4.01 Ncr,y=17710400.00 λ^*_y =0.04 Curva a: Φ_y =0.00 χ_y =1.00
 λ_z =6.96 Ncr,z=5882650.00 λ^*_z =0.07 Curva a: Φ_z =0.00 χ_z =1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.03+0.38+0.00=0.41
Verifica ZZ: 0.03+0.31+0.00=0.34

- Verifica in termini tensionali [4.2.4] - CC 49 SLU Xl=0.17 - Classe 3
Sollecitazioni: N=-880.37 T_z=-536.25 M_y=477.19 T_y=15.12 M_z=1.15 M_x=38.05
Tensioni: σ_N =-63.98 σ_M =-1126.00 τ =73.21 σ_{max} =-1189.98
Tensioni: σ_N =-63.98 σ_M =-3.54 τ =142.72 τ_{max} =142.72
Tensioni: σ_N =-63.98 σ_M =-1125.45 τ =76.21 $\sigma_{ID,max}$ =1196.74

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU Xl=0.17
Sollecitazioni: N=180.84 T_z=-536.92 M_y=492.57 T_y=19.63 M_x=41.80
V,Ed=19.63 Vc,Rd,Red=5558.00 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]
V,Ed=-536.92 Vc,Rd,Red=11116.00 V,Ed/Vc,Rd,Red=0.05

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3
Sollecitazioni: N=687.01 T_z=-375.92 M_y=368.14 T_y=-5.03 M_x=18.36
Tensioni: σ_N =49.93 σ_M =865.54 τ =35.34 σ_{max} =915.47
Tensioni: σ_N =49.93 σ_M =-0.00 τ =84.07 τ_{max} =84.07
Tensioni: σ_N =49.93 σ_M =865.54 τ =36.53 $\sigma_{ID,max}$ =917.65

Asta n. 3562 (-4997 -5051) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
Sollecitazioni: N,Ed=-729.93 My,Ed=610.63 Mz,Ed=2.97
Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 λ_y =4.01 Ncr,y=17710600.00 λ^*_y =0.04 Curva a: Φ_y =0.00 χ_y =1.00
 λ_z =6.96 Ncr,z=5882720.00 λ^*_z =0.07 Curva a: Φ_z =0.00 χ_z =1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.02+0.49+0.00=0.52
Verifica ZZ: 0.02+0.39+0.00=0.42

- Verifica in termini tensionali [4.2.4] - CC 68 SLU Xl=0.17 - Classe 3
Sollecitazioni: N=439.17 T_z=-519.48 M_y=637.64 T_y=47.55 M_z=7.15 M_x=39.67
Tensioni: σ_N =31.92 σ_M =1524.47 τ =76.34 σ_{max} =1556.39
Tensioni: σ_N =31.92 σ_M =-21.94 τ =143.68 τ_{max} =143.68
Tensioni: σ_N =31.92 σ_M =1524.47 τ =76.34 $\sigma_{ID,max}$ =1562.00

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 68 SLU Xl=0.05
Sollecitazioni: N=439.14 T_z=-518.35 M_y=572.42 T_y=52.74 M_x=39.67
V,Ed=52.74 Vc,Rd,Red=5576.75 V,Ed/Vc,Rd,Red=0.01

- Verifica a taglio e torsione dir. Z [4.2.25]
V,Ed=-518.35 Vc,Rd,Red=11153.50 V,Ed/Vc,Rd,Red=0.05

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3
Sollecitazioni: N=646.46 T_z=-361.19 M_y=459.38 T_y=34.39 M_z=4.39 M_x=18.54
Tensioni: σ_N =46.98 σ_M =1095.58 τ =35.67 σ_{max} =1142.56
Tensioni: σ_N =46.98 σ_M =-13.46 τ =82.49 τ_{max} =82.49
Tensioni: σ_N =46.98 σ_M =1095.58 τ =35.67 $\sigma_{ID,max}$ =1144.23

Asta n. 3562 (-5051 -5129) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
Sollecitazioni: N,Ed=-771.00 My,Ed=612.48 Mz,Ed=7.14
Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17710000.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882520.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.03+0.49+0.01=0.53
 Verifica ZZ: 0.03+0.39+0.01=0.43

- Verifica in termini tensionali [4.2.4] - CC 68 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=466.90 Tz=480.64 My=639.36 Ty=-59.68 Mz=9.14 Mx=-25.01
 Tensioni: $\sigma_N=33.93$ $\sigma_M=1535.58$ $\tau=48.12$ $\sigma_{max}=1569.51$
 Tensioni: $\sigma_N=33.93$ $\sigma_M=-28.05$ $\tau=110.42$ $\tau_{max}=110.42$
 Tensioni: $\sigma_N=33.93$ $\sigma_M=1535.58$ $\tau=48.12$ $\sigma_{ID,max}=1571.72$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 68 SLU Xl=0.14
 Sollecitazioni: N=466.93 Tz=479.38 My=571.49 Ty=-65.51 Mx=-25.01
 V,Ed=-65.51 Vc,Rd,Red=5706.20 V,Ed/Vc,Rd,Red=0.01

- Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=479.38 Vc,Rd,Red=11412.40 V,Ed/Vc,Rd,Red=0.04

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=555.80 Tz=322.35 My=460.88 Ty=-28.55 Mz=4.14 Mx=-22.69
 Tensioni: $\sigma_N=40.39$ $\sigma_M=1098.25$ $\tau=43.65$ $\sigma_{max}=1138.65$
 Tensioni: $\sigma_N=40.39$ $\sigma_M=-12.70$ $\tau=85.44$ $\tau_{max}=85.44$
 Tensioni: $\sigma_N=40.39$ $\sigma_M=1098.25$ $\tau=43.65$ $\sigma_{ID,max}=1141.15$

Asta n. 3562 (-5129 -5214) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: N,Ed=-1078.15 My,Ed=490.55 Mz,Ed=-2.42
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17709900.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882460.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.04+0.39+0.00=0.43
 Verifica ZZ: 0.04+0.32+0.00=0.35

- Verifica in termini tensionali [4.2.4] - CC 49 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-1078.15 Tz=488.34 My=490.55 Ty=-27.42 Mz=2.32 Mx=-27.74
 Tensioni: $\sigma_N=-78.35$ $\sigma_M=-1161.54$ $\tau=53.39$ $\sigma_{max}=-1239.90$
 Tensioni: $\sigma_N=-78.35$ $\sigma_M=-7.10$ $\tau=116.69$ $\tau_{max}=116.69$
 Tensioni: $\sigma_N=-78.35$ $\sigma_M=-1161.54$ $\tau=53.39$ $\sigma_{ID,max}=1243.34$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 68 SLU Xl=0.02
 Sollecitazioni: N=154.00 Tz=498.21 My=507.85 Ty=-21.36 Mx=-23.56
 V,Ed=-21.36 Vc,Rd,Red=5718.95 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=498.21 Vc,Rd,Red=11437.90 V,Ed/Vc,Rd,Red=0.04

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=416.46 Tz=336.04 My=379.49 Ty=-10.98 Mx=-22.83
 Tensioni: $\sigma_N=30.27$ $\sigma_M=892.23$ $\tau=43.94$ $\sigma_{max}=922.50$
 Tensioni: $\sigma_N=30.27$ $\sigma_M=-0.00$ $\tau=87.50$ $\tau_{max}=87.50$
 Tensioni: $\sigma_N=30.27$ $\sigma_M=892.23$ $\tau=43.94$ $\sigma_{ID,max}=925.63$

Asta n. 3562 (-5214 -5279) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: N,Ed=-1303.30 My,Ed=369.79 Mz,Ed=-1.59
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17710000.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882520.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.04+0.30+0.00=0.34
 Verifica ZZ: 0.04+0.24+0.00=0.28

- Verifica in termini tensionali [4.2.4] - CC 68 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-34.15 Tz=425.96 My=391.33 Mz=-1.11 Mx=-12.47
 Tensioni: $\sigma_N=-2.48$ $\sigma_M=-924.00$ $\tau=24.00$ $\sigma_{max}=-926.49$
 Tensioni: $\sigma_N=-2.48$ $\sigma_M=3.42$ $\tau=79.21$ $\tau_{max}=79.21$
 Tensioni: $\sigma_N=-2.48$ $\sigma_M=-924.00$ $\tau=24.00$ $\sigma_{ID,max}=927.42$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 49 SLU $X_1=0.00$
Sollecitazioni: $N=-1303.30$ $T_z=417.74$ $M_y=369.79$ $T_y=-7.48$ $M_x=-17.56$
 $V, Ed=-7.48$ $V_c, Rd, Red=5771.91$ $V, Ed/V_c, Rd, Red=0.00$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed=417.74$ $V_c, Rd, Red=11543.80$ $V, Ed/V_c, Rd, Red=0.04$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3
Sollecitazioni: $N=-374.81$ $T_z=309.92$ $M_y=296.34$ $T_y=-7.29$ $M_z=-1.14$ $M_x=-19.66$
Tensioni: $\sigma_N=-27.24$ $\sigma_M=-700.78$ $\tau=37.82$ $\sigma_{max}=-728.02$
Tensioni: $\sigma_N=-27.24$ $\sigma_M=3.50$ $\tau=77.99$ $\tau_{max}=77.99$
Tensioni: $\sigma_N=-27.24$ $\sigma_M=-700.78$ $\tau=37.82$ $\sigma_{ID, max}=730.96$

Asta n. 3562 (-5279 -5330) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
Sollecitazioni: $N, Ed=-1423.65$ $M_y, Ed=266.66$ $M_z, Ed=-1.19$
Resistenze: $N_c, Rd=30796.20$ $M_y, c, Rd=951.93$ $M_z, c, Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr, y}=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr, z}=5882520.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.05+0.21+0.00=0.26$
Verifica ZZ: $0.05+0.17+0.00=0.22$

- Verifica in termini tensionali [4.2.4] - CC 68 SLU $X_1=0.00$ - Classe 3
Sollecitazioni: $N=-103.29$ $T_z=386.75$ $M_y=284.78$ $T_y=4.24$ $M_z=-1.53$ $M_x=-2.13$
Tensioni: $\sigma_N=-7.51$ $\sigma_M=-674.96$ $\tau=4.11$ $\sigma_{max}=-682.46$
Tensioni: $\sigma_N=-7.51$ $\sigma_M=4.68$ $\tau=54.24$ $\tau_{max}=54.24$
Tensioni: $\sigma_N=-7.51$ $\sigma_M=-674.96$ $\tau=4.11$ $\sigma_{ID, max}=682.50$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 49 SLU $X_1=0.00$
Sollecitazioni: $N=-1423.65$ $T_z=372.10$ $M_y=266.66$ $T_y=-2.25$ $M_x=-7.66$
 $V, Ed=-2.25$ $V_c, Rd, Red=5859.33$ $V, Ed/V_c, Rd, Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed=372.10$ $V_c, Rd, Red=11718.70$ $V, Ed/V_c, Rd, Red=0.03$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3
Sollecitazioni: $N=-344.82$ $T_z=301.42$ $M_y=219.17$ $T_y=-6.01$ $M_z=-1.27$ $M_x=-17.17$
Tensioni: $\sigma_N=-25.06$ $\sigma_M=-519.81$ $\tau=33.03$ $\sigma_{max}=-544.87$
Tensioni: $\sigma_N=-25.06$ $\sigma_M=3.91$ $\tau=72.10$ $\tau_{max}=72.10$
Tensioni: $\sigma_N=-25.06$ $\sigma_M=-519.81$ $\tau=33.03$ $\sigma_{ID, max}=547.87$

Asta n. 3562 (-5330 -5384) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
Sollecitazioni: $N, Ed=-2282.17$ $M_y, Ed=150.31$ $M_z, Ed=0.67$
Resistenze: $N_c, Rd=30796.20$ $M_y, c, Rd=951.93$ $M_z, c, Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr, y}=17709900.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr, z}=5882460.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.07+0.12+0.00=0.20$
Verifica ZZ: $0.07+0.10+0.00=0.17$

- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X_1=0.00$ - Classe 3
Sollecitazioni: $N=-194.31$ $T_z=309.27$ $M_y=169.87$ $T_y=4.56$ $M_z=-1.03$
Tensioni: $\sigma_N=-14.12$ $\sigma_M=-403.02$ $\tau=0.00$ $\sigma_{max}=-417.14$
Tensioni: $\sigma_N=-14.12$ $\sigma_M=-3.15$ $\tau=40.09$ $\tau_{max}=40.09$
Tensioni: $\sigma_N=-14.12$ $\sigma_M=-403.02$ $\tau=0.00$ $\sigma_{ID, max}=417.14$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 68 SLU $X_1=0.00$
Sollecitazioni: $N=-127.66$ $T_z=317.76$ $M_y=190.35$ $T_y=4.77$ $M_x=9.08$
 $V, Ed=4.77$ $V_c, Rd, Red=5846.78$ $V, Ed/V_c, Rd, Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed=317.76$ $V_c, Rd, Red=11693.60$ $V, Ed/V_c, Rd, Red=0.03$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3
Sollecitazioni: $N=-323.18$ $T_z=277.85$ $M_y=145.03$ $T_y=5.22$ $M_x=15.45$
Tensioni: $\sigma_N=-23.49$ $\sigma_M=-340.99$ $\tau=29.72$ $\sigma_{max}=-364.48$
Tensioni: $\sigma_N=-23.49$ $\sigma_M=-0.00$ $\tau=65.74$ $\tau_{max}=65.74$
Tensioni: $\sigma_N=-23.49$ $\sigma_M=-340.99$ $\tau=30.97$ $\sigma_{ID, max}=368.40$

Asta n. 3562 (-5384 -5446) Tubo 60x120x4 mm - S235 Crit. 2

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-2401.20 My,Ed=88.49 Mz,Ed=-4.82
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=4.01$ Ncr,y=17710000.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00 \chi_y=1.00$

$\lambda_z=6.96$ Ncr,z=5882520.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00 \chi_z=1.00$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.08+0.07+0.01=0.16

Verifica ZZ: 0.08+0.06+0.01=0.14

- Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-2401.20 Tz=231.21 My=88.49 Ty=-36.14 Mz=1.42 Mx=4.98
 Tensioni: $\sigma_N=-174.51 \sigma_M=-213.09 \tau=9.58 \sigma_{max}=-387.59$
 Tensioni: $\sigma_N=-174.51 \sigma_M=4.36 \tau=39.55 \tau_{max}=39.55$
 Tensioni: $\sigma_N=-174.51 \sigma_M=-213.09 \tau=9.58 \sigma_{ID,max}=387.95$

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 68 SLU Xl=0.00
 Sollecitazioni: N=-128.57 Tz=301.18 My=111.62 Mx=13.59
 V,Ed=301.18 Vc,Rd,Red=11613.90 V,Ed/Vc,Rd,Red=0.03

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-443.06 Tz=186.75 My=77.67 Ty=2.83 Mx=16.19
 Tensioni: $\sigma_N=-32.20 \sigma_M=-182.61 \tau=31.16 \sigma_{max}=-214.81$
 Tensioni: $\sigma_N=-32.20 \sigma_M=-0.00 \tau=55.37 \tau_{max}=55.37$
 Tensioni: $\sigma_N=-32.20 \sigma_M=-182.61 \tau=31.83 \sigma_{ID,max}=221.77$

Asta n. 3562 (-5446 -5509) Tubo 60x120x4 mm - S235 Crit. 2

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-2781.63 My,Ed=34.81 Mz,Ed=-2.94
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=4.01$ Ncr,y=17710000.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00 \chi_y=1.00$

$\lambda_z=6.96$ Ncr,z=5882520.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00 \chi_z=1.00$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.09+0.03+0.00=0.12

Verifica ZZ: 0.09+0.02+0.00=0.12

- Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-2781.63 Tz=191.91 My=34.81 Ty=20.01 Mz=-2.94 Mx=32.27
 Tensioni: $\sigma_N=-202.15 \sigma_M=-92.24 \tau=62.10 \sigma_{max}=-294.39$
 Tensioni: $\sigma_N=-202.15 \sigma_M=-9.02 \tau=86.98 \tau_{max}=86.98$
 Tensioni: $\sigma_N=-202.15 \sigma_M=-86.78 \tau=75.19 \sigma_{ID,max}=316.93$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU Xl=0.06
 Sollecitazioni: N=-256.42 Tz=235.78 My=34.43 Ty=-14.95 Mx=51.15
 V,Ed=-14.95 Vc,Rd,Red=5475.48 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=235.78 Vc,Rd,Red=10951.00 V,Ed/Vc,Rd,Red=0.02

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-557.62 Tz=142.74 My=39.66 Ty=3.52 Mx=37.98
 Tensioni: $\sigma_N=-40.52 \sigma_M=-93.24 \tau=73.09 \sigma_{max}=-133.77$
 Tensioni: $\sigma_N=-40.52 \sigma_M=-0.00 \tau=91.59 \tau_{max}=91.59$
 Tensioni: $\sigma_N=-40.52 \sigma_M=-87.03 \tau=82.82 \sigma_{ID,max}=191.96$

Asta n. 3562 (-5509 -5604) Tubo 60x120x4 mm - S235 Crit. 2

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-2743.31 My,Ed=-41.28 Mz,Ed=0.89
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=4.01$ Ncr,y=17709800.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00 \chi_y=1.00$

$\lambda_z=6.96$ Ncr,z=5882460.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00 \chi_z=1.00$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.09+0.03+0.00=0.12

Verifica ZZ: 0.09+0.03+0.00=0.12

- Verifica a pressoflessione retta - CC 54 SLU Xl=0.17 - Classe 1
 Sollecitazioni: N=-285.27 Tz=202.23 My=-61.98 Ty=-10.01 Mx=37.96
 My,Ed=-61.98 My,c,Rd=1184.58
 N,Ed=-285.27 Nc,Rd=30796.20 n=N,Ed/Nc,Rd=0.01

MNy,c,Rd=1184.58 My,Ed/MNy,c,Rd=0.05

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU Xl=0.00
Sollecitazioni: N=-344.09 T_z=228.13 M_y=-9.90 T_y=-7.57 M_x=53.38
V,Ed=-7.57 Vc,Rd,Red=5455.76 V,Ed/Vc,Rd,Red=0.00
- Verifica a taglio e torsione dir. Z [4.2.25]
V,Ed=228.13 Vc,Rd,Red=10911.50 V,Ed/Vc,Rd,Red=0.02
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3
Sollecitazioni: N=-662.53 T_z=117.47 M_y=-41.13 T_y=-11.97 M_z=-1.37 M_x=41.74
Tensioni: σ_N =-48.15 σ_M =-101.56 τ =80.32 σ_{max} =-149.71
Tensioni: σ_N =-48.15 σ_M =-4.21 τ =95.55 τ_{max} =95.55
Tensioni: σ_N =-48.15 σ_M =-95.11 τ =88.33 $\sigma_{ID,max}$ =209.60

Asta n. 3562 (-5604 -5673) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
Sollecitazioni: N,Ed=-2778.39 My,Ed=-74.84 Mz,Ed=0.85
Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 λ_y =4.01 Ncr,y=17710000.00 λ^*_y =0.04 Curva a: Φ_y =0.00 χ_y =1.00
 λ_z =6.96 Ncr,z=5882520.00 λ^*_z =0.07 Curva a: Φ_z =0.00 χ_z =1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.09+0.06+0.00=0.15
Verifica ZZ: 0.09+0.05+0.00=0.14
- Verifica a pressoflessione retta - CC 54 SLU Xl=0.17 - Classe 1
Sollecitazioni: N=-352.86 T_z=141.39 M_y=-100.88 T_y=-8.01 M_x=46.62
My,Ed=-100.88 My,c,Rd=1184.58
N,Ed=-352.86 Nc,Rd=30796.20 n=N,Ed/Nc,Rd=0.01
MNy,c,Rd=1184.58 My,Ed/MNy,c,Rd=0.09

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU Xl=0.00
Sollecitazioni: N=-423.61 T_z=163.82 M_y=-64.09 T_y=-4.53 M_x=61.66
V,Ed=-4.53 Vc,Rd,Red=5382.67 V,Ed/Vc,Rd,Red=0.00
- Verifica a taglio e torsione dir. Z [4.2.25]
V,Ed=163.82 Vc,Rd,Red=10765.30 V,Ed/Vc,Rd,Red=0.02
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3
Sollecitazioni: N=-808.62 T_z=94.13 M_y=-63.73 T_y=-7.74 M_z=-1.21 M_x=44.43
Tensioni: σ_N =-58.77 σ_M =-154.13 τ =85.50 σ_{max} =-212.90
Tensioni: σ_N =-58.77 σ_M =-3.71 τ =97.70 τ_{max} =97.70
Tensioni: σ_N =-58.77 σ_M =-153.56 τ =87.03 $\sigma_{ID,max}$ =260.39

Asta n. 3562 (-5673 -5744) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
Sollecitazioni: N,Ed=-2841.74 My,Ed=-96.30 Mz,Ed=0.92
Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 λ_y =4.01 Ncr,y=17710000.00 λ^*_y =0.04 Curva a: Φ_y =0.00 χ_y =1.00
 λ_z =6.96 Ncr,z=5882520.00 λ^*_z =0.07 Curva a: Φ_z =0.00 χ_z =1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.09+0.08+0.00=0.17
Verifica ZZ: 0.09+0.06+0.00=0.16
- Verifica a pressoflessione retta - CC 54 SLU Xl=0.17 - Classe 1
Sollecitazioni: N=-416.85 T_z=96.72 M_y=-127.03 T_y=-7.45 M_x=55.28
My,Ed=-127.03 My,c,Rd=1184.58
N,Ed=-416.85 Nc,Rd=30796.20 n=N,Ed/Nc,Rd=0.01
MNy,c,Rd=1184.58 My,Ed/MNy,c,Rd=0.11

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU Xl=0.00
Sollecitazioni: N=-493.60 T_z=117.32 M_y=-101.96 T_y=-3.70 M_x=69.75
V,Ed=-3.70 Vc,Rd,Red=5311.27 V,Ed/Vc,Rd,Red=0.00
- Verifica a taglio e torsione dir. Z [4.2.25]
V,Ed=117.32 Vc,Rd,Red=10622.50 V,Ed/Vc,Rd,Red=0.01
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3
Sollecitazioni: N=-935.64 T_z=75.46 M_y=-83.00 T_y=-6.13 M_z=-1.12 M_x=47.14
Tensioni: σ_N =-68.00 σ_M =-199.11 τ =90.72 σ_{max} =-267.10
Tensioni: σ_N =-68.00 σ_M =-3.44 τ =100.50 τ_{max} =100.50
Tensioni: σ_N =-68.00 σ_M =-198.58 τ =91.93 $\sigma_{ID,max}$ =310.51

Asta n. 3562 (-5744 -5805) Tubo 60x120x4 mm - S235 Crit. 2

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-2918.25 My,Ed=-106.03 Mz,Ed=1.36
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17709800.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00 \chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882460.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00 \chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.09+0.09+0.00=0.18
 Verifica ZZ: 0.09+0.07+0.00=0.17

 - Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.06 - Classe 3
 Sollecitazioni: N=-2918.15 Tz=36.57 My=-102.37 Ty=-5.47 Mz=1.02 Mx=53.07
 Tensioni: $\sigma_N=-212.07 \sigma_M=-244.28 \tau=102.13 \sigma_{max}=-456.36$
 Tensioni: $\sigma_N=-212.07 \sigma_M=3.12 \tau=106.87 \tau_{max}=106.87$
 Tensioni: $\sigma_N=-212.07 \sigma_M=-243.80 \tau=103.21 \sigma_{ID,max}=489.68$

 - Verifica a taglio e torsione dir. Y [4.2.25] - CC 89 SLU Xl=0.00
 Sollecitazioni: N=-724.90 Tz=55.30 My=-122.52 Ty=-7.53 Mx=78.53
 V,Ed=-7.53 Vc,Rd,Red=5233.76 V,Ed/Vc,Rd,Red=0.00

 - Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=55.30 Vc,Rd,Red=10467.50 V,Ed/Vc,Rd,Red=0.01

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3
 Sollecitazioni: N=-1039.55 Tz=53.39 My=-96.43 Ty=-4.87 Mx=49.74
 Tensioni: $\sigma_N=-75.55 \sigma_M=-226.72 \tau=95.71 \sigma_{max}=-302.26$
 Tensioni: $\sigma_N=-75.55 \sigma_M=0.00 \tau=102.64 \tau_{max}=102.64$
 Tensioni: $\sigma_N=-75.55 \sigma_M=-226.72 \tau=96.87 \sigma_{ID,max}=345.71$

Asta n. 3562 (-5805 -5851) Tubo 60x120x4 mm - S235 Crit. 2

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-3039.84 My,Ed=-109.66 Mz,Ed=-4.11
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17710000.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00 \chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882520.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00 \chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.10+0.09+0.01=0.19
 Verifica ZZ: 0.10+0.07+0.01=0.18

 - Verifica in termini tensionali [4.2.4] - CC 49 SLU Xl=0.17 - Classe 3
 Sollecitazioni: N=-2196.23 Tz=16.69 My=-138.46 Ty=-25.34 Mz=-2.55 Mx=67.57
 Tensioni: $\sigma_N=-159.61 \sigma_M=-334.55 \tau=130.02 \sigma_{max}=-494.16$
 Tensioni: $\sigma_N=-159.61 \sigma_M=-303.83 \tau=136.05 \tau_{max}=136.05$
 Tensioni: $\sigma_N=-159.61 \sigma_M=-333.35 \tau=135.04 \sigma_{ID,max}=545.63$

 - Verifica a taglio e torsione dir. Y [4.2.25] - CC 45 SLU Xl=0.05
 Sollecitazioni: N=-3039.77 Tz=17.73 My=-107.91 Ty=-37.44 Mx=54.99
 V,Ed=-37.44 Vc,Rd,Red=5441.57 V,Ed/Vc,Rd,Red=0.01

 - Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=17.73 Vc,Rd,Red=10883.10 V,Ed/Vc,Rd,Red=0.00

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3
 Sollecitazioni: N=-1124.63 Tz=45.59 My=-107.19 Ty=-14.09 Mz=-2.05 Mx=50.37
 Tensioni: $\sigma_N=-81.73 \sigma_M=-259.29 \tau=96.92 \sigma_{max}=-341.02$
 Tensioni: $\sigma_N=-81.73 \sigma_M=-6.30 \tau=102.83 \tau_{max}=102.83$
 Tensioni: $\sigma_N=-81.73 \sigma_M=-258.32 \tau=99.72 \sigma_{ID,max}=381.40$

Asta n. 3562 (-5851 -5893) Tubo 60x120x4 mm - S235 Crit. 2

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-3565.29 My,Ed=-122.32 Mz,Ed=-4.31
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17709800.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00 \chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882460.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00 \chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.12+0.10+0.01=0.22
 Verifica ZZ: 0.12+0.08+0.01=0.20

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $X1=0.06$ - Classe 3
 Sollecitazioni: $N=-2679.24$ $T_z=66.90$ $M_y=-145.22$ $T_y=10.75$ $M_z=-1.15$ $M_x=31.77$
 Tensioni: $\sigma_N=-194.71$ $\sigma_M=-345.49$ $\tau=61.14$ $\sigma_{max}=-540.20$
 Tensioni: $\sigma_N=-194.71$ $\sigma_M=-3.53$ $\tau=69.81$ $\tau_{max}=69.81$
 Tensioni: $\sigma_N=-194.71$ $\sigma_M=-345.49$ $\tau=61.14$ $\sigma_{ID,max}=550.48$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU $X1=0.03$
 Sollecitazioni: $N=-844.87$ $T_z=69.01$ $M_y=-146.36$ $T_y=-11.53$ $M_x=44.49$
 $V,Ed=-11.53$ $Vc,Rd,Red=5534.27$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=69.01$ $Vc,Rd,Red=11068.50$ $V,Ed/Vc,Rd,Red=0.01$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.17$ - Classe 3
 Sollecitazioni: $N=-1462.02$ $T_z=42.33$ $M_y=-110.97$ $T_y=-14.40$ $M_z=-1.25$ $M_x=33.76$
 Tensioni: $\sigma_N=-106.25$ $\sigma_M=-265.31$ $\tau=64.96$ $\sigma_{max}=-371.56$
 Tensioni: $\sigma_N=-106.25$ $\sigma_M=-3.83$ $\tau=70.45$ $\tau_{max}=70.45$
 Tensioni: $\sigma_N=-106.25$ $\sigma_M=-264.72$ $\tau=67.82$ $\sigma_{ID,max}=389.13$

Asta n. 3562 (-5893 -5972) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: $N,Ed=-2703.61$ $M_y,Ed=-166.99$ $M_z,Ed=1.21$
 Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $Ncr,y=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $Ncr,z=5882520.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.09+0.13+0.00=0.22$
 Verifica ZZ: $0.09+0.11+0.00=0.20$

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $X1=0.02$ - Classe 3
 Sollecitazioni: $N=-2703.58$ $T_z=58.72$ $M_y=-158.50$ $T_y=-7.53$ $M_z=1.09$ $M_x=32.94$
 Tensioni: $\sigma_N=-196.48$ $\sigma_M=-376.50$ $\tau=63.39$ $\sigma_{max}=-572.98$
 Tensioni: $\sigma_N=-196.48$ $\sigma_M=3.34$ $\tau=71.00$ $\tau_{max}=71.00$
 Tensioni: $\sigma_N=-196.48$ $\sigma_M=-376.50$ $\tau=63.39$ $\sigma_{ID,max}=583.40$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 37 SLU $X1=0.00$
 Sollecitazioni: $N=-875.40$ $T_z=67.30$ $M_y=-145.72$ $T_y=-8.78$ $M_x=26.93$
 $V,Ed=-8.78$ $Vc,Rd,Red=5689.26$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=67.30$ $Vc,Rd,Red=11378.50$ $V,Ed/Vc,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.17$ - Classe 3
 Sollecitazioni: $N=-1573.84$ $T_z=36.80$ $M_y=-116.00$ $T_y=-10.31$ $M_z=-1.41$ $M_x=33.96$
 Tensioni: $\sigma_N=-114.38$ $\sigma_M=-277.72$ $\tau=65.34$ $\sigma_{max}=-392.10$
 Tensioni: $\sigma_N=-114.38$ $\sigma_M=-4.33$ $\tau=70.11$ $\tau_{max}=70.11$
 Tensioni: $\sigma_N=-114.38$ $\sigma_M=-277.06$ $\tau=67.39$ $\sigma_{ID,max}=408.46$

Asta n. 3562 (-5972 -6075) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: $N,Ed=-2780.41$ $M_y,Ed=-169.39$ $M_z,Ed=0.85$
 Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $Ncr,y=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $Ncr,z=5882520.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.09+0.14+0.00=0.23$
 Verifica ZZ: $0.09+0.11+0.00=0.20$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X1=0.00$ - Classe 3
 Sollecitazioni: $N=-3541.17$ $T_z=3.27$ $M_y=-135.98$ $T_y=-5.48$ $M_z=1.01$ $M_x=32.93$
 Tensioni: $\sigma_N=-257.35$ $\sigma_M=-323.28$ $\tau=63.36$ $\sigma_{max}=-580.63$
 Tensioni: $\sigma_N=-257.35$ $\sigma_M=-298.39$ $\tau=64.66$ $\tau_{max}=64.66$
 Tensioni: $\sigma_N=-257.35$ $\sigma_M=-323.28$ $\tau=63.36$ $\sigma_{ID,max}=590.91$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 74 SLU $X1=0.00$
 Sollecitazioni: $N=-1453.85$ $T_z=-7.02$ $M_y=-125.89$ $T_y=-13.04$ $M_x=28.99$
 $V,Ed=-13.04$ $Vc,Rd,Red=5671.07$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-7.02$ $Vc,Rd,Red=11342.10$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.13$ - Classe 3
 Sollecitazioni: $N=-1687.39$ $T_z=-20.87$ $M_y=-115.46$ $T_y=-6.43$ $M_z=-1.04$ $M_x=36.78$
 Tensioni: $\sigma_N=-122.63$ $\sigma_M=-275.15$ $\tau=70.78$ $\sigma_{max}=-397.78$
 Tensioni: $\sigma_N=-122.63$ $\sigma_M=3.20$ $\tau=73.48$ $\tau_{max}=73.48$
 Tensioni: $\sigma_N=-122.63$ $\sigma_M=-274.66$ $\tau=72.05$ $\sigma_{ID,max}=416.43$

Asta n. 3562 (-6075 -6143) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: $N,Ed=-2864.18$ $M_y,Ed=-165.83$ $M_z,Ed=0.76$
 Resistenze: $N_c,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr, $y=17709800.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr, $z=5882460.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.09+0.13+0.00=0.23$
 Verifica ZZ: $0.09+0.11+0.00=0.20$

- Verifica a pressoflessione retta - CC 41 SLU $X_1=0.00$ - Classe 1
 Sollecitazioni: $N=-1111.09$ $T_z=-42.69$ $M_y=-170.46$ $T_y=-3.58$ $M_x=60.00$
 $M_y,Ed=-170.46$ $M_y,c,Rd=1184.58$
 $N,Ed=-1111.09$ $N_c,Rd=30796.20$ $n=N,Ed/N_c,Rd=0.04$
 $MN_y,c,Rd=1184.58$ $M_y,Ed/MN_y,c,Rd=0.14$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 49 SLU $X_1=0.17$
 Sollecitazioni: $N=-2863.92$ $T_z=-57.93$ $M_y=-156.71$ $T_y=-4.53$ $M_x=47.70$
 $V,Ed=-4.53$ $V_c,Rd,Red=5505.95$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-57.93$ $V_c,Rd,Red=11011.90$ $V,Ed/V_c,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=-1785.34$ $T_z=-28.33$ $M_y=-113.09$ $T_y=-4.55$ $M_x=39.62$
 Tensioni: $\sigma_N=-129.75$ $\sigma_M=-265.89$ $\tau=76.24$ $\sigma_{max}=-395.64$
 Tensioni: $\sigma_N=-129.75$ $\sigma_M=0.00$ $\tau=79.91$ $\tau_{max}=79.91$
 Tensioni: $\sigma_N=-129.75$ $\sigma_M=-265.89$ $\tau=77.32$ $\sigma_{ID,max}=417.69$

Asta n. 3562 (-6143 -6200) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-3653.00$ $M_y,Ed=-119.43$ $M_z,Ed=1.35$
 Resistenze: $N_c,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr, $y=17709900.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr, $z=5882460.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.12+0.10+0.00=0.22$
 Verifica ZZ: $0.12+0.08+0.00=0.20$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=-3653.00$ $T_z=-84.65$ $M_y=-119.43$ $T_y=-2.10$ $M_z=1.35$ $M_x=44.59$
 Tensioni: $\sigma_N=-265.48$ $\sigma_M=-285.57$ $\tau=85.80$ $\sigma_{max}=-551.05$
 Tensioni: $\sigma_N=-265.48$ $\sigma_M=-4.15$ $\tau=96.77$ $\tau_{max}=96.77$
 Tensioni: $\sigma_N=-265.48$ $\sigma_M=-285.57$ $\tau=85.80$ $\sigma_{ID,max}=570.74$

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 41 SLU $X_1=0.17$
 Sollecitazioni: $N=-1150.66$ $T_z=-117.98$ $M_y=-134.99$ $M_x=67.58$
 $V,Ed=-117.98$ $V_c,Rd,Red=10661.00$ $V,Ed/V_c,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=-1860.49$ $T_z=-57.33$ $M_y=-103.80$ $T_y=-2.44$ $M_x=42.63$
 Tensioni: $\sigma_N=-135.21$ $\sigma_M=-244.05$ $\tau=82.03$ $\sigma_{max}=-379.26$
 Tensioni: $\sigma_N=-135.21$ $\sigma_M=0.00$ $\tau=89.47$ $\tau_{max}=89.47$
 Tensioni: $\sigma_N=-135.21$ $\sigma_M=-244.05$ $\tau=82.62$ $\sigma_{ID,max}=405.36$

Asta n. 3562 (-6200 -6252) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-3750.10$ $M_y,Ed=-95.10$ $M_z,Ed=-4.02$
 Resistenze: $N_c,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr, $y=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr, $z=5882520.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.12+0.08+0.01=0.20$

Verifica ZZ: $0.12+0.06+0.01=0.19$

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $X1=0.00$ - Classe 3
Sollecitazioni: $N=-3004.70$ $T_x=-118.71$ $M_y=-118.48$ $T_y=-26.60$ $M_z=2.17$ $M_x=56.16$
Tensioni: $\sigma_N=-218.37$ $\sigma_M=-286.23$ $\tau=108.07$ $\sigma_{max}=-504.59$
Tensioni: $\sigma_N=-218.37$ $\sigma_M=-6.65$ $\tau=123.46$ $\tau_{max}=123.46$
Tensioni: $\sigma_N=-218.37$ $\sigma_M=-285.20$ $\tau=113.34$ $\sigma_{ID,max}=540.49$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU $X1=0.17$
Sollecitazioni: $N=-1165.10$ $T_x=-124.20$ $M_y=-103.70$ $T_y=-2.68$ $M_x=68.44$
 $V,Ed=-2.68$ $Vc,Rd,Red=5322.86$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-124.20$ $Vc,Rd,Red=10645.70$ $V,Ed/Vc,Rd,Red=0.01$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3
Sollecitazioni: $N=-1926.09$ $T_x=-62.10$ $M_y=-87.99$ $T_y=-19.05$ $M_x=42.77$
Tensioni: $\sigma_N=-139.98$ $\sigma_M=-206.87$ $\tau=82.30$ $\sigma_{max}=-346.85$
Tensioni: $\sigma_N=-139.98$ $\sigma_M=0.00$ $\tau=90.35$ $\tau_{max}=90.35$
Tensioni: $\sigma_N=-139.98$ $\sigma_M=-206.87$ $\tau=86.84$ $\sigma_{ID,max}=378.05$

Asta n. 3562 (-6252 -6311) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
Sollecitazioni: $N,Ed=-4312.34$ $M_y,Ed=-89.32$ $M_z,Ed=-5.38$
Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $Ncr,y=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $Ncr,z=5882520.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
Verifica YY: $0.14+0.07+0.01=0.22$
Verifica ZZ: $0.14+0.06+0.01=0.21$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X1=0.17$ - Classe 3
Sollecitazioni: $N=-4312.07$ $T_x=48.05$ $M_y=-89.32$ $T_y=38.41$ $M_z=1.26$ $M_x=4.09$
Tensioni: $\sigma_N=-313.38$ $\sigma_M=-214.45$ $\tau=7.88$ $\sigma_{max}=-527.83$
Tensioni: $\sigma_N=-313.38$ $\sigma_M=196.01$ $\tau=17.03$ $\tau_{max}=17.03$
Tensioni: $\sigma_N=-313.38$ $\sigma_M=-214.45$ $\tau=7.88$ $\sigma_{ID,max}=528.00$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 45 SLU $X1=0.13$
Sollecitazioni: $N=-4312.14$ $T_x=50.85$ $M_y=-86.99$ $T_y=38.41$ $M_x=4.09$
 $V,Ed=38.41$ $Vc,Rd,Red=5890.77$ $V,Ed/Vc,Rd,Red=0.01$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=50.85$ $Vc,Rd,Red=11781.50$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.17$ - Classe 3
Sollecitazioni: $N=-2255.79$ $T_x=43.61$ $M_y=-81.63$ $T_y=-8.69$ $M_x=12.09$
Tensioni: $\sigma_N=-163.94$ $\sigma_M=-191.91$ $\tau=23.25$ $\sigma_{max}=-355.85$
Tensioni: $\sigma_N=-163.94$ $\sigma_M=0.00$ $\tau=28.91$ $\tau_{max}=28.91$
Tensioni: $\sigma_N=-163.94$ $\sigma_M=-191.91$ $\tau=25.32$ $\sigma_{ID,max}=358.54$

Asta n. 3562 (-6311 -6379) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
Sollecitazioni: $N,Ed=-4231.33$ $M_y,Ed=-101.02$ $M_z,Ed=1.41$
Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $Ncr,y=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $Ncr,z=5882520.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
Verifica YY: $0.14+0.08+0.00=0.22$
Verifica ZZ: $0.14+0.07+0.00=0.20$

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $X1=0.05$ - Classe 3
Sollecitazioni: $N=-3546.89$ $T_x=59.20$ $M_y=-119.29$ $T_y=-8.31$ $M_z=1.07$ $M_x=5.03$
Tensioni: $\sigma_N=-257.77$ $\sigma_M=-284.25$ $\tau=9.68$ $\sigma_{max}=-542.02$
Tensioni: $\sigma_N=-257.77$ $\sigma_M=3.29$ $\tau=17.36$ $\tau_{max}=17.36$
Tensioni: $\sigma_N=-257.77$ $\sigma_M=-284.25$ $\tau=9.68$ $\sigma_{ID,max}=542.28$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 37 SLU $X1=0.00$
Sollecitazioni: $N=-1482.54$ $T_x=72.84$ $M_y=-114.06$ $T_y=-9.35$ $M_x=-1.17$
 $V,Ed=-9.35$ $Vc,Rd,Red=5916.57$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica a taglio e torsione dir. Z [4.2.25]

V,Ed=72.84 Vc,Rd,Red=11833.10 V,Ed/Vc,Rd,Red=0.01

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3
Sollecitazioni: N=-2314.82 T_z=38.26 M_y=-88.68 T_y=-9.04 M_z=-1.32 M_x=12.14
Tensioni: σ_N =-168.23 σ_M =-213.16 τ =23.35 σ_{max} =-381.38
Tensioni: σ_N =-168.23 σ_M =-4.04 τ =28.31 τ_{max} =28.31
Tensioni: σ_N =-168.23 σ_M =-213.16 τ =23.35 $\sigma_{ID,max}$ =383.52

Asta n. 3562 (-6379 -6492) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
Sollecitazioni: N,Ed=-4241.41 M_y,Ed=-103.06 M_z,Ed=0.98
Resistenze: Nc,Rd=30796.20 M_y,c,Rd=951.93 M_z,c,Rd=632.38 L=17.28
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 λ_y =4.01 Ncr,y=17710000.00 λ^*_y =0.04 Curva a: Φ_y =0.00 χ_y =1.00
 λ_z =6.96 Ncr,z=5882520.00 λ^*_z =0.07 Curva a: Φ_z =0.00 χ_z =1.00
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96
Verifica YY: 0.14+0.08+0.00=0.22
Verifica ZZ: 0.14+0.07+0.00=0.21

- Verifica a pressoflessione retta - CC 41 SLU Xl=0.01 - Classe 1
Sollecitazioni: N=-1635.99 M_y=-134.74 T_y=-5.07 M_x=22.17
M_y,Ed=-134.74 M_y,c,Rd=1184.58
N,Ed=-1635.99 Nc,Rd=30796.20 n=N,Ed/Nc,Rd=0.05
M_{Ny},c,Rd=1184.58 M_y,Ed/M_{Ny},c,Rd=0.11

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 74 SLU Xl=0.00
Sollecitazioni: N=-2234.04 T_z=-5.73 M_y=-98.35 T_y=-11.76 M_x=8.69
V,Ed=-11.76 Vc,Rd,Red=5850.17 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]
V,Ed=-5.73 Vc,Rd,Red=11700.30 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.11 - Classe 3
Sollecitazioni: N=-2388.85 T_z=-17.70 M_y=-89.09 T_y=-4.68 M_z=-1.04 M_x=15.40
Tensioni: σ_N =-173.61 σ_M =-213.15 τ =29.63 σ_{max} =-386.76
Tensioni: σ_N =-173.61 σ_M =3.19 τ =31.93 τ_{max} =31.93
Tensioni: σ_N =-173.61 σ_M =-213.15 τ =29.63 $\sigma_{ID,max}$ =390.15

Asta n. 3562 (-6492 -6556) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
Sollecitazioni: N,Ed=-3660.08 M_y,Ed=-125.91 M_z,Ed=0.62
Resistenze: Nc,Rd=30796.20 M_y,c,Rd=951.93 M_z,c,Rd=632.38 L=17.28
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 λ_y =4.01 Ncr,y=17709800.00 λ^*_y =0.04 Curva a: Φ_y =0.00 χ_y =1.00
 λ_z =6.96 Ncr,z=5882460.00 λ^*_z =0.07 Curva a: Φ_z =0.00 χ_z =1.00
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96
Verifica YY: 0.12+0.10+0.00=0.22
Verifica ZZ: 0.12+0.08+0.00=0.20

- Verifica a pressoflessione retta - CC 41 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=-1691.66 T_z=-41.76 M_y=-131.70 T_y=-2.04 M_x=29.57
M_y,Ed=-131.70 M_y,c,Rd=1184.58
N,Ed=-1691.66 Nc,Rd=30796.20 n=N,Ed/Nc,Rd=0.05
M_{Ny},c,Rd=1184.58 M_y,Ed/M_{Ny},c,Rd=0.11

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 49 SLU Xl=0.17
Sollecitazioni: N=-3659.81 T_z=-56.51 M_y=-117.03 T_y=-2.66 M_x=20.28
V,Ed=-2.66 Vc,Rd,Red=5747.94 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]
V,Ed=-56.51 Vc,Rd,Red=11495.90 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-2450.00 T_z=-27.88 M_y=-86.90 T_y=-2.80 M_x=18.69
Tensioni: σ_N =-178.05 σ_M =-204.31 τ =35.96 σ_{max} =-382.37
Tensioni: σ_N =-178.05 σ_M =0.00 τ =39.57 τ_{max} =39.57
Tensioni: σ_N =-178.05 σ_M =-204.31 τ =36.62 $\sigma_{ID,max}$ =387.59

Asta n. 3562 (-6556 -6629) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
Sollecitazioni: N,Ed=-4303.29 M_y,Ed=-86.00 M_z,Ed=1.48
Resistenze: Nc,Rd=30796.20 M_y,c,Rd=951.93 M_z,c,Rd=632.38 L=17.28
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95

$\lambda_y=4.01$ Ncr, $y=17710000.00$ $\lambda_y^*=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr, $z=5882520.00$ $\lambda_z^*=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
 Verifica YY: $0.14+0.07+0.00=0.21$
 Verifica ZZ: $0.14+0.06+0.00=0.20$

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $Xl=0.02$ - Classe 3
 Sollecitazioni: $N=-3699.05$ $T_z=-108.79$ $M_y=-107.78$ $T_y=1.22$ $M_z=1.01$ $M_x=27.92$
 Tensioni: $\sigma_N=-268.83$ $\sigma_M=-257.00$ $\tau=53.73$ $\sigma_{max}=-525.83$
 Tensioni: $\sigma_N=-268.83$ $\sigma_M=-3.11$ $\tau=67.84$ $\tau_{max}=67.84$
 Tensioni: $\sigma_N=-268.83$ $\sigma_M=-257.00$ $\tau=53.73$ $\sigma_{ID,max}=534.00$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU $Xl=0.17$
 Sollecitazioni: $N=-1710.00$ $T_z=-118.13$ $M_y=-96.63$ $T_y=3.01$ $M_x=37.48$
 $V,Ed=3.01$ $Vc,Rd,Red=5596.15$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-118.13$ $Vc,Rd,Red=11192.30$ $V,Ed/Vc,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $Xl=0.00$ - Classe 3
 Sollecitazioni: $N=-2492.36$ $T_z=-62.02$ $M_y=-77.36$ $M_x=22.37$
 Tensioni: $\sigma_N=-181.13$ $\sigma_M=-181.89$ $\tau=43.05$ $\sigma_{max}=-363.02$
 Tensioni: $\sigma_N=-181.13$ $\sigma_M=0.00$ $\tau=51.09$ $\tau_{max}=51.09$
 Tensioni: $\sigma_N=-181.13$ $\sigma_M=-181.89$ $\tau=43.05$ $\sigma_{ID,max}=370.60$

Asta n. 3562 (-6629 -6693) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-4386.57$ $M_y,Ed=-61.28$ $M_z,Ed=-4.75$
 Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr, $y=17710000.00$ $\lambda_y^*=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr, $z=5882520.00$ $\lambda_z^*=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
 Verifica YY: $0.14+0.05+0.01=0.20$
 Verifica ZZ: $0.14+0.04+0.01=0.19$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $Xl=0.00$ - Classe 3
 Sollecitazioni: $N=-4386.57$ $T_z=-99.86$ $M_y=-61.28$ $T_y=-44.14$ $M_z=2.88$ $M_x=24.16$
 Tensioni: $\sigma_N=-318.79$ $\sigma_M=-154.27$ $\tau=46.49$ $\sigma_{max}=-473.06$
 Tensioni: $\sigma_N=-318.79$ $\sigma_M=-8.84$ $\tau=59.44$ $\tau_{max}=59.44$
 Tensioni: $\sigma_N=-318.79$ $\sigma_M=-152.91$ $\tau=55.24$ $\sigma_{ID,max}=481.31$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU $Xl=0.17$
 Sollecitazioni: $N=-1710.34$ $T_z=-123.92$ $M_y=-65.62$ $T_y=-7.26$ $M_x=38.54$
 $V,Ed=-7.26$ $Vc,Rd,Red=5586.76$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-123.92$ $Vc,Rd,Red=11173.50$ $V,Ed/Vc,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $Xl=0.00$ - Classe 3
 Sollecitazioni: $N=-2536.50$ $T_z=-67.54$ $M_y=-60.20$ $T_y=-22.83$ $M_x=22.79$
 Tensioni: $\sigma_N=-184.34$ $\sigma_M=-141.54$ $\tau=43.86$ $\sigma_{max}=-325.88$
 Tensioni: $\sigma_N=-184.34$ $\sigma_M=0.00$ $\tau=52.61$ $\tau_{max}=52.61$
 Tensioni: $\sigma_N=-184.34$ $\sigma_M=-141.54$ $\tau=49.29$ $\sigma_{ID,max}=336.88$

Asta n. 3562 (-6693 -6757) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-4935.56$ $M_y,Ed=-58.72$ $M_z,Ed=-6.77$
 Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr, $y=17709800.00$ $\lambda_y^*=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr, $z=5882460.00$ $\lambda_z^*=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
 Verifica YY: $0.16+0.05+0.01=0.22$
 Verifica ZZ: $0.16+0.04+0.01=0.21$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $Xl=0.17$ - Classe 3
 Sollecitazioni: $N=-4935.30$ $T_z=52.33$ $M_y=-58.72$ $T_y=49.62$ $M_z=1.81$ $M_x=-6.18$
 Tensioni: $\sigma_N=-358.67$ $\sigma_M=-144.44$ $\tau=11.89$ $\sigma_{max}=-503.11$
 Tensioni: $\sigma_N=-358.67$ $\sigma_M=-128.84$ $\tau=23.71$ $\tau_{max}=23.71$
 Tensioni: $\sigma_N=-358.67$ $\sigma_M=-143.59$ $\tau=21.72$ $\sigma_{ID,max}=503.67$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 45 SLU $Xl=0.13$

Sollecitazioni: $N=-4935.37$ $T_z=55.14$ $M_y=-56.18$ $T_y=49.62$ $M_x=-6.18$
 $V,Ed=49.62$ $Vc,Rd,Red=5872.38$ $V,Ed/Vc,Rd,Red=0.01$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=55.14$ $Vc,Rd,Red=11744.80$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.13$ - Classe 3
 Sollecitazioni: $N=-2831.30$ $T_z=44.29$ $M_y=-54.47$ $T_y=16.27$ $M_z=-1.13$ $M_x=-5.09$
 Tensioni: $\sigma_N=-205.76$ $\sigma_M=-132.07$ $\tau=9.80$ $\sigma_{max}=-337.83$
 Tensioni: $\sigma_N=-205.76$ $\sigma_M=3.47$ $\tau=15.54$ $\tau_{max}=15.54$
 Tensioni: $\sigma_N=-205.76$ $\sigma_M=-132.07$ $\tau=9.80$ $\sigma_{ID,max}=338.25$

Asta n. 3562 (-6757 -6842) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-4814.04$ $M_y,Ed=-71.36$ $M_z,Ed=1.49$
 Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $Ncr,y=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $Ncr,z=5882520.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.16+0.06+0.00=0.22$
 Verifica ZZ: $0.16+0.05+0.00=0.20$
- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X1=0.14$ - Classe 3
 Sollecitazioni: $N=-4813.82$ $T_z=41.87$ $M_y=-70.07$ $T_y=-3.40$ $M_z=1.01$ $M_x=-4.84$
 Tensioni: $\sigma_N=-349.84$ $\sigma_M=-168.32$ $\tau=9.32$ $\sigma_{max}=-518.16$
 Tensioni: $\sigma_N=-349.84$ $\sigma_M=-3.09$ $\tau=14.75$ $\tau_{max}=14.75$
 Tensioni: $\sigma_N=-349.84$ $\sigma_M=-168.32$ $\tau=9.32$ $\sigma_{ID,max}=518.41$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 37 SLU $X1=0.00$
 Sollecitazioni: $N=-1923.57$ $T_z=78.19$ $M_y=-94.34$ $T_y=-7.31$ $M_x=-19.22$
 $V,Ed=-7.31$ $Vc,Rd,Red=5757.27$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=78.19$ $Vc,Rd,Red=11514.50$ $V,Ed/Vc,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.17$ - Classe 3
 Sollecitazioni: $N=-2838.26$ $T_z=36.55$ $M_y=-64.59$ $T_y=-7.30$ $M_z=-1.13$ $M_x=-4.77$
 Tensioni: $\sigma_N=-206.27$ $\sigma_M=-155.87$ $\tau=9.18$ $\sigma_{max}=-362.14$
 Tensioni: $\sigma_N=-206.27$ $\sigma_M=3.48$ $\tau=13.92$ $\tau_{max}=13.92$
 Tensioni: $\sigma_N=-206.27$ $\sigma_M=-155.87$ $\tau=9.18$ $\sigma_{ID,max}=362.49$

Asta n. 3562 (-6842 -6901) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-4795.07$ $M_y,Ed=-73.71$ $M_z,Ed=0.87$
 Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $Ncr,y=17709900.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $Ncr,z=5882490.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.16+0.06+0.00=0.22$
 Verifica ZZ: $0.16+0.05+0.00=0.20$

- Verifica a pressoflessione retta - CC 37 SLU $X1=0.17$ - Classe 1
 Sollecitazioni: $N=-1961.54$ $T_z=3.22$ $M_y=-112.53$ $T_y=-2.69$ $M_x=-11.38$
 $M_y,Ed=-112.53$ $M_y,c,Rd=1184.58$
 $N,Ed=-1961.54$ $Nc,Rd=30796.20$ $n=N,Ed/Nc,Rd=0.06$
 $MNy,c,Rd=1184.58$ $M_y,Ed/MNy,c,Rd=0.09$

- Verifica a taglio dir. Y [4.2.16] - CC 74 SLU $X1=0.00$
 Sollecitazioni: $N=-2844.51$ $T_z=-6.06$ $M_y=-75.53$ $T_y=-9.94$
 $V,Ed=-9.94$ $Vc,Rd=5926.90$ $V,Ed/Vc,Rd=0.00$

- Verifica a taglio dir. Z [4.2.16]
 $V,Ed=-6.06$ $Vc,Rd=11853.80$ $V,Ed/Vc,Rd=0.00$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.17$ - Classe 3
 Sollecitazioni: $N=-2176.00$ $T_z=-15.78$ $M_y=-89.09$ $T_y=-2.59$ $M_x=4.63$
 Tensioni: $\sigma_N=-158.14$ $\sigma_M=-209.46$ $\tau=8.90$ $\sigma_{max}=-367.60$
 Tensioni: $\sigma_N=-158.14$ $\sigma_M=0.00$ $\tau=10.95$ $\tau_{max}=10.95$
 Tensioni: $\sigma_N=-158.14$ $\sigma_M=-209.46$ $\tau=9.52$ $\sigma_{ID,max}=367.97$

Asta n. 3562 (-6901 -7007) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-4799.47 My,Ed=-71.61 Mz,Ed=0.73
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17709900.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882490.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
 Verifica YY: 0.16+0.06+0.00=0.21
 Verifica ZZ: 0.16+0.05+0.00=0.20

- Verifica a pressoflessione retta - CC 37 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=-1975.73 Tz=-29.91 My=-111.51 Mx=-3.80
 My,Ed=-111.51 My,c,Rd=1184.58
 N,Ed=-1975.73 Nc,Rd=30796.20 n=N,Ed/Nc,Rd=0.06
 MNy,c,Rd=1184.58 My,Ed/MNy,c,Rd=0.09

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 49 SLU Xl=0.17
 Sollecitazioni: N=-4283.10 Tz=-55.08 My=-83.86 Mx=8.55
 V,Ed=-55.08 Vc,Rd,Red=11702.90 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-2194.60 Tz=-29.97 My=-87.92 Ty=-1.32 Mx=9.69
 Tensioni: $\sigma_N=-159.49$ $\sigma_M=-206.72$ $\tau=18.65$ $\sigma_{max}=-366.21$
 Tensioni: $\sigma_N=-159.49$ $\sigma_M=0.00$ $\tau=22.54$ $\tau_{max}=22.54$
 Tensioni: $\sigma_N=-159.49$ $\sigma_M=-206.72$ $\tau=18.96$ $\sigma_{ID,max}=367.68$

Asta n. 3562 (-7007 -7066) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-4810.81 My,Ed=-58.01 Mz,Ed=1.81
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17709900.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882490.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
 Verifica YY: 0.16+0.05+0.00=0.21
 Verifica ZZ: 0.16+0.04+0.00=0.20

- Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-4810.81 Tz=-85.19 My=-58.01 Ty=2.80 Mz=1.32 Mx=13.61
 Tensioni: $\sigma_N=-349.62$ $\sigma_M=-141.07$ $\tau=26.19$ $\sigma_{max}=-490.69$
 Tensioni: $\sigma_N=-349.62$ $\sigma_M=-4.06$ $\tau=37.24$ $\tau_{max}=37.24$
 Tensioni: $\sigma_N=-349.62$ $\sigma_M=-141.07$ $\tau=26.19$ $\sigma_{ID,max}=492.78$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 25 SLU Xl=0.16
 Sollecitazioni: N=-2716.42 Tz=-116.82 My=-62.91 Ty=4.61 Mx=15.80
 V,Ed=4.61 Vc,Rd,Red=5787.45 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=-116.82 Vc,Rd,Red=11574.90 V,Ed/Vc,Rd,Red=0.01

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-2191.73 Tz=-79.37 My=-77.48 Ty=-2.06 Mx=15.30
 Tensioni: $\sigma_N=-159.28$ $\sigma_M=-182.16$ $\tau=29.44$ $\sigma_{max}=-341.45$
 Tensioni: $\sigma_N=-159.28$ $\sigma_M=0.00$ $\tau=39.73$ $\tau_{max}=39.73$
 Tensioni: $\sigma_N=-159.28$ $\sigma_M=-182.16$ $\tau=29.93$ $\sigma_{ID,max}=345.36$

Asta n. 3562 (-7066 -7146) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-4883.88 My,Ed=-33.81 Mz,Ed=-5.43
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17709900.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882490.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
 Verifica YY: 0.16+0.03+0.01=0.19
 Verifica ZZ: 0.16+0.02+0.01=0.19

- Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-4883.88 Tz=-98.18 My=-33.81 Ty=-48.79 Mz=3.00 Mx=15.10
 Tensioni: $\sigma_N=-354.93$ $\sigma_M=-90.11$ $\tau=29.05$ $\sigma_{max}=-445.05$
 Tensioni: $\sigma_N=-354.93$ $\sigma_M=-9.22$ $\tau=41.78$ $\tau_{max}=41.78$
 Tensioni: $\sigma_N=-354.93$ $\sigma_M=-88.70$ $\tau=38.72$ $\sigma_{ID,max}=448.67$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU $X_1=0.17$
 Sollecitazioni: $N=-2104.95$ $T_2=-121.70$ $M_y=-36.18$ $T_y=-10.46$ $M_x=22.50$
 $V,Ed=-10.46$ $Vc,Rd,Red=5728.28$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-121.70$ $Vc,Rd,Red=11456.60$ $V,Ed/Vc,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=-2925.15$ $T_2=-67.99$ $M_y=-38.77$ $T_y=-24.48$ $M_x=12.04$
 Tensioni: $\sigma_N=-212.58$ $\sigma_M=-91.16$ $\tau=23.17$ $\sigma_{max}=-303.74$
 Tensioni: $\sigma_N=-212.58$ $\sigma_M=0.00$ $\tau=31.98$ $\tau_{max}=31.98$
 Tensioni: $\sigma_N=-212.58$ $\sigma_M=-91.16$ $\tau=29.00$ $\sigma_{ID,max}=307.87$

Asta n. 3562 (-7146 -7209) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-5402.74$ $M_y,Ed=-35.27$ $M_z,Ed=-8.03$
 Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr,y}=17709900.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882490.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.18+0.03+0.01=0.22$
 Verifica ZZ: $0.18+0.02+0.01=0.21$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X_1=0.17$ - Classe 3
 Sollecitazioni: $N=-5402.47$ $T_2=66.34$ $M_y=-35.27$ $T_y=59.13$ $M_z=2.19$ $M_x=-10.62$
 Tensioni: $\sigma_N=-392.62$ $\sigma_M=-90.65$ $\tau=20.44$ $\sigma_{max}=-483.27$
 Tensioni: $\sigma_N=-392.62$ $\sigma_M=-77.39$ $\tau=34.52$ $\tau_{max}=34.52$
 Tensioni: $\sigma_N=-392.62$ $\sigma_M=-89.62$ $\tau=32.16$ $\sigma_{ID,max}=485.45$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 45 SLU $X_1=0.13$
 Sollecitazioni: $N=-5402.54$ $T_2=69.15$ $M_y=-32.07$ $T_y=59.13$ $M_x=-10.62$
 $V,Ed=59.13$ $Vc,Rd,Red=5833.16$ $V,Ed/Vc,Rd,Red=0.01$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=69.15$ $Vc,Rd,Red=11666.30$ $V,Ed/Vc,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.17$ - Classe 3
 Sollecitazioni: $N=-3168.17$ $T_2=40.85$ $M_y=-37.28$ $T_y=26.26$ $M_x=-7.93$
 Tensioni: $\sigma_N=-230.25$ $\sigma_M=-87.66$ $\tau=15.25$ $\sigma_{max}=-317.90$
 Tensioni: $\sigma_N=-230.25$ $\sigma_M=-81.81$ $\tau=21.51$ $\tau_{max}=21.51$
 Tensioni: $\sigma_N=-230.25$ $\sigma_M=-87.66$ $\tau=21.50$ $\sigma_{ID,max}=320.07$

Asta n. 3562 (-7209 -7272) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-5249.65$ $M_y,Ed=-51.45$ $M_z,Ed=1.47$
 Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr,y}=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882520.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.17+0.04+0.00=0.21$
 Verifica ZZ: $0.17+0.03+0.00=0.21$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X_1=0.17$ - Classe 3
 Sollecitazioni: $N=-5249.39$ $T_2=53.76$ $M_y=-51.45$ $T_y=-2.57$ $M_z=1.02$ $M_x=-9.14$
 Tensioni: $\sigma_N=-381.50$ $\sigma_M=-124.58$ $\tau=17.58$ $\sigma_{max}=-506.08$
 Tensioni: $\sigma_N=-381.50$ $\sigma_M=-3.14$ $\tau=24.55$ $\tau_{max}=24.55$
 Tensioni: $\sigma_N=-381.50$ $\sigma_M=-124.58$ $\tau=17.58$ $\sigma_{ID,max}=506.99$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU $X_1=0.00$
 Sollecitazioni: $N=-2364.74$ $T_2=73.55$ $M_y=-60.93$ $T_y=-7.41$ $M_x=-10.46$
 $V,Ed=-7.41$ $Vc,Rd,Red=5834.59$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=73.55$ $Vc,Rd,Red=11669.20$ $V,Ed/Vc,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.17$ - Classe 3
 Sollecitazioni: $N=-3134.35$ $T_2=34.31$ $M_y=-46.99$ $M_x=-7.24$
 Tensioni: $\sigma_N=-227.79$ $\sigma_M=-110.49$ $\tau=13.93$ $\sigma_{max}=-338.27$
 Tensioni: $\sigma_N=-227.79$ $\sigma_M=0.00$ $\tau=18.38$ $\tau_{max}=18.38$
 Tensioni: $\sigma_N=-227.79$ $\sigma_M=-110.49$ $\tau=13.93$ $\sigma_{ID,max}=339.13$

Asta n. 3562 (-7272 -7306) Tubo 60x120x4 mm - S235 Crit. 2

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-5209.52 My,Ed=-57.01 Mz,Ed=0.67
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17709900.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882490.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
 Verifica YY: 0.17+0.05+0.00=0.22
 Verifica ZZ: 0.17+0.04+0.00=0.21
 - Verifica a pressoflessione retta - CC 37 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=-2146.73 Tz=-9.16 My=-86.86 Ty=-1.13 Mx=-18.94
 My,Ed=-86.86 My,c,Rd=1184.58
 N,Ed=-2146.73 Nc,Rd=30796.20 n=N,Ed/Nc,Rd=0.07
 MNy,c,Rd=1184.58 My,Ed/MNy,c,Rd=0.07
 - Verifica a taglio e torsione dir. Y [4.2.25] - CC 37 SLU Xl=0.17
 Sollecitazioni: N=-2146.47 Tz=-19.36 My=-84.40 Ty=-1.13 Mx=-18.94
 V,Ed=-1.13 Vc,Rd,Red=5759.72 V,Ed/Vc,Rd,Red=0.00
 - Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=-19.36 Vc,Rd,Red=11519.40 V,Ed/Vc,Rd,Red=0.00
 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.09 - Classe 3
 Sollecitazioni: N=-3135.15 Tz=7.52 My=-48.80 Ty=-1.48 Mz=-1.08 Mx=-3.34
 Tensioni: $\sigma_N=-227.84$ $\sigma_M=-118.57$ $\tau=6.42$ $\sigma_{max}=-346.41$
 Tensioni: $\sigma_N=-227.84$ $\sigma_M=3.32$ $\tau=7.39$ $\tau_{max}=7.39$
 Tensioni: $\sigma_N=-227.84$ $\sigma_M=-118.57$ $\tau=6.42$ $\sigma_{ID,max}=346.59$

Asta n. 3562 (-7306 -7356) Tubo 60x120x4 mm - S235 Crit. 2

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-5198.63 My,Ed=-56.26 Mz,Ed=0.60
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17709900.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882490.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
 Verifica YY: 0.17+0.05+0.00=0.22
 Verifica ZZ: 0.17+0.04+0.00=0.21
 - Verifica a pressoflessione retta - CC 37 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=-2136.50 Tz=-57.20 My=-81.48 Ty=1.19 Mx=-10.53
 My,Ed=-81.48 My,c,Rd=1184.58
 N,Ed=-2136.50 Nc,Rd=30796.20 n=N,Ed/Nc,Rd=0.07
 MNy,c,Rd=1184.58 My,Ed/MNy,c,Rd=0.07
 - Verifica a taglio e torsione dir. Y [4.2.25] - CC 37 SLU Xl=0.17
 Sollecitazioni: N=-2136.24 Tz=-67.40 My=-70.71 Ty=1.19 Mx=-10.53
 V,Ed=1.19 Vc,Rd,Red=5834.01 V,Ed/Vc,Rd,Red=0.00
 - Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=-67.40 Vc,Rd,Red=11668.00 V,Ed/Vc,Rd,Red=0.01
 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-3130.99 Tz=-25.55 My=-47.41 Mz=-1.13 Mx=3.19
 Tensioni: $\sigma_N=-227.54$ $\sigma_M=-115.46$ $\tau=6.14$ $\sigma_{max}=-343.00$
 Tensioni: $\sigma_N=-227.54$ $\sigma_M=3.45$ $\tau=9.45$ $\tau_{max}=9.45$
 Tensioni: $\sigma_N=-227.54$ $\sigma_M=-115.46$ $\tau=6.14$ $\sigma_{ID,max}=343.17$

Asta n. 3562 (-7356 -7472) Tubo 60x120x4 mm - S235 Crit. 2

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-5201.49 My,Ed=-45.99 Mz,Ed=1.04
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17710000.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882520.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
 Verifica YY: 0.17+0.04+0.00=0.21
 Verifica ZZ: 0.17+0.03+0.00=0.20
 - Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.14 - Classe 3
 Sollecitazioni: N=-5201.28 Tz=-80.36 My=-35.22 Ty=1.04 Mz=1.01 Mx=9.58

Tensioni: $\sigma_N=-378.00$ $\sigma_M=-86.37$ $\tau=18.44$ $\sigma_{max}=-464.37$

Tensioni: $\sigma_N=-378.00$ $\sigma_M=-3.09$ $\tau=28.86$ $\tau_{max}=28.86$

Tensioni: $\sigma_N=-378.00$ $\sigma_M=-86.37$ $\tau=18.44$ $\sigma_{ID,max}=465.46$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 37 SLU $X1=0.17$

Sollecitazioni: $N=-2105.60$ $T_z=-131.28$ $M_y=-40.69$ $T_y=5.01$ $M_x=-1.98$

$V,Ed=5.01$ $V_c,Rd,Red=5909.41$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]

$V,Ed=-131.28$ $V_c,Rd,Red=11818.80$ $V,Ed/V_c,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3

Sollecitazioni: $N=-3115.14$ $T_z=-62.77$ $M_y=-38.74$ $T_y=-1.66$ $M_x=6.99$

Tensioni: $\sigma_N=-226.39$ $\sigma_M=-91.07$ $\tau=13.45$ $\sigma_{max}=-317.46$

Tensioni: $\sigma_N=-226.39$ $\sigma_M=0.00$ $\tau=21.59$ $\tau_{max}=21.59$

Tensioni: $\sigma_N=-226.39$ $\sigma_M=-91.07$ $\tau=13.85$ $\sigma_{ID,max}=318.37$

Asta n. 3562 (-7472 -7508) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3

Sollecitazioni: $N,Ed=-5269.24$ $M_y,Ed=-25.16$ $M_z,Ed=-3.60$

Resistenze: $N_c,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=4.01$ $N_{cr,y}=17709900.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$

$\lambda_z=6.96$ $N_{cr,z}=5882490.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$

$K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$

Verifica YY: $0.17+0.02+0.01=0.20$

Verifica ZZ: $0.17+0.02+0.01=0.19$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X1=0.00$ - Classe 3

Sollecitazioni: $N=-5269.24$ $T_z=-85.16$ $M_y=-25.16$ $T_y=-31.27$ $M_z=1.81$ $M_x=11.09$

Tensioni: $\sigma_N=-382.94$ $\sigma_M=-65.54$ $\tau=21.34$ $\sigma_{max}=-448.48$

Tensioni: $\sigma_N=-382.94$ $\sigma_M=-5.54$ $\tau=32.39$ $\tau_{max}=32.39$

Tensioni: $\sigma_N=-382.94$ $\sigma_M=-64.69$ $\tau=27.54$ $\sigma_{ID,max}=450.16$

- Verifica a taglio dir. Y [4.2.16] - CC 37 SLU $X1=0.17$

Sollecitazioni: $N=-2076.12$ $T_z=-149.73$ $M_y=-3.91$ $T_y=-2.21$

$V,Ed=-2.21$ $V_c,Rd=5926.90$ $V,Ed/V_c,Rd=0.00$

- Verifica a taglio dir. Z [4.2.16]

$V,Ed=-149.73$ $V_c,Rd=11853.80$ $V,Ed/V_c,Rd=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3

Sollecitazioni: $N=-3114.56$ $T_z=-69.17$ $M_y=-22.40$ $T_y=-15.76$ $M_x=7.73$

Tensioni: $\sigma_N=-226.35$ $\sigma_M=-52.67$ $\tau=14.88$ $\sigma_{max}=-279.02$

Tensioni: $\sigma_N=-226.35$ $\sigma_M=0.00$ $\tau=23.84$ $\tau_{max}=23.84$

Tensioni: $\sigma_N=-226.35$ $\sigma_M=-52.67$ $\tau=18.63$ $\sigma_{ID,max}=280.88$

Asta n. 3562 (-7508 -7586) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3

Sollecitazioni: $N,Ed=-5298.27$ $M_y,Ed=-25.31$ $M_z,Ed=-3.86$

Resistenze: $N_c,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=4.01$ $N_{cr,y}=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$

$\lambda_z=6.96$ $N_{cr,z}=5882520.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$

$K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$

Verifica YY: $0.17+0.02+0.01=0.20$

Verifica ZZ: $0.17+0.02+0.01=0.19$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X1=0.17$ - Classe 3

Sollecitazioni: $N=-5298.00$ $T_z=86.55$ $M_y=-25.31$ $T_y=31.44$ $M_z=1.57$ $M_x=-10.54$

Tensioni: $\sigma_N=-385.03$ $\sigma_M=-65.07$ $\tau=20.28$ $\sigma_{max}=-450.10$

Tensioni: $\sigma_N=-385.03$ $\sigma_M=-4.82$ $\tau=31.50$ $\tau_{max}=31.50$

Tensioni: $\sigma_N=-385.03$ $\sigma_M=-64.33$ $\tau=26.51$ $\sigma_{ID,max}=451.70$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 25 SLU $X1=0.00$

Sollecitazioni: $N=-3097.00$ $T_z=121.71$ $M_y=-5.66$ $T_y=6.20$ $M_x=-13.86$

$V,Ed=6.20$ $V_c,Rd,Red=5804.60$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]

$V,Ed=121.71$ $V_c,Rd,Red=11609.20$ $V,Ed/V_c,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.17$ - Classe 3

Sollecitazioni: $N=-3106.97$ $T_z=54.13$ $M_y=-20.08$ $T_y=16.92$ $M_x=-10.21$

Tensioni: $\sigma_N=-225.80$ $\sigma_M=-47.21$ $\tau=19.65$ $\sigma_{max}=-273.01$
 Tensioni: $\sigma_N=-225.80$ $\sigma_M=0.00$ $\tau=26.67$ $\tau_{max}=26.67$
 Tensioni: $\sigma_N=-225.80$ $\sigma_M=-47.21$ $\tau=23.68$ $\sigma_{ID,max}=276.07$

Asta n. 3562 (-7586 -7671) Tubo 60x120x4 mm - S235 Crit. 2

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3

Sollecitazioni: $N, Ed=-5241.83$ $M_y, Ed=-46.50$ $M_z, Ed=1.21$
 Resistenze: $N_c, Rd=30796.20$ $M_y, c, Rd=951.93$ $M_z, c, Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr,y}=17709900.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882490.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.17+0.04+0.00=0.21$
 Verifica ZZ: $0.17+0.03+0.00=0.20$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X1=0.08$ - Classe 3

Sollecitazioni: $N=-5241.71$ $T_x=78.99$ $M_y=-39.31$ $T_y=-2.43$ $M_z=1.02$ $M_x=-9.05$
 Tensioni: $\sigma_N=-380.94$ $\sigma_M=-96.04$ $\tau=17.41$ $\sigma_{max}=-476.98$
 Tensioni: $\sigma_N=-380.94$ $\sigma_M=-3.13$ $\tau=27.64$ $\tau_{max}=27.64$
 Tensioni: $\sigma_N=-380.94$ $\sigma_M=-96.04$ $\tau=17.41$ $\sigma_{ID,max}=477.93$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 25 SLU $X1=0.02$

Sollecitazioni: $N=-3134.00$ $T_x=115.50$ $M_y=-37.78$ $T_y=-7.36$ $M_x=-12.57$
 $V, Ed=-7.36$ $V_c, Rd, Red=5815.96$ $V, Ed/V_c, Rd, Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]

$V, Ed=115.50$ $V_c, Rd, Red=11631.90$ $V, Ed/V_c, Rd, Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.17$ - Classe 3

Sollecitazioni: $N=-3102.93$ $T_x=50.23$ $M_y=-32.84$ $M_x=-9.83$
 Tensioni: $\sigma_N=-225.50$ $\sigma_M=-77.21$ $\tau=18.92$ $\sigma_{max}=-302.71$
 Tensioni: $\sigma_N=-225.50$ $\sigma_M=0.00$ $\tau=25.43$ $\tau_{max}=25.43$
 Tensioni: $\sigma_N=-225.50$ $\sigma_M=-77.21$ $\tau=18.92$ $\sigma_{ID,max}=304.48$

Asta n. 3562 (-7671 -7723) Tubo 60x120x4 mm - S235 Crit. 2

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3

Sollecitazioni: $N, Ed=-5254.81$ $M_y, Ed=-57.17$ $M_z, Ed=0.75$
 Resistenze: $N_c, Rd=30796.20$ $M_y, c, Rd=951.93$ $M_z, c, Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr,y}=17709900.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882490.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.17+0.05+0.00=0.22$
 Verifica ZZ: $0.17+0.04+0.00=0.21$

- Verifica a pressoflessione retta - CC 89 SLU $X1=0.17$ - Classe 1

Sollecitazioni: $N=-2920.80$ $T_x=39.07$ $M_y=-77.70$ $T_y=1.58$ $M_x=-9.32$
 $M_y, Ed=-77.70$ $M_y, c, Rd=1184.58$
 $N, Ed=-2920.80$ $N_c, Rd=30796.20$ $n=N, Ed/N_c, Rd=0.09$
 $MN_y, c, Rd=1184.58$ $M_y, Ed/MN_y, c, Rd=0.07$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 25 SLU $X1=0.00$

Sollecitazioni: $N=-3175.27$ $T_x=50.11$ $M_y=-62.30$ $T_y=-1.88$ $M_x=-4.31$
 $V, Ed=-1.88$ $V_c, Rd, Red=5888.88$ $V, Ed/V_c, Rd, Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]

$V, Ed=50.11$ $V_c, Rd, Red=11777.80$ $V, Ed/V_c, Rd, Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.17$ - Classe 3

Sollecitazioni: $N=-3115.72$ $T_x=17.06$ $M_y=-38.92$ $T_y=-1.13$ $M_z=-1.07$ $M_x=-6.34$
 Tensioni: $\sigma_N=-226.43$ $\sigma_M=-95.28$ $\tau=12.21$ $\sigma_{max}=-321.72$
 Tensioni: $\sigma_N=-226.43$ $\sigma_M=3.28$ $\tau=14.42$ $\tau_{max}=14.42$
 Tensioni: $\sigma_N=-226.43$ $\sigma_M=-95.28$ $\tau=12.21$ $\sigma_{ID,max}=322.41$

Asta n. 3562 (-7723 -7813) Tubo 60x120x4 mm - S235 Crit. 2

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3

Sollecitazioni: $N, Ed=-5284.52$ $M_y, Ed=-58.07$ $M_z, Ed=0.57$
 Resistenze: $N_c, Rd=30796.20$ $M_y, c, Rd=951.93$ $M_z, c, Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr,y}=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882520.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$

Verifica YY: $0.17+0.05+0.00=0.22$
 Verifica ZZ: $0.17+0.04+0.00=0.21$

- Verifica a pressoflessione retta - CC 89 SLU $X1=0.00$ - Classe 1
 Sollecitazioni: $N=-2935.72$ $M_y=-79.31$ $T_y=-2.45$
 $M_y, Ed=-79.31$ $M_y, c, Rd=1184.58$
 $N, Ed=-2935.72$ $Nc, Rd=30796.20$ $n=N, Ed/Nc, Rd=0.10$
 $MNy, c, Rd=1184.58$ $M_y, Ed/MNy, c, Rd=0.07$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 37 SLU $X1=0.17$
 Sollecitazioni: $N=-2061.59$ $T_x=-18.53$ $M_y=-11.97$ $T_y=1.79$ $M_x=-14.73$
 $V, Ed=1.79$ $Vc, Rd, Red=5796.86$ $V, Ed/Vc, Rd, Red=0.00$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed=-18.53$ $Vc, Rd, Red=11593.70$ $V, Ed/Vc, Rd, Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=-3118.29$ $T_x=9.44$ $M_y=-39.52$ $T_y=1.39$ $M_z=-1.14$ $M_x=4.83$
 Tensioni: $\sigma_N=-226.62$ $\sigma_M=-96.94$ $\tau=9.29$ $\sigma_{max}=-323.56$
 Tensioni: $\sigma_N=-226.62$ $\sigma_M=-3.49$ $\tau=10.52$ $\tau_{max}=10.52$
 Tensioni: $\sigma_N=-226.62$ $\sigma_M=-96.94$ $\tau=9.29$ $\sigma_{ID, max}=323.96$

Asta n. 3562 (-7813 -7937) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N, Ed=-5346.33$ $M_y, Ed=-53.01$ $M_z, Ed=1.36$
 Resistenze: $Nc, Rd=30796.20$ $M_y, c, Rd=951.93$ $M_z, c, Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $Ncr, y=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $Ncr, z=5882520.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.17+0.04+0.00=0.22$
 Verifica ZZ: $0.17+0.03+0.00=0.21$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X1=0.00$ - Classe 3
 Sollecitazioni: $N=-5346.33$ $T_x=-51.66$ $M_y=-53.01$ $M_z=1.21$ $M_x=9.61$
 Tensioni: $\sigma_N=-388.54$ $\sigma_M=-128.92$ $\tau=18.49$ $\sigma_{max}=-517.46$
 Tensioni: $\sigma_N=-388.54$ $\sigma_M=-3.71$ $\tau=25.19$ $\tau_{max}=25.19$
 Tensioni: $\sigma_N=-388.54$ $\sigma_M=-128.92$ $\tau=18.49$ $\sigma_{ID, max}=518.45$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU $X1=0.17$
 Sollecitazioni: $N=-2465.17$ $T_x=-72.68$ $M_y=-61.84$ $T_y=5.81$ $M_x=7.66$
 $V, Ed=5.81$ $Vc, Rd, Red=5859.27$ $V, Ed/Vc, Rd, Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed=-72.68$ $Vc, Rd, Red=11718.50$ $V, Ed/Vc, Rd, Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=-3117.22$ $T_x=-34.47$ $M_y=-36.98$ $T_y=-1.58$ $M_x=6.21$
 Tensioni: $\sigma_N=-226.54$ $\sigma_M=-86.95$ $\tau=11.95$ $\sigma_{max}=-313.49$
 Tensioni: $\sigma_N=-226.54$ $\sigma_M=0.00$ $\tau=16.42$ $\tau_{max}=16.42$
 Tensioni: $\sigma_N=-226.54$ $\sigma_M=-86.95$ $\tau=12.33$ $\sigma_{ID, max}=314.22$

Asta n. 3562 (-7937 -7983) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N, Ed=-5524.99$ $M_y, Ed=-37.33$ $M_z, Ed=-8.42$
 Resistenze: $Nc, Rd=30796.20$ $M_y, c, Rd=951.93$ $M_z, c, Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $Ncr, y=17709900.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $Ncr, z=5882490.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.18+0.03+0.01=0.22$
 Verifica ZZ: $0.18+0.02+0.01=0.22$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X1=0.00$ - Classe 3
 Sollecitazioni: $N=-5524.99$ $T_x=-64.97$ $M_y=-37.33$ $T_y=-63.55$ $M_z=2.57$ $M_x=11.14$
 Tensioni: $\sigma_N=-401.52$ $\sigma_M=-96.85$ $\tau=21.44$ $\sigma_{max}=-498.38$
 Tensioni: $\sigma_N=-401.52$ $\sigma_M=-81.92$ $\tau=36.57$ $\tau_{max}=36.57$
 Tensioni: $\sigma_N=-401.52$ $\sigma_M=-95.64$ $\tau=34.03$ $\sigma_{ID, max}=500.65$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 45 SLU $X1=0.03$
 Sollecitazioni: $N=-5524.94$ $T_x=-66.84$ $M_y=-35.26$ $T_y=-63.55$ $M_x=11.14$
 $V, Ed=-63.55$ $Vc, Rd, Red=5828.58$ $V, Ed/Vc, Rd, Red=0.01$

- Verifica a taglio e torsione dir. Z [4.2.25]

V,Ed=-66.84 Vc,Rd,Red=11657.20 V,Ed/Vc,Rd,Red=0.01

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-3151.72 T_z=-39.63 M_y=-27.37 T_y=-25.85 M_x=6.41
Tensioni: σ_N =-229.05 σ_M =-64.35 τ =12.34 σ_{max} =-293.40
Tensioni: σ_N =-229.05 σ_M =-60.06 τ =18.50 τ_{max} =18.50
Tensioni: σ_N =-229.05 σ_M =-64.35 τ =18.50 $\sigma_{ID,max}$ =295.15

Asta n. 3562 (-7983 -8037) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
Sollecitazioni: N,Ed=-5030.33 M_y,Ed=-34.78 M_z,Ed=-5.87
Resistenze: Nc,Rd=30796.20 M_y,c,Rd=951.93 M_z,c,Rd=632.38 L=17.28
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 λ_y =4.01 Ncr,y=17709900.00 λ^*_y =0.04 Curva a: Φ_y =0.00 χ_y =1.00
 λ_z =6.96 Ncr,z=5882490.00 λ^*_z =0.07 Curva a: Φ_z =0.00 χ_z =1.00
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96
Verifica YY: 0.16+0.03+0.01=0.20
Verifica ZZ: 0.16+0.02+0.01=0.19

- Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.17 - Classe 3
Sollecitazioni: N=-5030.07 T_z=92.84 M_y=-34.78 T_y=50.90 M_z=2.93 M_x=-13.29
Tensioni: σ_N =-365.56 σ_M =-92.14 τ =25.57 σ_{max} =-457.69
Tensioni: σ_N =-365.56 σ_M =-76.33 τ =37.69 τ_{max} =37.69
Tensioni: σ_N =-365.56 σ_M =-90.76 τ =35.65 $\sigma_{ID,max}$ =460.47

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU Xl=0.03
Sollecitazioni: N=-2257.05 T_z=114.41 M_y=-40.67 T_y=13.66 M_x=-24.06
V,Ed=13.66 Vc,Rd,Red=5714.53 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]
V,Ed=114.41 Vc,Rd,Red=11429.10 V,Ed/Vc,Rd,Red=0.01

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3
Sollecitazioni: N=-2905.14 T_z=54.49 M_y=-26.91 T_y=25.24 M_x=-13.12
Tensioni: σ_N =-211.13 σ_M =-63.27 τ =25.25 σ_{max} =-274.40
Tensioni: σ_N =-211.13 σ_M =0.00 τ =32.32 τ_{max} =32.32
Tensioni: σ_N =-211.13 σ_M =-63.27 τ =31.26 $\sigma_{ID,max}$ =279.69

Asta n. 3562 (-8037 -8163) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
Sollecitazioni: N,Ed=-4967.75 M_y,Ed=-57.53 M_z,Ed=2.08
Resistenze: Nc,Rd=30796.20 M_y,c,Rd=951.93 M_z,c,Rd=632.38 L=17.28
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 λ_y =4.01 Ncr,y=17709900.00 λ^*_y =0.04 Curva a: Φ_y =0.00 χ_y =1.00
 λ_z =6.96 Ncr,z=5882490.00 λ^*_z =0.07 Curva a: Φ_z =0.00 χ_z =1.00
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96
Verifica YY: 0.16+0.05+0.00=0.21
Verifica ZZ: 0.16+0.04+0.00=0.20

- Verifica in termini tensionali [4.2.4] - CC 49 SLU Xl=0.16 - Classe 3
Sollecitazioni: N=-4502.98 T_z=101.23 M_y=-74.85 T_y=-6.07 M_z=1.01 M_x=-14.26
Tensioni: σ_N =-327.25 σ_M =-179.54 τ =27.45 σ_{max} =-506.79
Tensioni: σ_N =-327.25 σ_M =-3.09 τ =40.57 τ_{max} =40.57
Tensioni: σ_N =-327.25 σ_M =-179.54 τ =27.45 $\sigma_{ID,max}$ =509.01

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU Xl=0.03
Sollecitazioni: N=-2280.56 T_z=107.76 M_y=-69.39 T_y=-6.67 M_x=-22.75
V,Ed=-6.67 Vc,Rd,Red=5726.11 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]
V,Ed=107.76 Vc,Rd,Red=11452.20 V,Ed/Vc,Rd,Red=0.01

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3
Sollecitazioni: N=-2883.03 T_z=49.01 M_y=-40.17 M_x=-12.64
Tensioni: σ_N =-209.52 σ_M =-94.45 τ =24.31 σ_{max} =-303.97
Tensioni: σ_N =-209.52 σ_M =0.00 τ =30.67 τ_{max} =30.67
Tensioni: σ_N =-209.52 σ_M =-94.45 τ =24.31 $\sigma_{ID,max}$ =306.88

Asta n. 3562 (-8163 -8237) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
Sollecitazioni: N,Ed=-4514.48 M_y,Ed=-90.78 M_z,Ed=0.56
Resistenze: Nc,Rd=30796.20 M_y,c,Rd=951.93 M_z,c,Rd=632.38 L=17.28

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17709900.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882490.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
 Verifica YY: 0.15+0.07+0.00=0.22
 Verifica ZZ: 0.15+0.06+0.00=0.21

- Verifica a pressoflessione retta - CC 89 SLU Xl=0.17 - Classe 1
 Sollecitazioni: N=-2734.53 Tz=36.44 My=-98.92 Ty=3.05 Mx=-16.44
 My,Ed=-98.92 My,c,Rd=1184.58
 N,Ed=-2734.53 Nc,Rd=30796.20 n=N,Ed/Nc,Rd=0.09
 MNy,c,Rd=1184.58 My,Ed/MNy,c,Rd=0.08

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 49 SLU Xl=0.00
 Sollecitazioni: N=-4514.48 Tz=48.73 My=-83.25 Mx=-6.36
 V,Ed=48.73 Vc,Rd,Red=11741.50 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3
 Sollecitazioni: N=-2874.16 Tz=16.54 My=-46.59 Mx=-9.41
 Tensioni: $\sigma_N=-208.88$ $\sigma_M=-109.55$ $\tau=18.10$ $\sigma_{max}=-318.42$
 Tensioni: $\sigma_N=-208.88$ $\sigma_M=0.00$ $\tau=20.25$ $\tau_{max}=20.25$
 Tensioni: $\sigma_N=-208.88$ $\sigma_M=-109.55$ $\tau=18.10$ $\sigma_{ID,max}=319.96$

Asta n. 3562 (-8237 -8325) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: N,Ed=-4518.42 My,Ed=-92.40 Mz,Ed=0.57
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17710000.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882520.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
 Verifica YY: 0.15+0.07+0.00=0.22
 Verifica ZZ: 0.15+0.06+0.00=0.21

- Verifica a pressoflessione retta - CC 89 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=-2721.59 Tz=-3.28 My=-100.36 Ty=-1.04 Mx=-8.12
 My,Ed=-100.36 My,c,Rd=1184.58
 N,Ed=-2721.59 Nc,Rd=30796.20 n=N,Ed/Nc,Rd=0.09
 MNy,c,Rd=1184.58 My,Ed/MNy,c,Rd=0.08

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 74 SLU Xl=0.17
 Sollecitazioni: N=-3079.05 Tz=2.10 My=-75.42 Ty=8.41 Mx=1.02
 V,Ed=8.41 Vc,Rd,Red=5917.94 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=2.10 Vc,Rd,Red=11835.90 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-2852.00 Tz=6.64 My=-47.30 Ty=2.68 Mz=-1.15 Mx=7.06
 Tensioni: $\sigma_N=-207.27$ $\sigma_M=-115.27$ $\tau=13.59$ $\sigma_{max}=-322.54$
 Tensioni: $\sigma_N=-207.27$ $\sigma_M=-3.53$ $\tau=14.45$ $\tau_{max}=14.45$
 Tensioni: $\sigma_N=-207.27$ $\sigma_M=-115.27$ $\tau=13.59$ $\sigma_{ID,max}=323.40$

Asta n. 3562 (-8325 -8386) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: N,Ed=-4529.35 My,Ed=-88.14 Mz,Ed=1.41
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17709900.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882490.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
 Verifica YY: 0.15+0.07+0.00=0.22
 Verifica ZZ: 0.15+0.06+0.00=0.21

- Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-5034.32 Tz=-45.46 My=-67.54 Ty=1.65 Mz=1.08 Mx=6.75
 Tensioni: $\sigma_N=-365.87$ $\sigma_M=-162.62$ $\tau=12.98$ $\sigma_{max}=-528.48$
 Tensioni: $\sigma_N=-365.87$ $\sigma_M=-3.32$ $\tau=18.87$ $\tau_{max}=18.87$
 Tensioni: $\sigma_N=-365.87$ $\sigma_M=-162.62$ $\tau=12.98$ $\sigma_{ID,max}=528.96$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU Xl=0.17
 Sollecitazioni: N=-2257.82 Tz=-75.97 My=-81.89 Ty=7.33 Mx=1.16
 V,Ed=7.33 Vc,Rd,Red=5916.66 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed = -75.97$ $Vc, Rd, Red = 11833.30$ $V, Ed/Vc, Rd, Red = 0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $Xl = 0.00$ - Classe 3
 Sollecitazioni: $N = -2823.23$ $Tz = -31.92$ $My = -45.10$ $Ty = -1.78$ $Mx = 8.53$
 Tensioni: $\sigma_N = -205.18$ $\sigma_M = -106.04$ $\tau = 16.40$ $\sigma_{max} = -311.21$
 Tensioni: $\sigma_N = -205.18$ $\sigma_M = 0.00$ $\tau = 20.54$ $\tau_{max} = 20.54$
 Tensioni: $\sigma_N = -205.18$ $\sigma_M = -106.04$ $\tau = 16.83$ $\sigma_{ID, max} = 312.57$

Asta n. 3562 (-8386 -8433) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N, Ed = -5185.04$ $My, Ed = -53.48$ $Mz, Ed = -7.19$
 Resistenze: $Nc, Rd = 30796.20$ $My, c, Rd = 951.93$ $Mz, c, Rd = 632.38$ $L = 17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 4.01$ $Ncr, y = 17709900.00$ $\lambda^*_y = 0.04$ Curva a: $\Phi_y = 0.00$ $\chi_y = 1.00$
 $\lambda_z = 6.96$ $Ncr, z = 5882490.00$ $\lambda^*_z = 0.07$ Curva a: $\Phi_z = 0.00$ $\chi_z = 1.00$
 $Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.17 + 0.04 + 0.01 = 0.22$
 Verifica ZZ: $0.17 + 0.03 + 0.01 = 0.21$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $Xl = 0.00$ - Classe 3
 Sollecitazioni: $N = -5185.04$ $Tz = -58.09$ $My = -53.48$ $Ty = -54.30$ $Mz = 2.19$ $Mx = 8.17$
 Tensioni: $\sigma_N = -376.82$ $\sigma_M = -133.51$ $\tau = 15.72$ $\sigma_{max} = -510.33$
 Tensioni: $\sigma_N = -376.82$ $\sigma_M = -117.36$ $\tau = 28.65$ $\tau_{max} = 28.65$
 Tensioni: $\sigma_N = -376.82$ $\sigma_M = -132.47$ $\tau = 26.48$ $\sigma_{ID, max} = 511.36$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 45 SLU $Xl = 0.03$
 Sollecitazioni: $N = -5184.99$ $Tz = -59.97$ $My = -51.63$ $Ty = -54.30$ $Mx = 8.17$
 $V, Ed = -54.30$ $Vc, Rd, Red = 5854.81$ $V, Ed/Vc, Rd, Red = 0.01$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed = -59.97$ $Vc, Rd, Red = 11709.60$ $V, Ed/Vc, Rd, Red = 0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $Xl = 0.00$ - Classe 3
 Sollecitazioni: $N = -2823.31$ $Tz = -36.99$ $My = -35.98$ $Ty = -17.25$ $Mx = 8.67$
 Tensioni: $\sigma_N = -205.18$ $\sigma_M = -84.59$ $\tau = 16.69$ $\sigma_{max} = -289.77$
 Tensioni: $\sigma_N = -205.18$ $\sigma_M = 0.00$ $\tau = 21.48$ $\tau_{max} = 21.48$
 Tensioni: $\sigma_N = -205.18$ $\sigma_M = -84.59$ $\tau = 20.80$ $\sigma_{ID, max} = 292.00$

Asta n. 3562 (-8433 -8486) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N, Ed = -4642.11$ $My, Ed = -51.62$ $Mz, Ed = -5.54$
 Resistenze: $Nc, Rd = 30796.20$ $My, c, Rd = 951.93$ $Mz, c, Rd = 632.38$ $L = 17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 4.01$ $Ncr, y = 17709900.00$ $\lambda^*_y = 0.04$ Curva a: $\Phi_y = 0.00$ $\chi_y = 1.00$
 $\lambda_z = 6.96$ $Ncr, z = 5882490.00$ $\lambda^*_z = 0.07$ Curva a: $\Phi_z = 0.00$ $\chi_z = 1.00$
 $Kyy, Kyz, Kzy, Kzz = 0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.15 + 0.04 + 0.01 = 0.20$
 Verifica ZZ: $0.15 + 0.03 + 0.01 = 0.19$

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $Xl = 0.17$ - Classe 3
 Sollecitazioni: $N = -4104.45$ $Tz = 102.23$ $My = -68.26$ $Ty = 38.74$ $Mz = 2.39$ $Mx = -21.77$
 Tensioni: $\sigma_N = -298.29$ $\sigma_M = -168.93$ $\tau = 41.88$ $\sigma_{max} = -467.21$
 Tensioni: $\sigma_N = -298.29$ $\sigma_M = -7.32$ $\tau = 55.14$ $\tau_{max} = 55.14$
 Tensioni: $\sigma_N = -298.29$ $\sigma_M = -167.80$ $\tau = 49.56$ $\sigma_{ID, max} = 473.93$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU $Xl = 0.03$
 Sollecitazioni: $N = -1972.64$ $Tz = 105.67$ $My = -60.15$ $Ty = 12.71$ $Mx = -34.55$
 $V, Ed = 12.71$ $Vc, Rd, Red = 5621.98$ $V, Ed/Vc, Rd, Red = 0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed = 105.67$ $Vc, Rd, Red = 11244.00$ $V, Ed/Vc, Rd, Red = 0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $Xl = 0.17$ - Classe 3
 Sollecitazioni: $N = -2535.87$ $Tz = 45.62$ $My = -34.65$ $Ty = 23.72$ $Mx = -16.85$
 Tensioni: $\sigma_N = -184.29$ $\sigma_M = -81.47$ $\tau = 32.42$ $\sigma_{max} = -265.76$
 Tensioni: $\sigma_N = -184.29$ $\sigma_M = 0.00$ $\tau = 38.34$ $\tau_{max} = 38.34$
 Tensioni: $\sigma_N = -184.29$ $\sigma_M = -81.47$ $\tau = 38.07$ $\sigma_{ID, max} = 273.82$

Asta n. 3562 (-8486 -8546) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: $N, Ed = -4051.27$ $My, Ed = -94.07$ $Mz, Ed = 1.53$

Resistenze: $N_c, R_d=30796.20$ $M_y, c, R_d=951.93$ $M_z, c, R_d=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr,y}=17709900.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882490.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.13+0.08+0.00=0.21$
 Verifica ZZ: $0.13+0.06+0.00=0.19$

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $X_l=0.17$ - Classe 3
 Sollecitazioni: $N=-4051.01$ $T_z=90.93$ $M_y=-94.07$ $T_y=-3.02$ $M_z=1.01$ $M_x=-20.15$
 Tensioni: $\sigma_N=-294.40$ $\sigma_M=-224.76$ $\tau=38.77$ $\sigma_{max}=-519.16$
 Tensioni: $\sigma_N=-294.40$ $\sigma_M=-3.11$ $\tau=50.56$ $\tau_{max}=50.56$
 Tensioni: $\sigma_N=-294.40$ $\sigma_M=-224.76$ $\tau=38.77$ $\sigma_{ID,max}=523.49$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU $X_l=0.00$
 Sollecitazioni: $N=-1979.07$ $T_z=100.44$ $M_y=-83.57$ $T_y=-4.48$ $M_x=-33.27$
 $V, Ed=-4.48$ $V_c, R_d, Red=5633.29$ $V, Ed/V_c, R_d, Red=0.00$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed=100.44$ $V_c, R_d, Red=11266.60$ $V, Ed/V_c, R_d, Red=0.01$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.17$ - Classe 3
 Sollecitazioni: $N=-2493.94$ $T_z=40.06$ $M_y=-45.83$ $M_x=-16.40$
 Tensioni: $\sigma_N=-181.25$ $\sigma_M=-107.75$ $\tau=31.57$ $\sigma_{max}=-289.00$
 Tensioni: $\sigma_N=-181.25$ $\sigma_M=0.00$ $\tau=36.76$ $\tau_{max}=36.76$
 Tensioni: $\sigma_N=-181.25$ $\sigma_M=-107.75$ $\tau=31.57$ $\sigma_{ID,max}=294.13$

Asta n. 3562 (-8546 -8635) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: $N, Ed=-4029.06$ $M_y, Ed=-106.14$ $M_z, Ed=0.53$
 Resistenze: $N_c, R_d=30796.20$ $M_y, c, R_d=951.93$ $M_z, c, R_d=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr,y}=17709900.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882490.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.13+0.09+0.00=0.22$
 Verifica ZZ: $0.13+0.07+0.00=0.20$
- Verifica a pressoflessione retta - CC 89 SLU $X_l=0.17$ - Classe 1
 Sollecitazioni: $N=-2354.34$ $T_z=27.60$ $M_y=-113.15$ $T_y=4.68$ $M_x=-27.82$
 $M_y, Ed=-113.15$ $M_y, c, R_d=1184.58$
 $N, Ed=-2354.34$ $N_c, R_d=30796.20$ $n=N, Ed/N_c, R_d=0.08$
 $MN_y, c, R_d=1184.58$ $M_y, Ed/MN_y, c, R_d=0.10$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 49 SLU $X_l=0.00$
 Sollecitazioni: $N=-4029.06$ $T_z=39.60$ $M_y=-100.18$ $T_y=1.15$ $M_x=-12.35$
 $V, Ed=1.15$ $V_c, R_d, Red=5817.90$ $V, Ed/V_c, R_d, Red=0.00$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed=39.60$ $V_c, R_d, Red=11635.80$ $V, Ed/V_c, R_d, Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.17$ - Classe 3
 Sollecitazioni: $N=-2457.99$ $T_z=10.27$ $M_y=-50.43$ $T_y=2.29$ $M_x=-13.44$
 Tensioni: $\sigma_N=-178.63$ $\sigma_M=-118.56$ $\tau=25.85$ $\sigma_{max}=-297.19$
 Tensioni: $\sigma_N=-178.63$ $\sigma_M=0.00$ $\tau=27.18$ $\tau_{max}=27.18$
 Tensioni: $\sigma_N=-178.63$ $\sigma_M=-118.56$ $\tau=26.40$ $\sigma_{ID,max}=300.69$

Asta n. 3562 (-8635 -8728) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: $N, Ed=-3994.09$ $M_y, Ed=-107.06$ $M_z, Ed=0.70$
 Resistenze: $N_c, R_d=30796.20$ $M_y, c, R_d=951.93$ $M_z, c, R_d=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $N_{cr,y}=17709900.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882490.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.13+0.09+0.00=0.22$
 Verifica ZZ: $0.13+0.07+0.00=0.20$
- Verifica a pressoflessione retta - CC 89 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $N=-2310.00$ $T_z=-12.05$ $M_y=-113.95$ $M_x=-19.59$
 $M_y, Ed=-113.95$ $M_y, c, R_d=1184.58$
 $N, Ed=-2310.00$ $N_c, R_d=30796.20$ $n=N, Ed/N_c, R_d=0.08$
 $MN_y, c, R_d=1184.58$ $M_y, Ed/MN_y, c, R_d=0.10$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 74 SLU $X_1=0.17$
Sollecitazioni: $N=-2601.81$ $T_z=-5.85$ $M_y=-84.84$ $T_y=10.30$ $M_x=-4.20$
 $V,Ed=10.30$ $Vc,Rd,Red=5889.82$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-5.85$ $Vc,Rd,Red=11779.60$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3
Sollecitazioni: $N=-2406.87$ $T_z=-6.64$ $M_y=-50.64$ $T_y=4.09$ $M_z=-1.16$ $M_x=-10.78$
Tensioni: $\sigma_N=-174.92$ $\sigma_M=-123.18$ $\tau=20.75$ $\sigma_{max}=-298.10$
Tensioni: $\sigma_N=-174.92$ $\sigma_M=-111.13$ $\tau=21.72$ $\tau_{max}=21.72$
Tensioni: $\sigma_N=-174.92$ $\sigma_M=-123.18$ $\tau=20.75$ $\sigma_{ID,max}=300.26$

Asta n. 3562 (-8728 -8809) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
Sollecitazioni: $N,Ed=-4523.57$ $M_y,Ed=-79.45$ $M_z,Ed=1.28$
Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $Ncr,y=17709900.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $Ncr,z=5882490.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
Verifica YY: $0.15+0.06+0.00=0.21$
Verifica ZZ: $0.15+0.05+0.00=0.20$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X_1=0.09$ - Classe 3
Sollecitazioni: $N=-4523.43$ $T_z=-56.85$ $M_y=-74.35$ $T_y=3.53$ $M_z=1.01$ $M_x=1.81$
Tensioni: $\sigma_N=-328.74$ $\sigma_M=-178.37$ $\tau=3.48$ $\sigma_{max}=-507.11$
Tensioni: $\sigma_N=-328.74$ $\sigma_M=-3.09$ $\tau=10.85$ $\tau_{max}=10.85$
Tensioni: $\sigma_N=-328.74$ $\sigma_M=-178.37$ $\tau=3.48$ $\sigma_{ID,max}=507.15$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU $X_1=0.17$
Sollecitazioni: $N=-1873.94$ $T_z=-84.69$ $M_y=-91.36$ $T_y=8.81$ $M_x=-9.67$
 $V,Ed=8.81$ $Vc,Rd,Red=5841.54$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-84.69$ $Vc,Rd,Red=11683.10$ $V,Ed/Vc,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3
Sollecitazioni: $N=-2346.74$ $T_z=-36.57$ $M_y=-47.15$ $T_y=7.95$ $M_z=-1.10$ $M_x=8.85$
Tensioni: $\sigma_N=-170.55$ $\sigma_M=-114.76$ $\tau=17.03$ $\sigma_{max}=-285.31$
Tensioni: $\sigma_N=-170.55$ $\sigma_M=3.38$ $\tau=21.77$ $\tau_{max}=21.77$
Tensioni: $\sigma_N=-170.55$ $\sigma_M=-114.76$ $\tau=17.03$ $\sigma_{ID,max}=286.83$

Asta n. 3562 (-8809 -8917) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
Sollecitazioni: $N,Ed=-4617.15$ $M_y,Ed=-63.99$ $M_z,Ed=-5.10$
Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $Ncr,y=17709900.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $Ncr,z=5882490.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
Verifica YY: $0.15+0.05+0.01=0.21$
Verifica ZZ: $0.15+0.04+0.01=0.20$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X_1=0.00$ - Classe 3
Sollecitazioni: $N=-4617.15$ $T_z=-63.34$ $M_y=-63.99$ $T_y=-37.85$ $M_z=1.44$ $M_x=3.06$
Tensioni: $\sigma_N=-335.55$ $\sigma_M=-155.54$ $\tau=5.88$ $\sigma_{max}=-491.09$
Tensioni: $\sigma_N=-335.55$ $\sigma_M=-140.42$ $\tau=14.91$ $\tau_{max}=14.91$
Tensioni: $\sigma_N=-335.55$ $\sigma_M=-155.54$ $\tau=5.88$ $\sigma_{ID,max}=491.20$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU $X_1=0.17$
Sollecitazioni: $N=-1812.08$ $T_z=-88.85$ $M_y=-69.56$ $T_y=4.13$ $M_x=-8.77$
 $V,Ed=4.13$ $Vc,Rd,Red=5849.47$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-88.85$ $Vc,Rd,Red=11698.90$ $V,Ed/Vc,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3
Sollecitazioni: $N=-2306.29$ $T_z=-41.04$ $M_y=-37.42$ $T_y=-7.15$ $M_x=8.93$
Tensioni: $\sigma_N=-167.61$ $\sigma_M=-87.97$ $\tau=17.19$ $\sigma_{max}=-255.58$
Tensioni: $\sigma_N=-167.61$ $\sigma_M=0.00$ $\tau=22.51$ $\tau_{max}=22.51$
Tensioni: $\sigma_N=-167.61$ $\sigma_M=-87.97$ $\tau=18.89$ $\sigma_{ID,max}=257.66$

Asta n. 3562 (-8917 -8991) Tubo 60x120x4 mm - S235 Crit. 2

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-3995.24 My,Ed=-62.49 Mz,Ed=-5.14
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17709900.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882490.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
 Verifica YY: 0.13+0.05+0.01=0.19
 Verifica ZZ: 0.13+0.04+0.01=0.18
 - Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.17 - Classe 3
 Sollecitazioni: N=-3994.97 Tz=86.72 My=-62.49 Ty=44.76 Mz=2.60 Mx=-29.26
 Tensioni: $\sigma_N=-290.33$ $\sigma_M=-156.12$ $\tau=56.29$ $\sigma_{max}=-446.45$
 Tensioni: $\sigma_N=-290.33$ $\sigma_M=-7.96$ $\tau=67.54$ $\tau_{max}=67.54$
 Tensioni: $\sigma_N=-290.33$ $\sigma_M=-154.89$ $\tau=65.17$ $\sigma_{ID,max}=459.31$
 - Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU Xl=0.00
 Sollecitazioni: N=-1513.11 Tz=107.31 My=-65.94 Ty=9.42 Mx=-51.66
 V,Ed=9.42 Vc,Rd,Red=5470.99 V,Ed/Vc,Rd,Red=0.00
 - Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=107.31 Vc,Rd,Red=10942.00 V,Ed/Vc,Rd,Red=0.01
 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3
 Sollecitazioni: N=-1990.76 Tz=43.99 My=-35.79 Ty=20.30 Mx=-22.65
 Tensioni: $\sigma_N=-144.68$ $\sigma_M=-84.14$ $\tau=43.58$ $\sigma_{max}=-228.82$
 Tensioni: $\sigma_N=-144.68$ $\sigma_M=0.00$ $\tau=49.28$ $\tau_{max}=49.28$
 Tensioni: $\sigma_N=-144.68$ $\sigma_M=-84.14$ $\tau=48.41$ $\sigma_{ID,max}=243.70$

Asta n. 3562 (-8991 -9100) Tubo 60x120x4 mm - S235 Crit. 2

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-3879.46 My,Ed=-83.81 Mz,Ed=1.47
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17709900.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882490.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
 Verifica YY: 0.13+0.07+0.00=0.20
 Verifica ZZ: 0.13+0.05+0.00=0.18
 - Verifica in termini tensionali [4.2.4] - CC 49 SLU Xl=0.17 - Classe 3
 Sollecitazioni: N=-3318.51 Tz=93.09 My=-105.58 Ty=1.40 Mz=1.06 Mx=-34.41
 Tensioni: $\sigma_N=-241.17$ $\sigma_M=-251.98$ $\tau=66.22$ $\sigma_{max}=-493.15$
 Tensioni: $\sigma_N=-241.17$ $\sigma_M=-3.26$ $\tau=78.29$ $\tau_{max}=78.29$
 Tensioni: $\sigma_N=-241.17$ $\sigma_M=-251.98$ $\tau=66.22$ $\sigma_{ID,max}=506.31$
 - Verifica a taglio e torsione dir. Z [4.2.25] - CC 25 SLU Xl=0.00
 Sollecitazioni: N=-1909.92 Tz=104.46 My=-89.83 Mx=-34.06
 V,Ed=104.46 Vc,Rd,Red=11252.50 V,Ed/Vc,Rd,Red=0.01
 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3
 Sollecitazioni: N=-1931.89 Tz=39.22 My=-45.97 Ty=1.28 Mx=-22.28
 Tensioni: $\sigma_N=-140.40$ $\sigma_M=-108.08$ $\tau=42.87$ $\sigma_{max}=-248.48$
 Tensioni: $\sigma_N=-140.40$ $\sigma_M=0.00$ $\tau=47.96$ $\tau_{max}=47.96$
 Tensioni: $\sigma_N=-140.40$ $\sigma_M=-108.08$ $\tau=43.18$ $\sigma_{ID,max}=259.49$

Asta n. 3562 (-9100 -9158) Tubo 60x120x4 mm - S235 Crit. 2

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: N,Ed=-3246.14 My,Ed=-118.36 Mz,Ed=0.74
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17709900.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882490.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.11+0.10+0.00=0.20
 Verifica ZZ: 0.11+0.08+0.00=0.18
 - Verifica a pressoflessione retta - CC 75 SLU Xl=0.17 - Classe 1
 Sollecitazioni: N=-2226.94 Tz=31.89 My=-122.26 Ty=8.12 Mx=-27.80
 My,Ed=-122.26 My,c,Rd=1184.58
 N,Ed=-2226.94 Nc,Rd=30796.20 n=N,Ed/Nc,Rd=0.07

MNy, c, Rd=1184.58 My, Ed/MNy, c, Rd=0.10

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 49 SLU Xl=0.00
Sollecitazioni: N=-3246.14 Tz=42.00 My=-111.99 Ty=4.45 Mx=-26.73
V, Ed=4.45 Vc, Rd, Red=5690.99 V, Ed/Vc, Rd, Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]
V, Ed=42.00 Vc, Rd, Red=11382.00 V, Ed/Vc, Rd, Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3
Sollecitazioni: N=-1869.90 Tz=12.75 My=-50.35 Ty=3.88 Mx=-19.56
Tensioni: $\sigma_N=-135.89$ $\sigma_M=-118.38$ $\tau=37.64$ $\sigma_{max}=-254.27$
Tensioni: $\sigma_N=-135.89$ $\sigma_M=0.00$ $\tau=39.29$ $\tau_{max}=39.29$
Tensioni: $\sigma_N=-135.89$ $\sigma_M=-118.38$ $\tau=38.56$ $\sigma_{ID, max}=262.90$

Asta n. 3562 (-9158 -9216) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
Sollecitazioni: N, Ed=-3150.58 My, Ed=-119.58 Mz, Ed=0.89
Resistenze: Nc, Rd=30796.20 My, c, Rd=951.93 Mz, c, Rd=632.38 L=17.28
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=4.01$ Ncr, y=17709900.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr, z=5882490.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.10+0.10+0.00=0.20
Verifica ZZ: 0.10+0.08+0.00=0.18

- Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.16 - Classe 3
Sollecitazioni: N=-3712.17 Tz=-14.73 My=-94.08 Ty=6.81 Mz=1.00 Mx=-15.56
Tensioni: $\sigma_N=-269.78$ $\sigma_M=-224.74$ $\tau=29.94$ $\sigma_{max}=-494.52$
Tensioni: $\sigma_N=-269.78$ $\sigma_M=3.07$ $\tau=31.85$ $\tau_{max}=31.85$
Tensioni: $\sigma_N=-269.78$ $\sigma_M=-224.74$ $\tau=29.94$ $\sigma_{ID, max}=497.23$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 74 SLU Xl=0.17
Sollecitazioni: N=-1903.28 Tz=-4.28 My=-93.90 Ty=12.30 Mx=-15.81
V, Ed=12.30 Vc, Rd, Red=5787.38 V, Ed/Vc, Rd, Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]
V, Ed=-4.28 Vc, Rd, Red=11574.80 V, Ed/Vc, Rd, Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-1790.73 Tz=8.65 My=-50.65 Ty=5.44 Mz=-1.14 Mx=-17.10
Tensioni: $\sigma_N=-130.14$ $\sigma_M=-123.13$ $\tau=32.91$ $\sigma_{max}=-253.27$
Tensioni: $\sigma_N=-130.14$ $\sigma_M=-111.16$ $\tau=34.20$ $\tau_{max}=34.20$
Tensioni: $\sigma_N=-130.14$ $\sigma_M=-123.13$ $\tau=32.91$ $\sigma_{ID, max}=259.61$

Asta n. 3562 (-9216 -9292) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
Sollecitazioni: N, Ed=-3636.80 My, Ed=-90.69 Mz, Ed=1.17
Resistenze: Nc, Rd=30796.20 My, c, Rd=951.93 Mz, c, Rd=632.38 L=17.28
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=4.01$ Ncr, y=17709900.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr, z=5882490.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.12+0.07+0.00=0.19
Verifica ZZ: 0.12+0.06+0.00=0.18

- Verifica in termini tensionali [4.2.4] - CC 49 SLU Xl=0.16 - Classe 3
Sollecitazioni: N=-3050.46 Tz=-76.17 My=-102.47 Ty=9.41 Mz=1.11 Mx=-11.13
Tensioni: $\sigma_N=-221.69$ $\sigma_M=-244.84$ $\tau=21.43$ $\sigma_{max}=-466.53$
Tensioni: $\sigma_N=-221.69$ $\sigma_M=3.39$ $\tau=31.30$ $\tau_{max}=31.30$
Tensioni: $\sigma_N=-221.69$ $\sigma_M=-244.84$ $\tau=21.43$ $\sigma_{ID, max}=468.00$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU Xl=0.17
Sollecitazioni: N=-1322.15 Tz=-84.62 My=-100.83 Ty=9.44 Mx=-26.91
V, Ed=9.44 Vc, Rd, Red=5689.39 V, Ed/Vc, Rd, Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]
V, Ed=-84.62 Vc, Rd, Red=11378.80 V, Ed/Vc, Rd, Red=0.01

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-1702.62 Tz=-33.26 My=-47.72 Ty=8.53 Mz=-1.13 Mx=-14.52
Tensioni: $\sigma_N=-123.74$ $\sigma_M=-116.21$ $\tau=27.95$ $\sigma_{max}=-239.95$
Tensioni: $\sigma_N=-123.74$ $\sigma_M=-3.47$ $\tau=32.26$ $\tau_{max}=32.26$

Tensioni: $\sigma_N=-123.74$ $\sigma_M=-115.68$ $\tau=29.64$ $\sigma_{ID,max}=244.86$

Asta n. 3562 (-9292 -9383) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3

Sollecitazioni: $N_{Ed}=-3627.72$ $M_{y,Ed}=-75.33$ $M_{z,Ed}=-1.73$

Resistenze: $N_{c,Rd}=30796.20$ $M_{y,c,Rd}=951.93$ $M_{z,c,Rd}=632.38$ $L=17.28$

α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95

$\lambda_y=4.01$ $N_{cr,y}=17709900.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$

$\lambda_z=6.96$ $N_{cr,z}=5882490.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$

K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.95 , 0.76 , 0.95

Verifica YY: $0.12+0.06+0.00=0.18$

Verifica ZZ: $0.12+0.05+0.00=0.17$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X1=0.11$ - Classe 3

Sollecitazioni: $N=-3627.56$ $T_x=-70.95$ $M_y=-67.89$ $T_y=-10.69$ $M_z=-1.06$ $M_x=-8.46$

Tensioni: $\sigma_N=-263.63$ $\sigma_M=-163.37$ $\tau=16.28$ $\sigma_{max}=-427.00$

Tensioni: $\sigma_N=-263.63$ $\sigma_M=-3.25$ $\tau=25.48$ $\tau_{max}=25.48$

Tensioni: $\sigma_N=-263.63$ $\sigma_M=-163.37$ $\tau=16.28$ $\sigma_{ID,max}=427.93$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU $X1=0.11$

Sollecitazioni: $N=-1229.77$ $T_x=-87.23$ $M_y=-84.35$ $T_y=11.75$ $M_x=-25.76$

$V_{Ed}=11.75$ $V_{c,Rd,Red}=5699.57$ $V_{Ed/V_{c,Rd,Red}}=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]

$V_{Ed}=-87.23$ $V_{c,Rd,Red}=11399.10$ $V_{Ed/V_{c,Rd,Red}}=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3

Sollecitazioni: $N=-1625.14$ $T_x=-38.26$ $M_y=-39.08$ $T_y=6.20$ $M_x=-14.18$

Tensioni: $\sigma_N=-118.11$ $\sigma_M=-91.89$ $\tau=27.28$ $\sigma_{max}=-210.00$

Tensioni: $\sigma_N=-118.11$ $\sigma_M=0.00$ $\tau=32.24$ $\tau_{max}=32.24$

Tensioni: $\sigma_N=-118.11$ $\sigma_M=-91.89$ $\tau=28.76$ $\sigma_{ID,max}=215.83$

Asta n. 3562 (-9383 -9449) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3

Sollecitazioni: $N_{Ed}=-2852.93$ $M_{y,Ed}=-63.56$ $M_{z,Ed}=-4.97$

Resistenze: $N_{c,Rd}=30796.20$ $M_{y,c,Rd}=951.93$ $M_{z,c,Rd}=632.38$ $L=17.28$

α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95

$\lambda_y=4.01$ $N_{cr,y}=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$

$\lambda_z=6.96$ $N_{cr,z}=5882510.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$

K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.95 , 0.76 , 0.95

Verifica YY: $0.09+0.05+0.01=0.15$

Verifica ZZ: $0.09+0.04+0.01=0.14$

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $X1=0.17$ - Classe 3

Sollecitazioni: $N=-2336.70$ $T_x=30.62$ $M_y=-80.26$ $T_y=31.61$ $M_z=1.91$ $M_x=-38.77$

Tensioni: $\sigma_N=-169.82$ $\sigma_M=-195.45$ $\tau=74.59$ $\sigma_{max}=-365.27$

Tensioni: $\sigma_N=-169.82$ $\sigma_M=-176.12$ $\tau=82.12$ $\tau_{max}=82.12$

Tensioni: $\sigma_N=-169.82$ $\sigma_M=-194.55$ $\tau=80.86$ $\sigma_{ID,max}=390.36$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 45 SLU $X1=0.10$

Sollecitazioni: $N=-2852.77$ $T_x=32.52$ $M_y=-61.45$ $T_y=43.07$ $M_x=-32.63$

$V_{Ed}=43.07$ $V_{c,Rd,Red}=5638.92$ $V_{Ed/V_{c,Rd,Red}}=0.01$

- Verifica a taglio e torsione dir. Z [4.2.25]

$V_{Ed}=32.52$ $V_{c,Rd,Red}=11277.80$ $V_{Ed/V_{c,Rd,Red}}=0.00$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3

Sollecitazioni: $N=-1314.48$ $T_x=27.99$ $M_y=-31.04$ $T_y=16.43$ $M_z=-2.39$ $M_x=-21.36$

Tensioni: $\sigma_N=-95.53$ $\sigma_M=-81.43$ $\tau=41.10$ $\sigma_{max}=-176.96$

Tensioni: $\sigma_N=-95.53$ $\sigma_M=-68.10$ $\tau=45.01$ $\tau_{max}=45.01$

Tensioni: $\sigma_N=-95.53$ $\sigma_M=-80.30$ $\tau=44.35$ $\sigma_{ID,max}=191.88$

Asta n. 3562 (-9449 -9507) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3

Sollecitazioni: $N_{Ed}=-2635.54$ $M_{y,Ed}=-69.40$ $M_{z,Ed}=1.97$

Resistenze: $N_{c,Rd}=30796.20$ $M_{y,c,Rd}=951.93$ $M_{z,c,Rd}=632.38$ $L=17.28$

α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95

$\lambda_y=4.01$ $N_{cr,y}=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$

$\lambda_z=6.96$ $N_{cr,z}=5882500.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$

K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.95 , 0.76 , 0.95

Verifica YY: $0.09+0.06+0.00=0.14$

Verifica ZZ: $0.09+0.04+0.00=0.13$

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $X_1=0.17$ - Classe 3
 Sollecitazioni: $N=-2180.95$ $T_x=15.06$ $M_y=-87.13$ $T_y=9.07$ $M_z=1.32$ $M_x=-36.73$
 Tensioni: $\sigma_N=-158.50$ $\sigma_M=-209.51$ $\tau=70.68$ $\sigma_{max}=-368.01$
 Tensioni: $\sigma_N=-158.50$ $\sigma_M=-191.19$ $\tau=72.84$ $\tau_{max}=72.84$
 Tensioni: $\sigma_N=-158.50$ $\sigma_M=-208.89$ $\tau=72.48$ $\sigma_{ID,max}=388.25$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 99 SLU $X_1=0.00$
 Sollecitazioni: $N=-203.81$ $T_x=32.14$ $M_y=-36.20$ $T_y=5.13$ $M_x=-7.21$
 $V,Ed=5.13$ $Vc,Rd,Red=5863.23$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=32.14$ $Vc,Rd,Red=11726.50$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.17$ - Classe 3
 Sollecitazioni: $N=-1237.00$ $T_x=16.09$ $M_y=-37.19$ $T_y=3.87$ $M_x=-20.77$
 Tensioni: $\sigma_N=-89.90$ $\sigma_M=-87.44$ $\tau=39.96$ $\sigma_{max}=-177.34$
 Tensioni: $\sigma_N=-89.90$ $\sigma_M=0.00$ $\tau=42.04$ $\tau_{max}=42.04$
 Tensioni: $\sigma_N=-89.90$ $\sigma_M=-87.44$ $\tau=40.88$ $\sigma_{ID,max}=190.95$

Asta n. 3562 (-9507 -9559) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: $N,Ed=-2013.85$ $M_y,Ed=-87.27$ $M_z,Ed=1.03$
 Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $Ncr,y=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $Ncr,z=5882500.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.07+0.07+0.00=0.14$
 Verifica ZZ: $0.07+0.06+0.00=0.12$

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $X_1=0.17$ - Classe 3
 Sollecitazioni: $N=-2013.59$ $T_x=-44.84$ $M_y=-80.41$ $T_y=8.98$ $M_z=1.03$ $M_x=-28.97$
 Tensioni: $\sigma_N=-146.34$ $\sigma_M=-192.71$ $\tau=55.74$ $\sigma_{max}=-339.05$
 Tensioni: $\sigma_N=-146.34$ $\sigma_M=3.17$ $\tau=61.55$ $\tau_{max}=61.55$
 Tensioni: $\sigma_N=-146.34$ $\sigma_M=-192.22$ $\tau=57.52$ $\sigma_{ID,max}=352.91$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 89 SLU $X_1=0.17$
 Sollecitazioni: $N=-1071.90$ $T_x=-57.96$ $M_y=-72.75$ $T_y=7.43$ $M_x=-46.87$
 $V,Ed=7.43$ $Vc,Rd,Red=5513.26$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-57.96$ $Vc,Rd,Red=11026.50$ $V,Ed/Vc,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=-1149.62$ $T_x=-25.76$ $M_y=-37.70$ $T_y=5.01$ $M_x=-18.18$
 Tensioni: $\sigma_N=-83.55$ $\sigma_M=-88.64$ $\tau=34.98$ $\sigma_{max}=-172.19$
 Tensioni: $\sigma_N=-83.55$ $\sigma_M=0.00$ $\tau=38.32$ $\tau_{max}=38.32$
 Tensioni: $\sigma_N=-83.55$ $\sigma_M=-88.64$ $\tau=36.17$ $\sigma_{ID,max}=183.23$

Asta n. 3562 (-9559 -9607) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-2176.21$ $M_y,Ed=-60.87$ $M_z,Ed=2.02$
 Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $Ncr,y=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $Ncr,z=5882510.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.07+0.05+0.00=0.12$
 Verifica ZZ: $0.07+0.04+0.00=0.11$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X_1=0.10$ - Classe 3
 Sollecitazioni: $N=-2176.05$ $T_x=-72.41$ $M_y=-53.68$ $T_y=14.63$ $M_z=1.01$ $M_x=-18.41$
 Tensioni: $\sigma_N=-158.14$ $\sigma_M=-129.77$ $\tau=35.42$ $\sigma_{max}=-287.92$
 Tensioni: $\sigma_N=-158.14$ $\sigma_M=3.09$ $\tau=44.81$ $\tau_{max}=44.81$
 Tensioni: $\sigma_N=-158.14$ $\sigma_M=-129.30$ $\tau=38.32$ $\sigma_{ID,max}=295.01$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU $X_1=0.17$
 Sollecitazioni: $N=-794.33$ $T_x=-101.97$ $M_y=-51.85$ $T_y=5.72$ $M_x=-36.01$
 $V,Ed=5.72$ $Vc,Rd,Red=5609.07$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-101.97$ $Vc,Rd,Red=11218.10$ $V,Ed/Vc,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=-1043.82$ $T_z=-41.68$ $M_y=-36.21$ $T_y=6.42$ $M_z=-1.09$ $M_x=-15.85$
 Tensioni: $\sigma_N=-75.86$ $\sigma_M=-89.00$ $\tau=30.50$ $\sigma_{max}=-164.86$
 Tensioni: $\sigma_N=-75.86$ $\sigma_M=-3.34$ $\tau=35.91$ $\tau_{max}=35.91$
 Tensioni: $\sigma_N=-75.86$ $\sigma_M=-88.49$ $\tau=31.78$ $\sigma_{ID,max}=173.32$

Asta n. 3562 (-9607 -9649) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-1913.44$ $M_y,Ed=-40.47$ $M_z,Ed=2.01$
 Resistenze: $N_c,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=4.01$ $N_{cr,y}=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882510.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.95 , 0.76 , 0.95
 Verifica YY: $0.06+0.03+0.00=0.10$
 Verifica ZZ: $0.06+0.03+0.00=0.09$

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $X1=0.00$ - Classe 3
 Sollecitazioni: $N=-1580.92$ $T_z=-142.82$ $M_y=-49.87$ $T_y=17.09$ $M_z=-1.16$ $M_x=-13.33$
 Tensioni: $\sigma_N=-114.89$ $\sigma_M=-121.35$ $\tau=25.65$ $\sigma_{max}=-236.24$
 Tensioni: $\sigma_N=-114.89$ $\sigma_M=-3.56$ $\tau=44.16$ $\tau_{max}=44.16$
 Tensioni: $\sigma_N=-114.89$ $\sigma_M=-120.80$ $\tau=29.03$ $\sigma_{ID,max}=241.00$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU $X1=0.16$
 Sollecitazioni: $N=-667.99$ $T_z=-164.47$ $M_y=-16.09$ $T_y=12.70$ $M_x=-28.14$
 $V,Ed=12.70$ $V_c,Rd,Red=5678.58$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-164.47$ $V_c,Rd,Red=11357.20$ $V,Ed/V_c,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=-920.34$ $T_z=-65.50$ $M_y=-31.33$ $T_y=10.29$ $M_z=-1.22$ $M_x=-13.48$
 Tensioni: $\sigma_N=-66.89$ $\sigma_M=-77.96$ $\tau=25.95$ $\sigma_{max}=-144.85$
 Tensioni: $\sigma_N=-66.89$ $\sigma_M=-3.74$ $\tau=34.44$ $\tau_{max}=34.44$
 Tensioni: $\sigma_N=-66.89$ $\sigma_M=-77.39$ $\tau=27.99$ $\sigma_{ID,max}=152.20$

Asta n. 3562 (-9649 -9747) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-1662.61$ $M_y,Ed=11.95$ $M_z,Ed=6.62$
 Resistenze: $N_c,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=4.01$ $N_{cr,y}=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $N_{cr,z}=5882500.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.95 , 0.76 , 0.95
 Verifica YY: $0.05+0.01+0.01=0.07$
 Verifica ZZ: $0.05+0.01+0.01=0.07$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X1=0.17$ - Classe 3
 Sollecitazioni: $N=-1662.35$ $T_z=-131.95$ $M_y=11.95$ $T_y=46.76$ $M_z=6.62$ $M_x=-11.64$
 Tensioni: $\sigma_N=-120.81$ $\sigma_M=-51.54$ $\tau=22.40$ $\sigma_{max}=-172.35$
 Tensioni: $\sigma_N=-120.81$ $\sigma_M=20.32$ $\tau=39.51$ $\tau_{max}=39.51$
 Tensioni: $\sigma_N=-120.81$ $\sigma_M=-51.54$ $\tau=22.40$ $\sigma_{ID,max}=176.66$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU $X1=0.06$
 Sollecitazioni: $N=-509.20$ $T_z=-162.60$ $M_y=10.54$ $T_y=25.33$ $M_x=-27.17$
 $V,Ed=25.33$ $V_c,Rd,Red=5687.12$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-162.60$ $V_c,Rd,Red=11374.20$ $V,Ed/V_c,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.17$ - Classe 3
 Sollecitazioni: $N=-506.14$ $T_z=-90.16$ $M_y=35.29$ $T_y=17.23$ $M_z=2.17$ $M_x=-17.78$
 Tensioni: $\sigma_N=-36.78$ $\sigma_M=-90.67$ $\tau=34.20$ $\sigma_{max}=-127.45$
 Tensioni: $\sigma_N=-36.78$ $\sigma_M=6.67$ $\tau=45.89$ $\tau_{max}=45.89$
 Tensioni: $\sigma_N=-36.78$ $\sigma_M=-90.67$ $\tau=34.20$ $\sigma_{ID,max}=140.55$

Asta n. 3562 (-9747 -9863) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
 Sollecitazioni: $N,Ed=-324.16$ $M_y,Ed=35.96$ $M_z,Ed=0.73$
 Resistenze: $N_c,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95

$\lambda_y=4.01$ Ncr, $y=17710000.00$ $\lambda_y^*=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr, $z=5882520.00$ $\lambda_z^*=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.01+0.04+0.00=0.05
 Verifica ZZ: 0.01+0.03+0.00=0.04

- Verifica in termini tensionali [4.2.4] - CC 49 SLU Xl=0.17 - Classe 3
 Sollecitazioni: N=-624.75 T_z=121.18 M_y=-3.39 T_y=16.24 M_z=2.16 M_x=-57.12
 Tensioni: $\sigma_N=-45.40$ $\sigma_M=-15.62$ $\tau=109.92$ $\sigma_{max}=-61.02$
 Tensioni: $\sigma_N=-45.40$ $\sigma_M=-6.63$ $\tau=125.63$ $\tau_{max}=125.63$
 Tensioni: $\sigma_N=-45.40$ $\sigma_M=-7.65$ $\tau=125.63$ $\sigma_{ID,max}=223.96$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU Xl=0.00
 Sollecitazioni: N=-332.38 T_z=137.80 M_y=30.33 T_y=-4.39 M_x=-69.59
 V,Ed=-4.39 Vc,Rd,Red=5312.69 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=137.80 Vc,Rd,Red=10625.40 V,Ed/Vc,Rd,Red=0.01

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-324.16 T_z=68.00 M_y=35.96 T_y=-4.39 M_x=-32.94
 Tensioni: $\sigma_N=-23.56$ $\sigma_M=-84.55$ $\tau=63.39$ $\sigma_{max}=-108.11$
 Tensioni: $\sigma_N=-23.56$ $\sigma_M=-0.00$ $\tau=72.20$ $\tau_{max}=72.20$
 Tensioni: $\sigma_N=-23.56$ $\sigma_M=-78.91$ $\tau=68.02$ $\sigma_{ID,max}=156.15$

Asta n. 3562 (-9863 -9974) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: N,Ed=-470.79 M_y,Ed=-32.51 M_z,Ed=2.21
 Resistenze: Nc,Rd=30796.20 M_y,c,Rd=951.93 M_z,c,Rd=632.38 L=17.28
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=4.01$ Ncr, $y=17710000.00$ $\lambda_y^*=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr, $z=5882520.00$ $\lambda_z^*=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.02+0.03+0.00=0.04
 Verifica ZZ: 0.02+0.02+0.00=0.04

- Verifica in termini tensionali [4.2.4] - CC 49 SLU Xl=0.17 - Classe 3
 Sollecitazioni: N=-470.52 T_z=101.04 M_y=-32.51 T_y=15.35 M_z=2.21 M_x=-54.49
 Tensioni: $\sigma_N=-34.20$ $\sigma_M=-84.24$ $\tau=104.85$ $\sigma_{max}=-118.44$
 Tensioni: $\sigma_N=-34.20$ $\sigma_M=-6.77$ $\tau=117.95$ $\tau_{max}=117.95$
 Tensioni: $\sigma_N=-34.20$ $\sigma_M=-79.15$ $\tau=111.74$ $\sigma_{ID,max}=224.29$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU Xl=0.00
 Sollecitazioni: N=-348.63 T_z=120.37 M_y=-4.09 T_y=-1.95 M_x=-67.03
 V,Ed=-1.95 Vc,Rd,Red=5335.27 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=120.37 Vc,Rd,Red=10670.50 V,Ed/Vc,Rd,Red=0.01

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.17 - Classe 3
 Sollecitazioni: N=-299.52 T_z=53.77 M_y=-30.20 T_y=2.00 M_x=-32.19
 Tensioni: $\sigma_N=-21.77$ $\sigma_M=-71.01$ $\tau=61.94$ $\sigma_{max}=-92.78$
 Tensioni: $\sigma_N=-21.77$ $\sigma_M=0.00$ $\tau=68.91$ $\tau_{max}=68.91$
 Tensioni: $\sigma_N=-21.77$ $\sigma_M=-66.28$ $\tau=65.61$ $\sigma_{ID,max}=143.75$

Asta n. 3562 (-9974 -10043) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 75 SLU - Classe 3
 Sollecitazioni: N,Ed=-440.88 M_y,Ed=-46.48 M_z,Ed=-0.87
 Resistenze: Nc,Rd=30796.20 M_y,c,Rd=951.93 M_z,c,Rd=632.38 L=17.28
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=4.01$ Ncr, $y=17710000.00$ $\lambda_y^*=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr, $z=5882510.00$ $\lambda_z^*=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.01+0.04+0.00=0.05
 Verifica ZZ: 0.01+0.03+0.00=0.05

- Verifica in termini tensionali [4.2.4] - CC 49 SLU Xl=0.17 - Classe 3
 Sollecitazioni: N=-305.27 T_z=48.36 M_y=-49.44 T_y=12.32 M_z=2.19 M_x=-46.51
 Tensioni: $\sigma_N=-22.19$ $\sigma_M=-124.01$ $\tau=89.49$ $\sigma_{max}=-146.19$
 Tensioni: $\sigma_N=-22.19$ $\sigma_M=-6.73$ $\tau=95.76$ $\tau_{max}=95.76$
 Tensioni: $\sigma_N=-22.19$ $\sigma_M=-122.97$ $\tau=91.94$ $\sigma_{ID,max}=215.47$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU Xl=0.00

Sollecitazioni: $N=-323.87$ $T_z=64.26$ $M_y=-32.37$ $T_y=3.20$ $M_x=-58.71$
 $V,Ed=3.20$ $Vc,Rd,Red=5408.77$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=64.26$ $Vc,Rd,Red=10817.50$ $V,Ed/Vc,Rd,Red=0.01$
- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=-251.45$ $T_z=39.78$ $M_y=-30.74$ $T_y=4.18$ $M_x=-29.47$
 Tensioni: $\sigma_N=-18.27$ $\sigma_M=-72.28$ $\tau=56.70$ $\sigma_{max}=-90.55$
 Tensioni: $\sigma_N=-18.27$ $\sigma_M=0.00$ $\tau=61.86$ $\tau_{max}=61.86$
 Tensioni: $\sigma_N=-18.27$ $\sigma_M=-72.28$ $\tau=57.70$ $\sigma_{ID,max}=134.85$

Asta n. 3562 (-10043 -10135) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 SLU - Classe 3
 Sollecitazioni: $N,Ed=-290.85$ $M_y,Ed=-51.11$ $M_z,Ed=-0.97$
 Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $Ncr,y=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $Ncr,z=5882520.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.01+0.04+0.00=0.05$
 Verifica ZZ: $0.01+0.03+0.00=0.04$

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $X1=0.13$ - Classe 3
 Sollecitazioni: $N=-154.07$ $T_z=-12.17$ $M_y=-50.68$ $T_y=9.16$ $M_z=1.35$ $M_x=-36.01$
 Tensioni: $\sigma_N=-11.20$ $\sigma_M=-123.92$ $\tau=69.29$ $\sigma_{max}=-135.12$
 Tensioni: $\sigma_N=-11.20$ $\sigma_M=-111.20$ $\tau=71.47$ $\tau_{max}=71.47$
 Tensioni: $\sigma_N=-11.20$ $\sigma_M=-123.28$ $\tau=71.11$ $\sigma_{ID,max}=182.35$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 74 SLU $X1=0.17$
 Sollecitazioni: $N=-286.17$ $T_z=-2.20$ $M_y=-33.66$ $T_y=12.79$ $M_x=-26.23$
 $V,Ed=12.79$ $Vc,Rd,Red=5695.36$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-2.20$ $Vc,Rd,Red=11390.70$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=-182.41$ $T_z=19.96$ $M_y=-29.16$ $T_y=4.93$ $M_x=-26.28$
 Tensioni: $\sigma_N=-13.26$ $\sigma_M=-68.57$ $\tau=50.57$ $\sigma_{max}=-81.82$
 Tensioni: $\sigma_N=-13.26$ $\sigma_M=0.00$ $\tau=53.16$ $\tau_{max}=53.16$
 Tensioni: $\sigma_N=-13.26$ $\sigma_M=-68.57$ $\tau=51.75$ $\sigma_{ID,max}=121.36$

Asta n. 3562 (-10135 -10201) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 SLU - Classe 3
 Sollecitazioni: $N,Ed=-183.58$ $M_y,Ed=-46.43$ $M_z,Ed=-0.89$
 Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=17.28$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ $Ncr,y=17710000.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ $Ncr,z=5882520.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.01+0.04+0.00=0.04$
 Verifica ZZ: $0.01+0.03+0.00=0.04$

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $X1=0.16$ - Classe 3
 Sollecitazioni: $N=-55.01$ $T_z=-69.26$ $M_y=-36.69$ $T_y=3.19$ $M_z=1.05$ $M_x=-26.62$
 Tensioni: $\sigma_N=-4.00$ $\sigma_M=-89.99$ $\tau=51.22$ $\sigma_{max}=-93.99$
 Tensioni: $\sigma_N=-4.00$ $\sigma_M=3.24$ $\tau=60.20$ $\tau_{max}=60.20$
 Tensioni: $\sigma_N=-4.00$ $\sigma_M=-89.49$ $\tau=51.86$ $\sigma_{ID,max}=129.65$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 25 SLU $X1=0.17$
 Sollecitazioni: $N=-183.32$ $T_z=-70.12$ $M_y=-35.19$ $T_y=8.13$ $M_x=-24.05$
 $V,Ed=8.13$ $Vc,Rd,Red=5714.63$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-70.12$ $Vc,Rd,Red=11429.30$ $V,Ed/Vc,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=-107.52$ $T_z=-34.67$ $M_y=-22.94$ $T_y=5.58$ $M_x=-23.28$
 Tensioni: $\sigma_N=-7.81$ $\sigma_M=-53.93$ $\tau=44.80$ $\sigma_{max}=-61.74$
 Tensioni: $\sigma_N=-7.81$ $\sigma_M=0.00$ $\tau=49.29$ $\tau_{max}=49.29$
 Tensioni: $\sigma_N=-7.81$ $\sigma_M=-53.93$ $\tau=46.13$ $\sigma_{ID,max}=100.97$

Asta n. 3562 (-10201 -10257) Tubo 60x120x4 mm - S235 Crit. 2

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 25 SLU - Classe 3
 Sollecitazioni: N,Ed=-71.39 My,Ed=-27.27 Mz,Ed=1.41
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.28
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.01$ Ncr,y=17710000.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.96$ Ncr,z=5882520.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.03
 Verifica ZZ: 0.00+0.02+0.00=0.02
- Verifica in termini tensionali [4.2.4] - CC 89 SLU Xl=0.17 - Classe 3
 Sollecitazioni: N=-72.43 Tz=-99.01 My=-6.78 Ty=14.97 Mz=1.24 Mx=-32.91
 Tensioni: $\sigma_N=-5.26$ $\sigma_M=-20.34$ $\tau=63.33$ $\sigma_{max}=-25.60$
 Tensioni: $\sigma_N=-5.26$ $\sigma_M=3.81$ $\tau=76.17$ $\tau_{max}=76.17$
 Tensioni: $\sigma_N=-5.26$ $\sigma_M=3.81$ $\tau=76.17$ $\sigma_{ID,max}=131.93$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 49 SLU Xl=0.17
 Sollecitazioni: N=-15.56 Tz=-119.93 My=-7.66 Ty=-1.27 Mx=-20.10
 V,Ed=-1.27 Vc,Rd,Red=5749.52 V,Ed/Vc,Rd,Red=0.00
- Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=-119.93 Vc,Rd,Red=11499.00 V,Ed/Vc,Rd,Red=0.01
- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.17 - Classe 3
 Sollecitazioni: N=-36.93 Tz=-56.55 My=-3.25 Ty=7.38 Mx=-21.32
 Tensioni: $\sigma_N=-2.68$ $\sigma_M=-7.65$ $\tau=41.02$ $\sigma_{max}=-10.33$
 Tensioni: $\sigma_N=-2.68$ $\sigma_M=0.00$ $\tau=48.35$ $\tau_{max}=48.35$
 Tensioni: $\sigma_N=-2.68$ $\sigma_M=0.00$ $\tau=48.35$ $\sigma_{ID,max}=83.79$
- Asta n. 3566 (-4526 -4524) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-3464.76 My,Ed=147.34 Mz,Ed=31.18
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=13.86
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=3.22$ Ncr,y=27515800.00 $\lambda^*_y=0.03$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=5.59$ Ncr,z=9139590.00 $\lambda^*_z=0.06$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.11+0.12+0.05=0.28
 Verifica ZZ: 0.11+0.09+0.05=0.25
- Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-3464.76 Tz=389.81 My=147.34 Ty=162.97 Mz=8.58 Mx=10.05
 Tensioni: $\sigma_N=-251.80$ $\sigma_M=-376.79$ $\tau=19.33$ $\sigma_{max}=-628.59$
 Tensioni: $\sigma_N=-251.80$ $\sigma_M=26.32$ $\tau=69.89$ $\tau_{max}=69.89$
 Tensioni: $\sigma_N=-251.80$ $\sigma_M=-372.74$ $\tau=51.63$ $\sigma_{ID,max}=630.91$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 37 SLU Xl=0.08
 Sollecitazioni: N=-3.34 Tz=-38.50 My=133.94 Ty=43.62 Mx=40.41
 V,Ed=43.62 Vc,Rd,Red=5570.26 V,Ed/Vc,Rd,Red=0.01
- Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=-38.50 Vc,Rd,Red=11140.50 V,Ed/Vc,Rd,Red=0.00
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.14 - Classe 3
 Sollecitazioni: N=85.64 Tz=-51.97 My=77.48 Ty=-27.21 Mz=-4.78 Mx=19.26
 Tensioni: $\sigma_N=6.22$ $\sigma_M=199.08$ $\tau=37.06$ $\sigma_{max}=205.30$
 Tensioni: $\sigma_N=6.22$ $\sigma_M=14.65$ $\tau=43.80$ $\tau_{max}=43.80$
 Tensioni: $\sigma_N=6.22$ $\sigma_M=196.82$ $\tau=42.45$ $\sigma_{ID,max}=215.95$
- Asta n. 3566 (-4528 -4526) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-3349.37 My,Ed=162.39 Mz,Ed=38.30
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=13.86
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=3.22$ Ncr,y=27515900.00 $\lambda^*_y=0.03$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=5.59$ Ncr,z=9139600.00 $\lambda^*_z=0.06$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.11+0.13+0.06=0.30
 Verifica ZZ: 0.11+0.10+0.06=0.27
- Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.14 - Classe 3
 Sollecitazioni: N=-3349.37 Tz=-216.91 My=162.39 Ty=451.80 Mz=38.30 Mx=-3.41

Tensioni: $\sigma_N=-243.41$ $\sigma_M=-517.35$ $\tau=6.56$ $\sigma_{max}=-760.76$
 Tensioni: $\sigma_N=-243.41$ $\sigma_M=356.35$ $\tau=114.13$ $\tau_{max}=114.13$
 Tensioni: $\sigma_N=-243.41$ $\sigma_M=-517.35$ $\tau=6.56$ $\sigma_{ID,max}=760.84$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X1=0.05$
 Sollecitazioni: $N=404.61$ $T_z=-270.96$ $M_y=121.08$ $T_y=-56.72$ $M_x=16.24$
 $V,Ed=-56.72$ $Vc,Rd,Red=5783.58$ $V,Ed/Vc,Rd,Red=0.01$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-270.96$ $Vc,Rd,Red=11567.20$ $V,Ed/Vc,Rd,Red=0.02$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.14$ - Classe 3
 Sollecitazioni: $N=221.65$ $T_z=-178.84$ $M_y=75.50$ $T_y=-37.01$ $M_z=-3.68$ $M_x=13.30$
 Tensioni: $\sigma_N=16.11$ $\sigma_M=190.53$ $\tau=25.58$ $\sigma_{max}=206.64$
 Tensioni: $\sigma_N=16.11$ $\sigma_M=11.28$ $\tau=48.77$ $\tau_{max}=48.77$
 Tensioni: $\sigma_N=16.11$ $\sigma_M=188.80$ $\tau=32.92$ $\sigma_{ID,max}=212.69$

Asta n. 3568 (-4532 -4528) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-2491.57$ $M_y,Ed=121.27$ $M_z,Ed=-15.27$
 Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=14.09$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=3.27$ $Ncr,y=26643900.00$ $\lambda^*_y=0.03$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=5.68$ $Ncr,z=8849960.00$ $\lambda^*_z=0.06$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.08+0.10+0.02=0.20$
 Verifica ZZ: $0.08+0.08+0.02=0.18$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X1=0.14$ - Classe 3
 Sollecitazioni: $N=-2491.57$ $T_z=-279.03$ $M_y=121.27$ $T_y=-77.27$ $M_z=-15.27$ $M_x=21.32$
 Tensioni: $\sigma_N=-181.07$ $\sigma_M=-339.17$ $\tau=41.02$ $\sigma_{max}=-520.24$
 Tensioni: $\sigma_N=-181.07$ $\sigma_M=46.85$ $\tau=77.20$ $\tau_{max}=77.20$
 Tensioni: $\sigma_N=-181.07$ $\sigma_M=-339.17$ $\tau=41.02$ $\sigma_{ID,max}=525.07$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X1=0.06$
 Sollecitazioni: $N=293.40$ $T_z=-352.11$ $M_y=62.60$ $T_y=7.98$ $M_x=34.04$
 $V,Ed=7.98$ $Vc,Rd,Red=5626.43$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-352.11$ $Vc,Rd,Red=11252.90$ $V,Ed/Vc,Rd,Red=0.03$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.14$ - Classe 3
 Sollecitazioni: $N=230.17$ $T_z=-223.83$ $M_y=42.20$ $T_y=5.28$ $M_x=20.90$
 Tensioni: $\sigma_N=16.73$ $\sigma_M=99.21$ $\tau=40.22$ $\sigma_{max}=115.94$
 Tensioni: $\sigma_N=16.73$ $\sigma_M=-0.00$ $\tau=69.24$ $\tau_{max}=69.24$
 Tensioni: $\sigma_N=16.73$ $\sigma_M=92.60$ $\tau=55.49$ $\sigma_{ID,max}=145.56$

Asta n. 3568 (-4539 -4532) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-2041.38$ $M_y,Ed=73.69$ $M_z,Ed=-4.03$
 Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=14.09$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=3.27$ $Ncr,y=26644100.00$ $\lambda^*_y=0.03$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=5.68$ $Ncr,z=8850050.00$ $\lambda^*_z=0.06$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.07+0.06+0.01=0.13$
 Verifica ZZ: $0.07+0.05+0.01=0.12$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X1=0.14$ - Classe 3
 Sollecitazioni: $N=-2041.38$ $T_z=-207.10$ $M_y=73.69$ $T_y=8.10$ $M_z=-2.89$ $M_x=23.54$
 Tensioni: $\sigma_N=-148.36$ $\sigma_M=-183.48$ $\tau=45.30$ $\sigma_{max}=-331.84$
 Tensioni: $\sigma_N=-148.36$ $\sigma_M=8.87$ $\tau=72.14$ $\tau_{max}=72.14$
 Tensioni: $\sigma_N=-148.36$ $\sigma_M=-183.48$ $\tau=45.30$ $\sigma_{ID,max}=340.99$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X1=0.14$
 Sollecitazioni: $N=235.94$ $T_z=-262.43$ $M_y=28.97$ $T_y=-1.52$ $M_x=37.39$
 $V,Ed=-1.52$ $Vc,Rd,Red=5596.86$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-262.43$ $Vc,Rd,Red=11193.70$ $V,Ed/Vc,Rd,Red=0.02$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.14$ - Classe 3
 Sollecitazioni: $N=272.04$ $T_z=-171.44$ $M_y=28.58$ $T_y=-2.62$ $M_x=22.67$

Tensioni: $\sigma_N=19.77$ $\sigma_M=67.20$ $\tau=43.62$ $\sigma_{max}=86.97$
 Tensioni: $\sigma_N=19.77$ $\sigma_M=-0.00$ $\tau=65.84$ $\tau_{max}=65.84$
 Tensioni: $\sigma_N=19.77$ $\sigma_M=62.72$ $\tau=55.31$ $\sigma_{TD,max}=126.42$

Asta n. 3568 (-4541 -4539) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3

Sollecitazioni: N,Ed=-1692.27 My,Ed=35.48 Mz,Ed=-6.38
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=14.09
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=3.27$ Ncr,y=26643900.00 $\lambda^*_y=0.03$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=5.68$ Ncr,z=8849960.00 $\lambda^*_z=0.06$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.05+0.03+0.01=0.09
 Verifica ZZ: 0.05+0.02+0.01=0.09

- Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.13 - Classe 3

Sollecitazioni: N=-1692.27 Tz=-198.80 My=32.93 Ty=38.62 Mz=-1.43 Mx=24.70
 Tensioni: $\sigma_N=-122.98$ $\sigma_M=-82.47$ $\tau=47.53$ $\sigma_{max}=-205.45$
 Tensioni: $\sigma_N=-122.98$ $\sigma_M=4.38$ $\tau=73.30$ $\tau_{max}=73.30$
 Tensioni: $\sigma_N=-122.98$ $\sigma_M=-81.79$ $\tau=55.18$ $\sigma_{TD,max}=225.99$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU Xl=0.14

Sollecitazioni: N=185.53 Tz=-252.49 My=-19.65 Ty=-4.32 Mx=39.27
 V,Ed=-4.32 Vc,Rd,Red=5580.34 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]

V,Ed=-252.49 Vc,Rd,Red=11160.70 V,Ed/Vc,Rd,Red=0.02

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3

Sollecitazioni: N=301.48 Tz=-162.55 My=-57.54 Ty=-6.59 Mx=23.69
 Tensioni: $\sigma_N=21.91$ $\sigma_M=135.29$ $\tau=45.59$ $\sigma_{max}=157.19$
 Tensioni: $\sigma_N=21.91$ $\sigma_M=0.00$ $\tau=66.67$ $\tau_{max}=66.67$
 Tensioni: $\sigma_N=21.91$ $\sigma_M=126.27$ $\tau=56.68$ $\sigma_{TD,max}=177.75$

Asta n. 3570 (-4554 -4541) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3

Sollecitazioni: N,Ed=-219.40 My,Ed=-92.47 Mz,Ed=-0.61
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.10
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=3.97$ Ncr,y=18092600.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.89$ Ncr,z=6009580.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.01+0.09+0.00=0.10
 Verifica ZZ: 0.01+0.07+0.00=0.08

- Verifica a pressoflessione retta - CC 68 SLU Xl=0.00 - Classe 1

Sollecitazioni: N=169.78 Tz=-187.01 My=-130.79 Ty=3.51 Mx=23.29
 My,Ed=-130.79 My,c,Rd=1184.58
 N,Ed=169.78 Nc,Rd=30796.20 n=N,Ed/Nc,Rd=0.01
 MNy,c,Rd=1184.58 My,Ed/MNy,c,Rd=0.11

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU Xl=0.17

Sollecitazioni: N=154.66 Tz=-208.62 My=-72.38 Ty=3.22 Mx=30.18
 V,Ed=3.22 Vc,Rd,Red=5660.57 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]

V,Ed=-208.62 Vc,Rd,Red=11321.10 V,Ed/Vc,Rd,Red=0.02

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3

Sollecitazioni: N=344.52 Tz=-140.17 My=-92.47 Ty=7.10 Mx=13.72
 Tensioni: $\sigma_N=25.04$ $\sigma_M=217.41$ $\tau=26.40$ $\sigma_{max}=242.45$
 Tensioni: $\sigma_N=25.04$ $\sigma_M=0.00$ $\tau=44.57$ $\tau_{max}=44.57$
 Tensioni: $\sigma_N=25.04$ $\sigma_M=217.41$ $\tau=28.09$ $\sigma_{TD,max}=247.28$

Asta n. 3570 (-4569 -4554) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3

Sollecitazioni: N,Ed=-294.71 My,Ed=-119.17 Mz,Ed=0.80
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.10
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=3.97$ Ncr,y=18092400.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.89$ Ncr,z=6009520.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: $0.01+0.12+0.00=0.13$
 Verifica ZZ: $0.01+0.10+0.00=0.11$

- Verifica a pressoflessione retta - CC 68 SLU $X_1=0.00$ - Classe 1
 Sollecitazioni: $N=139.59$ $T_z=-129.15$ $M_y=-162.62$ $T_y=-1.06$ $M_x=28.75$
 $M_y, Ed=-162.62$ $M_y, c, Rd=1184.58$
 $N, Ed=139.59$ $Nc, Rd=30796.20$ $n=N, Ed/Nc, Rd=0.00$
 $MNy, c, Rd=1184.58$ $M_y, Ed/MNy, c, Rd=0.14$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X_1=0.17$
 Sollecitazioni: $N=124.05$ $T_z=-151.20$ $M_y=-116.66$ $T_y=-1.12$ $M_x=35.29$
 $V, Ed=-1.12$ $Vc, Rd, Red=5615.44$ $V, Ed/Vc, Rd, Red=0.00$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed=-151.20$ $Vc, Rd, Red=11230.90$ $V, Ed/Vc, Rd, Red=0.01$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=403.90$ $T_z=-113.11$ $M_y=-119.17$ $T_y=1.89$ $M_x=16.11$
 Tensioni: $\sigma_N=29.35$ $\sigma_M=280.18$ $\tau=31.00$ $\sigma_{max}=309.54$
 Tensioni: $\sigma_N=29.35$ $\sigma_M=0.00$ $\tau=45.66$ $\tau_{max}=45.66$
 Tensioni: $\sigma_N=29.35$ $\sigma_M=280.18$ $\tau=31.45$ $\sigma_{ID, max}=314.29$

Asta n. 3570 (-4579 -4569) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N, Ed=-338.28$ $M_y, Ed=-141.01$ $M_z, Ed=0.71$
 Resistenze: $Nc, Rd=30796.20$ $M_y, c, Rd=951.93$ $M_z, c, Rd=632.38$ $L=17.10$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=3.97$ $Ncr, y=18092600.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.89$ $Ncr, z=6009580.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.01+0.14+0.00=0.15$
 Verifica ZZ: $0.01+0.11+0.00=0.12$

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=-719.38$ $T_z=-88.13$ $M_y=-125.07$ $T_y=13.66$ $M_z=-2.53$ $M_x=40.20$
 Tensioni: $\sigma_N=-52.28$ $\sigma_M=-303.02$ $\tau=77.35$ $\sigma_{max}=-355.30$
 Tensioni: $\sigma_N=-52.28$ $\sigma_M=7.77$ $\tau=88.78$ $\tau_{max}=88.78$
 Tensioni: $\sigma_N=-52.28$ $\sigma_M=-303.02$ $\tau=77.35$ $\sigma_{ID, max}=379.72$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X_1=0.17$
 Sollecitazioni: $N=84.20$ $T_z=-100.67$ $M_y=-148.38$ $T_y=-2.52$ $M_x=40.10$
 $V, Ed=-2.52$ $Vc, Rd, Red=5572.95$ $V, Ed/Vc, Rd, Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed=-100.67$ $Vc, Rd, Red=11145.90$ $V, Ed/Vc, Rd, Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=423.25$ $T_z=-92.08$ $M_y=-141.01$ $T_y=5.56$ $M_x=18.42$
 Tensioni: $\sigma_N=30.76$ $\sigma_M=331.52$ $\tau=35.44$ $\sigma_{max}=362.28$
 Tensioni: $\sigma_N=30.76$ $\sigma_M=0.00$ $\tau=47.37$ $\tau_{max}=47.37$
 Tensioni: $\sigma_N=30.76$ $\sigma_M=331.52$ $\tau=36.76$ $\sigma_{ID, max}=367.83$

Asta n. 3571 (-4540 -4553) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N, Ed=-251.78$ $M_y, Ed=-134.97$ $M_z, Ed=-0.77$
 Resistenze: $Nc, Rd=30796.20$ $M_y, c, Rd=951.93$ $M_z, c, Rd=632.38$ $L=17.10$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=3.97$ $Ncr, y=18092500.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.89$ $Ncr, z=6009570.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.01+0.13+0.00=0.14$
 Verifica ZZ: $0.01+0.11+0.00=0.12$

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $X_1=0.12$ - Classe 3
 Sollecitazioni: $N=-832.98$ $T_z=191.64$ $M_y=-63.27$ $T_y=17.75$ $M_z=-1.06$ $M_x=-30.88$
 Tensioni: $\sigma_N=-60.54$ $\sigma_M=-152.50$ $\tau=59.42$ $\sigma_{max}=-213.04$
 Tensioni: $\sigma_N=-60.54$ $\sigma_M=3.24$ $\tau=84.27$ $\tau_{max}=84.27$
 Tensioni: $\sigma_N=-60.54$ $\sigma_M=-152.00$ $\tau=62.94$ $\sigma_{ID, max}=238.87$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X_1=0.00$
 Sollecitazioni: $N=147.52$ $T_z=223.58$ $M_y=-83.76$ $T_y=-3.07$ $M_x=-30.52$
 $V, Ed=-3.07$ $Vc, Rd, Red=5657.57$ $V, Ed/Vc, Rd, Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]

V,Ed=223.58 Vc,Rd,Red=11315.10 V,Ed/Vc,Rd,Red=0.02

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3
Sollecitazioni: N=365.33 T_z=156.05 M_y=-134.97 T_y=-7.77 M_x=-12.49
Tensioni: $\sigma_N=26.55$ $\sigma_M=317.32$ $\tau=24.04$ $\sigma_{max}=343.87$
Tensioni: $\sigma_N=26.55$ $\sigma_M=0.00$ $\tau=44.27$ $\tau_{max}=44.27$
Tensioni: $\sigma_N=26.55$ $\sigma_M=317.32$ $\tau=25.89$ $\sigma_{TD,max}=346.79$

Asta n. 3571 (-4553 -4568) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-310.86 My,Ed=-165.11 Mz,Ed=0.92
Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.10
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=3.97$ Ncr,y=18092400.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.89$ Ncr,z=6009520.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.01+0.16+0.00=0.18
Verifica ZZ: 0.01+0.13+0.00=0.14

- Verifica a pressoflessione retta - CC 54 SLU Xl=0.17 - Classe 1
Sollecitazioni: N=113.06 T_z=155.85 M_y=-159.00 T_y=1.18 M_x=-35.64
My,Ed=-159.00 My,c,Rd=1184.58
N,Ed=113.06 Nc,Rd=30796.20 n=N,Ed/Nc,Rd=0.00
MNy,c,Rd=1184.58 My,Ed/MNy,c,Rd=0.13

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU Xl=0.00
Sollecitazioni: N=113.06 T_z=166.04 M_y=-131.48 T_y=1.18 M_x=-35.64
V,Ed=1.18 Vc,Rd,Red=5612.32 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]
V,Ed=166.04 Vc,Rd,Red=11224.60 V,Ed/Vc,Rd,Red=0.01

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3
Sollecitazioni: N=408.39 T_z=127.66 M_y=-165.11 T_y=-1.49 M_x=-14.63
Tensioni: $\sigma_N=29.68$ $\sigma_M=388.20$ $\tau=28.16$ $\sigma_{max}=417.88$
Tensioni: $\sigma_N=29.68$ $\sigma_M=0.00$ $\tau=44.71$ $\tau_{max}=44.71$
Tensioni: $\sigma_N=29.68$ $\sigma_M=388.20$ $\tau=28.51$ $\sigma_{TD,max}=420.79$

Asta n. 3571 (-4568 -4578) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-338.74 My,Ed=-190.32 Mz,Ed=0.75
Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=17.10
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=3.97$ Ncr,y=18092500.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.89$ Ncr,z=6009570.00 $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.01+0.19+0.00=0.20
Verifica ZZ: 0.01+0.15+0.00=0.16

- Verifica in termini tensionali [4.2.4] - CC 49 SLU Xl=0.17 - Classe 3
Sollecitazioni: N=-732.62 T_z=88.19 M_y=-127.70 T_y=-13.76 M_z=-2.54 M_x=-39.79
Tensioni: $\sigma_N=-53.24$ $\sigma_M=-309.21$ $\tau=76.57$ $\sigma_{max}=-362.45$
Tensioni: $\sigma_N=-53.24$ $\sigma_M=7.78$ $\tau=88.00$ $\tau_{max}=88.00$
Tensioni: $\sigma_N=-53.24$ $\sigma_M=-309.21$ $\tau=76.57$ $\sigma_{TD,max}=385.95$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU Xl=0.00
Sollecitazioni: N=70.86 T_z=115.39 M_y=-166.72 T_y=2.32 M_x=-40.53
V,Ed=2.32 Vc,Rd,Red=5569.23 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]
V,Ed=115.39 Vc,Rd,Red=11138.50 V,Ed/Vc,Rd,Red=0.01

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.17 - Classe 3
Sollecitazioni: N=412.81 T_z=105.07 M_y=-190.32 T_y=-5.57 M_x=-16.91
Tensioni: $\sigma_N=30.00$ $\sigma_M=447.45$ $\tau=32.54$ $\sigma_{max}=477.45$
Tensioni: $\sigma_N=30.00$ $\sigma_M=0.00$ $\tau=46.16$ $\tau_{max}=46.16$
Tensioni: $\sigma_N=30.00$ $\sigma_M=447.45$ $\tau=33.86$ $\sigma_{TD,max}=481.04$

Asta n. 3574 (-4594 -4579) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-384.79 My,Ed=-157.22 Mz,Ed=1.12
Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=14.26

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=3.31$ Ncr,y=26015300.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=5.74$ Ncr,z=8641160.00 $\lambda^*_z=0.06$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.01+0.16+0.00=0.17
 Verifica ZZ: 0.01+0.13+0.00=0.14

- Verifica in termini tensionali [4.2.4] - CC 49 SLU Xl=0.06 - Classe 3
 Sollecitazioni: N=-729.84 Tz=-64.62 My=-140.47 Ty=-23.44 Mz=-1.16 Mx=12.39
 Tensioni: $\sigma_N=-53.04$ $\sigma_M=-334.34$ $\tau=23.84$ $\sigma_{max}=-387.38$
 Tensioni: $\sigma_N=-53.04$ $\sigma_M=3.54$ $\tau=32.22$ $\tau_{max}=32.22$
 Tensioni: $\sigma_N=-53.04$ $\sigma_M=-333.80$ $\tau=28.49$ $\sigma_{ID,max}=389.97$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 45 SLU Xl=0.00
 Sollecitazioni: N=-1304.45 Tz=-51.19 My=-96.93 Ty=-41.60 Mz=16.34
 V,Ed=-41.60 Vc,Rd,Red=5782.73 V,Ed/Vc,Rd,Red=0.01

- Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=-51.19 Vc,Rd,Red=11565.50 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=455.84 Tz=-81.48 My=-157.22 Ty=15.18 Mz=-1.05 Mx=18.13
 Tensioni: $\sigma_N=33.13$ $\sigma_M=373.36$ $\tau=34.88$ $\sigma_{max}=406.49$
 Tensioni: $\sigma_N=33.13$ $\sigma_M=3.23$ $\tau=45.44$ $\tau_{max}=45.44$
 Tensioni: $\sigma_N=33.13$ $\sigma_M=372.86$ $\tau=37.89$ $\sigma_{ID,max}=411.26$

Asta n. 3574 (-4611 -4594) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-447.70 My,Ed=-170.27 Mz,Ed=1.39
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=14.26

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=3.31$ Ncr,y=26015000.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=5.74$ Ncr,z=8641060.00 $\lambda^*_z=0.06$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.01+0.17+0.00=0.19
 Verifica ZZ: 0.01+0.14+0.00=0.15

- Verifica in termini tensionali [4.2.4] - CC 49 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-817.62 Tz=-25.72 My=-151.84 Ty=-14.40 Mz=1.25 Mx=13.77
 Tensioni: $\sigma_N=-59.42$ $\sigma_M=-361.44$ $\tau=26.50$ $\sigma_{max}=-420.86$
 Tensioni: $\sigma_N=-59.42$ $\sigma_M=-333.20$ $\tau=29.93$ $\tau_{max}=29.93$
 Tensioni: $\sigma_N=-59.42$ $\sigma_M=-361.44$ $\tau=26.50$ $\sigma_{ID,max}=423.35$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 45 SLU Xl=0.05
 Sollecitazioni: N=-1448.92 Tz=-24.52 My=-102.01 Ty=-24.20 Mz=17.35
 V,Ed=-24.20 Vc,Rd,Red=5773.80 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=-24.52 Vc,Rd,Red=11547.60 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=516.61 Tz=-70.33 My=-170.27 Ty=7.84 Mz=1.39 Mx=18.32
 Tensioni: $\sigma_N=37.54$ $\sigma_M=405.25$ $\tau=35.25$ $\sigma_{max}=442.79$
 Tensioni: $\sigma_N=37.54$ $\sigma_M=-4.27$ $\tau=44.37$ $\tau_{max}=44.37$
 Tensioni: $\sigma_N=37.54$ $\sigma_M=405.25$ $\tau=35.25$ $\sigma_{ID,max}=446.98$

Asta n. 3574 (-4626 -4611) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-482.16 My,Ed=-185.19 Mz,Ed=1.28
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=14.26

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=3.31$ Ncr,y=26015300.00 $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=5.74$ Ncr,z=8641160.00 $\lambda^*_z=0.06$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.02+0.18+0.00=0.20
 Verifica ZZ: 0.02+0.15+0.00=0.17

- Verifica in termini tensionali [4.2.4] - CC 49 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-896.02 Tz=-115.59 My=-168.55 Ty=-45.51 Mz=5.91 Mx=5.85
 Tensioni: $\sigma_N=-65.12$ $\sigma_M=-417.20$ $\tau=11.26$ $\sigma_{max}=-482.32$
 Tensioni: $\sigma_N=-65.12$ $\sigma_M=-18.12$ $\tau=26.25$ $\tau_{max}=26.25$
 Tensioni: $\sigma_N=-65.12$ $\sigma_M=-417.20$ $\tau=11.26$ $\sigma_{ID,max}=482.71$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 45 SLU $X_1=0.12$
Sollecitazioni: $N=-1573.68$ $T_z=-104.04$ $M_y=-105.72$ $T_y=-72.39$ $M_x=10.45$
 $V, Ed=-72.39$ $Vc, Rd, Red=5834.71$ $V, Ed/Vc, Rd, Red=0.01$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed=-104.04$ $Vc, Rd, Red=11669.40$ $V, Ed/Vc, Rd, Red=0.01$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3
Sollecitazioni: $N=546.65$ $T_z=-97.87$ $M_y=-185.19$ $T_y=-5.09$ $M_z=1.28$ $M_x=-15.88$
Tensioni: $\sigma_N=39.73$ $\sigma_M=439.96$ $\tau=30.55$ $\sigma_{max}=479.69$
Tensioni: $\sigma_N=39.73$ $\sigma_M=3.94$ $\tau=43.24$ $\tau_{max}=43.24$
Tensioni: $\sigma_N=39.73$ $\sigma_M=439.96$ $\tau=30.55$ $\sigma_{ID, max}=482.60$

Asta n. 3575 (-4578 -4593) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: $N, Ed=-373.98$ $M_y, Ed=-207.66$ $M_z, Ed=1.18$
Resistenze: $Nc, Rd=30796.20$ $M_y, c, Rd=951.93$ $M_z, c, Rd=632.38$ $L=14.26$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=3.31$ $Ncr, y=26015300.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=5.74$ $Ncr, z=8641160.00$ $\lambda^*_z=0.06$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.01+0.21+0.00=0.22$
Verifica ZZ: $0.01+0.17+0.00=0.18$

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $X_1=0.08$ - Classe 3
Sollecitazioni: $N=-743.30$ $T_z=64.85$ $M_y=-142.97$ $T_y=24.38$ $M_z=-1.12$ $M_x=-11.39$
Tensioni: $\sigma_N=-54.02$ $\sigma_M=-340.08$ $\tau=21.91$ $\sigma_{max}=-394.10$
Tensioni: $\sigma_N=-54.02$ $\sigma_M=3.43$ $\tau=30.32$ $\tau_{max}=30.32$
Tensioni: $\sigma_N=-54.02$ $\sigma_M=-339.56$ $\tau=26.74$ $\sigma_{ID, max}=396.29$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 45 SLU $X_1=0.10$
Sollecitazioni: $N=-1315.65$ $T_z=54.16$ $M_y=-97.28$ $T_y=42.76$ $M_x=-15.50$
 $V, Ed=42.76$ $Vc, Rd, Red=5790.06$ $V, Ed/Vc, Rd, Red=0.01$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed=54.16$ $Vc, Rd, Red=11580.10$ $V, Ed/Vc, Rd, Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.14$ - Classe 3
Sollecitazioni: $N=433.60$ $T_z=93.29$ $M_y=-207.66$ $T_y=-14.33$ $M_z=1.18$ $M_x=-29.77$
Tensioni: $\sigma_N=31.51$ $\sigma_M=492.40$ $\tau=57.28$ $\sigma_{max}=523.91$
Tensioni: $\sigma_N=31.51$ $\sigma_M=-3.62$ $\tau=69.37$ $\tau_{max}=69.37$
Tensioni: $\sigma_N=31.51$ $\sigma_M=491.84$ $\tau=60.12$ $\sigma_{ID, max}=533.61$

Asta n. 3575 (-4593 -4610) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: $N, Ed=-425.46$ $M_y, Ed=-223.14$ $M_z, Ed=1.60$
Resistenze: $Nc, Rd=30796.20$ $M_y, c, Rd=951.93$ $M_z, c, Rd=632.38$ $L=14.26$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=3.31$ $Ncr, y=26014900.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=5.74$ $Ncr, z=8641060.00$ $\lambda^*_z=0.06$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.01+0.22+0.00=0.24$
Verifica ZZ: $0.01+0.18+0.00=0.19$

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $X_1=0.14$ - Classe 3
Sollecitazioni: $N=-830.18$ $T_z=24.10$ $M_y=-154.30$ $T_y=15.97$ $M_z=1.47$ $M_x=-12.73$
Tensioni: $\sigma_N=-60.33$ $\sigma_M=-367.97$ $\tau=24.50$ $\sigma_{max}=-428.30$
Tensioni: $\sigma_N=-60.33$ $\sigma_M=-338.60$ $\tau=28.30$ $\tau_{max}=28.30$
Tensioni: $\sigma_N=-60.33$ $\sigma_M=-367.97$ $\tau=24.50$ $\sigma_{ID, max}=430.40$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 45 SLU $X_1=0.03$
Sollecitazioni: $N=-1457.59$ $T_z=27.48$ $M_y=-102.87$ $T_y=26.61$ $M_x=-16.49$
 $V, Ed=26.61$ $Vc, Rd, Red=5781.40$ $V, Ed/Vc, Rd, Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed=27.48$ $Vc, Rd, Red=11562.80$ $V, Ed/Vc, Rd, Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.14$ - Classe 3
Sollecitazioni: $N=481.43$ $T_z=79.33$ $M_y=-223.14$ $T_y=-6.55$ $M_z=1.60$ $M_x=-29.90$
Tensioni: $\sigma_N=34.99$ $\sigma_M=530.30$ $\tau=57.54$ $\sigma_{max}=565.28$
Tensioni: $\sigma_N=34.99$ $\sigma_M=-4.91$ $\tau=67.83$ $\tau_{max}=67.83$
Tensioni: $\sigma_N=34.99$ $\sigma_M=530.30$ $\tau=57.54$ $\sigma_{ID, max}=574.00$

Asta n. 3575 (-4610 -4612) Tubo 60x120x4 mm - S235 Crit. 2

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-445.75 My,Ed=-242.72 Mz,Ed=1.24
 Resistenze: Nc,Rd=30796.20 My,c,Rd=951.93 Mz,c,Rd=632.38 L=14.26
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=3.31$ Ncr,y=26015300.00 $\lambda'_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=5.74$ Ncr,z=8641160.00 $\lambda'_z=0.06$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.01+0.24+0.00=0.26
 Verifica ZZ: 0.01+0.19+0.00=0.21
 - Verifica in termini tensionali [4.2.4] - CC 49 SLU Xl=0.14 - Classe 3
 Sollecitazioni: N=-840.63 Tz=139.10 My=-172.26 Ty=48.29 Mz=6.30 Mx=-4.63
 Tensioni: $\sigma_N=-61.09$ $\sigma_M=-427.30$ $\tau=8.91$ $\sigma_{max}=-488.39$
 Tensioni: $\sigma_N=-61.09$ $\sigma_M=-19.33$ $\tau=26.95$ $\tau_{max}=26.95$
 Tensioni: $\sigma_N=-61.09$ $\sigma_M=-427.30$ $\tau=8.91$ $\sigma_{ID,max}=488.63$
 - Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU Xl=0.00
 Sollecitazioni: N=16.96 Tz=165.32 My=-215.66 Ty=3.59 Mx=7.31
 V,Ed=3.59 Vc,Rd,Red=5862.43 V,Ed/Vc,Rd,Red=0.00
 - Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=165.32 Vc,Rd,Red=11724.90 V,Ed/Vc,Rd,Red=0.01
 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.14 - Classe 3
 Sollecitazioni: N=497.32 Tz=130.39 My=-242.72 Ty=3.37 Mz=1.24 Mx=30.19
 Tensioni: $\sigma_N=36.14$ $\sigma_M=575.05$ $\tau=58.10$ $\sigma_{max}=611.19$
 Tensioni: $\sigma_N=36.14$ $\sigma_M=3.81$ $\tau=75.00$ $\tau_{max}=75.00$
 Tensioni: $\sigma_N=36.14$ $\sigma_M=575.05$ $\tau=58.10$ $\sigma_{ID,max}=619.42$

Asta n. 3577 (-2478 -4526) Tubo circolare d=70x4 mm - S355 Crit. 3

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 1
 Sollecitazioni: N,Ed=-3366.49 M,Ed=4.29
 Resistenze: Nc,Rd=28041.00 M,c,Rd=575.38 L=202.59
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, ----, ----$
 $\lambda=86.66$ Ncr=22888.60 $\lambda'=1.13$
 Curva a: $\Phi=1.24$ $\chi_{min}=0.57$
 Kyy, Kyz, Kzy, Kzz=1.11, ----, ----, ----
 Verifica: 0.21+0.01=0.22
 - Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.01$ (L/31687)
 - Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.02$ (L/11383) $f_{z,L}=0.01$ (L/14180)
 - Verifica a compressione [4.2.9] - CC 45 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=-3366.49 T=8.48 Mx=-1.23
 N,Ed=-3366.49 Nc,Rd=-28041.00 N,Ed/Nc,Rd=0.12
 - Verifica a taglio e torsione dir. Z [4.2.25] - CC 68 SLU Xl=2.02
 Sollecitazioni: N=-1578.33 T=8.48 Mx=-7.33
 V,Ed=8.48 Vc,Rd,Red=10157.50 V,Ed/Vc,Rd,Red=0.00
 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.01 - Classe 3
 Sollecitazioni: N=-1028.35 M=3.18 Mx=-4.73
 Tensioni: $\sigma_N=-123.99$ $\sigma_M=-24.55$ $\tau=18.27$ $\sigma_{max}=-148.54$
 Tensioni: $\sigma_N=-123.99$ $\sigma_M=24.18$ $\tau=18.27$ $\tau_{max}=18.27$
 Tensioni: $\sigma_N=-123.99$ $\sigma_M=-24.55$ $\tau=18.27$ $\sigma_{ID,max}=151.88$

Asta n. 3578 (-2477 -4525) Tubo circolare d=70x4 mm - S355 Crit. 3

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 1
 Sollecitazioni: N,Ed=-3312.10 M,Ed=4.30
 Resistenze: Nc,Rd=28041.00 M,c,Rd=575.38 L=202.84
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, ----, ----$
 $\lambda=86.77$ Ncr=22832.90 $\lambda'=1.14$
 Curva a: $\Phi=1.24$ $\chi_{min}=0.57$
 Kyy, Kyz, Kzy, Kzz=1.11, ----, ----, ----
 Verifica: 0.21+0.01=0.21
 - Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.01$ (L/31490)

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.02$ (L/11382) $f_{z,l}=0.01$ (L/14135)
- Verifica a compressione [4.2.9] - CC 45 SLU $Xl=0.00$ - Classe 1
 Sollecitazioni: $N=-3312.10$ $T=8.48$ $M_x=1.47$
 $N,Ed=-3312.10$ $Nc,Rd=-28041.00$ $N,Ed/Nc,Rd=0.12$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 89 SLU $Xl=2.03$
 Sollecitazioni: $N=-354.51$ $T=8.48$ $M_x=-5.66$
 $V,Ed=8.48$ $Vc,Rd,Red=10191.40$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $Xl=1.01$ - Classe 3
 Sollecitazioni: $N=-722.51$ $M=3.18$ $M_x=10.23$
 Tensioni: $\sigma_N=-87.11$ $\sigma_M=-24.59$ $\tau=39.49$ $\sigma_{max}=-111.71$
 Tensioni: $\sigma_N=-87.11$ $\sigma_M=21.30$ $\tau=39.49$ $\tau_{max}=39.49$
 Tensioni: $\sigma_N=-87.11$ $\sigma_M=-24.59$ $\tau=39.49$ $\sigma_{ID,max}=130.98$

Asta n. 3579 (-4628 -4626) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N,Ed=-567.16$ $M_y,Ed=-172.16$ $M_z,Ed=-2.74$
 Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=15.67$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=3.64$ $Ncr,y=21535600.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.31$ $Ncr,z=7153210.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.02+0.17+0.00=0.19$
 Verifica ZZ: $0.02+0.14+0.00=0.16$

- Verifica in termini tensionali [4.2.4] - CC 54 SLU $Xl=0.15$ - Classe 3
 Sollecitazioni: $N=-50.78$ $T_z=72.84$ $M_y=-202.22$ $T_y=-12.78$ $M_z=-1.17$ $M_x=-29.23$
 Tensioni: $\sigma_N=-3.69$ $\sigma_M=-479.59$ $\tau=56.25$ $\sigma_{max}=-483.28$
 Tensioni: $\sigma_N=-3.69$ $\sigma_M=3.59$ $\tau=65.69$ $\tau_{max}=65.69$
 Tensioni: $\sigma_N=-3.69$ $\sigma_M=-479.59$ $\tau=56.25$ $\sigma_{ID,max}=493.00$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 45 SLU $Xl=0.03$
 Sollecitazioni: $N=-1060.49$ $T_z=53.15$ $M_y=-115.20$ $T_y=69.56$ $M_x=-18.85$
 $V,Ed=69.56$ $Vc,Rd,Red=5760.49$ $V,Ed/Vc,Rd,Red=0.01$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=53.15$ $Vc,Rd,Red=11521.00$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $Xl=0.15$ - Classe 3
 Sollecitazioni: $N=586.01$ $T_z=99.17$ $M_y=-172.16$ $T_y=-28.60$ $M_z=-2.74$ $M_x=-23.41$
 Tensioni: $\sigma_N=42.59$ $\sigma_M=414.45$ $\tau=45.04$ $\sigma_{max}=457.04$
 Tensioni: $\sigma_N=42.59$ $\sigma_M=8.40$ $\tau=57.89$ $\tau_{max}=57.89$
 Tensioni: $\sigma_N=42.59$ $\sigma_M=413.15$ $\tau=50.71$ $\sigma_{ID,max}=464.13$

Asta n. 3579 (-4643 -4628) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N,Ed=-635.14$ $M_y,Ed=-152.70$ $M_z,Ed=1.83$
 Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=15.67$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=3.64$ $Ncr,y=21535400.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.31$ $Ncr,z=7153130.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.02+0.15+0.00=0.18$
 Verifica ZZ: $0.02+0.12+0.00=0.15$

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $Xl=0.16$ - Classe 3
 Sollecitazioni: $N=-598.52$ $T_z=78.58$ $M_y=-156.01$ $T_y=-3.51$ $M_z=-1.23$ $M_x=-20.91$
 Tensioni: $\sigma_N=-43.50$ $\sigma_M=-371.15$ $\tau=40.24$ $\sigma_{max}=-414.65$
 Tensioni: $\sigma_N=-43.50$ $\sigma_M=3.77$ $\tau=50.43$ $\tau_{max}=50.43$
 Tensioni: $\sigma_N=-43.50$ $\sigma_M=-371.15$ $\tau=40.24$ $\sigma_{ID,max}=420.47$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 68 SLU $Xl=0.00$
 Sollecitazioni: $N=-36.97$ $T_z=134.48$ $M_y=-161.95$ $T_y=-2.22$ $M_x=-28.23$
 $V,Ed=-2.22$ $Vc,Rd,Red=5677.71$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=134.48$ $Vc,Rd,Red=11355.40$ $V,Ed/Vc,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $Xl=0.16$ - Classe 3
 Sollecitazioni: $N=638.04$ $T_z=96.39$ $M_y=-152.70$ $T_y=-8.29$ $M_x=-21.92$

Tensioni: $\sigma_N=46.37$ $\sigma_M=359.01$ $\tau=42.18$ $\sigma_{max}=405.38$
 Tensioni: $\sigma_N=46.37$ $\sigma_M=0.00$ $\tau=54.68$ $\tau_{max}=54.68$
 Tensioni: $\sigma_N=46.37$ $\sigma_M=359.01$ $\tau=44.16$ $\sigma_{TD,max}=412.53$

Asta n. 3579 (-4660 -4643) Tubo 60x120x4 mm - S235 Crit. 2

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3

Sollecitazioni: $N, Ed=-652.99$ $M_y, Ed=-130.86$ $M_z, Ed=1.70$
 Resistenze: $N_c, Rd=30796.20$ $M_y, c, Rd=951.93$ $M_z, c, Rd=632.38$ $L=15.67$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=3.64$ $N_{cr,y}=21535600.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.31$ $N_{cr,z}=7153210.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.02+0.13+0.00=0.15$
 Verifica ZZ: $0.02+0.10+0.00=0.13$

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $X_l=0.10$ - Classe 3

Sollecitazioni: $N=-547.56$ $T_z=122.42$ $M_y=-129.30$ $T_y=13.63$ $M_z=-1.04$ $M_x=-16.24$
 Tensioni: $\sigma_N=-39.79$ $\sigma_M=-307.68$ $\tau=31.24$ $\sigma_{max}=-347.48$
 Tensioni: $\sigma_N=-39.79$ $\sigma_M=3.19$ $\tau=47.11$ $\tau_{max}=47.11$
 Tensioni: $\sigma_N=-39.79$ $\sigma_M=-307.19$ $\tau=33.94$ $\sigma_{TD,max}=351.93$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 68 SLU $X_l=0.00$

Sollecitazioni: $N=-50.38$ $T_z=176.20$ $M_y=-125.14$ $T_y=1.04$ $M_x=-23.20$
 $V, Ed=1.04$ $V_c, Rd, Red=5722.11$ $V, Ed/V_c, Rd, Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]

$V, Ed=176.20$ $V_c, Rd, Red=11444.20$ $V, Ed/V_c, Rd, Red=0.02$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.16$ - Classe 3

Sollecitazioni: $N=-652.99$ $T_z=114.45$ $M_y=-130.86$ $T_y=16.42$ $M_z=1.15$ $M_x=-20.06$
 Tensioni: $\sigma_N=-47.46$ $\sigma_M=-311.72$ $\tau=38.59$ $\sigma_{max}=-359.17$
 Tensioni: $\sigma_N=-47.46$ $\sigma_M=-3.51$ $\tau=53.43$ $\tau_{max}=53.43$
 Tensioni: $\sigma_N=-47.46$ $\sigma_M=-311.18$ $\tau=41.85$ $\sigma_{TD,max}=365.88$

Asta n. 3580 (-4612 -4627) Tubo 60x120x4 mm - S235 Crit. 2

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3

Sollecitazioni: $N, Ed=-511.49$ $M_y, Ed=-219.93$ $M_z, Ed=-2.61$
 Resistenze: $N_c, Rd=30796.20$ $M_y, c, Rd=951.93$ $M_z, c, Rd=632.38$ $L=15.67$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=3.64$ $N_{cr,y}=21535600.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.31$ $N_{cr,z}=7153210.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.02+0.22+0.00=0.24$
 Verifica ZZ: $0.02+0.18+0.00=0.20$

- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X_l=0.00$ - Classe 3

Sollecitazioni: $N=-73.82$ $T_z=-90.79$ $M_y=-226.78$ $T_y=14.69$ $M_z=-1.49$ $M_x=32.10$
 Tensioni: $\sigma_N=-5.36$ $\sigma_M=-538.43$ $\tau=61.78$ $\sigma_{max}=-543.80$
 Tensioni: $\sigma_N=-5.36$ $\sigma_M=4.56$ $\tau=73.55$ $\tau_{max}=73.55$
 Tensioni: $\sigma_N=-5.36$ $\sigma_M=-538.43$ $\tau=61.78$ $\sigma_{TD,max}=554.23$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 45 SLU $X_l=0.10$

Sollecitazioni: $N=-1180.62$ $T_z=-51.93$ $M_y=-118.24$ $T_y=-63.74$ $M_x=20.55$
 $V, Ed=-63.74$ $V_c, Rd, Red=5745.55$ $V, Ed/V_c, Rd, Red=0.01$

- Verifica a taglio e torsione dir. Z [4.2.25]

$V, Ed=-51.93$ $V_c, Rd, Red=11491.10$ $V, Ed/V_c, Rd, Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.00$ - Classe 3

Sollecitazioni: $N=516.46$ $T_z=-146.72$ $M_y=-219.93$ $T_y=27.26$ $M_z=-2.61$ $M_x=35.89$
 Tensioni: $\sigma_N=37.53$ $\sigma_M=526.33$ $\tau=69.06$ $\sigma_{max}=563.86$
 Tensioni: $\sigma_N=37.53$ $\sigma_M=8.01$ $\tau=88.08$ $\tau_{max}=88.08$
 Tensioni: $\sigma_N=37.53$ $\sigma_M=525.10$ $\tau=74.47$ $\sigma_{TD,max}=577.22$

Asta n. 3580 (-4627 -4642) Tubo 60x120x4 mm - S235 Crit. 2

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3

Sollecitazioni: $N, Ed=-558.53$ $M_y, Ed=-186.84$ $M_z, Ed=1.81$
 Resistenze: $N_c, Rd=30796.20$ $M_y, c, Rd=951.93$ $M_z, c, Rd=632.38$ $L=15.67$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=3.64$ $N_{cr,y}=21535400.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.31$ $N_{cr,z}=7153130.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$

Verifica YY: $0.02+0.19+0.00=0.21$
 Verifica ZZ: $0.02+0.15+0.00=0.17$

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $X1=0.00$ - Classe 3
 Sollecitazioni: $N=-623.26$ $T_z=-91.21$ $M_y=-155.27$ $T_y=3.84$ $M_z=-1.18$ $M_x=22.47$
 Tensioni: $\sigma_N=-45.29$ $\sigma_M=-369.23$ $\tau=43.23$ $\sigma_{max}=-414.52$
 Tensioni: $\sigma_N=-45.29$ $\sigma_M=3.61$ $\tau=55.06$ $\tau_{max}=55.06$
 Tensioni: $\sigma_N=-45.29$ $\sigma_M=-369.23$ $\tau=43.23$ $\sigma_{ID,max}=421.23$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X1=0.16$
 Sollecitazioni: $N=-101.94$ $T_z=-135.55$ $M_y=-184.41$ $T_y=2.52$ $M_x=28.18$
 $V,Ed=2.52$ $Vc,Rd,Red=5678.16$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-135.55$ $Vc,Rd,Red=11356.30$ $V,Ed/Vc,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=-558.53$ $T_z=-159.54$ $M_y=-186.84$ $T_y=5.42$ $M_z=1.02$ $M_x=34.21$
 Tensioni: $\sigma_N=-40.59$ $\sigma_M=-442.90$ $\tau=65.82$ $\sigma_{max}=-483.49$
 Tensioni: $\sigma_N=-40.59$ $\sigma_M=-3.13$ $\tau=86.50$ $\tau_{max}=86.50$
 Tensioni: $\sigma_N=-40.59$ $\sigma_M=-442.90$ $\tau=65.82$ $\sigma_{ID,max}=496.75$

Asta n. 3580 (-4642 -4659) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N,Ed=-556.80$ $M_y,Ed=-150.61$ $M_z,Ed=1.27$
 Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=15.67$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=3.64$ $Ncr,y=21535600.00$ $\lambda^*_y=0.04$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.31$ $Ncr,z=7153210.00$ $\lambda^*_z=0.07$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.02+0.15+0.00=0.17$
 Verifica ZZ: $0.02+0.12+0.00=0.14$

- Verifica in termini tensionali [4.2.4] - CC 49 SLU $X1=0.06$ - Classe 3
 Sollecitazioni: $N=-564.34$ $T_z=-135.58$ $M_y=-124.98$ $T_y=-14.23$ $M_z=-1.03$ $M_x=17.74$
 Tensioni: $\sigma_N=-41.01$ $\sigma_M=-297.50$ $\tau=34.13$ $\sigma_{max}=-338.51$
 Tensioni: $\sigma_N=-41.01$ $\sigma_M=3.17$ $\tau=51.71$ $\tau_{max}=51.71$
 Tensioni: $\sigma_N=-41.01$ $\sigma_M=-297.01$ $\tau=36.95$ $\sigma_{ID,max}=344.03$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X1=0.16$
 Sollecitazioni: $N=-119.86$ $T_z=-178.37$ $M_y=-147.17$ $T_y=-3.02$ $M_x=22.99$
 $V,Ed=-3.02$ $Vc,Rd,Red=5723.96$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-178.37$ $Vc,Rd,Red=11447.90$ $V,Ed/Vc,Rd,Red=0.02$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=-556.80$ $T_z=-180.97$ $M_y=-150.61$ $T_y=-14.53$ $M_z=1.27$ $M_x=31.92$
 Tensioni: $\sigma_N=-40.47$ $\sigma_M=-358.60$ $\tau=61.43$ $\sigma_{max}=-399.06$
 Tensioni: $\sigma_N=-40.47$ $\sigma_M=-3.90$ $\tau=84.88$ $\tau_{max}=84.88$
 Tensioni: $\sigma_N=-40.47$ $\sigma_M=-358.00$ $\tau=64.31$ $\sigma_{ID,max}=413.74$

Asta n. 3595 (-2478 -2546) Tubo 60x80x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
 Sollecitazioni: $N,Ed=-42.63$ $M_y,Ed=-54.66$ $M_z,Ed=66.19$
 Resistenze: $Nc,Rd=43952.40$ $M_y,c,Rd=955.82$ $M_z,c,Rd=801.10$ $L=17.52$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=5.94$ $Ncr,y=7634880.00$ $\lambda^*_y=0.08$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=7.49$ $Ncr,z=4799230.00$ $\lambda^*_z=0.10$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.05+0.08=0.13$
 Verifica ZZ: $0.00+0.04+0.08=0.12$

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.00$ (L/3584)

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3450)

- Verifica in termini tensionali [4.2.4] - CC 89 SLU $X1=0.18$ - Classe 3
 Sollecitazioni: $N=655.19$ $T_z=702.40$ $M_y=-126.60$ $T_y=176.59$ $M_z=13.83$ $M_x=119.40$
 Tensioni: $\sigma_N=50.40$ $\sigma_M=506.18$ $\tau=289.46$ $\sigma_{max}=556.58$
 Tensioni: $\sigma_N=50.40$ $\sigma_M=48.64$ $\tau=397.40$ $\tau_{max}=397.40$

Tensioni: $\sigma_N=50.40$ $\sigma_M=450.21$ $\tau=359.34$ $\sigma_{ID,max}=798.74$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 68 SLU $X_1=0.03$
 Sollecitazioni: $N=613.65$ $T_z=773.54$ $T_y=201.00$ $M_z=-19.84$ $M_x=127.24$
 $V,Ed=201.00$ $V_c,Rd,Red=9157.17$ $V,Ed/V_c,Rd,Red=0.02$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=773.54$ $V_c,Rd,Red=12209.60$ $V,Ed/V_c,Rd,Red=0.06$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=444.65$ $T_z=478.70$ $M_y=103.38$ $T_y=235.67$ $M_z=81.05$ $M_x=84.55$

Tensioni: $\sigma_N=34.20$ $\sigma_M=707.73$ $\tau=204.96$ $\sigma_{max}=741.93$

Tensioni: $\sigma_N=34.20$ $\sigma_M=285.06$ $\tau=278.55$ $\tau_{max}=278.55$

Tensioni: $\sigma_N=34.20$ $\sigma_M=707.73$ $\tau=204.96$ $\sigma_{ID,max}=822.49$

Asta n. 3595 (-2546 -2592) Tubo 60x100x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3

Sollecitazioni: $N,Ed=-40.90$ $M_y,Ed=-77.22$ $M_z,Ed=48.13$

Resistenze: $N_c,Rd=50714.30$ $M_y,c,Rd=1327.02$ $M_z,c,Rd=972.02$ $L=9.18$

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=2.54$ $N_{cr,y}=48314900.00$ $\lambda^*_y=0.03$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$

$\lambda_z=3.83$ $N_{cr,z}=21233900.00$ $\lambda^*_z=0.05$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$

$K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$

Verifica YY: $0.00+0.06+0.05=0.10$

Verifica ZZ: $0.00+0.04+0.05=0.09$

- Verifica Freccia massima per soli carichi accidentali - CC 46

$f_{z,g}=0.00$ (L/3563)

- Verifica Freccia massima carichi totali - CC 46

$f_{z,g}=0.00$ (L/3375)

- Verifica in termini tensionali [4.2.4] - CC 89 SLU $X_1=0.09$ - Classe 3

Sollecitazioni: $N=656.52$ $T_z=701.67$ $M_y=-191.02$ $T_y=176.63$ $M_z=30.05$ $M_x=119.39$

Tensioni: $\sigma_N=43.77$ $\sigma_M=591.17$ $\tau=228.50$ $\sigma_{max}=634.94$

Tensioni: $\sigma_N=43.77$ $\sigma_M=87.09$ $\tau=315.67$ $\tau_{max}=315.67$

Tensioni: $\sigma_N=43.77$ $\sigma_M=573.76$ $\tau=256.67$ $\sigma_{ID,max}=760.90$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 45 SLU $X_1=0.01$

Sollecitazioni: $N=1047.96$ $T_z=691.05$ $M_y=-104.56$ $T_y=330.05$ $M_x=104.19$

$V,Ed=330.05$ $V_c,Rd,Red=9858.65$ $V,Ed/V_c,Rd,Red=0.03$

- Verifica a taglio e torsione dir. Z [4.2.25]

$V,Ed=691.05$ $V_c,Rd,Red=16431.10$ $V,Ed/V_c,Rd,Red=0.04$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3

Sollecitazioni: $N=445.89$ $T_z=478.36$ $M_y=-74.50$ $T_y=235.79$ $M_z=50.90$ $M_x=84.55$

Tensioni: $\sigma_N=29.73$ $\sigma_M=366.86$ $\tau=161.81$ $\sigma_{max}=396.58$

Tensioni: $\sigma_N=29.73$ $\sigma_M=147.54$ $\tau=221.26$ $\tau_{max}=221.26$

Tensioni: $\sigma_N=29.73$ $\sigma_M=347.88$ $\tau=196.55$ $\sigma_{ID,max}=508.41$

Asta n. 3595 (-2592 -3079) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3

Sollecitazioni: $N,Ed=-2507.85$ $M_y,Ed=-155.18$ $M_z,Ed=75.13$

Resistenze: $N_c,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=4.80$ $N_{cr,y}=17091500.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$

$\lambda_z=6.62$ $N_{cr,z}=8991340.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$

$K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$

Verifica YY: $0.04+0.06+0.04=0.14$

Verifica ZZ: $0.04+0.05+0.04=0.13$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X_1=0.00$ - Classe 3

Sollecitazioni: $N=-2507.85$ $T_z=-532.79$ $M_y=-155.18$ $T_y=174.60$ $M_z=37.87$ $M_x=103.06$

Tensioni: $\sigma_N=-131.99$ $\sigma_M=-324.57$ $\tau=119.48$ $\sigma_{max}=-456.56$

Tensioni: $\sigma_N=-131.99$ $\sigma_M=-67.08$ $\tau=173.58$ $\tau_{max}=173.58$

Tensioni: $\sigma_N=-131.99$ $\sigma_M=-303.91$ $\tau=152.11$ $\sigma_{ID,max}=509.34$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3

Sollecitazioni: $N=451.01$ $T_z=-228.37$ $M_y=-70.44$ $T_y=207.83$ $M_z=34.37$ $M_x=79.45$

Tensioni: $\sigma_N=23.74$ $\sigma_M=182.12$ $\tau=92.12$ $\sigma_{max}=205.85$

Tensioni: $\sigma_N=23.74$ $\sigma_M=103.15$ $\tau=122.24$ $\tau_{max}=122.24$

Tensioni: $\sigma_N=23.74$ $\sigma_M=173.42$ $\tau=115.79$ $\sigma_{ID,max}=281.23$

Asta n. 3595 (-3079 -4692) Tubo 80x120x5 mm - S355 Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N, Ed = -4322.93$ $M_y, Ed = -46.87$ $M_z, Ed = 121.96$
 Resistenze: $N_c, Rd = 64238.10$ $M_y, c, Rd = 2116.38$ $M_z, c, Rd = 1670.05$ $L = 21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 4.80$ $N_{cr, y} = 17091400.00$ $\lambda^*_y = 0.06$ Curva a: $\Phi_y = 0.00$ $\chi_y = 1.00$
 $\lambda_z = 6.62$ $N_{cr, z} = 8991300.00$ $\lambda^*_z = 0.09$ Curva a: $\Phi_z = 0.00$ $\chi_z = 1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.07 + 0.02 + 0.07 = 0.15$
 Verifica ZZ: $0.07 + 0.01 + 0.07 = 0.15$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X1 = 0.00$ - Classe 3
 Sollecitazioni: $N = -4322.93$ $T_z = -220.43$ $M_y = -46.87$ $T_y = 139.23$ $M_z = 92.25$ $M_x = 97.35$
 Tensioni: $\sigma_N = -227.52$ $\sigma_M = -261.63$ $\tau = 112.87$ $\sigma_{max} = -489.15$
 Tensioni: $\sigma_N = -227.52$ $\sigma_M = -163.41$ $\tau = 135.25$ $\tau_{max} = 135.25$
 Tensioni: $\sigma_N = -227.52$ $\sigma_M = -255.39$ $\tau = 126.37$ $\sigma_{ID, max} = 530.20$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 67 SLU $X1 = 0.17$
 Sollecitazioni: $N = -167.66$ $T_z = -406.53$ $T_y = 27.01$ $M_z = 53.14$ $M_x = 94.02$
 $V, Ed = 27.01$ $V_c, Rd, Red = 14007.10$ $V, Ed/V_c, Rd, Red = 0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed = -406.53$ $V_c, Rd, Red = 21010.70$ $V, Ed/V_c, Rd, Red = 0.02$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1 = 0.21$ - Classe 3
 Sollecitazioni: $N = -441.68$ $T_z = -297.49$ $M_y = 29.25$ $T_y = -116.92$ $M_z = 67.27$ $M_x = 80.06$
 Tensioni: $\sigma_N = -23.25$ $\sigma_M = -182.92$ $\tau = 92.82$ $\sigma_{max} = -206.16$
 Tensioni: $\sigma_N = -23.25$ $\sigma_M = -119.16$ $\tau = 123.02$ $\tau_{max} = 123.02$
 Tensioni: $\sigma_N = -23.25$ $\sigma_M = -179.02$ $\tau = 111.04$ $\sigma_{ID, max} = 279.11$

Asta n. 3596 (-2477 -2545) Tubo 60x80x5 mm - S355 Crit. 3

 - Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z, g} = 0.01$ (L/3556)

- Verifica Freccia massima carichi totali - CC 46
 $f_{z, g} = 0.01$ (L/3444)

- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X1 = 0.18$ - Classe 3
 Sollecitazioni: $N = 880.92$ $T_z = 805.26$ $M_y = -76.11$ $T_y = -89.49$ $M_z = -40.40$ $M_x = -132.84$
 Tensioni: $\sigma_N = 67.76$ $\sigma_M = 439.72$ $\tau = 322.03$ $\sigma_{max} = 507.49$
 Tensioni: $\sigma_N = 67.76$ $\sigma_M = 142.09$ $\tau = 445.76$ $\tau_{max} = 445.76$
 Tensioni: $\sigma_N = 67.76$ $\sigma_M = 406.07$ $\tau = 402.15$ $\sigma_{ID, max} = 842.43$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 45 SLU $X1 = 0.16$
 Sollecitazioni: $N = 1128.56$ $T_z = 729.58$ $M_y = -88.19$ $T_y = -297.49$ $M_x = -102.27$
 $V, Ed = -297.49$ $V_c, Rd, Red = 9494.47$ $V, Ed/V_c, Rd, Red = 0.03$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed = 729.58$ $V_c, Rd, Red = 12659.30$ $V, Ed/V_c, Rd, Red = 0.06$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1 = 0.00$ - Classe 3
 Sollecitazioni: $N = 400.27$ $T_z = 964.94$ $M_y = 121.59$ $T_y = -108.13$ $M_z = -37.41$ $M_x = -141.05$
 Tensioni: $\sigma_N = 30.79$ $\sigma_M = 587.99$ $\tau = 341.93$ $\sigma_{max} = 618.78$
 Tensioni: $\sigma_N = 30.79$ $\sigma_M = 131.58$ $\tau = 490.20$ $\tau_{max} = 490.20$
 Tensioni: $\sigma_N = 30.79$ $\sigma_M = 534.23$ $\tau = 437.93$ $\sigma_{ID, max} = 945.83$

Asta n. 3596 (-2545 -2591) Tubo 60x100x5 mm - S355 Crit. 3

 - Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z, g} = 0.00$ (L/3596)

- Verifica Freccia massima carichi totali - CC 46
 $f_{z, g} = 0.00$ (L/3563)

- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X1 = 0.09$ - Classe 3
 Sollecitazioni: $N = 882.21$ $T_z = 804.55$ $M_y = -150.00$ $T_y = -89.76$ $M_z = -48.64$ $M_x = -132.81$
 Tensioni: $\sigma_N = 58.81$ $\sigma_M = 551.36$ $\tau = 254.19$ $\sigma_{max} = 610.18$
 Tensioni: $\sigma_N = 58.81$ $\sigma_M = 141.00$ $\tau = 354.12$ $\tau_{max} = 354.12$
 Tensioni: $\sigma_N = 58.81$ $\sigma_M = 513.15$ $\tau = 312.61$ $\sigma_{ID, max} = 787.60$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 68 SLU $X1 = 0.08$
 Sollecitazioni: $N = 550.30$ $T_z = 289.12$ $T_y = 50.26$ $M_z = -34.23$ $M_x = -53.90$
 $V, Ed = 50.26$ $V_c, Rd, Red = 10400.00$ $V, Ed/V_c, Rd, Red = 0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]

V,Ed=289.12 Vc,Rd,Red=17333.30 V,Ed/Vc,Rd,Red=0.02

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.09 - Classe 3

Sollecitazioni: N=402.91 Tz=962.98 My=-149.66 Ty=-108.28 Mz=-30.73 Mx=-141.03

Tensioni: $\sigma_N=26.86$ $\sigma_M=488.16$ $\tau=269.91$ $\sigma_{max}=515.02$

Tensioni: $\sigma_N=26.86$ $\sigma_M=89.06$ $\tau=389.52$ $\tau_{max}=389.52$

Tensioni: $\sigma_N=26.86$ $\sigma_M=450.04$ $\tau=339.84$ $\sigma_{ID,max}=757.56$

Asta n. 3596 (-2591 -3078) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3

Sollecitazioni: N,Ed=-2362.89 My,Ed=-170.55 Mz,Ed=-74.65

Resistenze: Nc,Rd=64238.10 My,c,Rd=2116.38 Mz,c,Rd=1670.05 L=21.34

α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95

$\lambda_y=4.80$ Ncr,y=17091500.00 $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$

$\lambda_z=6.62$ Ncr,z=8991320.00 $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.04+0.06+0.04=0.14

Verifica ZZ: 0.04+0.05+0.04=0.13

- Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.00 - Classe 3

Sollecitazioni: N=-2362.89 Tz=-442.91 My=-170.55 Ty=-146.41 Mz=-43.40 Mx=-100.68

Tensioni: $\sigma_N=-124.36$ $\sigma_M=-360.33$ $\tau=116.73$ $\sigma_{max}=-484.69$

Tensioni: $\sigma_N=-124.36$ $\sigma_M=-76.89$ $\tau=161.69$ $\tau_{max}=161.69$

Tensioni: $\sigma_N=-124.36$ $\sigma_M=-360.33$ $\tau=116.73$ $\sigma_{ID,max}=525.17$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU Xl=0.17

Sollecitazioni: N=418.93 Tz=55.44 Ty=63.12 Mz=-22.44 Mx=-37.87

V,Ed=63.12 Vc,Rd,Red=14501.90 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]

V,Ed=55.44 Vc,Rd,Red=21752.80 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3

Sollecitazioni: N=390.45 Tz=-144.80 My=-135.41 Ty=39.77 Mz=-32.18 Mx=-134.99

Tensioni: $\sigma_N=20.55$ $\sigma_M=281.46$ $\tau=156.51$ $\sigma_{max}=302.01$

Tensioni: $\sigma_N=20.55$ $\sigma_M=-57.01$ $\tau=171.21$ $\tau_{max}=171.21$

Tensioni: $\sigma_N=20.55$ $\sigma_M=281.46$ $\tau=156.51$ $\sigma_{ID,max}=405.83$

Asta n. 3596 (-3078 -3569) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3

Sollecitazioni: N,Ed=-3910.43 My,Ed=-72.54 Mz,Ed=-99.64

Resistenze: Nc,Rd=64238.10 My,c,Rd=2116.38 Mz,c,Rd=1670.05 L=10.67

α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95

$\lambda_y=2.40$ Ncr,y=68365500.00 $\lambda^*_y=0.03$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$

$\lambda_z=3.31$ Ncr,z=35965100.00 $\lambda^*_z=0.04$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.06+0.03+0.06=0.14

Verifica ZZ: 0.06+0.02+0.06=0.14

- Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.00 - Classe 3

Sollecitazioni: N=-3910.43 Tz=-812.86 My=-72.54 Ty=-157.45 Mz=-82.84 Mx=-96.36

Tensioni: $\sigma_N=-205.81$ $\sigma_M=-283.58$ $\tau=111.72$ $\sigma_{max}=-489.39$

Tensioni: $\sigma_N=-205.81$ $\sigma_M=-146.74$ $\tau=194.24$ $\tau_{max}=194.24$

Tensioni: $\sigma_N=-205.81$ $\sigma_M=-273.92$ $\tau=161.50$ $\sigma_{ID,max}=555.33$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU Xl=0.00

Sollecitazioni: N=183.87 Tz=-16.41 Ty=59.46 Mz=-15.59 Mx=-36.66

V,Ed=59.46 Vc,Rd,Red=14512.60 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]

V,Ed=-16.41 Vc,Rd,Red=21768.80 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3

Sollecitazioni: N=-1329.11 Tz=-484.77 My=-99.07 Ty=89.31 Mz=-29.38 Mx=-138.08

Tensioni: $\sigma_N=-69.95$ $\sigma_M=-217.75$ $\tau=160.09$ $\sigma_{max}=-287.70$

Tensioni: $\sigma_N=-69.95$ $\sigma_M=-52.05$ $\tau=209.30$ $\tau_{max}=209.30$

Tensioni: $\sigma_N=-69.95$ $\sigma_M=-204.56$ $\tau=189.78$ $\sigma_{ID,max}=428.25$

Asta n. 3596 (-3569 -4688) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3

Sollecitazioni: $N, E_d = -4147.48$ $M_y, E_d = 15.86$ $M_z, E_d = -121.17$
 Resistenze: $N_c, R_d = 64238.10$ $M_y, c, R_d = 2116.38$ $M_z, c, R_d = 1670.05$ $L = 10.67$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 2.40$ $N_{cr, y} = 68365500.00$ $\lambda^*_y = 0.03$ Curva a: $\Phi_y = 0.00$ $\chi_y = 1.00$
 $\lambda_z = 3.31$ $N_{cr, z} = 35965100.00$ $\lambda^*_z = 0.04$ Curva a: $\Phi_z = 0.00$ $\chi_z = 1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.06 + 0.01 + 0.07 = 0.14$
 Verifica ZZ: $0.06 + 0.00 + 0.07 = 0.14$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X_l = 0.10$ - Classe 3
 Sollecitazioni: $N = -4145.65$ $T_z = 70.16$ $M_y = 8.57$ $T_y = -150.45$ $M_z = -121.17$ $M_x = -99.17$
 Tensioni: $\sigma_N = -218.19$ $\sigma_M = -259.01$ $\tau = 114.98$ $\sigma_{max} = -477.20$
 Tensioni: $\sigma_N = -218.19$ $\sigma_M = -12.55$ $\tau = 136.78$ $\tau_{max} = 136.78$
 Tensioni: $\sigma_N = -218.19$ $\sigma_M = -259.01$ $\tau = 114.98$ $\sigma_{ID, max} = 517.09$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 37 SLU $X_l = 0.07$
 Sollecitazioni: $N = -115.24$ $T_z = -410.99$ $T_y = -21.82$ $M_z = -48.69$ $M_x = -93.89$
 $V, E_d = -21.82$ $V_c, R_d, Red = 14008.30$ $V, E_d / V_c, R_d, Red = 0.00$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V, E_d = -410.99$ $V_c, R_d, Red = 21012.40$ $V, E_d / V_c, R_d, Red = 0.02$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l = 0.10$ - Classe 3
 Sollecitazioni: $N = -2091.17$ $T_z = -743.56$ $M_y = 34.68$ $T_y = 46.67$ $M_z = -28.53$ $M_x = -134.29$
 Tensioni: $\sigma_N = -110.06$ $\sigma_M = -113.17$ $\tau = 155.70$ $\sigma_{max} = -223.23$
 Tensioni: $\sigma_N = -110.06$ $\sigma_M = -50.55$ $\tau = 231.18$ $\tau_{max} = 231.18$
 Tensioni: $\sigma_N = -110.06$ $\sigma_M = -57.77$ $\tau = 231.18$ $\sigma_{ID, max} = 434.17$

Asta n. 3601 (-5043 -4682) Tubo 60x60x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N, E_d = -199.13$ $M_y, E_d = -2.05$
 Resistenze: $N_c, R_d = 20053.30$ $M_y, c, R_d = 351.16$ $L = 153.00$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 66.75$ $N_{cr, y} = 41677.70$ $\lambda^*_y = 0.71$ Curva a: $\Phi_y = 0.81$ $\chi_y = 0.84$
 $\lambda_z = 66.75$ $N_{cr, z} = 41677.70$ $\lambda^*_z = 0.71$ Curva a: $\Phi_z = 0.81$ $\chi_z = 0.84$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.00, 0.95$
 Verifica YY: $0.01 + 0.01 = 0.02$
 Verifica ZZ: $0.01 = 0.01$

- Verifica Freccia massima carichi totali - CC 46
 $f_{z, c} = 0.01$ (L/29141)
- Verifica a pressoflessione retta - CC 41 SLU $X_l = 0.76$ - Classe 1
 Sollecitazioni: $N = 33.77$ $M_y = -2.77$ $M_x = -1.10$
 $M_y, E_d = -2.77$ $M_y, c, R_d = 421.84$
 $N, E_d = 33.77$ $N_c, R_d = 20053.30$ $n = N, E_d / N_c, R_d = 0.00$
 $MN_y, c, R_d = 421.84$ $M_y, E_d / MN_y, c, R_d = 0.01$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 54 SLU $X_l = 1.53$
 Sollecitazioni: $N = 69.58$ $T_z = -7.26$ $M_x = -4.38$
 $V, E_d = -7.26$ $V_c, R_d, Red = 5710.93$ $V, E_d / V_c, R_d, Red = 0.00$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l = 0.76$ - Classe 3
 Sollecitazioni: $N = 255.84$ $M_y = -2.05$ $M_x = -9.37$
 Tensioni: $\sigma_N = 28.55$ $\sigma_M = 13.09$ $\tau = 37.35$ $\sigma_{max} = 41.64$
 Tensioni: $\sigma_N = 28.55$ $\sigma_M = 13.09$ $\tau = 37.35$ $\tau_{max} = 37.35$
 Tensioni: $\sigma_N = 28.55$ $\sigma_M = 13.09$ $\tau = 37.35$ $\sigma_{ID, max} = 76.94$

Asta n. 3602 (-5045 -4698) Tubo 60x60x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 1
 Sollecitazioni: $N, E_d = -67.69$ $M_y, E_d = -2.77$
 Resistenze: $N_c, R_d = 20053.30$ $M_y, c, R_d = 421.84$ $L = 153.00$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 66.75$ $N_{cr, y} = 41677.70$ $\lambda^*_y = 0.71$ Curva a: $\Phi_y = 0.81$ $\chi_y = 0.84$
 $\lambda_z = 66.75$ $N_{cr, z} = 41677.70$ $\lambda^*_z = 0.71$ Curva a: $\Phi_z = 0.81$ $\chi_z = 0.84$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00 + 0.01 = 0.01$
 Verifica ZZ: $0.00 = 0.00$
- Verifica Freccia massima carichi totali - CC 46
 $f_{z, c} = 0.01$ (L/28878)
- Verifica a pressoflessione retta - CC 41 SLU $X_l = 0.76$ - Classe 1
 Sollecitazioni: $N = 96.42$ $M_y = -2.77$ $M_x = 2.42$

My,Ed=-2.77 My,c,Rd=421.84
 N,Ed=96.42 Nc,Rd=20053.30 n=N,Ed/Nc,Rd=0.00
 MNy,c,Rd=421.84 My,Ed/MNy,c,Rd=0.01

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 89 SLU Xl=1.53
 Sollecitazioni: N=116.90 Tz=-7.26 Mx=2.94
 V,Ed=-7.26 Vc,Rd,Red=5736.63 V,Ed/Vc,Rd,Red=0.00
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.76 - Classe 3
 Sollecitazioni: N=138.35 My=-2.05 Mx=2.00
 Tensioni: $\sigma_N=15.44$ $\sigma_M=13.09$ $\tau=7.97$ $\sigma_{max}=28.53$
 Tensioni: $\sigma_N=15.44$ $\sigma_M=13.09$ $\tau=7.97$ $\tau_{max}=7.97$
 Tensioni: $\sigma_N=15.44$ $\sigma_M=13.09$ $\tau=7.97$ $\sigma_{ID,max}=31.69$

Asta n. 3622 (-5043 -5430) Tubo 60x60x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 1
 Sollecitazioni: N,Ed=-772.42 My,Ed=-2.77
 Resistenze: Nc,Rd=20053.30 My,c,Rd=421.84 L=153.00
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=66.75$ Ncr,y=41677.10 $\lambda^*_y=0.71$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=66.75$ Ncr,z=41677.10 $\lambda^*_z=0.71$ Curva a: $\Phi_z=0.81$ $\chi_z=0.84$
 Kyy, Kyz, Kzy, Kzz=0.97, 0.58, 0.00, 0.97
 Verifica YY: 0.04+0.01=0.04
 Verifica ZZ: 0.04=0.04
- Verifica Freccia massima carichi totali - CC 70
 $f_{z,L}=0.01$ (L/29682)
- Verifica a compressione [4.2.9] - CC 45 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=-772.42 Tz=7.26 Mx=1.48
 N,Ed=-772.42 Nc,Rd=-20053.30 N,Ed/Nc,Rd=0.04
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 54 SLU Xl=0.00
 Sollecitazioni: N=-130.93 Tz=7.26 Mx=6.10
 V,Ed=7.26 Vc,Rd,Red=5680.16 V,Ed/Vc,Rd,Red=0.00
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.77 - Classe 3
 Sollecitazioni: N=-345.17 My=-2.05 Mx=11.00
 Tensioni: $\sigma_N=-38.52$ $\sigma_M=-13.09$ $\tau=43.84$ $\sigma_{max}=-51.62$
 Tensioni: $\sigma_N=-38.52$ $\sigma_M=13.09$ $\tau=43.84$ $\tau_{max}=43.84$
 Tensioni: $\sigma_N=-38.52$ $\sigma_M=-13.09$ $\tau=43.84$ $\sigma_{ID,max}=91.82$

Asta n. 3623 (-5045 -5446) Tubo 60x60x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 1
 Sollecitazioni: N,Ed=-757.53 My,Ed=-2.77
 Resistenze: Nc,Rd=20053.30 My,c,Rd=421.84 L=153.00
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=66.75$ Ncr,y=41677.10 $\lambda^*_y=0.71$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=66.75$ Ncr,z=41677.10 $\lambda^*_z=0.71$ Curva a: $\Phi_z=0.81$ $\chi_z=0.84$
 Kyy, Kyz, Kzy, Kzz=0.97, 0.58, 0.00, 0.97
 Verifica YY: 0.04+0.01=0.04
 Verifica ZZ: 0.04=0.04
- Verifica Freccia massima carichi totali - CC 34
 $f_{z,L}=0.00$ (L/30824)
- Verifica a compressione [4.2.9] - CC 45 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=-757.53 Tz=7.26 Mx=-1.02
 N,Ed=-757.53 Nc,Rd=-20053.30 N,Ed/Nc,Rd=0.04
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 89 SLU Xl=0.00
 Sollecitazioni: N=-80.44 Tz=7.26 Mx=-4.70
 V,Ed=7.26 Vc,Rd,Red=5705.10 V,Ed/Vc,Rd,Red=0.00
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.77 - Classe 3
 Sollecitazioni: N=-323.48 My=-2.05 Mx=-3.26
 Tensioni: $\sigma_N=-36.10$ $\sigma_M=-13.09$ $\tau=12.99$ $\sigma_{max}=-49.19$
 Tensioni: $\sigma_N=-36.10$ $\sigma_M=13.09$ $\tau=12.99$ $\tau_{max}=12.99$
 Tensioni: $\sigma_N=-36.10$ $\sigma_M=-13.09$ $\tau=12.99$ $\sigma_{ID,max}=54.09$

Asta n. 3642 (-2442 -2495) Tubo 60x80x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,G}=0.01$ (L/3387)

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3080) $f_{z,L}=0.00$ (L/14885)
- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X1=0.00$ - Classe 3
 Sollecitazioni: $N=2881.02$ $T_z=1109.59$ $M_y=231.12$ $T_y=507.80$ $M_z=-206.82$ $M_x=118.71$
 Tensioni: $\sigma_N=221.62$ $\sigma_M=1690.41$ $\tau=287.77$ $\sigma_{max}=1912.02$
 Tensioni: $\sigma_N=221.62$ $\sigma_M=-727.40$ $\tau=458.36$ $\tau_{max}=458.36$
 Tensioni: $\sigma_N=221.62$ $\sigma_M=1690.41$ $\tau=287.77$ $\sigma_{ID,max}=1975.92$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 53 SLU $X1=0.22$
 Sollecitazioni: $N=2232.02$ $T_z=914.21$ $T_y=412.63$ $M_z=-75.60$ $M_x=108.86$
 $V,Ed=412.63$ $V_c,Rd,Red=9405.45$ $V,Ed/V_c,Rd,Red=0.04$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=914.21$ $V_c,Rd,Red=12540.60$ $V,Ed/V_c,Rd,Red=0.07$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=1226.73$ $T_z=685.78$ $M_y=197.28$ $T_y=252.44$ $M_z=-101.55$ $M_x=95.69$
 Tensioni: $\sigma_N=94.36$ $\sigma_M=1126.39$ $\tau=231.97$ $\sigma_{max}=1220.76$
 Tensioni: $\sigma_N=94.36$ $\sigma_M=-357.15$ $\tau=337.38$ $\tau_{max}=337.38$
 Tensioni: $\sigma_N=94.36$ $\sigma_M=1126.39$ $\tau=231.97$ $\sigma_{ID,max}=1285.18$
- Asta n. 3642 (-2495 -2698) Tubo 60x100x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.01$ (L/3429)
- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3162) $f_{z,L}=0.00$ (L/18648)
- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X1=0.21$ - Classe 3
 Sollecitazioni: $N=2887.19$ $T_z=1106.32$ $M_y=-274.68$ $T_y=506.83$ $M_z=24.80$ $M_x=118.72$
 Tensioni: $\sigma_N=192.48$ $\sigma_M=786.09$ $\tau=227.22$ $\sigma_{max}=978.57$
 Tensioni: $\sigma_N=192.48$ $\sigma_M=71.89$ $\tau=364.72$ $\tau_{max}=364.72$
 Tensioni: $\sigma_N=192.48$ $\sigma_M=771.72$ $\tau=308.02$ $\sigma_{ID,max}=1101.95$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 45 SLU $X1=0.17$
 Sollecitazioni: $N=2645.10$ $T_z=830.74$ $M_y=-198.65$ $T_y=303.40$ $M_x=79.45$
 $V,Ed=303.40$ $V_c,Rd,Red=10125.00$ $V,Ed/V_c,Rd,Red=0.03$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=830.74$ $V_c,Rd,Red=16874.90$ $V,Ed/V_c,Rd,Red=0.05$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.21$ - Classe 3
 Sollecitazioni: $N=1231.35$ $T_z=682.57$ $M_y=-119.02$ $T_y=252.29$ $M_z=14.15$ $M_x=95.68$
 Tensioni: $\sigma_N=82.09$ $\sigma_M=352.43$ $\tau=183.12$ $\sigma_{max}=434.52$
 Tensioni: $\sigma_N=82.09$ $\sigma_M=41.00$ $\tau=267.93$ $\tau_{max}=267.93$
 Tensioni: $\sigma_N=82.09$ $\sigma_M=313.91$ $\tau=246.69$ $\sigma_{ID,max}=582.57$
- Asta n. 3642 (-2698 -3322) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-1254.80$ $M_y,Ed=-220.99$ $M_z,Ed=85.64$
 Resistenze: $N_c,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ $N_{cr,y}=17091500.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ $N_{cr,z}=8991340.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.02+0.08+0.05=0.15$
 Verifica ZZ: $0.02+0.07+0.05=0.13$
- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X1=0.21$ - Classe 3
 Sollecitazioni: $N=2569.10$ $T_z=-437.74$ $M_y=-158.45$ $T_y=441.84$ $M_z=138.98$ $M_x=112.65$
 Tensioni: $\sigma_N=135.22$ $\sigma_M=534.48$ $\tau=130.61$ $\sigma_{max}=669.70$
 Tensioni: $\sigma_N=135.22$ $\sigma_M=232.03$ $\tau=194.65$ $\tau_{max}=194.65$
 Tensioni: $\sigma_N=135.22$ $\sigma_M=499.31$ $\tau=180.93$ $\sigma_{ID,max}=707.69$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.21$ - Classe 3
 Sollecitazioni: $N=1133.61$ $T_z=-174.49$ $M_y=-76.63$ $T_y=221.14$ $M_z=71.51$ $M_x=91.17$
 Tensioni: $\sigma_N=59.66$ $\sigma_M=267.19$ $\tau=105.70$ $\sigma_{max}=326.85$
 Tensioni: $\sigma_N=59.66$ $\sigma_M=112.22$ $\tau=137.75$ $\tau_{max}=137.75$
 Tensioni: $\sigma_N=59.66$ $\sigma_M=249.09$ $\tau=130.88$ $\sigma_{ID,max}=383.04$
- Asta n. 3642 (-3322 -5436) Tubo 80x120x5 mm - S355 Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: $N, E_d = -1711.15$ $M_y, E_d = -116.95$ $M_z, E_d = 200.97$
 Resistenze: $N_c, R_d = 64238.10$ $M_y, c, R_d = 2116.38$ $M_z, c, R_d = 1670.05$ $L = 21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 4.80$ $N_{cr,y} = 17091400.00$ $\lambda^*_y = 0.06$ Curva a: $\Phi_y = 0.00$ $\chi_y = 1.00$
 $\lambda_z = 6.62$ $N_{cr,z} = 8991280.00$ $\lambda^*_z = 0.09$ Curva a: $\Phi_z = 0.00$ $\chi_z = 1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.03 + 0.04 + 0.11 = 0.18$
 Verifica ZZ: $0.03 + 0.03 + 0.11 = 0.18$

- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X_1 = 0.21$ - Classe 3
 Sollecitazioni: $N = 971.51$ $T_z = -287.23$ $M_y = -86.65$ $T_y = 303.76$ $M_z = 239.59$ $M_x = 110.78$
 Tensioni: $\sigma_N = 51.13$ $\sigma_M = 623.48$ $\tau = 128.44$ $\sigma_{max} = 674.61$
 Tensioni: $\sigma_N = 51.13$ $\sigma_M = 126.89$ $\tau = 172.46$ $\tau_{max} = 172.46$
 Tensioni: $\sigma_N = 51.13$ $\sigma_M = 623.48$ $\tau = 128.44$ $\sigma_{ID,max} = 710.35$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1 = 0.21$ - Classe 3
 Sollecitazioni: $N = 1885.91$ $T_z = -142.59$ $M_y = -43.54$ $T_y = 139.87$ $M_z = 119.89$ $M_x = 89.22$
 Tensioni: $\sigma_N = 99.26$ $\sigma_M = 312.27$ $\tau = 103.44$ $\sigma_{max} = 411.53$
 Tensioni: $\sigma_N = 99.26$ $\sigma_M = 63.76$ $\tau = 123.71$ $\tau_{max} = 123.71$
 Tensioni: $\sigma_N = 99.26$ $\sigma_M = 312.27$ $\tau = 103.44$ $\sigma_{ID,max} = 448.84$

Asta n. 3643 (-2441 -2496) Tubo 60x80x5 mm - S355 Crit. 3

 - Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g} = 0.01$ (L/3381)

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g} = 0.01$ (L/3096) $f_{z,L} = 0.00$ (L/14081)

- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X_1 = 0.00$ - Classe 3
 Sollecitazioni: $N = 2840.15$ $T_z = 1068.30$ $M_y = 217.28$ $T_y = -451.44$ $M_z = 185.49$ $M_x = -91.33$
 Tensioni: $\sigma_N = 218.47$ $\sigma_M = 1551.43$ $\tau = 221.41$ $\sigma_{max} = 1769.90$
 Tensioni: $\sigma_N = 218.47$ $\sigma_M = -652.37$ $\tau = 385.65$ $\tau_{max} = 385.65$
 Tensioni: $\sigma_N = 218.47$ $\sigma_M = 1551.43$ $\tau = 221.41$ $\sigma_{ID,max} = 1810.97$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 45 SLU $X_1 = 0.18$
 Sollecitazioni: $N = 2645.58$ $T_z = 878.28$ $T_y = -292.76$ $M_z = 70.68$ $M_x = -81.22$
 $V, E_d = -292.76$ $V_c, R_d, Red = 9778.72$ $V, E_d, V_c, R_d, Red = 0.03$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V, E_d = 878.28$ $V_c, R_d, Red = 13038.30$ $V, E_d, V_c, R_d, Red = 0.07$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1 = 0.00$ - Classe 3
 Sollecitazioni: $N = 1359.62$ $T_z = 563.78$ $M_y = 179.98$ $T_y = -257.36$ $M_z = 100.17$ $M_x = -65.58$
 Tensioni: $\sigma_N = 104.59$ $\sigma_M = 1059.41$ $\tau = 158.97$ $\sigma_{max} = 1163.99$
 Tensioni: $\sigma_N = 104.59$ $\sigma_M = -352.31$ $\tau = 245.65$ $\tau_{max} = 245.65$
 Tensioni: $\sigma_N = 104.59$ $\sigma_M = 1059.41$ $\tau = 158.97$ $\sigma_{ID,max} = 1196.12$

Asta n. 3643 (-2496 -2699) Tubo 60x100x5 mm - S355 Crit. 3

 - Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g} = 0.01$ (L/3416)

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g} = 0.01$ (L/3140) $f_{z,L} = 0.00$ (L/16889)

- Verifica in termini tensionali [4.2.4] - CC 89 SLU $X_1 = 0.21$ - Classe 3
 Sollecitazioni: $N = 2183.57$ $T_z = 1056.05$ $M_y = -298.52$ $T_y = -417.66$ $M_z = -21.27$ $M_x = -121.80$
 Tensioni: $\sigma_N = 145.57$ $\sigma_M = 834.55$ $\tau = 233.11$ $\sigma_{max} = 980.12$
 Tensioni: $\sigma_N = 145.57$ $\sigma_M = 61.64$ $\tau = 364.34$ $\tau_{max} = 364.34$
 Tensioni: $\sigma_N = 145.57$ $\sigma_M = 822.22$ $\tau = 299.70$ $\sigma_{ID,max} = 1098.21$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 45 SLU $X_1 = 0.17$
 Sollecitazioni: $N = 2649.02$ $T_z = 876.49$ $M_y = -212.19$ $T_y = -291.39$ $M_z = -81.25$
 $V, E_d = -291.39$ $V_c, R_d, Red = 10105.60$ $V, E_d, V_c, R_d, Red = 0.03$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V, E_d = 876.49$ $V_c, R_d, Red = 16842.60$ $V, E_d, V_c, R_d, Red = 0.05$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_1 = 0.21$ - Classe 3
 Sollecitazioni: $N = 1484.37$ $T_z = 582.71$ $M_y = -147.02$ $T_y = -275.07$ $M_z = -15.09$ $M_x = -69.84$
 Tensioni: $\sigma_N = 98.96$ $\sigma_M = 427.07$ $\tau = 133.67$ $\sigma_{max} = 526.03$
 Tensioni: $\sigma_N = 98.96$ $\sigma_M = 43.74$ $\tau = 206.09$ $\tau_{max} = 206.09$

Tensioni: $\sigma_N=98.96$ $\sigma_M=418.32$ $\tau=177.52$ $\sigma_{ID,max}=601.76$

Asta n. 3643 (-2699 -3323) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3

Sollecitazioni: $N,Ed=-1225.46$ $M_y,Ed=-234.35$ $M_z,Ed=-85.23$
 Resistenze: $N_c,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=4.80$ $N_{cr,y}=17091500.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$

$\lambda_z=6.62$ $N_{cr,z}=8991320.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$

$K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$

Verifica YY: $0.02+0.09+0.05=0.15$

Verifica ZZ: $0.02+0.07+0.05=0.14$

- Verifica in termini tensionali [4.2.4] - CC 89 SLU $X1=0.00$ - Classe 3

Sollecitazioni: $N=2106.83$ $T_z=-507.49$ $M_y=-271.69$ $T_y=-396.58$ $M_z=-36.79$ $M_x=-117.88$

Tensioni: $\sigma_N=110.89$ $\sigma_M=508.51$ $\tau=136.67$ $\sigma_{max}=619.39$

Tensioni: $\sigma_N=110.89$ $\sigma_M=397.86$ $\tau=194.16$ $\tau_{max}=194.16$

Tensioni: $\sigma_N=110.89$ $\sigma_M=499.20$ $\tau=181.83$ $\sigma_{ID,max}=686.58$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.21$ - Classe 3

Sollecitazioni: $N=1243.55$ $T_z=-269.54$ $M_y=-79.36$ $T_y=-246.67$ $M_z=-76.96$ $M_x=-67.59$

Tensioni: $\sigma_N=65.45$ $\sigma_M=282.58$ $\tau=78.36$ $\sigma_{max}=348.03$

Tensioni: $\sigma_N=65.45$ $\sigma_M=116.21$ $\tau=114.12$ $\tau_{max}=114.12$

Tensioni: $\sigma_N=65.45$ $\sigma_M=263.11$ $\tau=106.45$ $\sigma_{ID,max}=376.76$

Asta n. 3643 (-3323 -5440) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3

Sollecitazioni: $N,Ed=-1788.07$ $M_y,Ed=-124.77$ $M_z,Ed=-199.90$
 Resistenze: $N_c,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=4.80$ $N_{cr,y}=17091500.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$

$\lambda_z=6.62$ $N_{cr,z}=8991320.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$

$K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$

Verifica YY: $0.03+0.05+0.11=0.19$

Verifica ZZ: $0.03+0.04+0.11=0.18$

- Verifica in termini tensionali [4.2.4] - CC 75 SLU $X1=0.21$ - Classe 3

Sollecitazioni: $N=1183.39$ $T_z=-294.66$ $M_y=-85.37$ $T_y=-306.39$ $M_z=-220.66$ $M_x=-89.82$

Tensioni: $\sigma_N=62.28$ $\sigma_M=583.11$ $\tau=104.14$ $\sigma_{max}=645.39$

Tensioni: $\sigma_N=62.28$ $\sigma_M=125.01$ $\tau=148.55$ $\tau_{max}=148.55$

Tensioni: $\sigma_N=62.28$ $\sigma_M=583.11$ $\tau=104.14$ $\sigma_{ID,max}=670.12$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.21$ - Classe 3

Sollecitazioni: $N=669.94$ $T_z=-209.39$ $M_y=-39.04$ $T_y=-175.35$ $M_z=-131.31$ $M_x=-63.74$

Tensioni: $\sigma_N=35.26$ $\sigma_M=328.19$ $\tau=73.90$ $\sigma_{max}=363.45$

Tensioni: $\sigma_N=35.26$ $\sigma_M=57.17$ $\tau=99.32$ $\tau_{max}=99.32$

Tensioni: $\sigma_N=35.26$ $\sigma_M=328.19$ $\tau=73.90$ $\sigma_{ID,max}=385.33$

Asta n. 3644 (-5439 -5851) Tubo 60x60x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 1

Sollecitazioni: $N,Ed=-1054.59$ $M_y,Ed=-2.77$
 Resistenze: $N_c,Rd=20053.30$ $M_y,c,Rd=421.84$ $L=153.00$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=66.75$ $N_{cr,y}=41677.10$ $\lambda^*_y=0.71$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$

$\lambda_z=66.75$ $N_{cr,z}=41677.10$ $\lambda^*_z=0.71$ Curva a: $\Phi_z=0.81$ $\chi_z=0.84$

$K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.98, 0.59, 0.00, 0.98$

Verifica YY: $0.05+0.01=0.06$

Verifica ZZ: $0.05=0.05$

- Verifica Freccia massima carichi totali - CC 83

$f_{z,c}=0.01$ (L/30242)

- Verifica a compressione [4.2.9] - CC 45 SLU $X1=0.00$ - Classe 1

Sollecitazioni: $N=-1054.59$ $T_z=7.26$ $M_x=2.05$
 $N,Ed=-1054.59$ $N_c,Rd=-20053.30$ $N,Ed/N_c,Rd=0.05$

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 45 SLU $X1=1.53$

Sollecitazioni: $N=-1054.34$ $T_z=-7.26$ $M_x=2.05$
 $V,Ed=-7.26$ $V_c,Rd,Red=5752.40$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.76$ - Classe 3

Sollecitazioni: $N=-519.91$ $M_y=-2.05$ $M_x=2.62$

Tensioni: $\sigma_N=-58.03$ $\sigma_M=-13.09$ $\tau=10.44$ $\sigma_{max}=-71.12$
 Tensioni: $\sigma_N=-58.03$ $\sigma_M=13.09$ $\tau=10.44$ $\tau_{max}=10.44$
 Tensioni: $\sigma_N=-58.03$ $\sigma_M=-13.09$ $\tau=10.44$ $\sigma_{ID,max}=73.38$

Asta n. 3645 (-5437 -5835) Tubo 60x60x4 mm - S235 Crit. 2

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 1

Sollecitazioni: N,Ed=-1061.38 My,Ed=-2.77
 Resistenze: Nc,Rd=20053.30 My,c,Rd=421.84 L=153.00
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=66.75$ Ncr,y=41677.10 $\lambda^*_y=0.71$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=66.75$ Ncr,z=41677.10 $\lambda^*_z=0.71$ Curva a: $\Phi_z=0.81$ $\chi_z=0.84$
 Kyy, Kyz, Kzy, Kzz=0.98, 0.59, 0.00, 0.98
 Verifica YY: 0.05+0.01=0.06
 Verifica ZZ: 0.05=0.05

- Verifica Freccia massima carichi totali - CC 42
 $f_{z,L}=0.00$ (L/30824)

- Verifica a compressione [4.2.9] - CC 45 SLU Xl=0.00 - Classe 1

Sollecitazioni: N=-1061.38 Tz=7.26 Mx=-2.02
 N,Ed=-1061.38 Nc,Rd=-20053.30 N,Ed/Nc,Rd=0.05

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 111 SLU Xl=1.53

Sollecitazioni: N=-157.94 Tz=-7.26 Mx=-2.47
 V,Ed=-7.26 Vc,Rd,Red=5744.92 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.76 - Classe 3

Sollecitazioni: N=-538.92 My=-2.05 Mx=-5.80
 Tensioni: $\sigma_N=-60.15$ $\sigma_M=-13.09$ $\tau=23.12$ $\sigma_{max}=-73.24$
 Tensioni: $\sigma_N=-60.15$ $\sigma_M=13.09$ $\tau=23.12$ $\tau_{max}=23.12$
 Tensioni: $\sigma_N=-60.15$ $\sigma_M=-13.09$ $\tau=23.12$ $\sigma_{ID,max}=83.47$

Asta n. 3646 (-2442 -6191) Tubo circolare d=90x4 mm - S355 Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 1

Sollecitazioni: N,Ed=-6982.24 M,Ed=5.94
 Resistenze: Nc,Rd=36538.20 M,c,Rd=976.45 L=212.44
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, ----, ----
 $\lambda=69.79$ Ncr=45984.70 $\lambda^*=0.91$
 Curva a: $\Phi=0.99$ $\chi_{,min}=0.73$
 Kyy, Kyz, Kzy, Kzz=1.13, ----, ----, ----
 Verifica: 0.26+0.01=0.27

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,G}=0.02$ (L/12134)

- Verifica Freccia massima carichi totali - CC 26
 $f_{z,G}=0.02$ (L/10862) $f_{z,L}=0.01$ (L/21514)

- Verifica a compressione [4.2.9] - CC 49 SLU Xl=0.00 - Classe 1

Sollecitazioni: N=-6982.24 T=11.20 Mx=-19.98
 N,Ed=-6982.24 Nc,Rd=-36538.20 N,Ed/Nc,Rd=0.19

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 54 SLU Xl=2.12

Sollecitazioni: N=-6882.57 T=11.20 Mx=-25.82
 V,Ed=11.20 Vc,Rd,Red=13031.00 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=1.06 - Classe 3

Sollecitazioni: N=-3022.94 M=4.40 Mx=-16.63
 Tensioni: $\sigma_N=-279.72$ $\sigma_M=-19.79$ $\tau=37.37$ $\sigma_{max}=-299.50$
 Tensioni: $\sigma_N=-279.72$ $\sigma_M=17.14$ $\tau=37.37$ $\tau_{max}=37.37$
 Tensioni: $\sigma_N=-279.72$ $\sigma_M=-19.79$ $\tau=37.37$ $\sigma_{ID,max}=306.42$

Asta n. 3647 (-2441 -6193) Tubo circolare d=90x4 mm - S355 Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 1

Sollecitazioni: N,Ed=-6932.69 M,Ed=5.95
 Resistenze: Nc,Rd=36538.20 M,c,Rd=976.45 L=212.52
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, ----, ----
 $\lambda=69.82$ Ncr=45947.00 $\lambda^*=0.91$
 Curva a: $\Phi=0.99$ $\chi_{,min}=0.72$
 Kyy, Kyz, Kzy, Kzz=1.13, ----, ----, ----
 Verifica: 0.26+0.01=0.27

- Verifica Freccia massima per soli carichi accidentali - CC 46

$f_{z,g}=0.02$ (L/12041)

- Verifica Freccia massima carichi totali - CC 26
 $f_{z,g}=0.02$ (L/10866) $f_{z,l}=0.01$ (L/21419)
- Verifica a compressione [4.2.9] - CC 49 SLU $X_l=0.00$ - Classe 1
Sollecitazioni: $N=-6932.69$ $T=11.20$ $M_x=20.94$
 $N,Ed=-6932.69$ $Nc,Rd=-36538.20$ $N,Ed/Nc,Rd=0.19$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 89 SLU $X_l=0.00$
Sollecitazioni: $N=-5271.77$ $T=11.20$ $M_x=32.00$
 $V,Ed=11.20$ $Vc,Rd,Red=12935.40$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_l=1.06$ - Classe 3
Sollecitazioni: $N=-3207.42$ $M=4.41$ $M_x=18.21$
Tensioni: $\sigma_N=-296.79$ $\sigma_M=-19.80$ $\tau=40.92$ $\sigma_{max}=-316.59$
Tensioni: $\sigma_N=-296.79$ $\sigma_M=15.17$ $\tau=40.92$ $\tau_{max}=40.92$
Tensioni: $\sigma_N=-296.79$ $\sigma_M=-19.80$ $\tau=40.92$ $\sigma_{ID,max}=324.42$

Asta n. 3662 (-2426 -2520) Tubo 60x80x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.01$ (L/3390) $f_{z,l}=0.00$ (L/25996)
- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3058) $f_{z,l}=0.00$ (L/13629)
- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X_l=0.00$ - Classe 3
Sollecitazioni: $N=3262.03$ $T_z=324.51$ $M_y=-15.90$ $T_y=333.66$ $M_z=-129.45$ $M_x=65.33$
Tensioni: $\sigma_N=250.93$ $\sigma_M=602.57$ $\tau=158.38$ $\sigma_{max}=853.50$
Tensioni: $\sigma_N=250.93$ $\sigma_M=49.23$ $\tau=224.74$ $\tau_{max}=224.74$
Tensioni: $\sigma_N=250.93$ $\sigma_M=602.57$ $\tau=158.38$ $\sigma_{ID,max}=896.50$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.00$ - Classe 3
Sollecitazioni: $N=1312.61$ $T_z=146.83$ $M_y=-15.12$ $T_y=163.58$ $M_z=-63.86$ $M_x=52.61$
Tensioni: $\sigma_N=100.97$ $\sigma_M=322.97$ $\tau=127.54$ $\sigma_{max}=423.94$
Tensioni: $\sigma_N=100.97$ $\sigma_M=46.79$ $\tau=160.06$ $\tau_{max}=160.06$
Tensioni: $\sigma_N=100.97$ $\sigma_M=322.97$ $\tau=127.54$ $\sigma_{ID,max}=478.04$

Asta n. 3662 (-2520 -2755) Tubo 60x100x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.01$ (L/3429)
- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3118) $f_{z,l}=0.00$ (L/16576)
- Verifica in termini tensionali [4.2.4] - CC 75 SLU $X_l=0.21$ - Classe 3
Sollecitazioni: $N=3307.56$ $T_z=388.07$ $M_y=-220.58$ $T_y=311.53$ $M_z=49.31$ $M_x=49.65$
Tensioni: $\sigma_N=220.50$ $\sigma_M=733.49$ $\tau=95.03$ $\sigma_{max}=953.99$
Tensioni: $\sigma_N=220.50$ $\sigma_M=505.79$ $\tau=156.05$ $\tau_{max}=156.05$
Tensioni: $\sigma_N=220.50$ $\sigma_M=733.49$ $\tau=95.03$ $\sigma_{ID,max}=968.08$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 75 SLU $X_l=0.06$
Sollecitazioni: $N=3305.38$ $T_z=389.23$ $M_y=-160.26$ $T_y=311.53$ $M_x=49.65$
 $V,Ed=311.53$ $Vc,Rd,Red=10445.70$ $V,Ed/Vc,Rd,Red=0.03$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=389.23$ $Vc,Rd,Red=17409.60$ $V,Ed/Vc,Rd,Red=0.02$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.21$ - Classe 3
Sollecitazioni: $N=1317.83$ $T_z=143.13$ $M_y=-90.55$ $T_y=163.99$ $M_z=25.95$ $M_x=52.60$
Tensioni: $\sigma_N=87.86$ $\sigma_M=320.98$ $\tau=100.67$ $\sigma_{max}=408.83$
Tensioni: $\sigma_N=87.86$ $\sigma_M=207.64$ $\tau=132.76$ $\tau_{max}=132.76$
Tensioni: $\sigma_N=87.86$ $\sigma_M=305.94$ $\tau=126.81$ $\sigma_{ID,max}=450.90$

Asta n. 3662 (-2755 -3450) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
Sollecitazioni: $N,Ed=-1203.78$ $M_y,Ed=-170.23$ $M_z,Ed=80.48$
Resistenze: $Nc,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ $Ncr,y=17091500.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ $Ncr,z=8991320.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.02+0.06+0.05=0.13$

Verifica ZZ: $0.02+0.05+0.05=0.11$

- Verifica in termini tensionali [4.2.4] - CC 75 SLU $X1=0.00$ - Classe 3
Sollecitazioni: $N=2879.09$ $T_z=-444.34$ $M_y=-200.67$ $T_y=268.42$ $M_z=60.99$ $M_x=46.87$
Tensioni: $\sigma_N=151.53$ $\sigma_M=444.04$ $\tau=54.34$ $\sigma_{max}=595.58$
Tensioni: $\sigma_N=151.53$ $\sigma_M=-108.03$ $\tau=99.48$ $\tau_{max}=99.48$
Tensioni: $\sigma_N=151.53$ $\sigma_M=444.04$ $\tau=54.34$ $\sigma_{ID,max}=602.97$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3
Sollecitazioni: $N=1124.11$ $T_z=-194.89$ $M_y=-83.75$ $T_y=136.69$ $M_z=32.20$ $M_x=49.85$
Tensioni: $\sigma_N=59.16$ $\sigma_M=198.97$ $\tau=57.80$ $\sigma_{max}=258.14$
Tensioni: $\sigma_N=59.16$ $\sigma_M=122.64$ $\tau=77.62$ $\tau_{max}=77.62$
Tensioni: $\sigma_N=59.16$ $\sigma_M=190.83$ $\tau=73.37$ $\sigma_{ID,max}=280.44$

Asta n. 3662 (-3450 -5841) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
Sollecitazioni: $N,Ed=-2605.06$ $M_y,Ed=-61.05$ $M_z,Ed=116.84$
Resistenze: $N_c,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ $N_{cr,y}=17091400.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ $N_{cr,z}=8991280.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.04+0.02+0.07=0.13$
Verifica ZZ: $0.04+0.02+0.07=0.13$

- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X1=0.21$ - Classe 3
Sollecitazioni: $N=2890.97$ $T_z=-113.63$ $M_y=-83.65$ $T_y=180.70$ $M_z=185.18$ $M_x=60.68$
Tensioni: $\sigma_N=152.16$ $\sigma_M=508.52$ $\tau=70.36$ $\sigma_{max}=660.68$
Tensioni: $\sigma_N=152.16$ $\sigma_M=122.49$ $\tau=96.54$ $\tau_{max}=96.54$
Tensioni: $\sigma_N=152.16$ $\sigma_M=508.52$ $\tau=70.36$ $\sigma_{ID,max}=671.83$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.21$ - Classe 3
Sollecitazioni: $N=1326.54$ $T_z=-84.09$ $M_y=-35.78$ $T_y=79.51$ $M_z=88.58$ $M_x=48.91$
Tensioni: $\sigma_N=69.82$ $\sigma_M=236.50$ $\tau=56.71$ $\sigma_{max}=306.31$
Tensioni: $\sigma_N=69.82$ $\sigma_M=52.40$ $\tau=68.23$ $\tau_{max}=68.23$
Tensioni: $\sigma_N=69.82$ $\sigma_M=236.50$ $\tau=56.71$ $\sigma_{ID,max}=321.68$

Asta n. 3663 (-2427 -2521) Tubo 60x80x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.01$ (L/3399) $f_{z,L}=0.00$ (L/25996)
- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3065) $f_{z,L}=0.00$ (L/13369)
- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X1=0.33$ - Classe 3
Sollecitazioni: $N=3075.95$ $T_z=399.78$ $M_y=-138.80$ $T_y=-304.84$ $M_z=18.41$ $M_x=-48.78$
Tensioni: $\sigma_N=236.61$ $\sigma_M=568.67$ $\tau=118.24$ $\sigma_{max}=805.28$
Tensioni: $\sigma_N=236.61$ $\sigma_M=364.84$ $\tau=179.80$ $\tau_{max}=179.80$
Tensioni: $\sigma_N=236.61$ $\sigma_M=555.72$ $\tau=165.42$ $\sigma_{ID,max}=842.54$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 60 SLU $X1=0.03$
Sollecitazioni: $N=1106.94$ $T_z=196.22$ $T_y=-98.01$ $M_z=36.45$ $M_x=-10.93$
 $V,Ed=-98.01$ $V_c,Rd,Red=10728.10$ $V,Ed/V_c,Rd,Red=0.01$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=196.22$ $V_c,Rd,Red=14304.20$ $V,Ed/V_c,Rd,Red=0.01$
- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.00$ - Classe 3
Sollecitazioni: $N=1417.86$ $T_z=165.05$ $M_y=-12.22$ $T_y=-185.00$ $M_z=71.73$ $M_x=-45.45$
Tensioni: $\sigma_N=109.07$ $\sigma_M=345.95$ $\tau=110.19$ $\sigma_{max}=455.01$
Tensioni: $\sigma_N=109.07$ $\sigma_M=37.83$ $\tau=146.98$ $\tau_{max}=146.98$
Tensioni: $\sigma_N=109.07$ $\sigma_M=345.95$ $\tau=110.19$ $\sigma_{ID,max}=493.42$

Asta n. 3663 (-2521 -2756) Tubo 60x100x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.01$ (L/3456)
- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3140) $f_{z,L}=0.00$ (L/17213)
- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X1=0.21$ - Classe 3
Sollecitazioni: $N=3078.87$ $T_z=398.26$ $M_y=-223.98$ $T_y=-305.50$ $M_z=-46.79$ $M_x=-48.74$

Tensioni: $\sigma_N=205.26$ $\sigma_M=733.37$ $\tau=93.29$ $\sigma_{max}=938.63$
 Tensioni: $\sigma_N=205.26$ $\sigma_M=513.58$ $\tau=153.14$ $\tau_{max}=153.14$
 Tensioni: $\sigma_N=205.26$ $\sigma_M=733.37$ $\tau=93.29$ $\sigma_{ID,max}=952.43$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 75 SLU $X1=0.06$
 Sollecitazioni: $N=3071.08$ $T_z=321.70$ $M_y=-140.56$ $T_y=-313.87$ $M_x=-53.35$
 $V,Ed=-313.87$ $V_c,Rd,Red=10405.90$ $V,Ed/V_c,Rd,Red=0.03$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=321.70$ $V_c,Rd,Red=17343.20$ $V,Ed/V_c,Rd,Red=0.02$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.21$ - Classe 3
 Sollecitazioni: $N=1423.38$ $T_z=162.33$ $M_y=-92.13$ $T_y=-185.76$ $M_z=-29.91$ $M_x=-45.44$
 Tensioni: $\sigma_N=94.89$ $\sigma_M=338.75$ $\tau=86.97$ $\sigma_{max}=433.64$
 Tensioni: $\sigma_N=94.89$ $\sigma_M=211.25$ $\tau=123.33$ $\tau_{max}=123.33$
 Tensioni: $\sigma_N=94.89$ $\sigma_M=321.41$ $\tau=116.58$ $\sigma_{ID,max}=462.69$

Asta n. 3663 (-2756 -3451) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-1255.86$ $M_y,Ed=-171.20$ $M_z,Ed=-80.42$
 Resistenze: $N_c,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ $N_{cr,y}=17091500.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ $N_{cr,z}=8991340.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.02+0.06+0.05=0.13$
 Verifica ZZ: $0.02+0.05+0.05=0.12$

- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X1=0.00$ - Classe 3
 Sollecitazioni: $N=2691.05$ $T_z=-452.09$ $M_y=-204.06$ $T_y=-270.35$ $M_z=-57.88$ $M_x=-47.60$
 Tensioni: $\sigma_N=141.63$ $\sigma_M=443.16$ $\tau=55.19$ $\sigma_{max}=584.79$
 Tensioni: $\sigma_N=141.63$ $\sigma_M=-102.52$ $\tau=101.11$ $\tau_{max}=101.11$
 Tensioni: $\sigma_N=141.63$ $\sigma_M=443.16$ $\tau=55.19$ $\sigma_{ID,max}=592.55$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.21$ - Classe 3
 Sollecitazioni: $N=1234.82$ $T_z=-186.19$ $M_y=-44.71$ $T_y=-161.17$ $M_z=-70.34$ $M_x=-43.78$
 Tensioni: $\sigma_N=64.99$ $\sigma_M=213.82$ $\tau=50.76$ $\sigma_{max}=278.81$
 Tensioni: $\sigma_N=64.99$ $\sigma_M=65.47$ $\tau=74.12$ $\tau_{max}=74.12$
 Tensioni: $\sigma_N=64.99$ $\sigma_M=213.82$ $\tau=50.76$ $\sigma_{ID,max}=292.34$

Asta n. 3663 (-3451 -5845) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: $N,Ed=-167.68$ $M_y,Ed=-84.46$ $M_z,Ed=-160.53$
 Resistenze: $N_c,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ $N_{cr,y}=17091400.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ $N_{cr,z}=8991280.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.03+0.09=0.13$
 Verifica ZZ: $0.00+0.02+0.09=0.12$

- Verifica in termini tensionali [4.2.4] - CC 75 SLU $X1=0.21$ - Classe 3
 Sollecitazioni: $N=2791.78$ $T_z=-114.80$ $M_y=-81.84$ $T_y=-185.60$ $M_z=-175.63$ $M_x=-47.59$
 Tensioni: $\sigma_N=146.94$ $\sigma_M=486.30$ $\tau=55.17$ $\sigma_{max}=633.24$
 Tensioni: $\sigma_N=146.94$ $\sigma_M=119.85$ $\tau=82.07$ $\tau_{max}=82.07$
 Tensioni: $\sigma_N=146.94$ $\sigma_M=486.30$ $\tau=55.17$ $\sigma_{ID,max}=640.41$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.21$ - Classe 3
 Sollecitazioni: $N=1365.27$ $T_z=-91.39$ $M_y=-35.53$ $T_y=-100.44$ $M_z=-102.03$ $M_x=-41.18$
 Tensioni: $\sigma_N=71.86$ $\sigma_M=263.31$ $\tau=47.75$ $\sigma_{max}=335.17$
 Tensioni: $\sigma_N=71.86$ $\sigma_M=52.02$ $\tau=62.30$ $\tau_{max}=62.30$
 Tensioni: $\sigma_N=71.86$ $\sigma_M=263.31$ $\tau=47.75$ $\sigma_{ID,max}=345.22$

Asta n. 3664 (-5842 -6234) Tubo 60x60x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 1
 Sollecitazioni: $N,Ed=-1193.73$ $M_y,Ed=-2.77$
 Resistenze: $N_c,Rd=20053.30$ $M_y,c,Rd=421.84$ $L=153.00$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=66.75$ $N_{cr,y}=41677.00$ $\lambda^*_y=0.71$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=66.75$ $N_{cr,z}=41677.00$ $\lambda^*_z=0.71$ Curva a: $\Phi_z=0.81$ $\chi_z=0.84$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.98, 0.59, 0.00, 0.98$

Verifica YY: $0.06+0.01=0.07$
 Verifica ZZ: $0.06=0.06$

- Verifica Freccia massima carichi totali - CC 42
 $f_{z,L}=0.01$ (L/29960)
- Verifica a compressione [4.2.9] - CC 45 SLU $X1=0.00$ - Classe 1
 Sollecitazioni: $N=-1193.73$ $T_z=7.26$ $M_x=-7.82$
 $N,Ed=-1193.73$ $Nc,Rd=-20053.30$ $N,Ed/Nc,Rd=0.06$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 49 SLU $X1=0.00$
 Sollecitazioni: $N=-1090.86$ $T_z=7.26$ $M_x=-8.00$
 $V,Ed=7.26$ $Vc,Rd,Red=5646.18$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.77$ - Classe 3
 Sollecitazioni: $N=-637.92$ $M_y=-2.05$ $M_x=-3.83$
 Tensioni: $\sigma_N=-71.20$ $\sigma_M=-13.09$ $\tau=15.25$ $\sigma_{max}=-84.29$
 Tensioni: $\sigma_N=-71.20$ $\sigma_M=13.09$ $\tau=15.25$ $\tau_{max}=15.25$
 Tensioni: $\sigma_N=-71.20$ $\sigma_M=-13.09$ $\tau=15.25$ $\sigma_{ID,max}=88.33$

Asta n. 3665 (-5844 -6252) Tubo 60x60x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 1
 Sollecitazioni: $N,Ed=-1186.14$ $M_y,Ed=2.77$
 Resistenze: $Nc,Rd=20053.30$ $M_y,c,Rd=421.84$ $L=153.00$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=66.75$ $Ncr,y=41677.00$ $\lambda^*_y=0.71$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=66.75$ $Ncr,z=41677.00$ $\lambda^*_z=0.71$ Curva a: $\Phi_z=0.81$ $\chi_z=0.84$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.98, 0.59, 0.00, 0.98$
 Verifica YY: $0.06+0.01=0.07$
 Verifica ZZ: $0.06=0.06$

- Verifica Freccia massima carichi totali - CC 55
 $f_{z,G}=0.01$ (L/29960)
- Verifica a compressione [4.2.9] - CC 45 SLU $X1=0.00$ - Classe 1
 Sollecitazioni: $N=-1186.14$ $T_z=7.26$ $M_x=7.80$
 $N,Ed=-1186.14$ $Nc,Rd=-20053.30$ $N,Ed/Nc,Rd=0.06$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 49 SLU $X1=0.00$
 Sollecitazioni: $N=-1081.65$ $T_z=7.26$ $M_x=7.98$
 $V,Ed=7.26$ $Vc,Rd,Red=5646.63$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.77$ - Classe 3
 Sollecitazioni: $N=-578.82$ $M_y=-2.05$ $M_x=3.80$
 Tensioni: $\sigma_N=-64.60$ $\sigma_M=-13.09$ $\tau=15.14$ $\sigma_{max}=-77.69$
 Tensioni: $\sigma_N=-64.60$ $\sigma_M=13.09$ $\tau=15.14$ $\tau_{max}=15.14$
 Tensioni: $\sigma_N=-64.60$ $\sigma_M=-13.09$ $\tau=15.14$ $\sigma_{ID,max}=82.00$

Asta n. 3667 (-2427 -6550) Tubo circolare d=70x4 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 1
 Sollecitazioni: $N,Ed=-5098.82$ $M,Ed=3.99$
 Resistenze: $Nc,Rd=28041.00$ $M,c,Rd=575.38$ $L=201.66$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, ----, ----$
 $\lambda=86.26$ $Ncr=23100.80$ $\lambda^*=1.13$
 Curva a: $\Phi=1.23$ $\chi_{min}=0.58$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=1.19, ----, ----, ----$
 Verifica: $0.32+0.01=0.32$

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,G}=0.02$ (L/10361)
- Verifica Freccia massima carichi totali - CC 26
 $f_{z,G}=0.02$ (L/8994) $f_{z,L}=0.01$ (L/15260)
- Verifica a compressione [4.2.9] - CC 49 SLU $X1=0.00$ - Classe 1
 Sollecitazioni: $N=-5098.82$ $T=7.91$ $M_x=1.53$
 $N,Ed=-5098.82$ $Nc,Rd=-28041.00$ $N,Ed/Nc,Rd=0.18$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 68 SLU $X1=0.00$
 Sollecitazioni: $N=-3655.84$ $T=7.91$ $M_x=5.07$
 $V,Ed=7.91$ $Vc,Rd,Red=10203.40$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=1.01$ - Classe 3
 Sollecitazioni: $N=-2283.35$ $M=2.95$ $M_x=2.54$

Tensioni: $\sigma_N=-275.31$ $\sigma_M=-22.81$ $\tau=9.79$ $\sigma_{max}=-298.12$
 Tensioni: $\sigma_N=-275.31$ $\sigma_M=22.47$ $\tau=9.79$ $\tau_{max}=9.79$
 Tensioni: $\sigma_N=-275.31$ $\sigma_M=-22.81$ $\tau=9.79$ $\sigma_{ID,max}=298.60$

Asta n. 3668 (-2426 -6548) Tubo circolare d=70x4 mm - S355 Crit. 3

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 1
 Sollecitazioni: N,Ed=-5103.24 M,Ed=3.99
 Resistenze: Nc,Rd=28041.00 M,c,Rd=575.38 L=201.66
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, \text{----}, \text{----}$
 $\lambda=86.26$ Ncr=23100.80 $\lambda'=1.13$
 Curva a: $\Phi=1.23$ $\chi_{,min}=0.58$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=1.19, \text{----}, \text{----}, \text{----}$
 Verifica: 0.32+0.01=0.32
 - Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.02$ (L/10412)
 - Verifica Freccia massima carichi totali - CC 26
 $f_{z,g}=0.02$ (L/8984) $f_{z,L}=0.01$ (L/15260)
 - Verifica a compressione [4.2.9] - CC 49 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=-5103.24 T=7.91 $M_x=-1.54$
 N,Ed=-5103.24 Nc,Rd=-28041.00 N,Ed/Nc,Rd=0.18
 - Verifica a taglio e torsione dir. Z [4.2.25] - CC 75 SLU Xl=0.00
 Sollecitazioni: N=-5015.12 T=7.91 $M_x=-2.70$
 V,Ed=7.91 Vc,Rd,Red=10251.80 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=1.01 - Classe 3
 Sollecitazioni: N=-2191.44 M=2.95 $M_x=-2.92$
 Tensioni: $\sigma_N=-264.23$ $\sigma_M=-22.81$ $\tau=11.28$ $\sigma_{max}=-287.04$
 Tensioni: $\sigma_N=-264.23$ $\sigma_M=19.76$ $\tau=11.28$ $\tau_{max}=11.28$
 Tensioni: $\sigma_N=-264.23$ $\sigma_M=-22.81$ $\tau=11.28$ $\sigma_{ID,max}=287.70$

Asta n. 3683 (-2405 -2543) Tubo 60x80x5 mm - S355 Crit. 3

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- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.01$ (L/3465) $f_{z,L}=0.00$ (L/22074)
 - Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3239) $f_{z,L}=0.00$ (L/11763)
 - Verifica in termini tensionali [4.2.4] - CC 75 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=1771.93 $T_z=211.82$ $M_y=-12.03$ $T_y=-239.73$ $M_z=104.08$ $M_x=-22.16$
 Tensioni: $\sigma_N=136.30$ $\sigma_M=481.79$ $\tau=53.72$ $\sigma_{max}=618.10$
 Tensioni: $\sigma_N=136.30$ $\sigma_M=37.23$ $\tau=101.42$ $\tau_{max}=101.42$
 Tensioni: $\sigma_N=136.30$ $\sigma_M=481.79$ $\tau=53.72$ $\sigma_{ID,max}=625.06$
 - Verifica a taglio e torsione dir. Y [4.2.25] - CC 89 SLU Xl=0.43
 Sollecitazioni: N=1235.11 $T_z=150.84$ $M_y=-84.86$ $T_y=-206.86$ $M_x=-33.33$
 V,Ed=-206.86 Vc,Rd,Red=10425.60 V,Ed/Vc,Rd,Red=0.02
 - Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=150.84 Vc,Rd,Red=13900.80 V,Ed/Vc,Rd,Red=0.01

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=1006.48 $T_z=112.32$ $M_y=-11.25$ $T_y=-135.66$ $M_z=58.44$ $M_x=-24.07$
 Tensioni: $\sigma_N=77.42$ $\sigma_M=286.43$ $\tau=58.36$ $\sigma_{max}=363.85$
 Tensioni: $\sigma_N=77.42$ $\sigma_M=34.82$ $\tau=85.34$ $\tau_{max}=85.34$
 Tensioni: $\sigma_N=77.42$ $\sigma_M=286.43$ $\tau=58.36$ $\sigma_{ID,max}=377.63$

Asta n. 3683 (-2543 -2812) Tubo 60x100x5 mm - S355 Crit. 3

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- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.01$ (L/3496)
 - Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3290) $f_{z,L}=0.00$ (L/19045)
 - Verifica in termini tensionali [4.2.4] - CC 54 SLU Xl=0.21 - Classe 3
 Sollecitazioni: N=1771.92 $T_z=278.24$ $M_y=-186.51$ $T_y=-233.88$ $M_z=-46.91$ $M_x=-19.17$
 Tensioni: $\sigma_N=118.13$ $\sigma_M=638.35$ $\tau=36.69$ $\sigma_{max}=756.47$
 Tensioni: $\sigma_N=118.13$ $\sigma_M=427.67$ $\tau=82.52$ $\tau_{max}=82.52$
 Tensioni: $\sigma_N=118.13$ $\sigma_M=638.35$ $\tau=36.69$ $\sigma_{ID,max}=759.14$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 89 SLU $X_1=0.00$
 Sollecitazioni: $N=1235.10$ $T_z=150.87$ $M_y=-84.86$ $T_y=-206.90$ $M_x=-33.32$
 $V,Ed=-206.90$ $V_c,Rd,Red=10621.60$ $V,Ed/V_c,Rd,Red=0.02$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=150.87$ $V_c,Rd,Red=17702.60$ $V,Ed/V_c,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_1=0.21$ - Classe 3
 Sollecitazioni: $N=1012.49$ $T_z=109.18$ $M_y=-76.92$ $T_y=-136.23$ $M_z=-28.48$ $M_x=-24.07$
 Tensioni: $\sigma_N=67.50$ $\sigma_M=295.04$ $\tau=46.07$ $\sigma_{max}=362.53$
 Tensioni: $\sigma_N=67.50$ $\sigma_M=176.39$ $\tau=72.74$ $\tau_{max}=72.74$
 Tensioni: $\sigma_N=67.50$ $\sigma_M=295.04$ $\tau=46.07$ $\sigma_{ID,max}=371.21$

Asta n. 3683 (-2812 -3697) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-1844.51$ $M_y,Ed=-139.80$ $M_z,Ed=-68.52$
 Resistenze: $N_c,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ $N_{cr,y}=17091500.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ $N_{cr,z}=8991320.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.03+0.05+0.04=0.12$
 Verifica ZZ: $0.03+0.04+0.04=0.11$

- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=1807.22$ $T_z=-396.63$ $M_y=-167.71$ $T_y=-209.25$ $M_z=-55.08$ $M_x=-18.95$
 Tensioni: $\sigma_N=95.12$ $\sigma_M=379.41$ $\tau=21.98$ $\sigma_{max}=474.52$
 Tensioni: $\sigma_N=95.12$ $\sigma_M=-97.56$ $\tau=62.27$ $\tau_{max}=62.27$
 Tensioni: $\sigma_N=95.12$ $\sigma_M=379.41$ $\tau=21.98$ $\sigma_{ID,max}=476.05$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=911.28$ $T_z=-172.37$ $M_y=-69.09$ $T_y=-120.12$ $M_z=-32.64$ $M_x=-23.19$
 Tensioni: $\sigma_N=47.96$ $\sigma_M=176.45$ $\tau=26.89$ $\sigma_{max}=224.41$
 Tensioni: $\sigma_N=47.96$ $\sigma_M=-57.82$ $\tau=44.40$ $\tau_{max}=44.40$
 Tensioni: $\sigma_N=47.96$ $\sigma_M=176.45$ $\tau=26.89$ $\sigma_{ID,max}=229.19$

Asta n. 3683 (-3697 -6247) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-2671.59$ $M_y,Ed=-48.58$ $M_z,Ed=-96.86$
 Resistenze: $N_c,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ $N_{cr,y}=17091500.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ $N_{cr,z}=8991320.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.04+0.02+0.06=0.11$
 Verifica ZZ: $0.04+0.01+0.06=0.11$

- Verifica in termini tensionali [4.2.4] - CC 75 SLU $X_1=0.21$ - Classe 3
 Sollecitazioni: $N=2715.97$ $T_z=-130.19$ $M_y=-66.65$ $T_y=-152.62$ $M_z=-147.04$ $M_x=-19.18$
 Tensioni: $\sigma_N=142.95$ $\sigma_M=404.16$ $\tau=22.23$ $\sigma_{max}=547.11$
 Tensioni: $\sigma_N=142.95$ $\sigma_M=97.60$ $\tau=44.36$ $\tau_{max}=44.36$
 Tensioni: $\sigma_N=142.95$ $\sigma_M=404.16$ $\tau=22.23$ $\sigma_{ID,max}=548.46$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_1=0.21$ - Classe 3
 Sollecitazioni: $N=1382.63$ $T_z=-112.32$ $M_y=-27.61$ $T_y=-82.01$ $M_z=-82.72$ $M_x=-21.70$
 Tensioni: $\sigma_N=72.77$ $\sigma_M=211.58$ $\tau=25.16$ $\sigma_{max}=284.35$
 Tensioni: $\sigma_N=72.77$ $\sigma_M=40.43$ $\tau=37.05$ $\tau_{max}=37.05$
 Tensioni: $\sigma_N=72.77$ $\sigma_M=211.58$ $\tau=25.16$ $\sigma_{ID,max}=287.67$

Asta n. 3684 (-2363 -2542) Tubo 60x80x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
 Sollecitazioni: $N,Ed=-96.77$ $M_y,Ed=-51.29$ $M_z,Ed=-50.44$
 Resistenze: $N_c,Rd=43952.40$ $M_y,c,Rd=955.82$ $M_z,c,Rd=801.10$ $L=43.60$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=14.78$ $N_{cr,y}=1232960.00$ $\lambda^*_y=0.19$ Curva a: $\Phi_y=0.52$ $\chi_y=1.00$
 $\lambda_z=18.65$ $N_{cr,z}=775029.00$ $\lambda^*_z=0.24$ Curva a: $\Phi_z=0.53$ $\chi_z=0.99$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.05+0.06=0.11$
 Verifica ZZ: $0.00+0.04+0.06=0.10$

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,G}=0.01$ (L/3470) $f_{z,L}=0.00$ (L/22301)

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3265) $f_{z,L}=0.00$ (L/11913)
 - Verifica in termini tensionali [4.2.4] - CC 54 SLU $X1=0.00$ - Classe 3
 Sollecitazioni: $N=1479.88$ $T_z=194.94$ $M_y=-15.74$ $T_y=248.68$ $M_z=-108.67$ $M_x=27.75$
 Tensioni: $\sigma_N=113.84$ $\sigma_M=514.33$ $\tau=67.28$ $\sigma_{max}=628.16$
 Tensioni: $\sigma_N=113.84$ $\sigma_M=48.71$ $\tau=116.74$ $\tau_{max}=116.74$
 Tensioni: $\sigma_N=113.84$ $\sigma_M=514.33$ $\tau=67.28$ $\sigma_{ID,max}=638.88$
 - Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X1=0.44$
 Sollecitazioni: $N=1485.18$ $T_z=192.13$ $M_y=-100.12$ $T_y=248.68$ $M_x=27.75$
 $V,Ed=248.68$ $Vc,Rd,Red=10500.80$ $V,Ed/Vc,Rd,Red=0.02$
 - Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=192.13$ $Vc,Rd,Red=14001.10$ $V,Ed/Vc,Rd,Red=0.01$
 - Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=982.66$ $T_z=103.02$ $M_y=-12.33$ $T_y=115.75$ $M_z=-50.44$ $M_x=19.41$
 Tensioni: $\sigma_N=75.59$ $\sigma_M=256.50$ $\tau=47.06$ $\sigma_{max}=332.09$
 Tensioni: $\sigma_N=75.59$ $\sigma_M=38.17$ $\tau=70.08$ $\tau_{max}=70.08$
 Tensioni: $\sigma_N=75.59$ $\sigma_M=256.50$ $\tau=47.06$ $\sigma_{ID,max}=341.95$
- Asta n. 3684 (-2542 -2811) Tubo 60x100x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
 Sollecitazioni: $N,Ed=-92.58$ $M_y,Ed=-72.27$ $M_z,Ed=24.86$
 Resistenze: $Nc,Rd=50714.30$ $M_y,c,Rd=1327.02$ $M_z,c,Rd=972.02$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=5.90$ $Ncr,y=8930630.00$ $\lambda^*_y=0.08$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=8.90$ $Ncr,z=3924920.00$ $\lambda^*_z=0.12$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.05+0.02=0.08$
 Verifica ZZ: $0.00+0.04+0.02=0.07$
 - Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.01$ (L/3496)
 - Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3278) $f_{z,L}=0.00$ (L/20115)
 - Verifica in termini tensionali [4.2.4] - CC 75 SLU $X1=0.21$ - Classe 3
 Sollecitazioni: $N=1500.01$ $T_z=255.58$ $M_y=-174.23$ $T_y=237.28$ $M_z=49.28$ $M_x=20.75$
 Tensioni: $\sigma_N=100.00$ $\sigma_M=615.32$ $\tau=39.70$ $\sigma_{max}=715.32$
 Tensioni: $\sigma_N=100.00$ $\sigma_M=399.52$ $\tau=86.18$ $\tau_{max}=86.18$
 Tensioni: $\sigma_N=100.00$ $\sigma_M=615.32$ $\tau=39.70$ $\sigma_{ID,max}=718.62$
 - Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X1=0.00$
 Sollecitazioni: $N=1485.17$ $T_z=192.16$ $M_y=-100.12$ $T_y=248.72$ $M_x=27.75$
 $V,Ed=248.72$ $Vc,Rd,Red=10681.50$ $V,Ed/Vc,Rd,Red=0.02$
 - Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=192.16$ $Vc,Rd,Red=17802.50$ $V,Ed/Vc,Rd,Red=0.01$
 - Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.21$ - Classe 3
 Sollecitazioni: $N=988.55$ $T_z=99.36$ $M_y=-72.27$ $T_y=116.31$ $M_z=24.86$ $M_x=19.41$
 Tensioni: $\sigma_N=65.90$ $\sigma_M=270.62$ $\tau=37.15$ $\sigma_{max}=336.52$
 Tensioni: $\sigma_N=65.90$ $\sigma_M=165.72$ $\tau=59.92$ $\tau_{max}=59.92$
 Tensioni: $\sigma_N=65.90$ $\sigma_M=270.62$ $\tau=37.15$ $\sigma_{ID,max}=342.62$
- Asta n. 3684 (-2811 -3696) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-1965.47$ $M_y,Ed=-137.69$ $M_z,Ed=68.02$
 Resistenze: $Nc,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ $Ncr,y=17091600.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ $Ncr,z=8991390.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.03+0.05+0.04=0.12$
 Verifica ZZ: $0.03+0.04+0.04=0.11$
 - Verifica in termini tensionali [4.2.4] - CC 75 SLU $X1=0.00$ - Classe 3
 Sollecitazioni: $N=1621.48$ $T_z=-374.53$ $M_y=-155.98$ $T_y=205.12$ $M_z=57.90$ $M_x=19.20$
 Tensioni: $\sigma_N=85.34$ $\sigma_M=366.39$ $\tau=22.26$ $\sigma_{max}=451.73$

Tensioni: $\sigma_N=85.34$ $\sigma_M=-102.56$ $\tau=60.31$ $\tau_{max}=60.31$
 Tensioni: $\sigma_N=85.34$ $\sigma_M=366.39$ $\tau=22.26$ $\sigma_{TD,max}=453.37$

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=889.67 T_z=-163.16 M_y=-64.90 T_y=96.85 M_z=28.89 M_x=18.10
 Tensioni: $\sigma_N=46.82$ $\sigma_M=162.16$ $\tau=20.98$ $\sigma_{max}=208.99$
 Tensioni: $\sigma_N=46.82$ $\sigma_M=-51.18$ $\tau=37.56$ $\tau_{max}=37.56$
 Tensioni: $\sigma_N=46.82$ $\sigma_M=162.16$ $\tau=20.98$ $\sigma_{TD,max}=212.13$

Asta n. 3684 (-3696 -6244) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-2695.78 My,Ed=-46.95 Mz,Ed=95.50
 Resistenze: Nc,Rd=64238.10 My,c,Rd=2116.38 Mz,c,Rd=1670.05 L=21.34
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=4.80$ Ncr,y=17091300.00 $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ Ncr,z=8991230.00 $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.04+0.02+0.05=0.11
 Verifica ZZ: 0.04+0.01+0.05=0.11

- Verifica in termini tensionali [4.2.4] - CC 54 SLU Xl=0.21 - Classe 3
 Sollecitazioni: N=2659.64 T_z=-150.35 M_y=-61.81 T_y=142.29 M_z=151.27 M_x=25.70
 Tensioni: $\sigma_N=139.98$ $\sigma_M=404.98$ $\tau=29.80$ $\sigma_{max}=544.96$
 Tensioni: $\sigma_N=139.98$ $\sigma_M=90.51$ $\tau=50.42$ $\tau_{max}=50.42$
 Tensioni: $\sigma_N=139.98$ $\sigma_M=404.98$ $\tau=29.80$ $\sigma_{TD,max}=547.39$

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.21 - Classe 3
 Sollecitazioni: N=1175.61 T_z=-101.60 M_y=-26.51 T_y=71.03 M_z=70.89 M_x=18.10
 Tensioni: $\sigma_N=61.87$ $\sigma_M=185.87$ $\tau=20.99$ $\sigma_{max}=247.75$
 Tensioni: $\sigma_N=61.87$ $\sigma_M=-125.58$ $\tau=31.31$ $\tau_{max}=31.31$
 Tensioni: $\sigma_N=61.87$ $\sigma_M=185.87$ $\tau=20.99$ $\sigma_{TD,max}=250.40$

Asta n. 3685 (-6238 -6666) Tubo 60x60x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 1
 Sollecitazioni: N,Ed=-1212.00 My,Ed=-2.77
 Resistenze: Nc,Rd=20053.30 My,c,Rd=421.84 L=153.00
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=66.75$ Ncr,y=41677.10 $\lambda^*_y=0.71$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=66.75$ Ncr,z=41677.10 $\lambda^*_z=0.71$ Curva a: $\Phi_z=0.81$ $\chi_z=0.84$
 Kyy, Kyz, Kzy, Kzz=0.98, 0.59, 0.00, 0.98
 Verifica YY: 0.06+0.01=0.07
 Verifica ZZ: 0.06=0.06

- Verifica Freccia massima carichi totali - CC 42
 $f_{z,g}=0.01$ (L/30242)

- Verifica a compressione [4.2.9] - CC 45 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=-1212.00 T_z=7.26 M_x=-10.73
 N,Ed=-1212.00 Nc,Rd=-20053.30 N,Ed/Nc,Rd=0.06

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 49 SLU Xl=0.00
 Sollecitazioni: N=-1117.56 T_z=7.26 M_x=-11.53
 V,Ed=7.26 Vc,Rd,Red=5583.17 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.77 - Classe 3
 Sollecitazioni: N=-645.66 M_y=-2.05 M_x=-5.58
 Tensioni: $\sigma_N=-72.06$ $\sigma_M=-13.09$ $\tau=22.23$ $\sigma_{max}=-85.15$
 Tensioni: $\sigma_N=-72.06$ $\sigma_M=13.09$ $\tau=22.23$ $\tau_{max}=22.23$
 Tensioni: $\sigma_N=-72.06$ $\sigma_M=-13.09$ $\tau=22.23$ $\sigma_{TD,max}=93.45$

Asta n. 3686 (-6246 -6693) Tubo 60x60x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 1
 Sollecitazioni: N,Ed=-1214.62 My,Ed=-2.77
 Resistenze: Nc,Rd=20053.30 My,c,Rd=421.84 L=153.00
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=66.75$ Ncr,y=41677.10 $\lambda^*_y=0.71$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=66.75$ Ncr,z=41677.10 $\lambda^*_z=0.71$ Curva a: $\Phi_z=0.81$ $\chi_z=0.84$
 Kyy, Kyz, Kzy, Kzz=0.98, 0.59, 0.00, 0.98
 Verifica YY: 0.06+0.01=0.07
 Verifica ZZ: 0.06=0.06

- Verifica Freccia massima carichi totali - CC 112

$f_{z,l}=0.01$ (L/30242)

- Verifica a compressione [4.2.9] - CC 45 SLU $X_l=0.00$ - Classe 1
Sollecitazioni: $N=-1214.62$ $T_z=7.26$ $M_x=10.69$
 $N,Ed=-1214.62$ $Nc,Rd=-20053.30$ $N,Ed/Nc,Rd=0.06$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 49 SLU $X_l=0.00$
Sollecitazioni: $N=-1121.77$ $T_z=7.26$ $M_x=11.48$
 $V,Ed=7.26$ $Vc,Rd,Red=5584.09$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.77$ - Classe 3
Sollecitazioni: $N=-579.56$ $M_y=-2.05$ $M_x=5.18$
Tensioni: $\sigma_N=-64.68$ $\sigma_M=-13.09$ $\tau=20.64$ $\sigma_{max}=-77.77$
Tensioni: $\sigma_N=-64.68$ $\sigma_M=13.09$ $\tau=20.64$ $\tau_{max}=20.64$
Tensioni: $\sigma_N=-64.68$ $\sigma_M=-13.09$ $\tau=20.64$ $\sigma_{ID,max}=85.60$

Asta n. 3687 (-2405 -6917) Tubo circolare $d=70 \times 4$ mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 1
Sollecitazioni: $N,Ed=-4183.65$ $M,Ed=3.49$
Resistenze: $Nc,Rd=28041.00$ $M,c,Rd=575.38$ $L=192.27$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, \text{----}, \text{----}$
 $\lambda=82.25$ $Ncr=25411.20$ $\lambda^*=1.08$
Curva a: $\Phi=1.17$ $\chi_{,min}=0.61$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=1.14, \text{----}, \text{----}, \text{----}$
Verifica: $0.24+0.01=0.25$

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.02$ (L/8466)

- Verifica Freccia massima carichi totali - CC 26
 $f_{z,g}=0.02$ (L/10281) $f_{z,l}=0.01$ (L/18319)

- Verifica a compressione [4.2.9] - CC 49 SLU $X_l=0.00$ - Classe 1
Sollecitazioni: $N=-4183.65$ $T=7.26$ $M_x=-4.62$
 $N,Ed=-4183.65$ $Nc,Rd=-28041.00$ $N,Ed/Nc,Rd=0.15$

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 75 SLU $X_l=0.00$
Sollecitazioni: $N=-4147.95$ $T=7.26$ $M_x=-4.76$
 $V,Ed=7.26$ $Vc,Rd,Red=10209.80$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_l=0.96$ - Classe 3
Sollecitazioni: $N=-1837.09$ $M=2.58$ $M_x=-4.09$
Tensioni: $\sigma_N=-221.50$ $\sigma_M=-19.95$ $\tau=15.78$ $\sigma_{max}=-241.45$
Tensioni: $\sigma_N=-221.50$ $\sigma_M=17.28$ $\tau=15.78$ $\tau_{max}=15.78$
Tensioni: $\sigma_N=-221.50$ $\sigma_M=-19.95$ $\tau=15.78$ $\sigma_{ID,max}=243.00$

Asta n. 3688 (-2363 -6915) Tubo circolare $d=70 \times 4$ mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 1
Sollecitazioni: $N,Ed=-4252.80$ $M,Ed=3.50$
Resistenze: $Nc,Rd=28041.00$ $M,c,Rd=575.38$ $L=192.84$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, \text{----}, \text{----}$
 $\lambda=82.49$ $Ncr=25261.50$ $\lambda^*=1.08$
Curva a: $\Phi=1.18$ $\chi_{,min}=0.61$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=1.14, \text{----}, \text{----}, \text{----}$
Verifica: $0.25+0.01=0.26$

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.02$ (L/8421)

- Verifica Freccia massima carichi totali - CC 26
 $f_{z,g}=0.02$ (L/10130) $f_{z,l}=0.01$ (L/18290)

- Verifica a compressione [4.2.9] - CC 49 SLU $X_l=0.00$ - Classe 1
Sollecitazioni: $N=-4252.80$ $T=7.27$ $M_x=4.56$
 $N,Ed=-4252.80$ $Nc,Rd=-28041.00$ $N,Ed/Nc,Rd=0.15$

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 54 SLU $X_l=0.00$
Sollecitazioni: $N=-4243.75$ $T=7.27$ $M_x=4.93$
 $V,Ed=7.27$ $Vc,Rd,Red=10206.30$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_l=0.96$ - Classe 3
Sollecitazioni: $N=-1821.14$ $M=2.59$ $M_x=3.98$
Tensioni: $\sigma_N=-219.58$ $\sigma_M=-20.03$ $\tau=15.38$ $\sigma_{max}=-239.61$
Tensioni: $\sigma_N=-219.58$ $\sigma_M=-18.82$ $\tau=15.38$ $\tau_{max}=15.38$

Tensioni: $\sigma_N = -219.58$ $\sigma_M = -20.03$ $\tau = 15.38$ $\sigma_{ID, \max} = 241.08$

Asta n. 3703 (-2360 -2554) Tubo 60x80x5 mm - S355 Crit. 3

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- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z, G} = 0.01$ (L/3507) $f_{z, L} = 0.00$ (L/23902)
 - Verifica Freccia massima carichi totali - CC 46
 $f_{z, G} = 0.01$ (L/3288) $f_{z, L} = 0.00$ (L/13261)
 - Verifica in termini tensionali [4.2.4] - CC 54 SLU $X1 = 0.00$ - Classe 3
 Sollecitazioni: $N = 1655.11$ $T_z = 119.06$ $M_y = -17.44$ $T_y = 165.24$ $M_z = -76.66$ $M_x = 14.19$
 Tensioni: $\sigma_N = 127.32$ $\sigma_M = 385.23$ $\tau = 34.41$ $\sigma_{\max} = 512.54$
 Tensioni: $\sigma_N = 127.32$ $\sigma_M = 53.97$ $\tau = 67.28$ $\tau_{\max} = 67.28$
 Tensioni: $\sigma_N = 127.32$ $\sigma_M = 385.23$ $\tau = 34.41$ $\sigma_{ID, \max} = 516.00$
 - Verifica a taglio e torsione dir. Y [4.2.25] - CC 49 SLU $X1 = 0.48$
 Sollecitazioni: $N = 1763.00$ $T_z = 164.89$ $M_y = -90.49$ $T_y = 137.69$ $M_x = 11.00$
 $V, Ed = 137.69$ $Vc, Rd, Red = 10727.10$ $V, Ed/Vc, Rd, Red = 0.01$
 - Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed = 164.89$ $Vc, Rd, Red = 14302.80$ $V, Ed/Vc, Rd, Red = 0.01$
 - Verifica in termini tensionali [4.2.4] - CC 9 SND $X1 = 0.00$ - Classe 3
 Sollecitazioni: $N = 866.67$ $T_z = 81.22$ $M_y = -19.23$ $T_y = 72.47$ $M_z = -33.67$ $M_x = 10.30$
 Tensioni: $\sigma_N = 66.67$ $\sigma_M = 210.15$ $\tau = 24.97$ $\sigma_{\max} = 276.82$
 Tensioni: $\sigma_N = 66.67$ $\sigma_M = 59.53$ $\tau = 39.40$ $\tau_{\max} = 39.40$
 Tensioni: $\sigma_N = 66.67$ $\sigma_M = 210.15$ $\tau = 24.97$ $\sigma_{ID, \max} = 280.18$

Asta n. 3703 (-2554 -2879) Tubo 60x100x5 mm - S355 Crit. 3

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- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z, G} = 0.01$ (L/3524)
 - Verifica Freccia massima carichi totali - CC 46
 $f_{z, G} = 0.01$ (L/3327)
 - Verifica in termini tensionali [4.2.4] - CC 75 SLU $X1 = 0.21$ - Classe 3
 Sollecitazioni: $N = 1668.78$ $T_z = 180.20$ $M_y = -133.58$ $T_y = 159.54$ $M_z = 35.11$ $M_x = 10.89$
 Tensioni: $\sigma_N = 111.25$ $\sigma_M = 462.45$ $\tau = 20.84$ $\sigma_{\max} = 573.70$
 Tensioni: $\sigma_N = 111.25$ $\sigma_M = 306.29$ $\tau = 52.10$ $\tau_{\max} = 52.10$
 Tensioni: $\sigma_N = 111.25$ $\sigma_M = 462.45$ $\tau = 20.84$ $\sigma_{ID, \max} = 574.84$
 - Verifica a taglio e torsione dir. Y [4.2.25] - CC 49 SLU $X1 = 0.00$
 Sollecitazioni: $N = 1762.99$ $T_z = 164.91$ $M_y = -90.49$ $T_y = 137.73$ $M_x = 11.00$
 $V, Ed = 137.73$ $Vc, Rd, Red = 10861.90$ $V, Ed/Vc, Rd, Red = 0.01$
 - Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed = 164.91$ $Vc, Rd, Red = 18103.10$ $V, Ed/Vc, Rd, Red = 0.01$
 - Verifica in termini tensionali [4.2.4] - CC 9 SND $X1 = 0.21$ - Classe 3
 Sollecitazioni: $N = 872.97$ $T_z = 77.86$ $M_y = -58.57$ $T_y = 72.91$ $M_z = 16.40$ $M_x = 10.30$
 Tensioni: $\sigma_N = 58.20$ $\sigma_M = 206.26$ $\tau = 19.71$ $\sigma_{\max} = 264.46$
 Tensioni: $\sigma_N = 58.20$ $\sigma_M = 134.31$ $\tau = 33.99$ $\tau_{\max} = 33.99$
 Tensioni: $\sigma_N = 58.20$ $\sigma_M = 206.26$ $\tau = 19.71$ $\sigma_{ID, \max} = 266.65$

Asta n. 3703 (-2879 -3985) Tubo 80x120x5 mm - S355 Crit. 3

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N, Ed = -2032.46$ $M_y, Ed = -107.61$ $M_z, Ed = 45.62$
 Resistenze: $Nc, Rd = 64238.10$ $My, c, Rd = 2116.38$ $Mz, c, Rd = 1670.05$ $L = 21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 4.80$ $Ncr, y = 17091400.00$ $\lambda^*_y = 0.06$ Curva a: $\Phi_y = 0.00$ $\chi_y = 1.00$
 $\lambda_z = 6.62$ $Ncr, z = 8991280.00$ $\lambda^*_z = 0.09$ Curva a: $\Phi_z = 0.00$ $\chi_z = 1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.03 + 0.04 + 0.03 = 0.10$
 Verifica ZZ: $0.03 + 0.03 + 0.03 = 0.09$
 - Verifica in termini tensionali [4.2.4] - CC 75 SLU $X1 = 0.00$ - Classe 3
 Sollecitazioni: $N = 1700.16$ $T_z = -292.59$ $M_y = -118.96$ $T_y = 140.38$ $M_z = 40.99$ $M_x = 10.05$
 Tensioni: $\sigma_N = 89.48$ $\sigma_M = 273.01$ $\tau = 11.65$ $\sigma_{\max} = 362.49$
 Tensioni: $\sigma_N = 89.48$ $\sigma_M = -72.60$ $\tau = 41.37$ $\tau_{\max} = 41.37$
 Tensioni: $\sigma_N = 89.48$ $\sigma_M = 273.01$ $\tau = 11.65$ $\sigma_{ID, \max} = 363.05$
 - Verifica a taglio e torsione dir. Y [4.2.25] - CC 60 SLU $X1 = 0.14$

Sollecitazioni: $N=619.63$ $T_z=-14.33$ $T_y=50.16$ $M_z=24.84$ $M_x=8.35$
 $V,Ed=50.16$ $V_c,Rd,Red=14762.00$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-14.33$ $V_c,Rd,Red=22143.10$ $V,Ed/V_c,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=805.55$ $T_z=-143.13$ $M_y=-52.23$ $T_y=61.33$ $M_z=18.91$ $M_x=9.59$
 Tensioni: $\sigma_N=42.40$ $\sigma_M=121.72$ $\tau=11.11$ $\sigma_{max}=164.11$
 Tensioni: $\sigma_N=42.40$ $\sigma_M=-33.49$ $\tau=25.65$ $\tau_{max}=25.65$
 Tensioni: $\sigma_N=42.40$ $\sigma_M=121.72$ $\tau=11.11$ $\sigma_{ID,max}=165.24$

Asta n. 3703 (-3985 -6670) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-2587.15$ $M_y,Ed=-43.57$ $M_z,Ed=62.52$
 Resistenze: $N_c,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ $N_{cr,y}=17091500.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ $N_{cr,z}=8991320.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.04+0.02+0.04=0.09$
 Verifica ZZ: $0.04+0.01+0.04=0.09$

- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X1=0.21$ - Classe 3
 Sollecitazioni: $N=2930.67$ $T_z=-72.88$ $M_y=-60.05$ $T_y=95.84$ $M_z=102.16$ $M_x=13.20$
 Tensioni: $\sigma_N=154.25$ $\sigma_M=302.76$ $\tau=15.31$ $\sigma_{max}=457.00$
 Tensioni: $\sigma_N=154.25$ $\sigma_M=87.94$ $\tau=29.20$ $\tau_{max}=29.20$
 Tensioni: $\sigma_N=154.25$ $\sigma_M=302.76$ $\tau=15.31$ $\sigma_{ID,max}=457.77$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.21$ - Classe 3
 Sollecitazioni: $N=1340.14$ $T_z=-74.11$ $M_y=-25.23$ $T_y=46.14$ $M_z=45.15$ $M_x=9.65$
 Tensioni: $\sigma_N=70.53$ $\sigma_M=131.71$ $\tau=11.19$ $\sigma_{max}=202.25$
 Tensioni: $\sigma_N=70.53$ $\sigma_M=-79.98$ $\tau=18.72$ $\tau_{max}=18.72$
 Tensioni: $\sigma_N=70.53$ $\sigma_M=131.71$ $\tau=11.19$ $\sigma_{ID,max}=203.17$

Asta n. 3704 (-2361 -2555) Tubo 60x80x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.01$ (L/3513) $f_{z,L}=0.00$ (L/24046)
- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3293) $f_{z,L}=0.00$ (L/13305)
- Verifica in termini tensionali [4.2.4] - CC 75 SLU $X1=0.00$ - Classe 3
 Sollecitazioni: $N=1452.98$ $T_z=126.98$ $M_y=-12.34$ $T_y=-155.89$ $M_z=72.34$ $M_x=-10.82$
 Tensioni: $\sigma_N=111.77$ $\sigma_M=348.93$ $\tau=26.24$ $\sigma_{max}=460.70$
 Tensioni: $\sigma_N=111.77$ $\sigma_M=38.18$ $\tau=57.25$ $\tau_{max}=57.25$
 Tensioni: $\sigma_N=111.77$ $\sigma_M=348.93$ $\tau=26.24$ $\sigma_{ID,max}=462.93$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X1=0.48$
 Sollecitazioni: $N=1446.34$ $T_z=188.04$ $M_y=-97.35$ $T_y=-151.88$ $M_x=-9.01$
 $V,Ed=-151.88$ $V_c,Rd,Red=10754.00$ $V,Ed/V_c,Rd,Red=0.01$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=188.04$ $V_c,Rd,Red=14338.70$ $V,Ed/V_c,Rd,Red=0.01$
- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=854.95$ $T_z=82.19$ $M_y=-23.30$ $T_y=-80.95$ $M_z=37.60$ $M_x=-13.10$
 Tensioni: $\sigma_N=65.77$ $\sigma_M=241.11$ $\tau=31.75$ $\sigma_{max}=306.87$
 Tensioni: $\sigma_N=65.77$ $\sigma_M=72.11$ $\tau=47.86$ $\tau_{max}=47.86$
 Tensioni: $\sigma_N=65.77$ $\sigma_M=241.11$ $\tau=31.75$ $\sigma_{ID,max}=311.76$

Asta n. 3704 (-2555 -2880) Tubo 60x100x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.01$ (L/3524)
- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3327)
- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X1=0.21$ - Classe 3
 Sollecitazioni: $N=1449.34$ $T_z=186.42$ $M_y=-137.31$ $T_y=-151.91$ $M_z=-33.29$ $M_x=-9.01$
 Tensioni: $\sigma_N=96.62$ $\sigma_M=465.61$ $\tau=17.24$ $\sigma_{max}=562.23$
 Tensioni: $\sigma_N=96.62$ $\sigma_M=314.85$ $\tau=47.02$ $\tau_{max}=47.02$

Tensioni: $\sigma_N=96.62$ $\sigma_M=465.61$ $\tau=17.24$ $\sigma_{ID,max}=563.02$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X1=0.00$
 Sollecitazioni: $N=1446.35$ $T_z=188.01$ $M_y=-97.35$ $T_y=-151.91$ $M_x=-9.01$
 $V,Ed=-151.91$ $V_c,Rd,Red=10883.30$ $V,Ed/V_c,Rd,Red=0.01$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=188.01$ $V_c,Rd,Red=18138.80$ $V,Ed/V_c,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.21$ - Classe 3
 Sollecitazioni: $N=861.23$ $T_z=79.09$ $M_y=-58.65$ $T_y=-81.43$ $M_z=-18.32$ $M_x=-13.10$

Tensioni: $\sigma_N=57.42$ $\sigma_M=213.13$ $\tau=25.07$ $\sigma_{max}=270.55$
 Tensioni: $\sigma_N=57.42$ $\sigma_M=134.49$ $\tau=41.01$ $\tau_{max}=41.01$
 Tensioni: $\sigma_N=57.42$ $\sigma_M=213.13$ $\tau=25.07$ $\sigma_{ID,max}=274.01$

Asta n. 3704 (-2880 -3986) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3

Sollecitazioni: $N,Ed=-2112.90$ $M_y,Ed=-105.98$ $M_z,Ed=-44.92$
 Resistenze: $N_c,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=4.80$ $N_{cr,y}=17091400.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ $N_{cr,z}=8991300.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.03+0.04+0.03=0.10$
 Verifica ZZ: $0.03+0.03+0.03=0.09$

- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X1=0.00$ - Classe 3
 Sollecitazioni: $N=1528.20$ $T_z=-298.37$ $M_y=-122.57$ $T_y=-137.84$ $M_z=-38.71$ $M_x=-9.08$

Tensioni: $\sigma_N=80.43$ $\sigma_M=274.17$ $\tau=10.53$ $\sigma_{max}=354.60$
 Tensioni: $\sigma_N=80.43$ $\sigma_M=-68.57$ $\tau=40.84$ $\tau_{max}=40.84$
 Tensioni: $\sigma_N=80.43$ $\sigma_M=274.17$ $\tau=10.53$ $\sigma_{ID,max}=355.07$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 115 SLU $X1=0.00$
 Sollecitazioni: $N=575.18$ $T_z=-3.41$ $T_y=-50.67$ $M_z=-17.00$ $M_x=-7.26$
 $V,Ed=-50.67$ $V_c,Rd,Red=14771.60$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-3.41$ $V_c,Rd,Red=22157.40$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=774.17$ $T_z=-143.86$ $M_y=-52.23$ $T_y=-72.91$ $M_z=-20.79$ $M_x=-12.65$

Tensioni: $\sigma_N=40.75$ $\sigma_M=125.53$ $\tau=14.67$ $\sigma_{max}=166.28$
 Tensioni: $\sigma_N=40.75$ $\sigma_M=-36.83$ $\tau=29.28$ $\tau_{max}=29.28$
 Tensioni: $\sigma_N=40.75$ $\sigma_M=125.53$ $\tau=14.67$ $\sigma_{ID,max}=168.21$

Asta n. 3704 (-3986 -6673) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3

Sollecitazioni: $N,Ed=-2701.78$ $M_y,Ed=-41.78$ $M_z,Ed=-61.81$
 Resistenze: $N_c,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=4.80$ $N_{cr,y}=17091500.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ $N_{cr,z}=8991320.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.04+0.02+0.04=0.09$
 Verifica ZZ: $0.04+0.01+0.04=0.09$

- Verifica in termini tensionali [4.2.4] - CC 75 SLU $X1=0.21$ - Classe 3
 Sollecitazioni: $N=2718.33$ $T_z=-77.02$ $M_y=-58.21$ $T_y=-100.83$ $M_z=-98.24$ $M_x=-9.21$

Tensioni: $\sigma_N=143.07$ $\sigma_M=291.87$ $\tau=10.68$ $\sigma_{max}=434.94$
 Tensioni: $\sigma_N=143.07$ $\sigma_M=85.24$ $\tau=25.30$ $\tau_{max}=25.30$
 Tensioni: $\sigma_N=143.07$ $\sigma_M=291.87$ $\tau=10.68$ $\sigma_{ID,max}=435.33$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=1456.90$ $T_z=-90.87$ $M_y=-39.37$ $T_y=-50.72$ $M_z=-40.02$ $M_x=-11.87$

Tensioni: $\sigma_N=76.68$ $\sigma_M=143.91$ $\tau=13.76$ $\sigma_{max}=220.59$
 Tensioni: $\sigma_N=76.68$ $\sigma_M=-70.89$ $\tau=22.99$ $\tau_{max}=22.99$
 Tensioni: $\sigma_N=76.68$ $\sigma_M=143.91$ $\tau=13.76$ $\sigma_{ID,max}=221.87$

Asta n. 3705 (-6672 -7146) Tubo 60x60x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 1

Sollecitazioni: $N,Ed=-1194.44$ $M_y,Ed=-2.77$
 Resistenze: $N_c,Rd=20053.30$ $M_y,c,Rd=421.84$ $L=153.00$

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=66.75$ Ncr,y=41677.00 $\lambda_y^*=0.71$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=66.75$ Ncr,z=41677.00 $\lambda_z^*=0.71$ Curva a: $\Phi_z=0.81$ $\chi_z=0.84$
 Kyy, Kyz, Kzy, Kzz=0.98, 0.59, 0.00, 0.98
 Verifica YY: 0.06+0.01=0.07
 Verifica ZZ: 0.06=0.06

- Verifica Freccia massima carichi totali - CC 26
 $f_{z,6}=0.01$ (L/30242)
- Verifica a compressione [4.2.9] - CC 45 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=-1194.44 $T_z=7.26$ $M_x=11.36$
 N,Ed=-1194.44 Nc,Rd=-20053.30 N,Ed/Nc,Rd=0.06
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 49 SLU Xl=1.53
 Sollecitazioni: N=-1098.62 $T_z=-7.26$ $M_x=12.32$
 V,Ed=-7.26 Vc,Rd,Red=5569.08 V,Ed/Vc,Rd,Red=0.00
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.76 - Classe 3
 Sollecitazioni: N=-536.64 $M_y=-2.05$ $M_x=5.90$
 Tensioni: $\sigma_N=-59.89$ $\sigma_M=-13.09$ $\tau=23.50$ $\sigma_{max}=-72.98$
 Tensioni: $\sigma_N=-59.89$ $\sigma_M=13.09$ $\tau=23.50$ $\tau_{max}=23.50$
 Tensioni: $\sigma_N=-59.89$ $\sigma_M=-13.09$ $\tau=23.50$ $\sigma_{ID,max}=83.57$

Asta n. 3706 (-6689 -7130) Tubo 60x60x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 1
 Sollecitazioni: N,Ed=-1195.91 $M_y,Ed=-2.77$
 Resistenze: Nc,Rd=20053.30 $M_y,c,Rd=421.84$ L=153.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=66.75$ Ncr,y=41677.00 $\lambda_y^*=0.71$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=66.75$ Ncr,z=41677.00 $\lambda_z^*=0.71$ Curva a: $\Phi_z=0.81$ $\chi_z=0.84$
 Kyy, Kyz, Kzy, Kzz=0.98, 0.59, 0.00, 0.98
 Verifica YY: 0.06+0.01=0.07
 Verifica ZZ: 0.06=0.06
- Verifica Freccia massima carichi totali - CC 42
 $f_{z,L}=0.01$ (L/29960)
- Verifica a compressione [4.2.9] - CC 45 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=-1195.91 $T_z=7.26$ $M_x=-11.34$
 N,Ed=-1195.91 Nc,Rd=-20053.30 N,Ed/Nc,Rd=0.06
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 49 SLU Xl=1.53
 Sollecitazioni: N=-1100.88 $T_z=-7.26$ $M_x=-12.30$
 V,Ed=-7.26 Vc,Rd,Red=5569.50 V,Ed/Vc,Rd,Red=0.00
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.76 - Classe 3
 Sollecitazioni: N=-601.98 $M_y=-2.05$ $M_x=-6.39$
 Tensioni: $\sigma_N=-67.19$ $\sigma_M=-13.09$ $\tau=25.46$ $\sigma_{max}=-80.28$
 Tensioni: $\sigma_N=-67.19$ $\sigma_M=13.09$ $\tau=25.46$ $\tau_{max}=25.46$
 Tensioni: $\sigma_N=-67.19$ $\sigma_M=-13.09$ $\tau=25.46$ $\sigma_{ID,max}=91.59$

Asta n. 3707 (-2360 -7263) Tubo circolare d=70x4 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 1
 Sollecitazioni: N,Ed=-2387.53 M,Ed=3.00
 Resistenze: Nc,Rd=28041.00 M,c,Rd=575.38 L=181.75
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, ----, ----$
 $\lambda=77.74$ Ncr=28440.60 $\lambda^*=1.02$
 Curva a: $\Phi=1.10$ $\chi_{min}=0.65$
 Kyy, Kyz, Kzy, Kzz=1.05, ----, ----, ----
 Verifica: 0.13+0.01=0.14
- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,6}=0.03$ (L/7054)
- Verifica Freccia massima carichi totali - CC 46
 $f_{z,6}=0.02$ (L/8191) $f_{z,L}=0.01$ (L/22673)
- Verifica a compressione [4.2.9] - CC 49 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=-2387.53 T=6.60 $M_x=6.56$
 N,Ed=-2387.53 Nc,Rd=-28041.00 N,Ed/Nc,Rd=0.09
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 54 SLU Xl=0.00
 Sollecitazioni: N=-2205.14 T=6.60 $M_x=7.45$

V,Ed=6.60 Vc,Rd,Red=10154.90 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.91 - Classe 3
Sollecitazioni: N=-1226.53 M=2.22 M_x=5.15
Tensioni: $\sigma_N=-147.88$ $\sigma_M=-17.15$ $\tau=19.89$ $\sigma_{max}=-165.03$
Tensioni: $\sigma_N=-147.88$ $\sigma_M=-0.00$ $\tau=19.89$ $\tau_{max}=19.89$
Tensioni: $\sigma_N=-147.88$ $\sigma_M=-17.15$ $\tau=19.89$ $\sigma_{ID,max}=168.59$

Asta n. 3708 (-2361 -7265) Tubo circolare d=70x4 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 1
Sollecitazioni: N,Ed=-2412.92 M,Ed=3.00
Resistenze: Nc,Rd=28041.00 M,c,Rd=575.38 L=181.75
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, \text{----}, \text{----}$
 $\lambda=77.74$ Ncr=28440.60 $\lambda'=1.02$
Curva a: $\Phi=1.10$ $\chi_{min}=0.65$
Kyy, Kyz, Kzy, Kzz=1.05, ----, ----, ----
Verifica: 0.13+0.01=0.14
- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.03$ (L/7080)
- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.02$ (L/8245) $f_{z,L}=0.01$ (L/22407)

- Verifica a compressione [4.2.9] - CC 49 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=-2412.92 T=6.60 M_x=-6.58
N,Ed=-2412.92 Nc,Rd=-28041.00 N,Ed/Nc,Rd=0.09

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 75 SLU Xl=0.00
Sollecitazioni: N=-2245.38 T=6.60 M_x=-6.92
V,Ed=6.60 Vc,Rd,Red=10165.90 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.91 - Classe 3
Sollecitazioni: N=-1235.98 M=2.22 M_x=-5.51
Tensioni: $\sigma_N=-149.02$ $\sigma_M=-17.15$ $\tau=21.29$ $\sigma_{max}=-166.17$
Tensioni: $\sigma_N=-149.02$ $\sigma_M=-16.11$ $\tau=21.29$ $\tau_{max}=21.29$
Tensioni: $\sigma_N=-149.02$ $\sigma_M=-17.15$ $\tau=21.29$ $\sigma_{ID,max}=170.21$

Asta n. 3723 (-2356 -2562) Tubo 60x80x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 75 SLU - Classe 3
Sollecitazioni: N,Ed=-119.89 My,Ed=-41.61 Mz,Ed=-35.75
Resistenze: Nc,Rd=43952.40 My,c,Rd=955.82 Mz,c,Rd=801.10 L=52.54
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=17.81$ Ncr,y=849037.00 $\lambda'_y=0.23$ Curva a: $\Phi_y=0.53$ $\chi_y=0.99$
 $\lambda_z=22.47$ Ncr,z=533698.00 $\lambda'_z=0.29$ Curva a: $\Phi_z=0.55$ $\chi_z=0.98$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.03+0.04=0.08
Verifica ZZ: 0.00+0.03+0.04=0.07

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.01$ (L/3660) $f_{z,L}=0.00$ (L/31708)

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3594) $f_{z,L}=0.00$ (L/20789)

- Verifica in termini tensionali [4.2.4] - CC 54 SLU Xl=0.00 - Classe 3
Sollecitazioni: N=2.15 T_z=2.26 M_y=-18.86 T_y=79.03 M_z=-35.51 M_x=5.92
Tensioni: $\sigma_N=0.17$ $\sigma_M=216.57$ $\tau=14.35$ $\sigma_{max}=216.74$
Tensioni: $\sigma_N=0.17$ $\sigma_M=58.36$ $\tau=30.05$ $\tau_{max}=30.05$
Tensioni: $\sigma_N=0.17$ $\sigma_M=216.57$ $\tau=14.35$ $\sigma_{ID,max}=218.16$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 53 SLU Xl=0.43
Sollecitazioni: N=98.43 T_z=-33.43 M_y=-5.63 T_y=62.21 M_x=5.60
V,Ed=62.21 Vc,Rd,Red=10800.10 V,Ed/Vc,Rd,Red=0.01

- Verifica a taglio e torsione dir. Z [4.2.25]
V,Ed=-33.43 Vc,Rd,Red=14400.20 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-591.56 T_z=59.22 M_y=-23.11 T_y=35.35 M_z=-16.55 M_x=4.59
Tensioni: $\sigma_N=-45.50$ $\sigma_M=-151.58$ $\tau=11.13$ $\sigma_{max}=-197.09$
Tensioni: $\sigma_N=-45.50$ $\sigma_M=-58.21$ $\tau=20.24$ $\tau_{max}=20.24$
Tensioni: $\sigma_N=-45.50$ $\sigma_M=-151.58$ $\tau=11.13$ $\sigma_{ID,max}=198.03$

Asta n. 3723 (-2562 -2965) Tubo 60x100x5 mm - S355 Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 75 SLU - Classe 3
 Sollecitazioni: N,Ed=-113.49 My,Ed=-53.23 Mz,Ed=21.75
 Resistenze: Nc,Rd=50714.30 My,c,Rd=1327.02 Mz,c,Rd=972.02 L=21.34
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=5.90$ Ncr,y=8930630.00 $\lambda^*_y=0.08$ Curva a: $\Phi_y=0.00 \chi_y=1.00$
 $\lambda_z=8.90$ Ncr,z=3924920.00 $\lambda^*_z=0.12$ Curva a: $\Phi_z=0.00 \chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.03+0.02=0.05
 Verifica ZZ: 0.00+0.02+0.02=0.05

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.01$ (L/3653)

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3594)

- Verifica in termini tensionali [4.2.4] - CC 75 SLU Xl=0.21 - Classe 3
 Sollecitazioni: N=-110.49 Tz=53.62 My=-53.23 Ty=77.83 Mz=21.75 Mx=4.60
 Tensioni: $\sigma_N=-7.37 \sigma_M=-211.28 \tau=8.80 \sigma_{max}=-218.64$
 Tensioni: $\sigma_N=-7.37 \sigma_M=122.05 \tau=24.04 \tau_{max}=24.04$
 Tensioni: $\sigma_N=-7.37 \sigma_M=-211.28 \tau=8.80 \sigma_{ID,max}=219.18$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 53 SLU Xl=0.06
 Sollecitazioni: N=100.33 Tz=-34.44 Ty=62.20 Mz=8.77 Mx=5.60
 V,Ed=62.20 Vc,Rd,Red=10920.00 V,Ed/Vc,Rd,Red=0.01

- Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=-34.44 Vc,Rd,Red=18200.10 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.21 - Classe 3
 Sollecitazioni: N=-584.01 Tz=55.96 My=-38.12 Ty=34.29 Mz=9.46 Mx=4.59
 Tensioni: $\sigma_N=-38.93 \sigma_M=-130.00 \tau=8.79 \sigma_{max}=-168.94$
 Tensioni: $\sigma_N=-38.93 \sigma_M=27.41 \tau=15.75 \tau_{max}=15.75$
 Tensioni: $\sigma_N=-38.93 \sigma_M=-130.00 \tau=8.79 \sigma_{ID,max}=169.62$

Asta n. 3723 (-2965 -4251) Tubo 80x120x5 mm - S355 Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-3020.88 My,Ed=-54.48 Mz,Ed=24.83
 Resistenze: Nc,Rd=64238.10 My,c,Rd=2116.38 Mz,c,Rd=1670.05 L=21.34
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ Ncr,y=17091500.00 $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00 \chi_y=1.00$
 $\lambda_z=6.62$ Ncr,z=8991360.00 $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00 \chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.05+0.02+0.01=0.08
 Verifica ZZ: 0.05+0.02+0.01=0.08

- Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-3020.88 Tz=-370.32 My=-54.48 Ty=51.86 Mz=13.77 Mx=4.38
 Tensioni: $\sigma_N=-158.99 \sigma_M=-114.89 \tau=5.08 \sigma_{max}=-273.89$
 Tensioni: $\sigma_N=-158.99 \sigma_M=-24.38 \tau=42.68 \tau_{max}=42.68$
 Tensioni: $\sigma_N=-158.99 \sigma_M=-114.89 \tau=5.08 \sigma_{ID,max}=274.03$

- Verifica a taglio dir. Y [4.2.16] - CC 68 SLU Xl=0.21
 Sollecitazioni: N=259.85 Tz=45.44 Ty=32.01 Mz=22.69
 V,Ed=32.01 Vc,Rd=14835.60 V,Ed/Vc,Rd=0.00

- Verifica a taglio dir. Z [4.2.16]
 V,Ed=45.44 Vc,Rd=22253.40 V,Ed/Vc,Rd=0.00

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=525.02 Tz=-101.22 My=-33.73 Ty=28.96 Mz=10.91 Mx=4.26
 Tensioni: $\sigma_N=27.63 \sigma_M=75.97 \tau=4.94 \sigma_{max}=103.61$
 Tensioni: $\sigma_N=27.63 \sigma_M=-19.33 \tau=15.21 \tau_{max}=15.21$
 Tensioni: $\sigma_N=27.63 \sigma_M=75.97 \tau=4.94 \sigma_{ID,max}=103.96$

Asta n. 3723 (-4251 -7136) Tubo 80x120x5 mm - S355 Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-3206.23 My,Ed=-22.56 Mz,Ed=31.36
 Resistenze: Nc,Rd=64238.10 My,c,Rd=2116.38 Mz,c,Rd=1670.05 L=21.34
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ Ncr,y=17091300.00 $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00 \chi_y=1.00$

$\lambda_z=6.62$ Ncr, z=8991240.00 $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.05+0.01+0.02=0.08
 Verifica ZZ: 0.05+0.01+0.02=0.07

- Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.21 - Classe 3
 Sollecitazioni: N=-3202.49 Tz=99.06 My=-22.56 Ty=23.82 Mz=31.36 Mx=4.35
 Tensioni: $\sigma_N=-168.55$ $\sigma_M=-99.54$ $\tau=5.04$ $\sigma_{max}=-268.09$
 Tensioni: $\sigma_N=-168.55$ $\sigma_M=55.56$ $\tau=15.10$ $\tau_{max}=15.10$
 Tensioni: $\sigma_N=-168.55$ $\sigma_M=-99.54$ $\tau=5.04$ $\sigma_{ID,max}=268.24$
- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=986.53 Tz=-60.13 My=-24.50 Ty=20.28 Mz=18.32 Mx=4.30
 Tensioni: $\sigma_N=51.92$ $\sigma_M=76.21$ $\tau=4.98$ $\sigma_{max}=128.14$
 Tensioni: $\sigma_N=51.92$ $\sigma_M=-32.44$ $\tau=11.09$ $\tau_{max}=11.09$
 Tensioni: $\sigma_N=51.92$ $\sigma_M=76.21$ $\tau=4.98$ $\sigma_{ID,max}=128.43$

Asta n. 3724 (-2357 -2563) Tubo 60x80x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 54 SLU - Classe 3
 Sollecitazioni: N,Ed=-181.10 My,Ed=-44.55 Mz,Ed=35.27
 Resistenze: Nc,Rd=43952.40 My,c,Rd=955.82 Mz,c,Rd=801.10 L=52.54
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=17.81$ Ncr, y=849037.00 $\lambda^*_y=0.23$ Curva a: $\Phi_y=0.53$ $\chi_y=0.99$
 $\lambda_z=22.47$ Ncr, z=533698.00 $\lambda^*_z=0.29$ Curva a: $\Phi_z=0.55$ $\chi_z=0.98$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.04+0.04=0.08
 Verifica ZZ: 0.00+0.03+0.04=0.07

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.01$ (L/3654) $f_{z,L}=0.00$ (L/32407)

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3583) $f_{z,L}=0.00$ (L/21395)

- Verifica in termini tensionali [4.2.4] - CC 89 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-106.36 Tz=-1.92 My=-26.22 Ty=-60.89 Mz=27.91 Mx=-7.09
 Tensioni: $\sigma_N=-8.18$ $\sigma_M=-210.56$ $\tau=17.20$ $\sigma_{max}=-218.74$
 Tensioni: $\sigma_N=-8.18$ $\sigma_M=81.16$ $\tau=29.30$ $\tau_{max}=29.30$
 Tensioni: $\sigma_N=-8.18$ $\sigma_M=-210.56$ $\tau=17.20$ $\sigma_{ID,max}=220.76$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU Xl=0.48
 Sollecitazioni: N=-149.96 Tz=14.01 My=-32.33 Ty=-60.35 Mx=-6.62
 V,Ed=-60.35 Vc,Rd,Red=10786.30 V,Ed/Vc,Rd,Red=0.01

- Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=14.01 Vc,Rd,Red=14381.70 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-661.23 Tz=61.92 My=-28.58 Ty=-36.60 Mz=17.01 Mx=-4.12
 Tensioni: $\sigma_N=-50.86$ $\sigma_M=-172.90$ $\tau=9.98$ $\sigma_{max}=-223.76$
 Tensioni: $\sigma_N=-50.86$ $\sigma_M=-59.83$ $\tau=19.51$ $\tau_{max}=19.51$
 Tensioni: $\sigma_N=-50.86$ $\sigma_M=-172.90$ $\tau=9.98$ $\sigma_{ID,max}=224.43$

Asta n. 3724 (-2563 -2966) Tubo 60x100x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 54 SLU - Classe 3
 Sollecitazioni: N,Ed=-174.70 My,Ed=-58.52 Mz,Ed=-20.93
 Resistenze: Nc,Rd=50714.30 My,c,Rd=1327.02 Mz,c,Rd=972.02 L=21.34
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=5.90$ Ncr, y=8930640.00 $\lambda^*_y=0.08$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=8.90$ Ncr, z=3924930.00 $\lambda^*_z=0.12$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.03+0.02=0.06
 Verifica ZZ: 0.00+0.03+0.02=0.05

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.01$ (L/3653)

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3566)

- Verifica in termini tensionali [4.2.4] - CC 54 SLU Xl=0.21 - Classe 3
 Sollecitazioni: N=-171.70 Tz=64.67 My=-58.52 Ty=-76.07 Mz=-20.93 Mx=-3.72
 Tensioni: $\sigma_N=-11.45$ $\sigma_M=-221.90$ $\tau=7.13$ $\sigma_{max}=-233.35$

Tensioni: $\sigma_N=-11.45$ $\sigma_M=134.18$ $\tau=22.02$ $\tau_{max}=22.02$
 Tensioni: $\sigma_N=-11.45$ $\sigma_M=-221.90$ $\tau=7.13$ $\sigma_{ID,max}=233.68$

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.21 - Classe 3
 Sollecitazioni: $N=-653.49$ $T_z=58.36$ $M_y=-34.06$ $T_y=-35.74$ $M_z=-9.89$ $M_x=-4.12$
 Tensioni: $\sigma_N=-43.57$ $\sigma_M=-121.19$ $\tau=7.88$ $\sigma_{max}=-164.75$
 Tensioni: $\sigma_N=-43.57$ $\sigma_M=28.67$ $\tau=15.14$ $\tau_{max}=15.14$
 Tensioni: $\sigma_N=-43.57$ $\sigma_M=-121.19$ $\tau=7.88$ $\sigma_{ID,max}=165.32$

Asta n. 3724 (-2966 -4252) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-3030.23$ $M_y,Ed=-54.36$ $M_z,Ed=-24.67$
 Resistenze: $N_c,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ $Ncr,y=17091500.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ $Ncr,z=8991330.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.05+0.02+0.01=0.08$
 Verifica ZZ: $0.05+0.02+0.01=0.08$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.00 - Classe 3
 Sollecitazioni: $N=-3030.23$ $T_z=-369.42$ $M_y=-54.36$ $T_y=-51.95$ $M_z=-13.58$ $M_x=-4.53$
 Tensioni: $\sigma_N=-159.49$ $\sigma_M=-114.33$ $\tau=5.25$ $\sigma_{max}=-273.82$
 Tensioni: $\sigma_N=-159.49$ $\sigma_M=-24.06$ $\tau=42.76$ $\tau_{max}=42.76$
 Tensioni: $\sigma_N=-159.49$ $\sigma_M=-114.33$ $\tau=5.25$ $\sigma_{ID,max}=273.97$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 89 SLU Xl=0.21
 Sollecitazioni: $N=284.46$ $T_z=-95.54$ $T_y=-52.35$ $M_z=-29.97$ $M_x=-6.88$
 $V,Ed=-52.35$ $V_c,Rd,Red=14774.90$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-95.54$ $V_c,Rd,Red=22162.40$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
 Sollecitazioni: $N=519.90$ $T_z=-89.00$ $M_y=-30.18$ $T_y=-30.10$ $M_z=-11.38$ $M_x=-3.97$
 Tensioni: $\sigma_N=27.36$ $\sigma_M=71.24$ $\tau=4.60$ $\sigma_{max}=98.61$
 Tensioni: $\sigma_N=27.36$ $\sigma_M=-20.16$ $\tau=13.64$ $\tau_{max}=13.64$
 Tensioni: $\sigma_N=27.36$ $\sigma_M=71.24$ $\tau=4.60$ $\sigma_{ID,max}=98.93$

Asta n. 3724 (-4252 -7140) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-3266.13$ $M_y,Ed=-22.49$ $M_z,Ed=-31.46$
 Resistenze: $N_c,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ $Ncr,y=17091400.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ $Ncr,z=8991280.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.05+0.01+0.02=0.08$
 Verifica ZZ: $0.05+0.01+0.02=0.08$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.21 - Classe 3
 Sollecitazioni: $N=-3262.33$ $T_z=97.11$ $M_y=-22.49$ $T_y=-25.78$ $M_z=-31.46$ $M_x=-4.02$
 Tensioni: $\sigma_N=-171.70$ $\sigma_M=-99.63$ $\tau=4.67$ $\sigma_{max}=-271.33$
 Tensioni: $\sigma_N=-171.70$ $\sigma_M=55.74$ $\tau=14.53$ $\tau_{max}=14.53$
 Tensioni: $\sigma_N=-171.70$ $\sigma_M=-99.63$ $\tau=4.67$ $\sigma_{ID,max}=271.45$

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
 Sollecitazioni: $N=1112.95$ $T_z=-73.01$ $M_y=-24.84$ $T_y=-22.93$ $M_z=-18.75$ $M_x=-3.69$
 Tensioni: $\sigma_N=58.58$ $\sigma_M=77.64$ $\tau=4.27$ $\sigma_{max}=136.22$
 Tensioni: $\sigma_N=58.58$ $\sigma_M=-33.22$ $\tau=11.69$ $\tau_{max}=11.69$
 Tensioni: $\sigma_N=58.58$ $\sigma_M=77.64$ $\tau=4.27$ $\sigma_{ID,max}=136.42$

Asta n. 3725 (-7137 -7492) Tubo 60x60x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 1
 Sollecitazioni: $N,Ed=-1137.33$ $M_y,Ed=-2.77$
 Resistenze: $N_c,Rd=20053.30$ $M_y,c,Rd=421.84$ $L=153.00$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=66.75$ $Ncr,y=41677.10$ $\lambda^*_y=0.71$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=66.75$ $Ncr,z=41677.10$ $\lambda^*_z=0.71$ Curva a: $\Phi_z=0.81$ $\chi_z=0.84$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.98, 0.59, 0.00, 0.98$
 Verifica YY: $0.06+0.01=0.06$

Verifica ZZ: 0.06=0.06

- Verifica Freccia massima carichi totali - CC 62
 $f_{z,g}=0.01$ (L/29410)
- Verifica a compressione [4.2.9] - CC 45 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $N=-1137.33$ $T_z=7.26$ $M_x=-11.52$
 $N,Ed=-1137.33$ $N_c,Rd=-20053.30$ $N,Ed/N_c,Rd=0.06$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 49 SLU $X_l=0.00$
 Sollecitazioni: $N=-1031.01$ $T_z=7.26$ $M_x=-12.55$
 $V,Ed=7.26$ $V_c,Rd,Red=5564.90$ $V,Ed/V_c,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.77$ - Classe 3
 Sollecitazioni: $N=-513.46$ $M_y=-2.05$ $M_x=-6.57$
 Tensioni: $\sigma_N=-57.31$ $\sigma_M=-13.09$ $\tau=26.20$ $\sigma_{max}=-70.40$
 Tensioni: $\sigma_N=-57.31$ $\sigma_M=13.09$ $\tau=26.20$ $\tau_{max}=26.20$
 Tensioni: $\sigma_N=-57.31$ $\sigma_M=-13.09$ $\tau=26.20$ $\sigma_{TD,max}=83.76$

Asta n. 3726 (-7139 -7508) Tubo 60x60x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 1
 Sollecitazioni: $N,Ed=-1138.08$ $M_y,Ed=-2.77$
 Resistenze: $N_c,Rd=20053.30$ $M_y,c,Rd=421.84$ $L=153.00$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=66.75$ $N_{cr,y}=41677.10$ $\lambda_y^*=0.71$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=66.75$ $N_{cr,z}=41677.10$ $\lambda_z^*=0.71$ Curva a: $\Phi_z=0.81$ $\chi_z=0.84$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.98, 0.59, 0.00, 0.98$
 Verifica YY: 0.06+0.01=0.06
 Verifica ZZ: 0.06=0.06

- Verifica Freccia massima carichi totali - CC 55
 $f_{z,L}=0.01$ (L/29410)
- Verifica a compressione [4.2.9] - CC 45 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $N=-1138.08$ $T_z=7.26$ $M_x=11.52$
 $N,Ed=-1138.08$ $N_c,Rd=-20053.30$ $N,Ed/N_c,Rd=0.06$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 49 SLU $X_l=0.00$
 Sollecitazioni: $N=-1032.11$ $T_z=7.26$ $M_x=12.55$
 $V,Ed=7.26$ $V_c,Rd,Red=5564.90$ $V,Ed/V_c,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_l=0.77$ - Classe 3
 Sollecitazioni: $N=-385.12$ $M_y=-2.05$ $M_x=8.10$
 Tensioni: $\sigma_N=-42.98$ $\sigma_M=-13.09$ $\tau=32.29$ $\sigma_{max}=-56.07$
 Tensioni: $\sigma_N=-42.98$ $\sigma_M=13.09$ $\tau=32.29$ $\tau_{max}=32.29$
 Tensioni: $\sigma_N=-42.98$ $\sigma_M=-13.09$ $\tau=32.29$ $\sigma_{TD,max}=79.20$

Asta n. 3727 (-2356 -4104) Tubo circolare d=70x4 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
 Sollecitazioni: $N,Ed=-782.16$ $M,Ed=1.45$
 Resistenze: $N_c,Rd=28041.00$ $M,c,Rd=437.84$ $L=147.13$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, ----, ----$
 $\lambda=62.93$ $N_{cr}=43400.20$ $\lambda^*=0.82$
 Curva a: $\Phi=0.90$ $\chi_{min}=0.78$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.97, ----, ----, ----$
 Verifica: 0.03+0.00=0.03

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.02$ (L/6316)
- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.02$ (L/6342) $f_{z,L}=0.00$ (L/43416)
- Verifica a compressione [4.2.9] - CC 45 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $N=-639.04$ $T=5.34$ $M_x=-1.97$
 $N,Ed=-639.04$ $N_c,Rd=-28041.00$ $N,Ed/N_c,Rd=0.02$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 75 SLU $X_l=0.00$
 Sollecitazioni: $N=-195.15$ $T=5.34$ $M_x=-2.36$
 $V,Ed=5.34$ $V_c,Rd,Red=10258.70$ $V,Ed/V_c,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_l=0.73$ - Classe 3
 Sollecitazioni: $N=-779.47$ $M=1.45$ $M_x=-1.29$
 Tensioni: $\sigma_N=-93.98$ $\sigma_M=-11.23$ $\tau=4.97$ $\sigma_{max}=-105.21$

Tensioni: $\sigma_N=-93.98$ $\sigma_M=11.06$ $\tau=4.97$ $\tau_{max}=4.97$
 Tensioni: $\sigma_N=-93.98$ $\sigma_M=-11.23$ $\tau=4.97$ $\sigma_{ID,max}=105.56$

Asta n. 3728 (-2357 -4105) Tubo circolare d=70x4 mm - S355 Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3

Sollecitazioni: N,Ed=-854.15 M,Ed=1.45
 Resistenze: Nc,Rd=28041.00 M,c,Rd=437.84 L=147.13

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, \text{----}, \text{----}$

$\lambda=62.93$ Ncr=43400.20 $\lambda^*=0.82$

Curva a: $\Phi=0.90$ $\chi_{,min}=0.78$

Kyy, Kyz, Kzy, Kzz=0.97, ----, ----, ----

Verifica: 0.03+0.00=0.03

- Verifica Freccia massima per soli carichi accidentali - CC 46

$f_{z,g}=0.02$ (L/6303)

- Verifica Freccia massima carichi totali - CC 46

$f_{z,g}=0.02$ (L/6342) $f_{z,L}=0.00$ (L/42226)

- Verifica a compressione [4.2.9] - CC 45 SLU Xl=0.00 - Classe 1

Sollecitazioni: N=-635.71 T=5.34 $M_x=1.96$

N,Ed=-635.71 Nc,Rd=-28041.00 N,Ed/Nc,Rd=0.02

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 54 SLU Xl=0.00

Sollecitazioni: N=-158.63 T=5.34 $M_x=2.56$

V,Ed=5.34 Vc,Rd,Red=10254.60 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.73 - Classe 3

Sollecitazioni: N=-851.47 M=1.45 $M_x=1.31$

Tensioni: $\sigma_N=-102.66$ $\sigma_M=-11.23$ $\tau=5.07$ $\sigma_{max}=-113.89$

Tensioni: $\sigma_N=-102.66$ $\sigma_M=9.73$ $\tau=5.07$ $\tau_{max}=5.07$

Tensioni: $\sigma_N=-102.66$ $\sigma_M=-11.23$ $\tau=5.07$ $\sigma_{ID,max}=114.23$

Asta n. 3739 (-2352 -2589) Tubo 60x80x5 mm - S355 Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 75 SLU - Classe 3

Sollecitazioni: N,Ed=-1873.91 My,Ed=-28.89 Mz,Ed=10.30

Resistenze: Nc,Rd=43952.40 My,c,Rd=955.82 Mz,c,Rd=801.10 L=56.32

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=19.09$ Ncr,y=739023.00 $\lambda^*_y=0.25$ Curva a: $\Phi_y=0.54$ $\chi_y=0.99$

$\lambda_z=24.08$ Ncr,z=464545.00 $\lambda^*_z=0.32$ Curva a: $\Phi_z=0.56$ $\chi_z=0.97$

Kyy, Kyz, Kzy, Kzz=0.96, 0.96, 0.76, 0.96

Verifica YY: 0.04+0.02+0.01=0.08

Verifica ZZ: 0.04+0.02+0.01=0.07

- Verifica Freccia massima per soli carichi accidentali - CC 46

$f_{z,g}=0.01$ (L/3853) $f_{z,L}=0.00$ (L/36907)

- Verifica Freccia massima carichi totali - CC 46

$f_{z,g}=0.01$ (L/4044) $f_{z,L}=0.00$ (L/31494)

- Verifica in termini tensionali [4.2.4] - CC 75 SLU Xl=0.00 - Classe 3

Sollecitazioni: N=-1873.91 Tz=-95.28 My=-28.89 Ty=-23.54 Mz=10.30 $M_x=-3.19$

Tensioni: $\sigma_N=-144.15$ $\sigma_M=-145.64$ $\tau=7.73$ $\sigma_{max}=-289.79$

Tensioni: $\sigma_N=-144.15$ $\sigma_M=36.22$ $\tau=22.37$ $\tau_{max}=22.37$

Tensioni: $\sigma_N=-144.15$ $\sigma_M=-145.64$ $\tau=7.73$ $\sigma_{ID,max}=290.10$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 75 SLU Xl=0.46

Sollecitazioni: N=-1868.30 Tz=-98.25 My=15.70 Ty=-23.54 $M_x=-3.19$

V,Ed=-23.54 Vc,Rd,Red=10832.60 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]

V,Ed=-98.25 Vc,Rd,Red=14443.50 V,Ed/Vc,Rd,Red=0.01

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3

Sollecitazioni: N=-1119.56 Tz=-61.52 My=-26.79 Ty=-31.99 Mz=14.66 $M_x=-6.74$

Tensioni: $\sigma_N=-86.12$ $\sigma_M=-156.63$ $\tau=16.34$ $\sigma_{max}=-242.75$

Tensioni: $\sigma_N=-86.12$ $\sigma_M=51.56$ $\tau=25.80$ $\tau_{max}=25.80$

Tensioni: $\sigma_N=-86.12$ $\sigma_M=-156.63$ $\tau=16.34$ $\sigma_{ID,max}=244.39$

Asta n. 3739 (-2589 -3065) Tubo 60x100x5 mm - S355 Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 75 SLU - Classe 3

Sollecitazioni: N,Ed=-1867.05 My,Ed=47.07 Mz,Ed=-7.99

Resistenze: Nc,Rd=50714.30 My,c,Rd=1327.02 Mz,c,Rd=972.02 L=21.34

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=5.90$ Ncr,y=8930630.00 $\lambda^*_y=0.08$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=8.90$ Ncr,z=3924920.00 $\lambda^*_z=0.12$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.04+0.03+0.01=0.07
 Verifica ZZ: 0.04+0.02+0.01=0.07

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.01$ (L/3841)
- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3996)
- Verifica in termini tensionali [4.2.4] - CC 75 SLU Xl=0.21 - Classe 3
 Sollecitazioni: N=-1864.06 $T_z=-100.52$ $M_y=47.07$ $T_y=-23.58$ $M_z=-7.99$ $M_x=-3.19$
 Tensioni: $\sigma_N=-124.27$ $\sigma_M=-147.74$ $\tau=6.10$ $\sigma_{max}=-272.01$
 Tensioni: $\sigma_N=-124.27$ $\sigma_M=-23.17$ $\tau=18.59$ $\tau_{max}=18.59$
 Tensioni: $\sigma_N=-124.27$ $\sigma_M=-147.74$ $\tau=6.10$ $\sigma_{ID,max}=272.22$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 68 SLU Xl=0.21
 Sollecitazioni: N=-1360.46 $T_z=-43.98$ $T_y=-13.12$ $M_z=-3.72$ $M_x=-1.42$
 $V_{,Ed}=-13.12$ $V_{c,Rd,Red}=10965.00$ $V_{,Ed/Vc,Rd,Red}=0.00$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V_{,Ed}=-43.98$ $V_{c,Rd,Red}=18275.00$ $V_{,Ed/Vc,Rd,Red}=0.00$
- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.21 - Classe 3
 Sollecitazioni: N=-1111.38 $T_z=-65.89$ $M_y=26.85$ $T_y=-30.75$ $M_z=-9.93$ $M_x=-6.74$
 Tensioni: $\sigma_N=-74.09$ $\sigma_M=-102.93$ $\tau=12.90$ $\sigma_{max}=-177.02$
 Tensioni: $\sigma_N=-74.09$ $\sigma_M=-28.77$ $\tau=21.09$ $\tau_{max}=21.09$
 Tensioni: $\sigma_N=-74.09$ $\sigma_M=-102.93$ $\tau=12.90$ $\sigma_{ID,max}=178.42$

Asta n. 3739 (-3065 -4493) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-4103.64 $M_y,Ed=45.62$ $M_z,Ed=-9.49$
 Resistenze: Nc,Rd=64238.10 $M_{y,c,Rd}=2116.38$ $M_{z,c,Rd}=1670.05$ L=21.34
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ Ncr,y=17091500.00 $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ Ncr,z=8991320.00 $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.06+0.02+0.01=0.09
 Verifica ZZ: 0.06+0.01+0.01=0.08
- Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.21 - Classe 3
 Sollecitazioni: N=-4099.84 $T_z=-276.03$ $M_y=45.62$ $T_y=-23.44$ $M_z=-9.49$ $M_x=-2.33$
 Tensioni: $\sigma_N=-215.78$ $\sigma_M=-92.08$ $\tau=2.70$ $\sigma_{max}=-307.86$
 Tensioni: $\sigma_N=-215.78$ $\sigma_M=-16.81$ $\tau=30.72$ $\tau_{max}=30.72$
 Tensioni: $\sigma_N=-215.78$ $\sigma_M=-92.08$ $\tau=2.70$ $\sigma_{ID,max}=307.90$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 67 SLU Xl=0.12
 Sollecitazioni: N=-510.99 $T_z=-96.39$ $T_y=-12.91$ $M_z=-4.79$ $M_x=-1.64$
 $V_{,Ed}=-12.91$ $V_{c,Rd,Red}=14821.10$ $V_{,Ed/Vc,Rd,Red}=0.00$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V_{,Ed}=-96.39$ $V_{c,Rd,Red}=22231.70$ $V_{,Ed/Vc,Rd,Red}=0.00$
- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.21 - Classe 3
 Sollecitazioni: N=-599.64 $T_z=53.64$ $M_y=24.16$ $T_y=-21.36$ $M_z=-15.40$ $M_x=-6.27$
 Tensioni: $\sigma_N=-31.56$ $\sigma_M=-69.76$ $\tau=7.27$ $\sigma_{max}=-101.32$
 Tensioni: $\sigma_N=-31.56$ $\sigma_M=27.28$ $\tau=12.71$ $\tau_{max}=12.71$
 Tensioni: $\sigma_N=-31.56$ $\sigma_M=-69.76$ $\tau=7.27$ $\sigma_{ID,max}=102.10$

Asta n. 3739 (-4493 -7502) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-4002.00 $M_y,Ed=16.38$ $M_z,Ed=-9.53$
 Resistenze: Nc,Rd=64238.10 $M_{y,c,Rd}=2116.38$ $M_{z,c,Rd}=1670.05$ L=21.34
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ Ncr,y=17091500.00 $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ Ncr,z=8991320.00 $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.06+0.01+0.01=0.07
 Verifica ZZ: 0.06+0.00+0.01=0.07

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=-4002.00$ $T_z=82.98$ $M_y=16.38$ $T_y=-3.58$ $M_z=-8.77$ $M_x=-2.34$
 Tensioni: $\sigma_N=-210.63$ $\sigma_M=-43.92$ $\tau=2.71$ $\sigma_{max}=-254.55$
 Tensioni: $\sigma_N=-210.63$ $\sigma_M=15.53$ $\tau=11.14$ $\tau_{max}=11.14$
 Tensioni: $\sigma_N=-210.63$ $\sigma_M=-43.92$ $\tau=2.71$ $\sigma_{ID,max}=254.59$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 45 SLU $X_1=0.19$
 Sollecitazioni: $N=-3998.55$ $T_z=81.15$ $T_y=-3.58$ $M_z=-9.46$ $M_x=-2.34$
 $V,Ed=-3.58$ $V_c,Rd,Red=14815.00$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=81.15$ $V_c,Rd,Red=22222.50$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=772.30$ $T_z=-32.42$ $M_y=-8.34$ $T_y=-5.78$ $M_z=-16.62$ $M_x=-6.07$
 Tensioni: $\sigma_N=40.65$ $\sigma_M=46.96$ $\tau=7.04$ $\sigma_{max}=87.61$
 Tensioni: $\sigma_N=40.65$ $\sigma_M=-29.44$ $\tau=10.33$ $\tau_{max}=10.33$
 Tensioni: $\sigma_N=40.65$ $\sigma_M=46.96$ $\tau=7.04$ $\sigma_{ID,max}=88.45$

Asta n. 3740 (-2351 -2588) Tubo 60x80x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 54 SLU - Classe 3
 Sollecitazioni: $N,Ed=-1869.04$ $M_y,Ed=-34.18$ $M_z,Ed=-10.25$
 Resistenze: $N_c,Rd=43952.40$ $M_y,c,Rd=955.82$ $M_z,c,Rd=801.10$ $L=56.32$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=19.09$ $N_{cr,y}=739023.00$ $\lambda^*_y=0.25$ Curva a: $\Phi_y=0.54$ $\chi_y=0.99$
 $\lambda_z=24.08$ $N_{cr,z}=464544.00$ $\lambda^*_z=0.32$ Curva a: $\Phi_z=0.56$ $\chi_z=0.97$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.96, 0.96, 0.76, 0.96$
 Verifica YY: $0.04+0.03+0.01=0.08$
 Verifica ZZ: $0.04+0.02+0.01=0.08$

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.01$ (L/3859) $f_{z,L}=0.00$ (L/37197)

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/4037) $f_{z,L}=0.00$ (L/31705)

- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=-1869.04$ $T_z=-111.32$ $M_y=-34.18$ $T_y=23.63$ $M_z=-10.25$ $M_x=2.88$
 Tensioni: $\sigma_N=-143.77$ $\sigma_M=-164.16$ $\tau=6.97$ $\sigma_{max}=-307.94$
 Tensioni: $\sigma_N=-143.77$ $\sigma_M=36.04$ $\tau=24.08$ $\tau_{max}=24.08$
 Tensioni: $\sigma_N=-143.77$ $\sigma_M=-164.16$ $\tau=6.97$ $\sigma_{ID,max}=308.17$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 53 SLU $X_1=0.46$
 Sollecitazioni: $N=-1428.23$ $T_z=-119.57$ $M_y=23.21$ $T_y=18.94$ $M_x=1.88$
 $V,Ed=18.94$ $V_c,Rd,Red=10850.30$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-119.57$ $V_c,Rd,Red=14467.10$ $V,Ed/V_c,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=-1063.59$ $T_z=-55.84$ $M_y=-21.57$ $T_y=30.53$ $M_z=-14.10$ $M_x=6.18$
 Tensioni: $\sigma_N=-81.81$ $\sigma_M=-135.81$ $\tau=14.99$ $\sigma_{max}=-217.62$
 Tensioni: $\sigma_N=-81.81$ $\sigma_M=49.59$ $\tau=23.57$ $\tau_{max}=23.57$
 Tensioni: $\sigma_N=-81.81$ $\sigma_M=-135.81$ $\tau=14.99$ $\sigma_{ID,max}=219.16$

Asta n. 3740 (-2588 -3064) Tubo 60x100x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 54 SLU - Classe 3
 Sollecitazioni: $N,Ed=-1862.18$ $M_y,Ed=54.23$ $M_z,Ed=8.11$
 Resistenze: $N_c,Rd=50714.30$ $M_y,c,Rd=1327.02$ $M_z,c,Rd=972.02$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=5.90$ $N_{cr,y}=8930630.00$ $\lambda^*_y=0.08$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=8.90$ $N_{cr,z}=3924920.00$ $\lambda^*_z=0.12$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.04+0.03+0.01=0.08$
 Verifica ZZ: $0.04+0.03+0.01=0.07$

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.01$ (L/3809)

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3960)

- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X_1=0.21$ - Classe 3
 Sollecitazioni: $N=-1859.19$ $T_z=-116.55$ $M_y=54.23$ $T_y=23.67$ $M_z=8.11$ $M_x=2.88$

Tensioni: $\sigma_N=-123.95$ $\sigma_M=-166.39$ $\tau=5.50$ $\sigma_{max}=-290.34$
 Tensioni: $\sigma_N=-123.95$ $\sigma_M=-23.52$ $\tau=19.98$ $\tau_{max}=19.98$
 Tensioni: $\sigma_N=-123.95$ $\sigma_M=-166.39$ $\tau=5.50$ $\sigma_{ID,max}=290.49$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 74 SLU $X_1=0.08$
 Sollecitazioni: $N=-1392.80$ $T_z=-33.81$ $T_y=17.59$ $M_z=2.88$ $M_x=2.87$
 $V,Ed=17.59$ $V_c,Rd,Red=10949.40$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-33.81$ $V_c,Rd,Red=18249.00$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_1=0.21$ - Classe 3
 Sollecitazioni: $N=-1055.61$ $T_z=-60.40$ $M_y=28.24$ $T_y=29.29$ $M_z=9.35$ $M_x=6.18$
 Tensioni: $\sigma_N=-70.37$ $\sigma_M=-104.48$ $\tau=11.83$ $\sigma_{max}=-174.86$
 Tensioni: $\sigma_N=-70.37$ $\sigma_M=-27.10$ $\tau=19.34$ $\tau_{max}=19.34$
 Tensioni: $\sigma_N=-70.37$ $\sigma_M=-104.48$ $\tau=11.83$ $\sigma_{ID,max}=176.05$

Asta n. 3740 (-3064 -4492) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-4101.21$ $M_y,Ed=45.90$ $M_z,Ed=9.50$
 Resistenze: $N_c,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ $N_{cr,y}=17091400.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ $N_{cr,z}=8991300.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.06+0.02+0.01=0.09$
 Verifica ZZ: $0.06+0.01+0.01=0.08$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X_1=0.21$ - Classe 3
 Sollecitazioni: $N=-4097.41$ $T_z=-276.07$ $M_y=45.90$ $T_y=22.61$ $M_z=9.50$ $M_x=2.26$
 Tensioni: $\sigma_N=-215.65$ $\sigma_M=-92.56$ $\tau=2.61$ $\sigma_{max}=-308.21$
 Tensioni: $\sigma_N=-215.65$ $\sigma_M=-16.83$ $\tau=30.64$ $\tau_{max}=30.64$
 Tensioni: $\sigma_N=-215.65$ $\sigma_M=-92.56$ $\tau=2.61$ $\sigma_{ID,max}=308.24$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 111 SLU $X_1=0.00$
 Sollecitazioni: $N=-405.96$ $T_z=-50.02$ $T_y=8.47$ $M_z=2.96$ $M_x=1.43$
 $V,Ed=8.47$ $V_c,Rd,Red=14822.90$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-50.02$ $V_c,Rd,Red=22234.40$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=-610.70$ $T_z=56.34$ $M_y=27.80$ $T_y=19.67$ $M_z=10.39$ $M_x=5.64$
 Tensioni: $\sigma_N=-32.14$ $\sigma_M=-65.45$ $\tau=6.54$ $\sigma_{max}=-97.59$
 Tensioni: $\sigma_N=-32.14$ $\sigma_M=18.41$ $\tau=12.26$ $\tau_{max}=12.26$
 Tensioni: $\sigma_N=-32.14$ $\sigma_M=-65.45$ $\tau=6.54$ $\sigma_{ID,max}=98.24$

Asta n. 3740 (-4492 -7498) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-3948.80$ $M_y,Ed=16.55$ $M_z,Ed=9.54$
 Resistenze: $N_c,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ $N_{cr,y}=17091500.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ $N_{cr,z}=8991320.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.06+0.01+0.01=0.07$
 Verifica ZZ: $0.06+0.00+0.01=0.07$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=-3948.80$ $T_z=83.95$ $M_y=16.55$ $T_y=2.55$ $M_z=9.00$ $M_x=2.45$
 Tensioni: $\sigma_N=-207.83$ $\sigma_M=-44.66$ $\tau=2.85$ $\sigma_{max}=-252.49$
 Tensioni: $\sigma_N=-207.83$ $\sigma_M=15.95$ $\tau=11.37$ $\tau_{max}=11.37$
 Tensioni: $\sigma_N=-207.83$ $\sigma_M=-44.66$ $\tau=2.85$ $\sigma_{ID,max}=252.54$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 45 SLU $X_1=0.19$
 Sollecitazioni: $N=-3945.41$ $T_z=82.15$ $T_y=2.55$ $M_z=9.49$ $M_x=2.45$
 $V,Ed=2.55$ $V_c,Rd,Red=14814.00$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=82.15$ $V_c,Rd,Red=22220.90$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=636.17$ $T_z=-27.49$ $M_y=-8.27$ $T_y=5.88$ $M_z=15.98$ $M_x=5.74$

Tensioni: $\sigma_N=33.48$ $\sigma_M=45.56$ $\tau=6.66$ $\sigma_{max}=79.04$
 Tensioni: $\sigma_N=33.48$ $\sigma_M=-28.31$ $\tau=9.45$ $\tau_{max}=9.45$
 Tensioni: $\sigma_N=33.48$ $\sigma_M=45.56$ $\tau=6.66$ $\sigma_{ID,max}=79.88$

Asta n. 3741 (-7974 -7492) Tubo 60x60x4 mm - S235 Crit. 2

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 1

Sollecitazioni: N,Ed=-1083.24 My,Ed=-2.77
 Resistenze: Nc,Rd=20053.30 My,c,Rd=421.84 L=153.00
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=66.75$ Ncr,y=41677.10 $\lambda^*_y=0.71$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=66.75$ Ncr,z=41677.10 $\lambda^*_z=0.71$ Curva a: $\Phi_z=0.81$ $\chi_z=0.84$
 Kyy, Kyz, Kzy, Kzz=0.98, 0.59, 0.00, 0.98
 Verifica YY: 0.05+0.01=0.06
 Verifica ZZ: 0.05=0.05

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,c}=0.01$ (L/28369)

- Verifica a compressione [4.2.9] - CC 45 SLU Xl=1.53 - Classe 1

Sollecitazioni: N=-1083.24 Tz=-7.26 Mx=11.69
 N,Ed=-1083.24 Nc,Rd=-20053.30 N,Ed/Nc,Rd=0.05

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 49 SLU Xl=0.00

Sollecitazioni: N=-960.34 Tz=7.26 Mx=12.78
 V,Ed=7.26 Vc,Rd,Red=5560.93 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.77 - Classe 3

Sollecitazioni: N=-534.72 My=-2.05 Mx=5.84
 Tensioni: $\sigma_N=-59.68$ $\sigma_M=-13.09$ $\tau=23.28$ $\sigma_{max}=-72.77$
 Tensioni: $\sigma_N=-59.68$ $\sigma_M=13.09$ $\tau=23.28$ $\tau_{max}=23.28$
 Tensioni: $\sigma_N=-59.68$ $\sigma_M=-13.09$ $\tau=23.28$ $\sigma_{ID,max}=83.19$

Asta n. 3742 (-7976 -7508) Tubo 60x60x4 mm - S235 Crit. 2

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 1

Sollecitazioni: N,Ed=-1078.51 My,Ed=-2.77
 Resistenze: Nc,Rd=20053.30 My,c,Rd=421.84 L=153.00
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=66.75$ Ncr,y=41677.10 $\lambda^*_y=0.71$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=66.75$ Ncr,z=41677.10 $\lambda^*_z=0.71$ Curva a: $\Phi_z=0.81$ $\chi_z=0.84$
 Kyy, Kyz, Kzy, Kzz=0.98, 0.59, 0.00, 0.98
 Verifica YY: 0.05+0.01=0.06
 Verifica ZZ: 0.05=0.05

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,c}=0.01$ (L/27635)

- Verifica a compressione [4.2.9] - CC 45 SLU Xl=1.53 - Classe 1

Sollecitazioni: N=-1078.51 Tz=-7.26 Mx=-11.69
 N,Ed=-1078.51 Nc,Rd=-20053.30 N,Ed/Nc,Rd=0.05

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 49 SLU Xl=0.00

Sollecitazioni: N=-954.35 Tz=7.26 Mx=-12.77
 V,Ed=7.26 Vc,Rd,Red=5561.02 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.77 - Classe 3

Sollecitazioni: N=-426.44 My=-2.05 Mx=-7.13
 Tensioni: $\sigma_N=-47.59$ $\sigma_M=-13.09$ $\tau=28.40$ $\sigma_{max}=-60.69$
 Tensioni: $\sigma_N=-47.59$ $\sigma_M=13.09$ $\tau=28.41$ $\tau_{max}=28.41$
 Tensioni: $\sigma_N=-47.59$ $\sigma_M=-13.09$ $\tau=28.41$ $\sigma_{ID,max}=78.12$

Asta n. 3743 (-2408 -4104) Tubo circolare d=70x4 mm - S355 Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3

Sollecitazioni: N,Ed=-248.12 M,Ed=1.50
 Resistenze: Nc,Rd=28041.00 M,c,Rd=437.84 L=147.13
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, ----, ----
 $\lambda=62.93$ Ncr=43400.20 $\lambda^*=0.82$
 Curva a: $\Phi=0.90$ $\chi_{min}=0.78$
 Kyy, Kyz, Kzy, Kzz=0.96, ----, ----, ----
 Verifica: 0.01+0.00=0.01

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,c}=0.02$ (L/6355)

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.02$ (L/6032) $f_{z,L}=0.00$ (L/41446)
- Verifica a trazione [4.2.5] - CC 75 SLU $X_1=1.47$ - Classe 1
 Sollecitazioni: $N=962.92$ $T=5.49$ $M_x=1.58$
 $N,Ed=962.92$ $N_{pl},Rd=28041.00$ $Nu,Rd=30454.90$ $N,Ed/Nt,Rd=0.03$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 74 SLU $X_1=1.47$
 Sollecitazioni: $N=835.41$ $T=5.49$ $M_x=1.61$
 $V,Ed=5.49$ $Vc,Rd,Red=10273.90$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_1=0.73$ - Classe 3
 Sollecitazioni: $N=688.04$ $M=1.50$
 Tensioni: $\sigma_N=82.96$ $\sigma_M=11.55$ $\tau=0.00$ $\sigma_{max}=94.51$
 Tensioni: $\sigma_N=0.00$ $\sigma_M=0.00$ $\tau=0.00$ $\tau_{max}=0.00$
 Tensioni: $\sigma_N=82.96$ $\sigma_M=11.55$ $\tau=0.00$ $\sigma_{ID,max}=94.51$

Asta n. 3744 (-2409 -4105) Tubo circolare $d=70 \times 4$ mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
 Sollecitazioni: $N,Ed=-184.34$ $M,Ed=1.50$
 Resistenze: $Nc,Rd=28041.00$ $M,c,Rd=437.84$ $L=147.13$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, \text{----}, \text{----}$
 $\lambda=62.93$ $Ncr=43400.20$ $\lambda^*=0.82$
 Curva a: $\Phi=0.90$ $\chi_{min}=0.78$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, \text{----}, \text{----}, \text{----}$
 Verifica: $0.01+0.00=0.01$

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.02$ (L/6368)

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.02$ (L/6020) $f_{z,L}=0.00$ (L/41726)

- Verifica a trazione [4.2.5] - CC 68 SLU $X_1=1.47$ - Classe 1
 Sollecitazioni: $N=974.15$ $T=5.49$ $M_x=-1.66$
 $N,Ed=974.15$ $N_{pl},Rd=28041.00$ $Nu,Rd=30454.90$ $N,Ed/Nt,Rd=0.03$

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 67 SLU $X_1=1.47$
 Sollecitazioni: $N=827.88$ $T=5.49$ $M_x=-1.89$
 $V,Ed=5.49$ $Vc,Rd,Red=10268.20$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_1=0.73$ - Classe 3
 Sollecitazioni: $N=620.88$ $M=1.50$
 Tensioni: $\sigma_N=74.86$ $\sigma_M=11.55$ $\tau=0.00$ $\sigma_{max}=86.41$
 Tensioni: $\sigma_N=0.00$ $\sigma_M=0.00$ $\tau=0.00$ $\tau_{max}=0.00$
 Tensioni: $\sigma_N=74.86$ $\sigma_M=11.55$ $\tau=0.00$ $\sigma_{ID,max}=86.41$

Asta n. 3756 (-2409 -2639) Tubo $60 \times 80 \times 5$ mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 89 SLU - Classe 3
 Sollecitazioni: $N,Ed=-823.44$ $M_y,Ed=-42.18$ $M_z,Ed=-14.83$
 Resistenze: $Nc,Rd=43952.40$ $M_y,c,Rd=955.82$ $M_z,c,Rd=801.10$ $L=52.54$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=17.81$ $Ncr,y=849037.00$ $\lambda^*_y=0.23$ Curva a: $\Phi_y=0.53$ $\chi_y=0.99$
 $\lambda_z=22.47$ $Ncr,z=533698.00$ $\lambda^*_z=0.29$ Curva a: $\Phi_z=0.55$ $\chi_z=0.98$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.02+0.03+0.02=0.07$
 Verifica ZZ: $0.02+0.03+0.02=0.06$

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.01$ (L/3741) $f_{z,L}=0.00$ (L/40809)

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3760) $f_{z,L}=0.00$ (L/28619)

- Verifica in termini tensionali [4.2.4] - CC 89 SLU $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=-823.44$ $T_2=-91.16$ $M_y=-42.18$ $T_y=34.09$ $M_z=-14.83$ $M_x=7.56$
 Tensioni: $\sigma_N=-63.34$ $\sigma_M=-211.77$ $\tau=18.34$ $\sigma_{max}=-275.11$
 Tensioni: $\sigma_N=-63.34$ $\sigma_M=52.15$ $\tau=32.35$ $\tau_{max}=32.35$
 Tensioni: $\sigma_N=-63.34$ $\sigma_M=-211.77$ $\tau=18.34$ $\sigma_{ID,max}=276.94$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 115 SLU $X_1=0.53$
 Sollecitazioni: $N=-210.18$ $T_2=-96.63$ $M_y=29.23$ $T_y=11.90$ $M_x=3.61$
 $V,Ed=11.90$ $Vc,Rd,Red=10827.00$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
V,Ed=-96.63 Vc,Rd,Red=14436.00 V,Ed/Vc,Rd,Red=0.01
- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-483.74 Tz=-60.49 My=-23.20 Ty=53.66 Mz=-23.55 Mx=9.10
Tensioni: $\sigma_N=-37.21$ $\sigma_M=-181.42$ $\tau=22.06$ $\sigma_{max}=-218.63$
Tensioni: $\sigma_N=-37.21$ $\sigma_M=71.79$ $\tau=32.74$ $\tau_{max}=32.74$
Tensioni: $\sigma_N=-37.21$ $\sigma_M=-181.42$ $\tau=22.06$ $\sigma_{ID,max}=221.95$

Asta n. 3756 (-2639 -3189) Tubo 60x100x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 75 SLU - Classe 3
Sollecitazioni: N,Ed=-884.83 My,Ed=34.45 Mz,Ed=10.81
Resistenze: Nc,Rd=50714.30 My,c,Rd=1327.02 Mz,c,Rd=972.02 L=21.34
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=5.90$ Ncr,y=8930650.00 $\lambda^*_y=0.08$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=8.90$ Ncr,z=3924940.00 $\lambda^*_z=0.12$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.02+0.02+0.01=0.05
Verifica ZZ: 0.02+0.02+0.01=0.04

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.01$ (L/3761)

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3792)

- Verifica in termini tensionali [4.2.4] - CC 75 SLU Xl=0.21 - Classe 3
Sollecitazioni: N=-881.83 Tz=-92.96 My=34.45 Ty=35.40 Mz=10.81 Mx=1.10
Tensioni: $\sigma_N=-58.79$ $\sigma_M=-125.38$ $\tau=2.10$ $\sigma_{max}=-184.16$
Tensioni: $\sigma_N=-58.79$ $\sigma_M=-31.33$ $\tau=13.65$ $\tau_{max}=13.65$
Tensioni: $\sigma_N=-58.79$ $\sigma_M=-125.38$ $\tau=2.10$ $\sigma_{ID,max}=184.20$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 115 SLU Xl=0.04
Sollecitazioni: N=-209.63 Tz=-96.92 My=32.99 Ty=11.90 Mz=3.61
V,Ed=11.90 Vc,Rd,Red=10941.50 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]
V,Ed=-96.92 Vc,Rd,Red=18235.80 V,Ed/Vc,Rd,Red=0.01

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.21 - Classe 3
Sollecitazioni: N=-476.91 Tz=-64.42 My=30.69 Ty=52.55 Mz=15.87 Mx=9.10
Tensioni: $\sigma_N=-31.79$ $\sigma_M=-133.39$ $\tau=17.42$ $\sigma_{max}=-165.18$
Tensioni: $\sigma_N=-31.79$ $\sigma_M=-70.38$ $\tau=27.71$ $\tau_{max}=27.71$
Tensioni: $\sigma_N=-31.79$ $\sigma_M=-133.39$ $\tau=17.42$ $\sigma_{ID,max}=167.91$

Asta n. 3756 (-3189 -5014) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
Sollecitazioni: N,Ed=-3536.89 My,Ed=45.99 Mz,Ed=7.27
Resistenze: Nc,Rd=64238.10 My,c,Rd=2116.38 Mz,c,Rd=1670.05 L=21.34
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ Ncr,y=17091500.00 $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ Ncr,z=8991320.00 $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.06+0.02+0.00=0.08
Verifica ZZ: 0.06+0.01+0.00=0.07

- Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.21 - Classe 3
Sollecitazioni: N=-3533.09 Tz=-286.17 My=45.99 Ty=1.37 Mz=7.27 Mx=1.55
Tensioni: $\sigma_N=-185.95$ $\sigma_M=-88.18$ $\tau=1.80$ $\sigma_{max}=-274.14$
Tensioni: $\sigma_N=-185.95$ $\sigma_M=-12.88$ $\tau=30.85$ $\tau_{max}=30.85$
Tensioni: $\sigma_N=-185.95$ $\sigma_M=-88.18$ $\tau=1.80$ $\sigma_{ID,max}=274.15$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 49 SLU Xl=0.00
Sollecitazioni: N=-2297.41 Tz=-167.74 Ty=16.94 Mz=10.63 Mx=1.32
V,Ed=16.94 Vc,Rd,Red=14823.90 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]
V,Ed=-167.74 Vc,Rd,Red=22235.90 V,Ed/Vc,Rd,Red=0.01

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-298.59 Tz=72.46 My=28.17 Ty=36.64 Mz=17.31 Mx=8.65
Tensioni: $\sigma_N=-15.72$ $\sigma_M=-80.04$ $\tau=10.02$ $\sigma_{max}=-95.75$
Tensioni: $\sigma_N=-15.72$ $\sigma_M=30.66$ $\tau=17.38$ $\tau_{max}=17.38$

Tensioni: $\sigma_N=-15.72$ $\sigma_M=-80.04$ $\tau=10.02$ $\sigma_{ID,max}=97.31$

Asta n. 3756 (-5014 -7977) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3

Sollecitazioni: $N,Ed=-3554.66$ $M_y,Ed=18.90$ $M_z,Ed=13.49$
 Resistenze: $N_c,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$

α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95

$\lambda_y=4.80$ $N_{cr,y}=17091400.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$

$\lambda_z=6.62$ $N_{cr,z}=8991270.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$

K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.95 , 0.76 , 0.95

Verifica YY: $0.06+0.01+0.01=0.07$

Verifica ZZ: $0.06+0.01+0.01=0.07$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X1=0.00$ - Classe 3

Sollecitazioni: $N=-3554.66$ $T_z=135.11$ $M_y=18.90$ $T_y=17.29$ $M_z=9.81$ $M_x=1.29$

Tensioni: $\sigma_N=-187.09$ $\sigma_M=-50.04$ $\tau=1.50$ $\sigma_{max}=-237.13$

Tensioni: $\sigma_N=-187.09$ $\sigma_M=17.37$ $\tau=15.22$ $\tau_{max}=15.22$

Tensioni: $\sigma_N=-187.09$ $\sigma_M=-50.04$ $\tau=1.50$ $\sigma_{ID,max}=237.14$

- Verifica a taglio dir. Y [4.2.16] - CC 49 SLU $X1=0.02$

Sollecitazioni: $N=-1366.88$ $T_z=62.92$ $T_y=22.57$ $M_z=18.50$

$V,Ed=22.57$ $V_c,Rd=14835.60$ $V,Ed/V_c,Rd=0.00$

- Verifica a taglio dir. Z [4.2.16]

$V,Ed=62.92$ $V_c,Rd=22253.40$ $V,Ed/V_c,Rd=0.00$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.00$ - Classe 3

Sollecitazioni: $N=1072.46$ $T_z=-53.70$ $M_y=-18.03$ $T_y=20.08$ $M_z=28.83$ $M_x=8.27$

Tensioni: $\sigma_N=56.45$ $\sigma_M=87.17$ $\tau=9.59$ $\sigma_{max}=143.62$

Tensioni: $\sigma_N=56.45$ $\sigma_M=-51.07$ $\tau=15.04$ $\tau_{max}=15.04$

Tensioni: $\sigma_N=56.45$ $\sigma_M=87.17$ $\tau=9.59$ $\sigma_{ID,max}=144.57$

Asta n. 3757 (-2408 -2638) Tubo 60x80x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 54 SLU - Classe 3

Sollecitazioni: $N,Ed=-874.08$ $M_y,Ed=-37.43$ $M_z,Ed=16.17$
 Resistenze: $N_c,Rd=43952.40$ $M_y,c,Rd=955.82$ $M_z,c,Rd=801.10$ $L=52.54$

α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95

$\lambda_y=17.81$ $N_{cr,y}=849038.00$ $\lambda^*_y=0.23$ Curva a: $\Phi_y=0.53$ $\chi_y=0.99$

$\lambda_z=22.47$ $N_{cr,z}=533699.00$ $\lambda^*_z=0.29$ Curva a: $\Phi_z=0.55$ $\chi_z=0.98$

K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.95 , 0.76 , 0.95

Verifica YY: $0.02+0.03+0.02=0.07$

Verifica ZZ: $0.02+0.02+0.02=0.06$

- Verifica Freccia massima per soli carichi accidentali - CC 46

$f_{z,g}=0.01$ (L/3741) $f_{z,L}=0.00$ (L/40435)

- Verifica Freccia massima carichi totali - CC 46

$f_{z,g}=0.01$ (L/3760) $f_{z,L}=0.00$ (L/28252)

- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X1=0.00$ - Classe 3

Sollecitazioni: $N=-874.08$ $T_z=-105.04$ $M_y=-37.43$ $T_y=-37.15$ $M_z=16.17$ $M_x=-2.79$

Tensioni: $\sigma_N=-67.24$ $\sigma_M=-200.63$ $\tau=6.76$ $\sigma_{max}=-267.87$

Tensioni: $\sigma_N=-67.24$ $\sigma_M=56.87$ $\tau=22.91$ $\tau_{max}=22.91$

Tensioni: $\sigma_N=-67.24$ $\sigma_M=-200.63$ $\tau=6.76$ $\sigma_{ID,max}=268.12$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 53 SLU $X1=0.48$

Sollecitazioni: $N=-610.06$ $T_z=-119.96$ $M_y=22.80$ $T_y=-27.67$ $M_x=-3.94$

$V,Ed=-27.67$ $V_c,Rd,Red=10822.50$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]

$V,Ed=-119.96$ $V_c,Rd,Red=14430.00$ $V,Ed/V_c,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.00$ - Classe 3

Sollecitazioni: $N=-518.97$ $T_z=-67.22$ $M_y=-23.75$ $T_y=-48.02$ $M_z=21.04$ $M_x=-7.00$

Tensioni: $\sigma_N=-39.92$ $\sigma_M=-172.80$ $\tau=16.96$ $\sigma_{max}=-212.72$

Tensioni: $\sigma_N=-39.92$ $\sigma_M=74.00$ $\tau=27.31$ $\tau_{max}=27.31$

Tensioni: $\sigma_N=-39.92$ $\sigma_M=-172.80$ $\tau=16.96$ $\sigma_{ID,max}=214.74$

Asta n. 3757 (-2638 -3193) Tubo 60x100x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 54 SLU - Classe 3

Sollecitazioni: $N,Ed=-867.68$ $M_y,Ed=41.97$ $M_z,Ed=-11.28$
 Resistenze: $N_c,Rd=50714.30$ $M_y,c,Rd=1327.02$ $M_z,c,Rd=972.02$ $L=21.34$

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=5.90$ Ncr,y=8930650.00 $\lambda^*_y=0.08$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=8.90$ Ncr,z=3924930.00 $\lambda^*_z=0.12$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.02+0.02+0.01=0.05
 Verifica ZZ: 0.02+0.02+0.01=0.05

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.01$ (L/3729)
- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3761)
- Verifica in termini tensionali [4.2.4] - CC 53 SLU Xl=0.21 - Classe 3
 Sollecitazioni: N=-606.61 T_z=-121.80 M_y=54.37 T_y=-27.70 M_z=-8.00 M_x=-3.94
 Tensioni: $\sigma_N=-40.44$ $\sigma_M=-166.34$ $\tau=7.54$ $\sigma_{max}=-206.78$
 Tensioni: $\sigma_N=-40.44$ $\sigma_M=-23.18$ $\tau=22.67$ $\tau_{max}=22.67$
 Tensioni: $\sigma_N=-40.44$ $\sigma_M=-166.34$ $\tau=7.54$ $\sigma_{ID,max}=207.19$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 60 SLU Xl=0.04
 Sollecitazioni: N=-205.53 T_z=-97.13 M_y=32.67 T_y=-12.40 M_z=-3.72
 V,Ed=-12.40 Vc,Rd,Red=10940.20 V,Ed/Vc,Rd,Red=0.00
- Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=-97.13 Vc,Rd,Red=18233.70 V,Ed/Vc,Rd,Red=0.01
- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.21 - Classe 3
 Sollecitazioni: N=-512.29 T_z=-71.33 M_y=29.82 T_y=-46.87 M_z=-14.19 M_x=-7.00
 Tensioni: $\sigma_N=-34.15$ $\sigma_M=-125.34$ $\tau=13.39$ $\sigma_{max}=-159.49$
 Tensioni: $\sigma_N=-34.15$ $\sigma_M=-68.38$ $\tau=22.58$ $\tau_{max}=22.58$
 Tensioni: $\sigma_N=-34.15$ $\sigma_M=-125.34$ $\tau=13.39$ $\sigma_{ID,max}=161.17$

Asta n. 3757 (-3193 -5013) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-3535.40 My,Ed=46.28 Mz,Ed=-7.26
 Resistenze: Nc,Rd=64238.10 My,c,Rd=2116.38 Mz,c,Rd=1670.05 L=21.34
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ Ncr,y=17091500.00 $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ Ncr,z=8991360.00 $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.06+0.02+0.00=0.08
 Verifica ZZ: 0.06+0.01+0.00=0.07
- Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.21 - Classe 3
 Sollecitazioni: N=-3531.60 T_z=-285.82 M_y=46.28 T_y=-1.27 M_z=-7.26 M_x=-1.55
 Tensioni: $\sigma_N=-185.87$ $\sigma_M=-88.63$ $\tau=1.80$ $\sigma_{max}=-274.50$
 Tensioni: $\sigma_N=-185.87$ $\sigma_M=-12.86$ $\tau=30.81$ $\tau_{max}=30.81$
 Tensioni: $\sigma_N=-185.87$ $\sigma_M=-88.63$ $\tau=1.80$ $\sigma_{ID,max}=274.52$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 49 SLU Xl=0.00
 Sollecitazioni: N=-2298.10 T_z=-166.97 T_y=-16.71 M_z=-10.70 M_x=-1.29
 V,Ed=-16.71 Vc,Rd,Red=14824.20 V,Ed/Vc,Rd,Red=0.00
- Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=-166.97 Vc,Rd,Red=22236.40 V,Ed/Vc,Rd,Red=0.01
- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-311.35 T_z=56.68 M_y=27.76 T_y=-31.40 M_z=-15.54 M_x=-6.48
 Tensioni: $\sigma_N=-16.39$ $\sigma_M=-75.80$ $\tau=7.51$ $\sigma_{max}=-92.19$
 Tensioni: $\sigma_N=-16.39$ $\sigma_M=27.52$ $\tau=13.26$ $\tau_{max}=13.26$
 Tensioni: $\sigma_N=-16.39$ $\sigma_M=-75.80$ $\tau=7.51$ $\sigma_{ID,max}=93.10$

Asta n. 3757 (-5013 -7973) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-3499.35 My,Ed=19.07 Mz,Ed=-13.46
 Resistenze: Nc,Rd=64238.10 My,c,Rd=2116.38 Mz,c,Rd=1670.05 L=21.34
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ Ncr,y=17091200.00 $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ Ncr,z=8991190.00 $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.05+0.01+0.01=0.07
 Verifica ZZ: 0.05+0.01+0.01=0.07

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=-3499.35$ $T_z=136.92$ $M_y=19.07$ $T_y=-17.21$ $M_z=-9.85$ $M_x=-1.41$
 Tensioni: $\sigma_N=-184.18$ $\sigma_M=-50.41$ $\tau=1.63$ $\sigma_{max}=-234.58$
 Tensioni: $\sigma_N=-184.18$ $\sigma_M=17.45$ $\tau=15.53$ $\tau_{max}=15.53$
 Tensioni: $\sigma_N=-184.18$ $\sigma_M=-50.41$ $\tau=1.63$ $\sigma_{ID,max}=234.60$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 45 SLU $X_1=0.13$
 Sollecitazioni: $N=-3496.98$ $T_z=135.66$ $T_y=-17.21$ $M_z=-12.15$ $M_x=-1.41$
 $V,Ed=-17.21$ $V_c,Rd,Red=14823.20$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=135.66$ $V_c,Rd,Red=22234.80$ $V,Ed/V_c,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=941.97$ $T_z=-40.21$ $M_y=-17.21$ $T_y=-20.45$ $M_z=-25.77$ $M_x=-6.55$
 Tensioni: $\sigma_N=49.58$ $\sigma_M=79.66$ $\tau=7.60$ $\sigma_{max}=129.24$
 Tensioni: $\sigma_N=49.58$ $\sigma_M=-45.66$ $\tau=11.68$ $\tau_{max}=11.68$
 Tensioni: $\sigma_N=49.58$ $\sigma_M=79.66$ $\tau=7.60$ $\sigma_{ID,max}=129.91$

Asta n. 3758 (-2438 -7807) Tubo circolare $d=70 \times 4$ mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 37 SLU - Classe 1
 Sollecitazioni: $N,Ed=-1604.65$ $M,Ed=2.97$
 Resistenze: $N_c,Rd=28041.00$ $M,c,Rd=575.38$ $L=181.75$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, \text{----}, \text{----}$
 $\lambda=77.74$ $N_{cr}=28440.60$ $\lambda^*=1.02$
 Curva a: $\Phi=1.10$ $\chi_{min}=0.65$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=1.02, \text{----}, \text{----}, \text{----}$
 Verifica: $0.09+0.01=0.09$

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.03$ (L/7041)

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.02$ (L/7483) $f_{z,L}=0.01$ (L/21986)

- Verifica a compressione [4.2.9] - CC 37 SLU $X_1=0.00$ - Classe 1
 Sollecitazioni: $N=-1604.65$ $T=6.55$ $M_x=4.15$
 $N,Ed=-1604.65$ $N_c,Rd=-28041.00$ $N,Ed/N_c,Rd=0.06$

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 75 SLU $X_1=1.82$
 Sollecitazioni: $N=-957.85$ $T=6.80$ $M_x=9.49$
 $V,Ed=6.80$ $V_c,Rd,Red=10113.30$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_1=0.90$ - Classe 3
 Sollecitazioni: $N=-1164.93$ $M=2.29$ $M_x=4.46$
 Tensioni: $\sigma_N=-140.46$ $\sigma_M=-17.67$ $\tau=17.23$ $\sigma_{max}=-158.13$
 Tensioni: $\sigma_N=-140.46$ $\sigma_M=13.53$ $\tau=17.23$ $\tau_{max}=17.23$
 Tensioni: $\sigma_N=-140.46$ $\sigma_M=-17.67$ $\tau=17.23$ $\sigma_{ID,max}=160.92$

Asta n. 3759 (-2437 -7805) Tubo circolare $d=70 \times 4$ mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 37 SLU - Classe 1
 Sollecitazioni: $N,Ed=-1594.61$ $M,Ed=2.97$
 Resistenze: $N_c,Rd=28041.00$ $M,c,Rd=575.38$ $L=181.75$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, \text{----}, \text{----}$
 $\lambda=77.74$ $N_{cr}=28440.60$ $\lambda^*=1.02$
 Curva a: $\Phi=1.10$ $\chi_{min}=0.65$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=1.02, \text{----}, \text{----}, \text{----}$
 Verifica: $0.09+0.01=0.09$

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.03$ (L/7054)

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.02$ (L/7483) $f_{z,L}=0.01$ (L/21907)

- Verifica a compressione [4.2.9] - CC 37 SLU $X_1=0.00$ - Classe 1
 Sollecitazioni: $N=-1594.61$ $T=6.55$ $M_x=-4.15$
 $N,Ed=-1594.61$ $N_c,Rd=-28041.00$ $N,Ed/N_c,Rd=0.06$

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 54 SLU $X_1=1.82$
 Sollecitazioni: $N=-952.46$ $T=6.80$ $M_x=-10.09$
 $V,Ed=6.80$ $V_c,Rd,Red=10101.10$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_1=0.90$ - Classe 3

Sollecitazioni: $N=-1125.74$ $M=2.29$ $M_x=-4.08$
 Tensioni: $\sigma_N=-135.73$ $\sigma_M=-17.67$ $\tau=15.75$ $\sigma_{max}=-153.40$
 Tensioni: $\sigma_N=-135.73$ $\sigma_M=-17.40$ $\tau=15.75$ $\tau_{max}=15.75$
 Tensioni: $\sigma_N=-135.73$ $\sigma_M=-17.67$ $\tau=15.75$ $\sigma_{ID,max}=155.81$

Asta n. 3760 (-8426 -7983) Tubo 60x60x4 mm - S235 Crit. 2

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 1
 Sollecitazioni: $N,Ed=-1162.51$ $M_y,Ed=-2.77$
 Resistenze: $N_c,Rd=20053.30$ $M_y,c,Rd=421.84$ $L=153.00$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=66.75$ $N_{cr,y}=41677.10$ $\lambda^*_y=0.71$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=66.75$ $N_{cr,z}=41677.00$ $\lambda^*_z=0.71$ Curva a: $\Phi_z=0.81$ $\chi_z=0.84$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.98, 0.59, 0.00, 0.98$
 Verifica YY: $0.06+0.01=0.06$
 Verifica ZZ: $0.06=0.06$

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/27875)

- Verifica a compressione [4.2.9] - CC 45 SLU $X_1=1.53$ - Classe 1
 Sollecitazioni: $N=-1162.51$ $T_z=-7.26$ $M_x=-11.62$
 $N,Ed=-1162.51$ $N_c,Rd=-20053.30$ $N,Ed/N_c,Rd=0.06$

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 49 SLU $X_1=0.00$
 Sollecitazioni: $N=-1057.21$ $T_z=7.26$ $M_x=-12.66$
 $V,Ed=7.26$ $V_c,Rd,Red=5562.94$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.77$ - Classe 3
 Sollecitazioni: $N=-534.13$ $M_y=-2.05$ $M_x=-5.26$
 Tensioni: $\sigma_N=-59.61$ $\sigma_M=-13.09$ $\tau=20.97$ $\sigma_{max}=-72.70$
 Tensioni: $\sigma_N=-59.61$ $\sigma_M=13.09$ $\tau=20.97$ $\tau_{max}=20.97$
 Tensioni: $\sigma_N=-59.61$ $\sigma_M=-13.09$ $\tau=20.97$ $\sigma_{ID,max}=81.27$

Asta n. 3761 (-8424 -7967) Tubo 60x60x4 mm - S235 Crit. 2

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 1
 Sollecitazioni: $N,Ed=-1166.74$ $M_y,Ed=-2.77$
 Resistenze: $N_c,Rd=20053.30$ $M_y,c,Rd=421.84$ $L=153.00$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=66.75$ $N_{cr,y}=41677.00$ $\lambda^*_y=0.71$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=66.75$ $N_{cr,z}=41677.00$ $\lambda^*_z=0.71$ Curva a: $\Phi_z=0.81$ $\chi_z=0.84$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.98, 0.59, 0.00, 0.98$
 Verifica YY: $0.06+0.01=0.06$
 Verifica ZZ: $0.06=0.06$

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/28369)

- Verifica a compressione [4.2.9] - CC 45 SLU $X_1=1.53$ - Classe 1
 Sollecitazioni: $N=-1166.74$ $T_z=-7.26$ $M_x=11.61$
 $N,Ed=-1166.74$ $N_c,Rd=-20053.30$ $N,Ed/N_c,Rd=0.06$

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 49 SLU $X_1=0.00$
 Sollecitazioni: $N=-1062.60$ $T_z=7.26$ $M_x=12.66$
 $V,Ed=7.26$ $V_c,Rd,Red=5563.04$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.77$ - Classe 3
 Sollecitazioni: $N=-599.21$ $M_y=-2.05$ $M_x=5.41$
 Tensioni: $\sigma_N=-66.88$ $\sigma_M=-13.09$ $\tau=21.57$ $\sigma_{max}=-79.97$
 Tensioni: $\sigma_N=-66.88$ $\sigma_M=13.09$ $\tau=21.57$ $\tau_{max}=21.57$
 Tensioni: $\sigma_N=-66.88$ $\sigma_M=-13.09$ $\tau=21.57$ $\sigma_{ID,max}=88.27$

Asta n. 3775 (-2437 -2697) Tubo 60x80x5 mm - S355 Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
 Sollecitazioni: $N,Ed=-348.96$ $M_y,Ed=-32.10$ $M_z,Ed=39.46$
 Resistenze: $N_c,Rd=43952.40$ $M_y,c,Rd=955.82$ $M_z,c,Rd=801.10$ $L=47.59$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=16.13$ $N_{cr,y}=1035060.00$ $\lambda^*_y=0.21$ Curva a: $\Phi_y=0.52$ $\chi_y=1.00$
 $\lambda_z=20.35$ $N_{cr,z}=650632.00$ $\lambda^*_z=0.27$ Curva a: $\Phi_z=0.54$ $\chi_z=0.99$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.01+0.03+0.05=0.09$
 Verifica ZZ: $0.01+0.03+0.05=0.08$

- Verifica Freccia massima per soli carichi accidentali - CC 46

$f_{z,g}=0.01$ (L/3602) $f_{z,L}=0.00$ (L/32453)

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3429) $f_{z,L}=0.00$ (L/18829)
- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X_1=0.00$ - Classe 3
Sollecitazioni: $N=646.07$ $T_z=-4.36$ $M_y=-28.87$ $T_y=-128.75$ $M_z=56.65$ $M_x=-12.37$
Tensioni: $\sigma_N=49.70$ $\sigma_M=341.22$ $\tau=29.98$ $\sigma_{max}=390.91$
Tensioni: $\sigma_N=49.70$ $\sigma_M=89.35$ $\tau=55.57$ $\tau_{max}=55.57$
Tensioni: $\sigma_N=49.70$ $\sigma_M=341.22$ $\tau=29.98$ $\sigma_{ID,max}=394.35$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X_1=0.43$
Sollecitazioni: $N=651.34$ $T_z=-7.15$ $M_y=-26.38$ $T_y=-128.75$ $M_x=-12.37$
 $V,Ed=-128.75$ $Vc,Rd,Red=10708.70$ $V,Ed/Vc,Rd,Red=0.01$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-7.15$ $Vc,Rd,Red=14278.20$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_1=0.00$ - Classe 3
Sollecitazioni: $N=781.38$ $T_z=62.76$ $M_y=-15.97$ $T_y=-91.03$ $M_z=39.46$ $M_x=-11.88$
Tensioni: $\sigma_N=60.11$ $\sigma_M=223.04$ $\tau=28.81$ $\sigma_{max}=283.14$
Tensioni: $\sigma_N=60.11$ $\sigma_M=49.43$ $\tau=46.91$ $\tau_{max}=46.91$
Tensioni: $\sigma_N=60.11$ $\sigma_M=223.04$ $\tau=28.81$ $\sigma_{ID,max}=287.51$

Asta n. 3775 (-2697 -3309) Tubo 60x100x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
Sollecitazioni: $N,Ed=-345.08$ $M_y,Ed=-44.53$ $M_z,Ed=-23.06$
Resistenze: $Nc,Rd=50714.30$ $M_y,c,Rd=1327.02$ $M_z,c,Rd=972.02$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=5.90$ $Ncr,y=8930640.00$ $\lambda^*_y=0.08$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=8.90$ $Ncr,z=3924930.00$ $\lambda^*_z=0.12$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.01+0.03+0.02=0.06$
Verifica ZZ: $0.01+0.03+0.02=0.05$

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.01$ (L/3638)
- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3496)
- Verifica in termini tensionali [4.2.4] - CC 75 SLU $X_1=0.21$ - Classe 3
Sollecitazioni: $N=641.61$ $T_z=57.35$ $M_y=-63.25$ $T_y=-128.16$ $M_z=-32.84$ $M_x=-8.44$
Tensioni: $\sigma_N=42.77$ $\sigma_M=275.38$ $\tau=16.15$ $\sigma_{max}=318.15$
Tensioni: $\sigma_N=42.77$ $\sigma_M=145.04$ $\tau=41.23$ $\tau_{max}=41.23$
Tensioni: $\sigma_N=42.77$ $\sigma_M=275.38$ $\tau=16.15$ $\sigma_{ID,max}=319.38$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 53 SLU $X_1=0.12$
Sollecitazioni: $N=521.80$ $T_z=-47.26$ $T_y=-100.07$ $M_z=-14.72$ $M_x=-12.55$
 $V,Ed=-100.07$ $Vc,Rd,Red=10845.20$ $V,Ed/Vc,Rd,Red=0.01$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-47.26$ $Vc,Rd,Red=18075.30$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_1=0.21$ - Classe 3
Sollecitazioni: $N=788.31$ $T_z=59.26$ $M_y=-44.53$ $T_y=-89.97$ $M_z=-23.06$ $M_x=-11.88$
Tensioni: $\sigma_N=52.55$ $\sigma_M=193.64$ $\tau=22.74$ $\sigma_{max}=246.19$
Tensioni: $\sigma_N=52.55$ $\sigma_M=102.10$ $\tau=40.35$ $\tau_{max}=40.35$
Tensioni: $\sigma_N=52.55$ $\sigma_M=193.64$ $\tau=22.74$ $\sigma_{ID,max}=249.33$

Asta n. 3775 (-3309 -5418) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
Sollecitazioni: $N,Ed=-2635.85$ $M_y,Ed=-57.63$ $M_z,Ed=-28.63$
Resistenze: $Nc,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ $Ncr,y=17091400.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ $Ncr,z=8991280.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.04+0.02+0.02=0.08$
Verifica ZZ: $0.04+0.02+0.02=0.07$
- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X_1=0.00$ - Classe 3
Sollecitazioni: $N=-2635.85$ $T_z=-388.52$ $M_y=-57.63$ $T_y=-34.72$ $M_z=-21.22$ $M_x=-6.35$

Tensioni: $\sigma_N=-138.73$ $\sigma_M=-135.03$ $\tau=7.36$ $\sigma_{max}=-273.76$

Tensioni: $\sigma_N=-138.73$ $\sigma_M=-37.59$ $\tau=46.80$ $\tau_{max}=46.80$

Tensioni: $\sigma_N=-138.73$ $\sigma_M=-135.03$ $\tau=7.36$ $\sigma_{ID,max}=274.06$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X1=0.21$
Sollecitazioni: $N=858.48$ $T_z=-91.98$ $T_y=-92.53$ $M_z=-55.23$ $M_x=-11.45$
 $V,Ed=-92.53$ $V_c,Rd,Red=14734.70$ $V,Ed/V_c,Rd,Red=0.01$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-91.98$ $V_c,Rd,Red=22102.00$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.00$ - Classe 3
Sollecitazioni: $N=777.89$ $T_z=-114.27$ $M_y=-38.53$ $T_y=-57.27$ $M_z=-25.37$ $M_x=-10.99$
Tensioni: $\sigma_N=40.94$ $\sigma_M=112.92$ $\tau=12.74$ $\sigma_{max}=153.86$
Tensioni: $\sigma_N=40.94$ $\sigma_M=-44.94$ $\tau=24.35$ $\tau_{max}=24.35$
Tensioni: $\sigma_N=40.94$ $\sigma_M=112.92$ $\tau=12.74$ $\sigma_{ID,max}=155.43$

Asta n. 3775 (-5418 -8423) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
Sollecitazioni: $N,Ed=-2911.18$ $M_y,Ed=-24.15$ $M_z,Ed=-43.48$
Resistenze: $N_c,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ $N_{cr,y}=17091500.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ $N_{cr,z}=8991320.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.05+0.01+0.02=0.08$
Verifica ZZ: $0.05+0.01+0.02=0.08$

- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X1=0.21$ - Classe 3
Sollecitazioni: $N=2490.22$ $T_z=-19.22$ $M_y=-31.21$ $T_y=-66.40$ $M_z=-79.72$ $M_x=-11.49$
Tensioni: $\sigma_N=131.06$ $\sigma_M=211.25$ $\tau=13.32$ $\sigma_{max}=342.32$
Tensioni: $\sigma_N=131.06$ $\sigma_M=45.70$ $\tau=22.94$ $\tau_{max}=22.94$
Tensioni: $\sigma_N=131.06$ $\sigma_M=211.25$ $\tau=13.32$ $\sigma_{ID,max}=343.10$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 60 SLU $X1=0.00$
Sollecitazioni: $N=1123.26$ $T_z=54.10$ $T_y=-23.59$ $M_z=-26.91$ $M_x=-8.54$
 $V,Ed=-23.59$ $V_c,Rd,Red=14760.30$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=54.10$ $V_c,Rd,Red=22140.40$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.21$ - Classe 3
Sollecitazioni: $N=1326.64$ $T_z=-50.96$ $M_y=-20.12$ $T_y=-43.38$ $M_z=-52.07$ $M_x=-11.19$
Tensioni: $\sigma_N=69.82$ $\sigma_M=137.55$ $\tau=12.98$ $\sigma_{max}=207.38$
Tensioni: $\sigma_N=69.82$ $\sigma_M=29.46$ $\tau=19.26$ $\tau_{max}=19.26$
Tensioni: $\sigma_N=69.82$ $\sigma_M=137.55$ $\tau=12.98$ $\sigma_{ID,max}=208.59$

Asta n. 3776 (-2438 -2692) Tubo 60x80x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
Sollecitazioni: $N,Ed=-368.69$ $M_y,Ed=-36.40$ $M_z,Ed=-43.72$
Resistenze: $N_c,Rd=43952.40$ $M_y,c,Rd=955.82$ $M_z,c,Rd=801.10$ $L=47.59$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=16.13$ $N_{cr,y}=1035060.00$ $\lambda^*_y=0.21$ Curva a: $\Phi_y=0.52$ $\chi_y=1.00$
 $\lambda_z=20.35$ $N_{cr,z}=650633.00$ $\lambda^*_z=0.27$ Curva a: $\Phi_z=0.54$ $\chi_z=0.99$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.01+0.04+0.05=0.10$
Verifica ZZ: $0.01+0.03+0.05=0.09$

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.01$ (L/3596) $f_{z,L}=0.00$ (L/33828)

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3465) $f_{z,L}=0.00$ (L/19191)

- Verifica in termini tensionali [4.2.4] - CC 75 SLU $X1=0.00$ - Classe 3
Sollecitazioni: $N=578.20$ $T_z=10.11$ $M_y=-24.66$ $T_y=122.88$ $M_z=-54.00$ $M_x=9.15$
Tensioni: $\sigma_N=44.48$ $\sigma_M=315.12$ $\tau=22.17$ $\sigma_{max}=359.60$
Tensioni: $\sigma_N=44.48$ $\sigma_M=76.32$ $\tau=46.59$ $\tau_{max}=46.59$
Tensioni: $\sigma_N=44.48$ $\sigma_M=315.12$ $\tau=22.17$ $\sigma_{ID,max}=361.64$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 75 SLU $X1=0.43$
Sollecitazioni: $N=583.47$ $T_z=7.32$ $M_y=-28.43$ $T_y=122.88$ $M_x=9.15$
 $V,Ed=122.88$ $V_c,Rd,Red=10752.20$ $V,Ed/V_c,Rd,Red=0.01$

- Verifica a taglio e torsione dir. Z [4.2.25]
V,Ed=7.32 Vc,Rd,Red=14336.30 V,Ed/Vc,Rd,Red=0.00
- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
Sollecitazioni: N=782.27 Tz=64.13 My=-14.78 Ty=100.92 Mz=-43.72 Mx=14.76
Tensioni: $\sigma_N=60.17$ $\sigma_M=236.78$ $\tau=35.78$ $\sigma_{max}=296.96$
Tensioni: $\sigma_N=60.17$ $\sigma_M=45.74$ $\tau=55.84$ $\tau_{max}=55.84$
Tensioni: $\sigma_N=60.17$ $\sigma_M=236.78$ $\tau=35.78$ $\sigma_{ID,max}=303.36$

Asta n. 3776 (-2692 -3317) Tubo 60x100x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
Sollecitazioni: N,Ed=-365.00 My,Ed=-49.13 Mz,Ed=25.63
Resistenze: Nc,Rd=50714.30 My,c,Rd=1327.02 Mz,c,Rd=972.02 L=21.34
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=5.90$ Ncr,y=8930630.00 $\lambda^*_y=0.08$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=8.90$ Ncr,z=3924920.00 $\lambda^*_z=0.12$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.01+0.04+0.03=0.07
Verifica ZZ: 0.01+0.03+0.03=0.06

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.01$ (L/3609)

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3442)

- Verifica in termini tensionali [4.2.4] - CC 54 SLU Xl=0.21 - Classe 3
Sollecitazioni: N=584.38 Tz=72.76 My=-69.76 Ty=123.06 Mz=31.66 Mx=5.35
Tensioni: $\sigma_N=38.96$ $\sigma_M=287.84$ $\tau=10.24$ $\sigma_{max}=326.80$
Tensioni: $\sigma_N=38.96$ $\sigma_M=159.96$ $\tau=34.33$ $\tau_{max}=34.33$
Tensioni: $\sigma_N=38.96$ $\sigma_M=287.84$ $\tau=10.24$ $\sigma_{ID,max}=327.28$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 111 SLU Xl=0.00
Sollecitazioni: N=322.18 Tz=-31.26 Ty=58.24 Mz=1.59 Mx=5.25
V,Ed=58.24 Vc,Rd,Red=10923.80 V,Ed/Vc,Rd,Red=0.01

- Verifica a taglio e torsione dir. Z [4.2.25]
V,Ed=-31.26 Vc,Rd,Red=18206.30 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.21 - Classe 3
Sollecitazioni: N=789.39 Tz=60.51 My=-49.13 Ty=99.90 Mz=25.63 Mx=14.76
Tensioni: $\sigma_N=52.63$ $\sigma_M=214.31$ $\tau=28.25$ $\sigma_{max}=266.94$
Tensioni: $\sigma_N=52.63$ $\sigma_M=112.66$ $\tau=47.80$ $\tau_{max}=47.80$
Tensioni: $\sigma_N=52.63$ $\sigma_M=214.31$ $\tau=28.25$ $\sigma_{ID,max}=271.38$

Asta n. 3776 (-3317 -5397) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
Sollecitazioni: N,Ed=-2652.46 My,Ed=-57.55 Mz,Ed=28.51
Resistenze: Nc,Rd=64238.10 My,c,Rd=2116.38 Mz,c,Rd=1670.05 L=21.34
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=4.80$ Ncr,y=17091500.00 $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ Ncr,z=8991320.00 $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.04+0.02+0.02=0.08
Verifica ZZ: 0.04+0.02+0.02=0.07

- Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl=0.00 - Classe 3
Sollecitazioni: N=-2652.46 Tz=-388.22 My=-57.55 Ty=36.25 Mz=20.77 Mx=6.45
Tensioni: $\sigma_N=-139.60$ $\sigma_M=-134.00$ $\tau=7.48$ $\sigma_{max}=-273.60$
Tensioni: $\sigma_N=-139.60$ $\sigma_M=-36.80$ $\tau=46.89$ $\tau_{max}=46.89$
Tensioni: $\sigma_N=-139.60$ $\sigma_M=-134.00$ $\tau=7.48$ $\sigma_{ID,max}=273.91$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 89 SLU Xl=0.17
Sollecitazioni: N=618.25 Tz=-113.18 Ty=84.46 Mz=43.40 Mx=18.69
V,Ed=84.46 Vc,Rd,Red=14670.90 V,Ed/Vc,Rd,Red=0.01

- Verifica a taglio e torsione dir. Z [4.2.25]
V,Ed=-113.18 Vc,Rd,Red=22006.40 V,Ed/Vc,Rd,Red=0.01

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
Sollecitazioni: N=815.02 Tz=-135.42 My=-42.71 Ty=67.14 Mz=27.97 Mx=14.03
Tensioni: $\sigma_N=42.90$ $\sigma_M=124.87$ $\tau=16.27$ $\sigma_{max}=167.77$

Tensioni: $\sigma_N=42.90$ $\sigma_M=-49.55$ $\tau=30.02$ $\tau_{max}=30.02$
 Tensioni: $\sigma_N=42.90$ $\sigma_M=124.87$ $\tau=16.27$ $\sigma_{TD,max}=170.12$

Asta n. 3776 (-5397 -8427) Tubo 80x120x5 mm - S355 Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3

Sollecitazioni: N,Ed=-2978.71 My,Ed=-23.95 Mz,Ed=43.32
 Resistenze: Nc,Rd=64238.10 My,c,Rd=2116.38 Mz,c,Rd=1670.05 L=21.34

α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95

$\lambda_y=4.80$ Ncr,y=17091500.00 $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$

$\lambda_z=6.62$ Ncr,z=8991320.00 $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.05+0.01+0.02=0.08

Verifica ZZ: 0.05+0.01+0.02=0.08

- Verifica in termini tensionali [4.2.4] - CC 75 SLU Xl=0.21 - Classe 3

Sollecitazioni: N=2347.24 Tz=-26.24 My=-31.68 Ty=71.09 Mz=76.80 Mx=7.83

Tensioni: $\sigma_N=123.54$ $\sigma_M=206.09$ $\tau=9.08$ $\sigma_{max}=329.63$

Tensioni: $\sigma_N=123.54$ $\sigma_M=46.40$ $\tau=19.38$ $\tau_{max}=19.38$

Tensioni: $\sigma_N=123.54$ $\sigma_M=206.09$ $\tau=9.08$ $\sigma_{TD,max}=330.00$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 115 SLU Xl=0.02

Sollecitazioni: N=1109.38 Tz=53.17 Ty=25.88 Mz=26.51 Mx=8.08

V,Ed=25.88 Vc,Rd,Red=14764.40 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione dir. Z [4.2.25]

V,Ed=53.17 Vc,Rd,Red=22146.50 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3

Sollecitazioni: N=1473.96 Tz=-62.90 My=-31.40 Ty=44.12 Mz=48.31 Mx=13.37

Tensioni: $\sigma_N=77.58$ $\sigma_M=147.96$ $\tau=15.50$ $\sigma_{max}=225.54$

Tensioni: $\sigma_N=77.58$ $\sigma_M=45.98$ $\tau=21.90$ $\tau_{max}=21.90$

Tensioni: $\sigma_N=77.58$ $\sigma_M=147.96$ $\tau=15.50$ $\sigma_{TD,max}=227.13$

Asta n. 3777 (-2464 -8230) Tubo circolare d=70x4 mm - S355 Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 1

Sollecitazioni: N,Ed=-3056.00 M,Ed=3.58

Resistenze: Nc,Rd=28041.00 M,c,Rd=575.38 L=192.27

α_{my} , α_{mz} , $\alpha_{LT}=0.95$, ----, ----

$\lambda=82.25$ Ncr=25411.20 $\lambda^*=1.08$

Curva a: $\Phi=1.17$ $\chi_{,min}=0.61$

Kyy, Kyz, Kzy, Kzz=1.09, ----, ----, ----

Verifica: 0.18+0.01=0.18

- Verifica Freccia massima per soli carichi accidentali - CC 46

$f_{z,g}=0.02$ (L/8502)

- Verifica Freccia massima carichi totali - CC 46

$f_{z,g}=0.02$ (L/10661) $f_{z,L}=0.01$ (L/17972)

- Verifica a compressione [4.2.9] - CC 49 SLU Xl=0.00 - Classe 1

Sollecitazioni: N=-3056.00 T=7.46 Mx=7.25

N,Ed=-3056.00 Nc,Rd=-28041.00 N,Ed/Nc,Rd=0.11

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 75 SLU Xl=0.00

Sollecitazioni: N=-2998.09 T=7.46 Mx=7.42

V,Ed=7.46 Vc,Rd,Red=10155.50 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.96 - Classe 3

Sollecitazioni: N=-2144.88 M=2.65 Mx=3.03

Tensioni: $\sigma_N=-258.61$ $\sigma_M=-20.49$ $\tau=11.69$ $\sigma_{max}=-279.10$

Tensioni: $\sigma_N=-258.61$ $\sigma_M=20.18$ $\tau=11.69$ $\tau_{max}=11.69$

Tensioni: $\sigma_N=-258.61$ $\sigma_M=-20.49$ $\tau=11.69$ $\sigma_{TD,max}=279.84$

Asta n. 3778 (-2463 -8228) Tubo circolare d=70x4 mm - S355 Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 1

Sollecitazioni: N,Ed=-3064.71 M,Ed=3.59

Resistenze: Nc,Rd=28041.00 M,c,Rd=575.38 L=192.39

α_{my} , α_{mz} , $\alpha_{LT}=0.95$, ----, ----

$\lambda=82.30$ Ncr=25380.80 $\lambda^*=1.08$

Curva a: $\Phi=1.17$ $\chi_{,min}=0.61$

Kyy, Kyz, Kzy, Kzz=1.09, ----, ----, ----

Verifica: 0.18+0.01=0.19

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.02$ (L/8525)
- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.02$ (L/10840) $f_{z,l}=0.01$ (L/17843)
- Verifica a compressione [4.2.9] - CC 49 SLU $Xl=0.00$ - Classe 1
 Sollecitazioni: $N=-3064.71$ $T=7.46$ $M_x=-7.20$
 $N,Ed=-3064.71$ $N_c,Rd=-28041.00$ $N,Ed/N_c,Rd=0.11$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 54 SLU $Xl=1.92$
 Sollecitazioni: $N=-3027.48$ $T=7.46$ $M_x=-7.70$
 $V,Ed=7.46$ $V_c,Rd,Red=10149.90$ $V,Ed/V_c,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 9 SND $Xl=0.96$ - Classe 3
 Sollecitazioni: $N=-2072.42$ $M=2.66$ $M_x=-3.09$
 Tensioni: $\sigma_N=-249.88$ $\sigma_M=-20.51$ $\tau=11.93$ $\sigma_{max}=-270.38$
 Tensioni: $\sigma_N=-249.88$ $\sigma_M=17.76$ $\tau=11.93$ $\tau_{max}=11.93$
 Tensioni: $\sigma_N=-249.88$ $\sigma_M=-20.51$ $\tau=11.93$ $\sigma_{ID,max}=271.17$

Asta n. 3779 (-8908 -8417) Tubo 60x60x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 1
 Sollecitazioni: $N,Ed=-1224.85$ $M_y,Ed=-2.77$
 Resistenze: $N_c,Rd=20053.30$ $M_y,c,Rd=421.84$ $L=153.00$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=66.75$ $N_{cr,y}=41677.00$ $\lambda_y^*=0.71$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=66.75$ $N_{cr,z}=41677.00$ $\lambda_z^*=0.71$ Curva a: $\Phi_z=0.81$ $\chi_z=0.84$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.99, 0.59, 0.00, 0.99$
 Verifica YY: $0.06+0.01=0.07$
 Verifica ZZ: $0.06=0.06$

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/27875)
- Verifica a compressione [4.2.9] - CC 45 SLU $Xl=1.53$ - Classe 1
 Sollecitazioni: $N=-1224.85$ $T_z=-7.26$ $M_x=11.19$
 $N,Ed=-1224.85$ $N_c,Rd=-20053.30$ $N,Ed/N_c,Rd=0.06$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 49 SLU $Xl=0.00$
 Sollecitazioni: $N=-1124.95$ $T_z=7.26$ $M_x=12.14$
 $V,Ed=7.26$ $V_c,Rd,Red=5572.33$ $V,Ed/V_c,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $Xl=0.77$ - Classe 3
 Sollecitazioni: $N=-626.21$ $M_y=-2.05$ $M_x=4.87$
 Tensioni: $\sigma_N=-69.89$ $\sigma_M=-13.09$ $\tau=19.40$ $\sigma_{max}=-82.98$
 Tensioni: $\sigma_N=-69.89$ $\sigma_M=13.09$ $\tau=19.40$ $\tau_{max}=19.40$
 Tensioni: $\sigma_N=-69.89$ $\sigma_M=-13.09$ $\tau=19.40$ $\sigma_{ID,max}=89.53$

Asta n. 3780 (-8910 -8433) Tubo 60x60x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 1
 Sollecitazioni: $N,Ed=-1222.38$ $M_y,Ed=-2.77$
 Resistenze: $N_c,Rd=20053.30$ $M_y,c,Rd=421.84$ $L=153.00$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=66.75$ $N_{cr,y}=41677.00$ $\lambda_y^*=0.71$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=66.75$ $N_{cr,z}=41677.00$ $\lambda_z^*=0.71$ Curva a: $\Phi_z=0.81$ $\chi_z=0.84$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.99, 0.59, 0.00, 0.99$
 Verifica YY: $0.06+0.01=0.07$
 Verifica ZZ: $0.06=0.06$

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/28880)
- Verifica a compressione [4.2.9] - CC 45 SLU $Xl=1.53$ - Classe 1
 Sollecitazioni: $N=-1222.38$ $T_z=-7.26$ $M_x=-11.21$
 $N,Ed=-1222.38$ $N_c,Rd=-20053.30$ $N,Ed/N_c,Rd=0.06$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 49 SLU $Xl=0.00$
 Sollecitazioni: $N=-1122.04$ $T_z=7.26$ $M_x=-12.16$
 $V,Ed=7.26$ $V_c,Rd,Red=5571.98$ $V,Ed/V_c,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $Xl=0.77$ - Classe 3
 Sollecitazioni: $N=-565.98$ $M_y=-2.05$ $M_x=-4.81$
 Tensioni: $\sigma_N=-63.17$ $\sigma_M=-13.09$ $\tau=19.19$ $\sigma_{max}=-76.26$

Tensioni: $\sigma_N=-63.17$ $\sigma_M=13.09$ $\tau=19.19$ $\tau_{max}=19.19$
 Tensioni: $\sigma_N=-63.17$ $\sigma_M=-13.09$ $\tau=19.19$ $\sigma_{TD,max}=83.19$

Asta n. 3795 (-2464 -2750) Tubo 60x80x5 mm - S355 Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3

Sollecitazioni: N,Ed=-229.48 My,Ed=-45.26 Mz,Ed=-61.13
 Resistenze: Nc,Rd=43952.40 My,c,Rd=955.82 Mz,c,Rd=801.10 L=42.63

α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95

$\lambda_y=14.45$ Ncr,y=1289660.00 $\lambda^*_y=0.19$ Curva a: $\Phi_y=0.52$ $\chi_y=1.00$

$\lambda_z=18.23$ Ncr,z=810673.00 $\lambda^*_z=0.24$ Curva a: $\Phi_z=0.53$ $\chi_z=0.99$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.01+0.05+0.07=0.12

Verifica ZZ: 0.01+0.04+0.07=0.11

- Verifica Freccia massima per soli carichi accidentali - CC 46

$f_{z,g}=0.01$ (L/3568) $f_{z,L}=0.00$ (L/28381)

- Verifica Freccia massima carichi totali - CC 46

$f_{z,g}=0.01$ (L/3399) $f_{z,L}=0.00$ (L/15152)

- Verifica in termini tensionali [4.2.4] - CC 75 SLU Xl=0.00 - Classe 3

Sollecitazioni: N=905.31 Tz=91.81 My=-22.93 Ty=216.25 Mz=-88.79 Mx=16.36

Tensioni: $\sigma_N=69.64$ $\sigma_M=455.84$ $\tau=39.65$ $\sigma_{max}=525.48$

Tensioni: $\sigma_N=69.64$ $\sigma_M=70.97$ $\tau=82.64$ $\tau_{max}=82.64$

Tensioni: $\sigma_N=69.64$ $\sigma_M=455.84$ $\tau=39.65$ $\sigma_{TD,max}=529.94$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 115 SLU Xl=0.39

Sollecitazioni: N=378.00 Tz=-37.11 Ty=87.80 Mz=-2.77 Mx=14.36

V,Ed=87.80 Vc,Rd,Red=10681.80 V,Ed/Vc,Rd,Red=0.01

- Verifica a taglio e torsione dir. Z [4.2.25]

V,Ed=-37.11 Vc,Rd,Red=14242.40 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3

Sollecitazioni: N=836.91 Tz=93.57 My=-9.70 Ty=149.37 Mz=-61.13 Mx=19.71

Tensioni: $\sigma_N=64.38$ $\sigma_M=292.29$ $\tau=47.79$ $\sigma_{max}=356.67$

Tensioni: $\sigma_N=64.38$ $\sigma_M=30.03$ $\tau=77.48$ $\tau_{max}=77.48$

Tensioni: $\sigma_N=64.38$ $\sigma_M=292.29$ $\tau=47.79$ $\sigma_{TD,max}=366.15$

Asta n. 3795 (-2750 -3441) Tubo 60x100x5 mm - S355 Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3

Sollecitazioni: N,Ed=-226.09 My,Ed=-64.54 Mz,Ed=34.24

Resistenze: Nc,Rd=50714.30 My,c,Rd=1327.02 Mz,c,Rd=972.02 L=21.34

α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95

$\lambda_y=5.90$ Ncr,y=8930640.00 $\lambda^*_y=0.08$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$

$\lambda_z=8.90$ Ncr,z=3924930.00 $\lambda^*_z=0.12$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.00+0.05+0.03=0.08

Verifica ZZ: 0.00+0.04+0.03=0.07

- Verifica Freccia massima per soli carichi accidentali - CC 46

$f_{z,g}=0.01$ (L/3552)

- Verifica Freccia massima carichi totali - CC 46

$f_{z,g}=0.01$ (L/3365)

- Verifica in termini tensionali [4.2.4] - CC 54 SLU Xl=0.21 - Classe 3

Sollecitazioni: N=919.47 Tz=157.34 My=-119.91 Ty=213.37 Mz=49.65 Mx=10.51

Tensioni: $\sigma_N=61.30$ $\sigma_M=478.18$ $\tau=20.12$ $\sigma_{max}=539.47$

Tensioni: $\sigma_N=61.30$ $\sigma_M=274.94$ $\tau=61.90$ $\tau_{max}=61.90$

Tensioni: $\sigma_N=61.30$ $\sigma_M=478.18$ $\tau=20.12$ $\sigma_{TD,max}=540.60$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 115 SLU Xl=0.00

Sollecitazioni: N=378.47 Tz=-37.37 Ty=87.79 Mz=14.36

V,Ed=87.79 Vc,Rd,Red=10825.70 V,Ed/Vc,Rd,Red=0.01

- Verifica a taglio e torsione dir. Z [4.2.25]

V,Ed=-37.37 Vc,Rd,Red=18042.90 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.21 - Classe 3

Sollecitazioni: N=843.44 Tz=90.19 My=-64.54 Ty=148.45 Mz=34.24 Mx=19.71

Tensioni: $\sigma_N=56.23$ $\sigma_M=283.53$ $\tau=37.73$ $\sigma_{max}=339.75$

Tensioni: $\sigma_N=56.23$ $\sigma_M=148.00$ $\tau=66.78$ $\tau_{max}=66.78$

Tensioni: $\sigma_N=56.23$ $\sigma_M=283.53$ $\tau=37.73$ $\sigma_{ID,max}=345.98$

Asta n. 3795 (-3441 -5817) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3

Sollecitazioni: $N_{Ed}=-2397.84$ $M_y,Ed=-90.14$ $M_z,Ed=51.45$
Resistenze: $N_c,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$

α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95

$\lambda_y=4.80$ $N_{cr,y}=17091500.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$

$\lambda_z=6.62$ $N_{cr,z}=8991330.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$

K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.95 , 0.76 , 0.95

Verifica YY: $0.04+0.03+0.03=0.10$

Verifica ZZ: $0.04+0.03+0.03=0.09$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X1=0.00$ - Classe 3

Sollecitazioni: $N=-2397.84$ $T_z=-475.26$ $M_y=-90.14$ $T_y=78.13$ $M_z=34.77$ $M_x=11.76$

Tensioni: $\sigma_N=-126.20$ $\sigma_M=-214.39$ $\tau=13.64$ $\sigma_{max}=-340.60$

Tensioni: $\sigma_N=-126.20$ $\sigma_M=-61.60$ $\tau=61.89$ $\tau_{max}=61.89$

Tensioni: $\sigma_N=-126.20$ $\sigma_M=-214.39$ $\tau=13.64$ $\sigma_{ID,max}=341.41$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 111 SLU $X1=0.21$

Sollecitazioni: $N=539.57$ $T_z=-63.70$ $T_y=76.84$ $M_z=42.13$ $M_x=9.17$

$V,Ed=76.84$ $V_c,Rd,Red=14754.80$ $V,Ed/V_c,Rd,Red=0.01$

- Verifica a taglio e torsione dir. Z [4.2.25]

$V,Ed=-63.70$ $V_c,Rd,Red=22132.20$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.00$ - Classe 3

Sollecitazioni: $N=863.70$ $T_z=-170.59$ $M_y=-56.46$ $T_y=102.31$ $M_z=37.66$ $M_x=18.75$

Tensioni: $\sigma_N=45.46$ $\sigma_M=166.43$ $\tau=21.74$ $\sigma_{max}=211.89$

Tensioni: $\sigma_N=45.46$ $\sigma_M=-66.71$ $\tau=39.06$ $\tau_{max}=39.06$

Tensioni: $\sigma_N=45.46$ $\sigma_M=166.43$ $\tau=21.74$ $\sigma_{ID,max}=215.21$

Asta n. 3795 (-5817 -8911) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3

Sollecitazioni: $N_{Ed}=-2920.98$ $M_y,Ed=-27.37$ $M_z,Ed=75.83$
Resistenze: $N_c,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$

α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95

$\lambda_y=4.80$ $N_{cr,y}=17091400.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$

$\lambda_z=6.62$ $N_{cr,z}=8991270.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$

K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.95 , 0.76 , 0.95

Verifica YY: $0.05+0.01+0.04=0.10$

Verifica ZZ: $0.05+0.01+0.04=0.10$

- Verifica in termini tensionali [4.2.4] - CC 75 SLU $X1=0.21$ - Classe 3

Sollecitazioni: $N=2398.60$ $T_z=-85.64$ $M_y=-35.53$ $T_y=119.79$ $M_z=126.22$ $M_x=13.99$

Tensioni: $\sigma_N=126.24$ $\sigma_M=312.28$ $\tau=16.22$ $\sigma_{max}=438.52$

Tensioni: $\sigma_N=126.24$ $\sigma_M=52.03$ $\tau=33.58$ $\tau_{max}=33.58$

Tensioni: $\sigma_N=126.24$ $\sigma_M=312.28$ $\tau=16.22$ $\sigma_{ID,max}=439.42$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.21$ - Classe 3

Sollecitazioni: $N=1374.39$ $T_z=-78.85$ $M_y=-19.41$ $T_y=69.29$ $M_z=82.56$ $M_x=17.74$

Tensioni: $\sigma_N=72.34$ $\sigma_M=198.16$ $\tau=20.56$ $\sigma_{max}=270.50$

Tensioni: $\sigma_N=72.34$ $\sigma_M=28.43$ $\tau=30.61$ $\tau_{max}=30.61$

Tensioni: $\sigma_N=72.34$ $\sigma_M=198.16$ $\tau=20.56$ $\sigma_{ID,max}=272.83$

Asta n. 3796 (-2463 -2749) Tubo 60x80x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3

Sollecitazioni: $N_{Ed}=-216.90$ $M_y,Ed=-42.76$ $M_z,Ed=54.24$
Resistenze: $N_c,Rd=43952.40$ $M_y,c,Rd=955.82$ $M_z,c,Rd=801.10$ $L=42.83$

α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95

$\lambda_y=14.52$ $N_{cr,y}=1277870.00$ $\lambda^*_y=0.19$ Curva a: $\Phi_y=0.52$ $\chi_y=1.00$

$\lambda_z=18.31$ $N_{cr,z}=803258.00$ $\lambda^*_z=0.24$ Curva a: $\Phi_z=0.53$ $\chi_z=0.99$

K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.95 , 0.76 , 0.95

Verifica YY: $0.00+0.04+0.06=0.11$

Verifica ZZ: $0.00+0.03+0.06=0.10$

- Verifica Freccia massima per soli carichi accidentali - CC 46

$f_{z,G}=0.01$ (L/3571) $f_{z,L}=0.00$ (L/28740)

- Verifica Freccia massima carichi totali - CC 46

$f_{z,G}=0.01$ (L/3421) $f_{z,L}=0.00$ (L/15158)

- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X1=0.00$ - Classe 3
 Sollecitazioni: $N=865.08$ $T_z=76.26$ $M_y=-25.87$ $T_y=-225.47$ $M_z=92.70$ $M_x=-21.08$
 Tensioni: $\sigma_N=66.54$ $\sigma_M=482.74$ $\tau=51.09$ $\sigma_{max}=549.29$
 Tensioni: $\sigma_N=66.54$ $\sigma_M=80.08$ $\tau=95.90$ $\tau_{max}=95.90$
 Tensioni: $\sigma_N=66.54$ $\sigma_M=482.74$ $\tau=51.09$ $\sigma_{TD,max}=556.37$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 67 SLU $X1=0.43$
 Sollecitazioni: $N=572.08$ $T_z=-13.92$ $M_y=-8.15$ $T_y=-106.88$ $M_x=-4.80$
 $V,Ed=-106.88$ $V_c,Rd,Red=10810.90$ $V,Ed/V_c,Rd,Red=0.01$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-13.92$ $V_c,Rd,Red=14414.60$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=779.94$ $T_z=86.88$ $M_y=-10.18$ $T_y=-132.59$ $M_z=54.24$ $M_x=-16.08$
 Tensioni: $\sigma_N=60.00$ $\sigma_M=264.95$ $\tau=38.99$ $\sigma_{max}=324.94$
 Tensioni: $\sigma_N=60.00$ $\sigma_M=31.52$ $\tau=65.35$ $\tau_{max}=65.35$
 Tensioni: $\sigma_N=60.00$ $\sigma_M=264.95$ $\tau=38.99$ $\sigma_{TD,max}=331.89$

Asta n. 3796 (-2749 -3440) Tubo 60x100x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
 Sollecitazioni: $N,Ed=-213.34$ $M_y,Ed=-60.53$ $M_z,Ed=-30.64$
 Resistenze: $N_c,Rd=50714.30$ $M_y,c,Rd=1327.02$ $M_z,c,Rd=972.02$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=5.90$ $N_{cr,y}=8930620.00$ $\lambda^*_y=0.08$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=8.90$ $N_{cr,z}=3924920.00$ $\lambda^*_z=0.12$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.04+0.03=0.08$
 Verifica ZZ: $0.00+0.03+0.03=0.07$

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.01$ (L/3580)

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3442)

- Verifica in termini tensionali [4.2.4] - CC 75 SLU $X1=0.21$ - Classe 3
 Sollecitazioni: $N=869.14$ $T_z=140.78$ $M_y=-112.29$ $T_y=-221.48$ $M_z=-51.82$ $M_x=-15.04$
 Tensioni: $\sigma_N=57.94$ $\sigma_M=466.34$ $\tau=28.78$ $\sigma_{max}=524.28$
 Tensioni: $\sigma_N=57.94$ $\sigma_M=257.49$ $\tau=72.13$ $\tau_{max}=72.13$
 Tensioni: $\sigma_N=57.94$ $\sigma_M=466.34$ $\tau=28.78$ $\sigma_{TD,max}=526.64$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 67 SLU $X1=0.00$
 Sollecitazioni: $N=572.08$ $T_z=-13.93$ $M_y=-8.15$ $T_y=-106.87$ $M_x=-4.80$
 $V,Ed=-106.87$ $V_c,Rd,Red=10928.70$ $V,Ed/V_c,Rd,Red=0.01$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=-13.93$ $V_c,Rd,Red=18214.40$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.21$ - Classe 3
 Sollecitazioni: $N=786.34$ $T_z=83.47$ $M_y=-60.53$ $T_y=-131.63$ $M_z=-30.64$ $M_x=-16.08$
 Tensioni: $\sigma_N=52.42$ $\sigma_M=260.78$ $\tau=30.78$ $\sigma_{max}=313.21$
 Tensioni: $\sigma_N=52.42$ $\sigma_M=138.80$ $\tau=56.55$ $\tau_{max}=56.55$
 Tensioni: $\sigma_N=52.42$ $\sigma_M=260.78$ $\tau=30.78$ $\sigma_{TD,max}=317.71$

Asta n. 3796 (-3440 -5807) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-2425.82$ $M_y,Ed=-89.48$ $M_z,Ed=-51.36$
 Resistenze: $N_c,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ $N_{cr,y}=17091600.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ $N_{cr,z}=8991370.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.04+0.03+0.03=0.10$
 Verifica ZZ: $0.04+0.03+0.03=0.09$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X1=0.00$ - Classe 3
 Sollecitazioni: $N=-2425.82$ $T_z=-473.95$ $M_y=-89.48$ $T_y=-73.87$ $M_z=-35.60$ $M_x=-11.45$
 Tensioni: $\sigma_N=-127.67$ $\sigma_M=-215.02$ $\tau=13.27$ $\sigma_{max}=-342.69$
 Tensioni: $\sigma_N=-127.67$ $\sigma_M=-63.06$ $\tau=61.38$ $\tau_{max}=61.38$
 Tensioni: $\sigma_N=-127.67$ $\sigma_M=-215.02$ $\tau=13.27$ $\sigma_{TD,max}=343.46$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 99 SLU $X1=0.08$

Sollecitazioni: $N=570.31$ $T_z=-49.80$ $T_y=-86.60$ $M_z=-36.62$ $M_x=-15.53$
 $V, Ed=-86.60$ $Vc, Rd, Red=14698.70$ $V, Ed/Vc, Rd, Red=0.01$

- Verifica a taglio e torsione dir. Z [4.2.25]

$V, Ed=-49.80$ $Vc, Rd, Red=22048.10$ $V, Ed/Vc, Rd, Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.00$ - Classe 3

Sollecitazioni: $N=788.86$ $T_z=-153.86$ $M_y=-52.81$ $T_y=-85.15$ $M_z=-34.04$ $M_x=-14.83$

Tensioni: $\sigma_N=41.52$ $\sigma_M=153.27$ $\tau=17.20$ $\sigma_{max}=194.79$

Tensioni: $\sigma_N=41.52$ $\sigma_M=-60.29$ $\tau=32.82$ $\tau_{max}=32.82$

Tensioni: $\sigma_N=41.52$ $\sigma_M=153.27$ $\tau=17.20$ $\sigma_{TD, max}=197.05$

Asta n. 3796 (-5807 -8907) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3

Sollecitazioni: $N, Ed=-2887.92$ $M_y, Ed=-27.03$ $M_z, Ed=-75.64$

Resistenze: $Nc, Rd=64238.10$ $M_y, c, Rd=2116.38$ $M_z, c, Rd=1670.05$ $L=21.34$

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=4.80$ $Ncr, y=17091300.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$

$\lambda_z=6.62$ $Ncr, z=8991240.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$

$K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$

Verifica YY: $0.04+0.01+0.04=0.10$

Verifica ZZ: $0.04+0.01+0.04=0.10$

- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X1=0.21$ - Classe 3

Sollecitazioni: $N=2478.99$ $T_z=-82.07$ $M_y=-34.14$ $T_y=-111.71$ $M_z=-130.73$ $M_x=-19.47$

Tensioni: $\sigma_N=130.47$ $\sigma_M=319.20$ $\tau=22.58$ $\sigma_{max}=449.67$

Tensioni: $\sigma_N=130.47$ $\sigma_M=49.99$ $\tau=38.76$ $\tau_{max}=38.76$

Tensioni: $\sigma_N=130.47$ $\sigma_M=319.20$ $\tau=22.58$ $\sigma_{TD, max}=451.37$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.21$ - Classe 3

Sollecitazioni: $N=1219.77$ $T_z=-71.82$ $M_y=-19.51$ $T_y=-64.34$ $M_z=-73.57$ $M_x=-15.11$

Tensioni: $\sigma_N=64.20$ $\sigma_M=180.11$ $\tau=17.52$ $\sigma_{max}=244.31$

Tensioni: $\sigma_N=64.20$ $\sigma_M=28.56$ $\tau=26.85$ $\tau_{max}=26.85$

Tensioni: $\sigma_N=64.20$ $\sigma_M=180.11$ $\tau=17.52$ $\sigma_{TD, max}=246.18$

Asta n. 3797 (-2487 -8539) Tubo circolare $d=70x4$ mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 1

Sollecitazioni: $N, Ed=-3970.52$ $M, Ed=4.08$

Resistenze: $Nc, Rd=28041.00$ $M, c, Rd=575.38$ $L=201.66$

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, ----, ----$

$\lambda=86.26$ $Ncr=23100.80$ $\lambda^*=1.13$

Curva a: $\Phi=1.23$ $\chi_{min}=0.58$

$K_{yy}, K_{yz}, K_{zy}, K_{zz}=1.14, ----, ----, ----$

Verifica: $0.25+0.01=0.25$

- Verifica Freccia massima per soli carichi accidentali - CC 46

$f_{z,6}=0.02$ (L/10335)

- Verifica Freccia massima carichi totali - CC 26

$f_{z,6}=0.02$ (L/10310) $f_{z,1}=0.01$ (L/14911)

- Verifica a compressione [4.2.9] - CC 49 SLU $X1=0.00$ - Classe 1

Sollecitazioni: $N=-3970.52$ $T=8.10$ $M_x=1.74$

$N, Ed=-3970.52$ $Nc, Rd=-28041.00$ $N, Ed/Nc, Rd=0.14$

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 68 SLU $X1=2.02$

Sollecitazioni: $N=-2792.98$ $T=8.10$ $M_x=-2.48$

$V, Ed=8.10$ $Vc, Rd, Red=10256.30$ $V, Ed/Vc, Rd, Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=1.00$ - Classe 3

Sollecitazioni: $N=-2521.58$ $M=3.02$ $M_x=2.81$

Tensioni: $\sigma_N=-304.03$ $\sigma_M=-23.34$ $\tau=10.87$ $\sigma_{max}=-327.37$

Tensioni: $\sigma_N=-304.03$ $\sigma_M=22.99$ $\tau=10.87$ $\tau_{max}=10.87$

Tensioni: $\sigma_N=-304.03$ $\sigma_M=-23.34$ $\tau=10.87$ $\sigma_{TD, max}=327.91$

Asta n. 3798 (-2486 -8537) Tubo circolare $d=70x4$ mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 54 SLU - Classe 1

Sollecitazioni: $N, Ed=-4003.85$ $M, Ed=4.08$

Resistenze: $Nc, Rd=28041.00$ $M, c, Rd=575.38$ $L=201.66$

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, ----, ----$

$\lambda=86.26$ $Ncr=23100.80$ $\lambda^*=1.13$

Curva a: $\Phi=1.23$ $\chi_{min}=0.58$

Kyy, Kyz, Kzy, Kzz=1.14, ----, ----, ----
 Verifica: $0.25+0.01=0.26$

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.02$ (L/10310)
- Verifica Freccia massima carichi totali - CC 26
 $f_{z,g}=0.02$ (L/10260) $f_{z,l}=0.01$ (L/14937)
- Verifica a compressione [4.2.9] - CC 54 SLU $Xl=0.00$ - Classe 1
 Sollecitazioni: $N=-4003.85$ $T=8.10$
 $N,Ed=-4003.85$ $Nc,Rd=-28041.00$ $N,Ed/Nc,Rd=0.14$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 68 SLU $Xl=2.02$
 Sollecitazioni: $N=-2725.09$ $T=8.10$ $M_x=-3.82$
 $V,Ed=8.10$ $Vc,Rd,Red=10229.00$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 9 SND $Xl=1.00$ - Classe 3
 Sollecitazioni: $N=-2421.11$ $M=3.02$ $M_x=-2.23$
 Tensioni: $\sigma_N=-291.92$ $\sigma_M=-23.34$ $\tau=8.62$ $\sigma_{max}=-315.26$
 Tensioni: $\sigma_N=-291.92$ $\sigma_M=-0.00$ $\tau=8.62$ $\tau_{max}=8.62$
 Tensioni: $\sigma_N=-291.92$ $\sigma_M=-23.34$ $\tau=8.62$ $\sigma_{ID,max}=315.61$

Asta n. 3799 (-9376 -8917) Tubo 60x60x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 1
 Sollecitazioni: $N,Ed=-1298.88$ $My,Ed=-2.77$
 Resistenze: $Nc,Rd=20053.30$ $My,c,Rd=421.84$ $L=153.00$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=66.75$ $Ncr,y=41677.00$ $\lambda_y^*=0.71$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=66.75$ $Ncr,z=41677.00$ $\lambda_z^*=0.71$ Curva a: $\Phi_z=0.81$ $\chi_z=0.84$
 $Kyy, Kyz, Kzy, Kzz=0.99, 0.59, 0.00, 0.99$
 Verifica YY: $0.06+0.01=0.07$
 Verifica ZZ: $0.06=0.06$
- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/28369)
- Verifica a compressione [4.2.9] - CC 45 SLU $Xl=1.53$ - Classe 1
 Sollecitazioni: $N=-1298.88$ $T_z=-7.26$ $M_x=-9.46$
 $N,Ed=-1298.88$ $Nc,Rd=-20053.30$ $N,Ed/Nc,Rd=0.06$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 49 SLU $Xl=1.53$
 Sollecitazioni: $N=-1180.00$ $T_z=-7.26$ $M_x=-10.02$
 $V,Ed=-7.26$ $Vc,Rd,Red=5610.16$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $Xl=0.76$ - Classe 3
 Sollecitazioni: $N=-567.56$ $My=-2.05$ $M_x=-3.77$
 Tensioni: $\sigma_N=-63.34$ $\sigma_M=-13.09$ $\tau=15.03$ $\sigma_{max}=-76.44$
 Tensioni: $\sigma_N=-63.34$ $\sigma_M=13.09$ $\tau=15.03$ $\tau_{max}=15.03$
 Tensioni: $\sigma_N=-63.34$ $\sigma_M=-13.09$ $\tau=15.03$ $\sigma_{ID,max}=80.74$

Asta n. 3800 (-9374 -8901) Tubo 60x60x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 1
 Sollecitazioni: $N,Ed=-1301.27$ $My,Ed=-2.77$
 Resistenze: $Nc,Rd=20053.30$ $My,c,Rd=421.84$ $L=153.00$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=66.75$ $Ncr,y=41677.00$ $\lambda_y^*=0.71$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=66.75$ $Ncr,z=41677.00$ $\lambda_z^*=0.71$ Curva a: $\Phi_z=0.81$ $\chi_z=0.84$
 $Kyy, Kyz, Kzy, Kzz=0.99, 0.59, 0.00, 0.99$
 Verifica YY: $0.06+0.01=0.07$
 Verifica ZZ: $0.06=0.06$
- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/28369)
- Verifica a compressione [4.2.9] - CC 45 SLU $Xl=1.53$ - Classe 1
 Sollecitazioni: $N=-1301.27$ $T_z=-7.26$ $M_x=9.39$
 $N,Ed=-1301.27$ $Nc,Rd=-20053.30$ $N,Ed/Nc,Rd=0.06$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 49 SLU $Xl=1.53$
 Sollecitazioni: $N=-1183.10$ $T_z=-7.26$ $M_x=9.94$
 $V,Ed=-7.26$ $Vc,Rd,Red=5611.64$ $V,Ed/Vc,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $Xl=0.77$ - Classe 3

Sollecitazioni: $N=-620.48$ $M_y=-2.05$ $M_x=3.62$
 Tensioni: $\sigma_N=-69.25$ $\sigma_M=-13.09$ $\tau=14.44$ $\sigma_{max}=-82.34$
 Tensioni: $\sigma_N=-69.25$ $\sigma_M=13.09$ $\tau=14.44$ $\tau_{max}=14.44$
 Tensioni: $\sigma_N=-69.25$ $\sigma_M=-13.09$ $\tau=14.44$ $\sigma_{ID,max}=86.05$

Asta n. 3815 (-2486 -2806) Tubo 60x80x5 mm - S355 Crit. 3

-
- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.01$ (L/3474) $f_{z,L}=0.00$ (L/26239)
 - Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3154) $f_{z,L}=0.00$ (L/13243)
 - Verifica in termini tensionali [4.2.4] - CC 54 SLU $X1=0.00$ - Classe 3
 Sollecitazioni: $N=2662.45$ $T_z=229.10$ $M_y=-33.46$ $T_y=-306.36$ $M_z=105.46$ $M_x=-46.47$
 Tensioni: $\sigma_N=204.80$ $\sigma_M=563.41$ $\tau=112.66$ $\sigma_{max}=768.22$
 Tensioni: $\sigma_N=204.80$ $\sigma_M=103.55$ $\tau=173.57$ $\tau_{max}=173.57$
 Tensioni: $\sigma_N=204.80$ $\sigma_M=563.41$ $\tau=112.66$ $\sigma_{ID,max}=792.61$
 - Verifica a taglio e torsione dir. Y [4.2.25] - CC 49 SLU $X1=0.33$
 Sollecitazioni: $N=2629.35$ $T_z=266.26$ $M_y=-120.37$ $T_y=-253.49$ $M_x=-37.42$
 $V,Ed=-253.49$ $Vc,Rd,Red=10370.30$ $V,Ed/Vc,Rd,Red=0.02$
 - Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=266.26$ $Vc,Rd,Red=13827.10$ $V,Ed/Vc,Rd,Red=0.02$
 - Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=1593.15$ $T_z=150.33$ $M_y=-13.17$ $T_y=-163.43$ $M_z=56.19$ $M_x=-26.74$
 Tensioni: $\sigma_N=122.55$ $\sigma_M=283.70$ $\tau=64.82$ $\sigma_{max}=406.25$
 Tensioni: $\sigma_N=122.55$ $\sigma_M=40.75$ $\tau=97.32$ $\tau_{max}=97.32$
 Tensioni: $\sigma_N=122.55$ $\sigma_M=283.70$ $\tau=64.82$ $\sigma_{ID,max}=421.47$

Asta n. 3815 (-2806 -3674) Tubo 60x100x5 mm - S355 Crit. 3

-
- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.01$ (L/3524)
 - Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3219) $f_{z,L}=0.00$ (L/19249)
 - Verifica in termini tensionali [4.2.4] - CC 75 SLU $X1=0.21$ - Classe 3
 Sollecitazioni: $N=2690.09$ $T_z=295.65$ $M_y=-189.54$ $T_y=-296.94$ $M_z=-61.73$ $M_x=-36.14$
 Tensioni: $\sigma_N=179.34$ $\sigma_M=697.62$ $\tau=69.17$ $\sigma_{max}=876.96$
 Tensioni: $\sigma_N=179.34$ $\sigma_M=434.62$ $\tau=127.32$ $\tau_{max}=127.32$
 Tensioni: $\sigma_N=179.34$ $\sigma_M=697.62$ $\tau=69.17$ $\sigma_{ID,max}=885.11$
 - Verifica a taglio e torsione dir. Y [4.2.25] - CC 49 SLU $X1=0.00$
 Sollecitazioni: $N=2629.34$ $T_z=266.27$ $M_y=-120.37$ $T_y=-253.57$ $M_x=-37.42$
 $V,Ed=-253.57$ $Vc,Rd,Red=10577.50$ $V,Ed/Vc,Rd,Red=0.02$
 - Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=266.27$ $Vc,Rd,Red=17629.10$ $V,Ed/Vc,Rd,Red=0.02$
 - Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.21$ - Classe 3
 Sollecitazioni: $N=1598.60$ $T_z=147.45$ $M_y=-89.50$ $T_y=-162.68$ $M_z=-33.26$ $M_x=-26.74$
 Tensioni: $\sigma_N=106.57$ $\sigma_M=343.72$ $\tau=51.17$ $\sigma_{max}=450.29$
 Tensioni: $\sigma_N=106.57$ $\sigma_M=205.22$ $\tau=83.02$ $\tau_{max}=83.02$
 Tensioni: $\sigma_N=106.57$ $\sigma_M=343.72$ $\tau=51.17$ $\sigma_{ID,max}=458.93$

Asta n. 3815 (-3674 -6221) Tubo 80x120x5 mm - S355 Crit. 3

-
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N,Ed=-1588.12$ $M_y,Ed=-141.15$ $M_z,Ed=-62.82$
 Resistenze: $Nc,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ $Ncr,y=17091400.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ $Ncr,z=8991280.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.02+0.05+0.04=0.11$
 Verifica ZZ: $0.02+0.04+0.04=0.10$
 - Verifica in termini tensionali [4.2.4] - CC 75 SLU $X1=0.00$ - Classe 3
 Sollecitazioni: $N=2479.57$ $T_z=-455.18$ $M_y=-168.51$ $T_y=-186.01$ $M_z=-68.91$ $M_x=-34.12$
 Tensioni: $\sigma_N=130.50$ $\sigma_M=408.71$ $\tau=39.56$ $\sigma_{max}=539.21$
 Tensioni: $\sigma_N=130.50$ $\sigma_M=-122.07$ $\tau=85.78$ $\tau_{max}=85.78$

Tensioni: $\sigma_N=130.50$ $\sigma_M=408.71$ $\tau=39.56$ $\sigma_{ID,max}=543.55$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.00$ - Classe 3
Sollecitazioni: $N=1384.34$ $T_z=-212.86$ $M_y=-79.54$ $T_y=-101.25$ $M_z=-37.44$ $M_x=-25.03$
Tensioni: $\sigma_N=72.86$ $\sigma_M=202.88$ $\tau=29.02$ $\sigma_{max}=275.74$
Tensioni: $\sigma_N=72.86$ $\sigma_M=-66.33$ $\tau=50.64$ $\tau_{max}=50.64$
Tensioni: $\sigma_N=72.86$ $\sigma_M=202.88$ $\tau=29.02$ $\sigma_{ID,max}=280.28$

Asta n. 3815 (-6221 -9373) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
Sollecitazioni: $N,Ed=-2586.04$ $M_y,Ed=-40.07$ $M_z,Ed=-90.92$
Resistenze: $N_c,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ $N_{cr,y}=17091500.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ $N_{cr,z}=8991320.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.04+0.01+0.05=0.11$
Verifica ZZ: $0.04+0.01+0.05=0.10$

- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X1=0.21$ - Classe 3
Sollecitazioni: $N=3035.53$ $T_z=-117.44$ $M_y=-55.89$ $T_y=-145.72$ $M_z=-163.43$ $M_x=-43.18$
Tensioni: $\sigma_N=159.76$ $\sigma_M=420.16$ $\tau=50.06$ $\sigma_{max}=579.92$
Tensioni: $\sigma_N=159.76$ $\sigma_M=81.85$ $\tau=71.18$ $\tau_{max}=71.18$
Tensioni: $\sigma_N=159.76$ $\sigma_M=420.16$ $\tau=50.06$ $\sigma_{ID,max}=586.37$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.21$ - Classe 3
Sollecitazioni: $N=1435.00$ $T_z=-69.85$ $M_y=-29.06$ $T_y=-76.95$ $M_z=-83.92$ $M_x=-25.12$
Tensioni: $\sigma_N=75.53$ $\sigma_M=216.31$ $\tau=29.13$ $\sigma_{max}=291.83$
Tensioni: $\sigma_N=75.53$ $\sigma_M=42.56$ $\tau=40.28$ $\tau_{max}=40.28$
Tensioni: $\sigma_N=75.53$ $\sigma_M=216.31$ $\tau=29.13$ $\sigma_{ID,max}=296.16$

Asta n. 3816 (-2487 -2807) Tubo 60x80x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
Sollecitazioni: $N,Ed=-25.43$ $M_y,Ed=-60.12$ $M_z,Ed=-62.49$
Resistenze: $N_c,Rd=43952.40$ $M_y,c,Rd=955.82$ $M_z,c,Rd=801.10$ $L=33.47$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.35$ $N_{cr,y}=2092230.00$ $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=14.31$ $N_{cr,z}=1315160.00$ $\lambda^*_z=0.19$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.00+0.06+0.07=0.13$
Verifica ZZ: $0.00+0.05+0.07=0.12$

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,G}=0.01$ (L/3474) $f_{z,L}=0.00$ (L/26487)

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,G}=0.01$ (L/3147) $f_{z,L}=0.00$ (L/13498)

- Verifica in termini tensionali [4.2.4] - CC 75 SLU $X1=0.00$ - Classe 3
Sollecitazioni: $N=2620.96$ $T_z=239.13$ $M_y=-29.00$ $T_y=290.66$ $M_z=-99.54$ $M_x=38.47$
Tensioni: $\sigma_N=201.61$ $\sigma_M=522.70$ $\tau=93.26$ $\sigma_{max}=724.32$
Tensioni: $\sigma_N=201.61$ $\sigma_M=89.77$ $\tau=151.07$ $\tau_{max}=151.07$
Tensioni: $\sigma_N=201.61$ $\sigma_M=522.70$ $\tau=93.26$ $\sigma_{ID,max}=742.11$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X1=0.33$
Sollecitazioni: $N=2661.31$ $T_z=307.61$ $M_y=-125.83$ $T_y=282.18$ $M_x=28.65$
 $V,Ed=282.18$ $V_c,Rd,Red=10488.70$ $V,Ed/V_c,Rd,Red=0.03$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=307.61$ $V_c,Rd,Red=13984.90$ $V,Ed/V_c,Rd,Red=0.02$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.00$ - Classe 3
Sollecitazioni: $N=1680.85$ $T_z=155.46$ $M_y=-11.85$ $T_y=181.52$ $M_z=-62.49$ $M_x=31.55$
Tensioni: $\sigma_N=129.30$ $\sigma_M=305.65$ $\tau=76.48$ $\sigma_{max}=434.94$
Tensioni: $\sigma_N=129.30$ $\sigma_M=36.67$ $\tau=112.58$ $\tau_{max}=112.58$
Tensioni: $\sigma_N=129.30$ $\sigma_M=305.65$ $\tau=76.48$ $\sigma_{ID,max}=454.67$

Asta n. 3816 (-2807 -3675) Tubo 60x100x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
Sollecitazioni: $N,Ed=-22.71$ $M_y,Ed=-92.69$ $M_z,Ed=36.96$
Resistenze: $N_c,Rd=50714.30$ $M_y,c,Rd=1327.02$ $M_z,c,Rd=972.02$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=5.90$ Ncr, $y=8930630.00$ $\lambda_y^*=0.08$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=8.90$ Ncr, $z=3924920.00$ $\lambda_z^*=0.12$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.07+0.04=0.10
 Verifica ZZ: 0.00+0.05+0.04=0.09

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,G}=0.01$ (L/3469)
- Verifica Freccia massima carichi totali - CC 46
 $f_{z,G}=0.01$ (L/3196) $f_{z,L}=0.00$ (L/19459)
- Verifica in termini tensionali [4.2.4] - CC 54 SLU Xl=0.21 - Classe 3
 Sollecitazioni: N=2664.29 T_z=306.06 M_y=-191.31 T_y=282.26 M_z=59.37 M_x=28.65
 Tensioni: $\sigma_N=177.62$ $\sigma_M=693.94$ $\tau=54.83$ $\sigma_{max}=871.56$
 Tensioni: $\sigma_N=177.62$ $\sigma_M=438.68$ $\tau=110.12$ $\tau_{max}=110.12$
 Tensioni: $\sigma_N=177.62$ $\sigma_M=693.94$ $\tau=54.83$ $\sigma_{ID,max}=876.72$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU Xl=0.00
 Sollecitazioni: N=2661.30 T_z=307.64 M_y=-125.83 T_y=282.26 M_z=28.65
 V,Ed=282.26 Vc,Rd,Red=10671.90 V,Ed/Vc,Rd,Red=0.03
- Verifica a taglio e torsione dir. Z [4.2.25]
 V,Ed=307.64 Vc,Rd,Red=17786.40 V,Ed/Vc,Rd,Red=0.02
- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.21 - Classe 3
 Sollecitazioni: N=1686.38 T_z=152.62 M_y=-92.69 T_y=180.81 M_z=36.96 M_x=31.54
 Tensioni: $\sigma_N=112.42$ $\sigma_M=364.74$ $\tau=60.37$ $\sigma_{max}=477.16$
 Tensioni: $\sigma_N=112.42$ $\sigma_M=212.55$ $\tau=95.77$ $\tau_{max}=95.77$
 Tensioni: $\sigma_N=112.42$ $\sigma_M=364.74$ $\tau=60.37$ $\sigma_{ID,max}=488.49$

Asta n. 3816 (-3675 -6230) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-1581.48 M_y,Ed=-140.40 M_z,Ed=62.91
 Resistenze: Nc,Rd=64238.10 M_y,c,Rd=2116.38 M_z,c,Rd=1670.05 L=21.34
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=4.80$ Ncr, $y=17091500.00$ $\lambda_y^*=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ Ncr, $z=8991320.00$ $\lambda_z^*=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.02+0.05+0.04=0.11
 Verifica ZZ: 0.02+0.04+0.04=0.10
- Verifica in termini tensionali [4.2.4] - CC 54 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=2449.98 T_z=-453.70 M_y=-170.57 T_y=177.13 M_z=65.85 M_x=28.21
 Tensioni: $\sigma_N=128.95$ $\sigma_M=405.80$ $\tau=32.71$ $\sigma_{max}=534.74$
 Tensioni: $\sigma_N=128.95$ $\sigma_M=-116.64$ $\tau=78.78$ $\tau_{max}=78.78$
 Tensioni: $\sigma_N=128.95$ $\sigma_M=405.80$ $\tau=32.71$ $\sigma_{ID,max}=537.74$
- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=1471.71 T_z=-225.24 M_y=-82.40 T_y=119.84 M_z=41.23 M_x=30.22
 Tensioni: $\sigma_N=77.46$ $\sigma_M=215.10$ $\tau=35.04$ $\sigma_{max}=292.56$
 Tensioni: $\sigma_N=77.46$ $\sigma_M=-73.04$ $\tau=57.91$ $\tau_{max}=57.91$
 Tensioni: $\sigma_N=77.46$ $\sigma_M=215.10$ $\tau=35.04$ $\sigma_{ID,max}=298.79$

Asta n. 3816 (-6230 -9377) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: N,Ed=-2623.39 M_y,Ed=-39.78 M_z,Ed=90.76
 Resistenze: Nc,Rd=64238.10 M_y,c,Rd=2116.38 M_z,c,Rd=1670.05 L=21.34
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=4.80$ Ncr, $y=17091500.00$ $\lambda_y^*=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ Ncr, $z=8991320.00$ $\lambda_z^*=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.04+0.01+0.05=0.11
 Verifica ZZ: 0.04+0.01+0.05=0.10
- Verifica in termini tensionali [4.2.4] - CC 75 SLU Xl=0.21 - Classe 3
 Sollecitazioni: N=2947.82 T_z=-117.23 M_y=-56.01 T_y=154.34 M_z=157.21 M_x=34.28
 Tensioni: $\sigma_N=155.15$ $\sigma_M=407.74$ $\tau=39.75$ $\sigma_{max}=562.88$
 Tensioni: $\sigma_N=155.15$ $\sigma_M=82.03$ $\tau=62.11$ $\tau_{max}=62.11$
 Tensioni: $\sigma_N=155.15$ $\sigma_M=407.74$ $\tau=39.75$ $\sigma_{ID,max}=567.08$
- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.21 - Classe 3
 Sollecitazioni: N=1570.04 T_z=-77.07 M_y=-29.28 T_y=81.01 M_z=93.15 M_x=28.71

Tensioni: $\sigma_N=82.63$ $\sigma_M=235.36$ $\tau=33.29$ $\sigma_{max}=318.00$
 Tensioni: $\sigma_N=82.63$ $\sigma_M=42.88$ $\tau=45.03$ $\tau_{max}=45.03$
 Tensioni: $\sigma_N=82.63$ $\sigma_M=235.36$ $\tau=33.29$ $\sigma_{ID,max}=323.18$

Asta n. 3817 (-2541 -8982) Tubo circolare d=90x4 mm - S355 Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 54 SLU - Classe 1

Sollecitazioni: N,Ed=-6097.03 M,Ed=6.06
 Resistenze: Nc,Rd=36538.20 M,c,Rd=976.45 L=212.44
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, \text{----}, \text{----}$
 $\lambda=69.79$ Ncr=45984.70 $\lambda^*=0.91$
 Curva a: $\Phi=0.99$ $\chi_{min}=0.73$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=1.11, \text{----}, \text{----}, \text{----}$
 Verifica: 0.23+0.01=0.24

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.02$ (L/11876)

- Verifica Freccia massima carichi totali - CC 26
 $f_{z,g}=0.02$ (L/12268) $f_{z,l}=0.01$ (L/21056)

- Verifica a compressione [4.2.9] - CC 54 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=-6097.03 T=11.42 $M_x=18.91$
 N,Ed=-6097.03 Nc,Rd=-36538.20 N,Ed/Nc,Rd=0.17

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 54 SLU Xl=0.00
 Sollecitazioni: N=-6097.03 T=11.42 $M_x=18.91$
 V,Ed=11.42 Vc,Rd,Red=13137.70 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=1.06 - Classe 3
 Sollecitazioni: N=-3382.50 M=4.49 $M_x=12.22$
 Tensioni: $\sigma_N=-312.99$ $\sigma_M=-20.18$ $\tau=27.45$ $\sigma_{max}=-333.17$
 Tensioni: $\sigma_N=-312.99$ $\sigma_M=-19.87$ $\tau=27.45$ $\tau_{max}=27.45$
 Tensioni: $\sigma_N=-312.99$ $\sigma_M=-20.18$ $\tau=27.45$ $\sigma_{ID,max}=336.54$

Asta n. 3818 (-2539 -8984) Tubo circolare d=90x4 mm - S355 Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 54 SLU - Classe 1

Sollecitazioni: N,Ed=-6130.82 M,Ed=6.06
 Resistenze: Nc,Rd=36538.20 M,c,Rd=976.45 L=212.52
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, \text{----}, \text{----}$
 $\lambda=69.82$ Ncr=45947.00 $\lambda^*=0.91$
 Curva a: $\Phi=0.99$ $\chi_{min}=0.72$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=1.11, \text{----}, \text{----}, \text{----}$
 Verifica: 0.23+0.01=0.24

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.02$ (L/11880)

- Verifica Freccia massima carichi totali - CC 26
 $f_{z,g}=0.02$ (L/12206) $f_{z,l}=0.01$ (L/21115)

- Verifica a compressione [4.2.9] - CC 54 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=-6130.82 T=11.42 $M_x=-12.46$
 N,Ed=-6130.82 Nc,Rd=-36538.20 N,Ed/Nc,Rd=0.17

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 89 SLU Xl=2.12
 Sollecitazioni: N=-4358.15 T=11.42 $M_x=-26.67$
 V,Ed=11.42 Vc,Rd,Red=13017.70 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=1.06 - Classe 3
 Sollecitazioni: N=-3570.52 M=4.49 $M_x=-14.85$
 Tensioni: $\sigma_N=-330.39$ $\sigma_M=-20.19$ $\tau=33.36$ $\sigma_{max}=-350.57$
 Tensioni: $\sigma_N=-330.39$ $\sigma_M=-3.51$ $\tau=33.36$ $\tau_{max}=33.36$
 Tensioni: $\sigma_N=-330.39$ $\sigma_M=-20.19$ $\tau=33.36$ $\sigma_{ID,max}=355.30$

Asta n. 3819 (-9727 -9367) Tubo 60x60x4 mm - S235 Crit. 2

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 1

Sollecitazioni: N,Ed=-1416.58 $M_y, Ed=-2.77$
 Resistenze: Nc,Rd=20053.30 $M_y, c, Rd=421.84$ L=153.00
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=66.75$ Ncr,y=41677.10 $\lambda_y^*=0.71$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=66.75$ Ncr,z=41677.10 $\lambda_z^*=0.71$ Curva a: $\Phi_z=0.81$ $\chi_z=0.84$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.99, 0.59, 0.00, 0.99$
 Verifica YY: 0.07+0.01=0.08

Verifica ZZ: 0.07=0.07

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/28622)
- Verifica a compressione [4.2.9] - CC 45 SLU $X_1=1.53$ - Classe 1
 Sollecitazioni: $N=-1416.58$ $T_z=-7.26$ $M_x=6.51$
 $N,Ed=-1416.58$ $N_c,Rd=-20053.30$ $N,Ed/N_c,Rd=0.07$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 45 SLU $X_1=0.00$
 Sollecitazioni: $N=-1416.32$ $T_z=7.26$ $M_x=6.51$
 $V,Ed=7.26$ $V_c,Rd,Red=5672.77$ $V,Ed/V_c,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.77$ - Classe 3
 Sollecitazioni: $N=-535.72$ $M_y=-2.05$ $M_x=2.64$
 Tensioni: $\sigma_N=-59.79$ $\sigma_M=-13.09$ $\tau=10.54$ $\sigma_{max}=-72.88$
 Tensioni: $\sigma_N=-59.79$ $\sigma_M=13.09$ $\tau=10.54$ $\tau_{max}=10.54$
 Tensioni: $\sigma_N=-59.79$ $\sigma_M=-13.09$ $\tau=10.54$ $\sigma_{ID,max}=75.13$

Asta n. 3820 (-9740 -9383) Tubo 60x60x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 1
 Sollecitazioni: $N,Ed=-1414.39$ $M_y,Ed=-2.77$
 Resistenze: $N_c,Rd=20053.30$ $M_y,c,Rd=421.84$ $L=153.00$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=66.75$ $N_{cr,y}=41677.10$ $\lambda_y^*=0.71$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=66.75$ $N_{cr,z}=41677.10$ $\lambda_z^*=0.71$ Curva a: $\Phi_z=0.81$ $\chi_z=0.84$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.99, 0.59, 0.00, 0.99$
 Verifica YY: 0.07+0.01=0.08
 Verifica ZZ: 0.07=0.07

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/28880)
- Verifica a compressione [4.2.9] - CC 45 SLU $X_1=1.53$ - Classe 1
 Sollecitazioni: $N=-1414.39$ $T_z=-7.26$ $M_x=-6.63$
 $N,Ed=-1414.39$ $N_c,Rd=-20053.30$ $N,Ed/N_c,Rd=0.07$
- Verifica a taglio e torsione dir. Z [4.2.25] - CC 49 SLU $X_1=0.00$
 Sollecitazioni: $N=-1176.60$ $T_z=7.26$ $M_x=-6.65$
 $V,Ed=7.26$ $V_c,Rd,Red=5670.34$ $V,Ed/V_c,Rd,Red=0.00$
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.77$ - Classe 3
 Sollecitazioni: $N=-501.51$ $M_y=-2.05$ $M_x=-2.60$
 Tensioni: $\sigma_N=-55.97$ $\sigma_M=-13.09$ $\tau=10.37$ $\sigma_{max}=-69.06$
 Tensioni: $\sigma_N=-55.97$ $\sigma_M=13.09$ $\tau=10.37$ $\tau_{max}=10.37$
 Tensioni: $\sigma_N=-55.97$ $\sigma_M=-13.09$ $\tau=10.37$ $\sigma_{ID,max}=71.36$

Asta n. 3837 (-2541 -2872) Tubo 60x80x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.01$ (L/3590)
- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3376)
- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=1689.83$ $T_z=1111.90$ $M_y=125.51$ $T_y=-628.98$ $M_z=250.99$ $M_x=-85.10$
 Tensioni: $\sigma_N=129.99$ $\sigma_M=1503.25$ $\tau=206.30$ $\sigma_{max}=1633.23$
 Tensioni: $\sigma_N=129.99$ $\sigma_M=-882.74$ $\tau=377.34$ $\tau_{max}=377.34$
 Tensioni: $\sigma_N=129.99$ $\sigma_M=1503.25$ $\tau=206.30$ $\sigma_{ID,max}=1671.87$
- Verifica a taglio e torsione dir. Y [4.2.25] - CC 37 SLU $X_1=0.11$
 Sollecitazioni: $N=1087.45$ $T_z=542.82$ $T_y=-330.44$ $M_z=97.89$ $M_x=-32.64$
 $V,Ed=-330.44$ $V_c,Rd,Red=10434.80$ $V,Ed/V_c,Rd,Red=0.03$
- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=542.82$ $V_c,Rd,Red=13913.10$ $V,Ed/V_c,Rd,Red=0.04$
- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=1058.44$ $T_z=508.96$ $M_y=63.21$ $T_y=-301.01$ $M_z=120.78$ $M_x=-41.19$
 Tensioni: $\sigma_N=81.42$ $\sigma_M=733.29$ $\tau=99.84$ $\sigma_{max}=814.71$
 Tensioni: $\sigma_N=81.42$ $\sigma_M=-424.77$ $\tau=178.14$ $\tau_{max}=178.14$
 Tensioni: $\sigma_N=81.42$ $\sigma_M=733.29$ $\tau=99.84$ $\sigma_{ID,max}=832.87$

Asta n. 3837 (-2872 -3956) Tubo 60x100x5 mm - S355 Crit. 3

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- Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z,g}=0.01$ (L/3609)
 - Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/3442) $f_{z,L}=0.00$ (L/11700)
 - Verifica in termini tensionali [4.2.4] - CC 54 SLU $X1=0.21$ - Classe 3
 Sollecitazioni: $N=1695.76$ $T_z=1108.77$ $M_y=-381.41$ $T_y=-629.00$ $M_z=-36.16$ $M_x=-85.10$
 Tensioni: $\sigma_N=113.05$ $\sigma_M=1097.50$ $\tau=162.86$ $\sigma_{max}=1210.55$
 Tensioni: $\sigma_N=113.05$ $\sigma_M=104.80$ $\tau=300.75$ $\tau_{max}=300.75$
 Tensioni: $\sigma_N=113.05$ $\sigma_M=1076.54$ $\tau=263.14$ $\sigma_{ID,max}=1273.92$
 - Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X1=0.16$
 Sollecitazioni: $N=1694.94$ $T_z=1109.21$ $M_y=-316.86$ $T_y=-629.00$ $M_x=-85.10$
 $V,Ed=-629.00$ $V_c,Rd,Red=10064.20$ $V,Ed/V_c,Rd,Red=0.06$
 - Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=1109.21$ $V_c,Rd,Red=16773.60$ $V,Ed/V_c,Rd,Red=0.07$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.21$ - Classe 3
 Sollecitazioni: $N=892.38$ $T_z=581.97$ $M_y=-185.46$ $T_y=-257.38$ $M_z=-18.27$ $M_x=-42.84$
 Tensioni: $\sigma_N=59.49$ $\sigma_M=536.06$ $\tau=81.99$ $\sigma_{max}=595.55$
 Tensioni: $\sigma_N=59.49$ $\sigma_M=52.96$ $\tau=154.32$ $\tau_{max}=154.32$
 Tensioni: $\sigma_N=59.49$ $\sigma_M=525.47$ $\tau=123.02$ $\sigma_{ID,max}=622.56$

Asta n. 3837 (-3956 -6659) Tubo 80x120x5 mm - S355 Crit. 3

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: $N,Ed=-98.70$ $M_y,Ed=-330.82$ $M_z,Ed=-101.61$
 Resistenze: $N_c,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ $N_{cr,y}=17091500.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ $N_{cr,z}=8991320.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.12+0.06=0.18$
 Verifica ZZ: $0.00+0.10+0.06=0.16$

- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X1=0.00$ - Classe 3
 Sollecitazioni: $N=2126.74$ $T_z=-831.47$ $M_y=-338.81$ $T_y=-376.77$ $M_z=-51.25$ $M_x=-80.85$
 Tensioni: $\sigma_N=111.93$ $\sigma_M=645.01$ $\tau=93.73$ $\sigma_{max}=756.94$
 Tensioni: $\sigma_N=111.93$ $\sigma_M=-90.78$ $\tau=178.17$ $\tau_{max}=178.17$
 Tensioni: $\sigma_N=111.93$ $\sigma_M=632.04$ $\tau=136.64$ $\sigma_{ID,max}=780.71$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=1039.58$ $T_z=-395.07$ $M_y=-164.89$ $T_y=-152.35$ $M_z=-23.88$ $M_x=-40.67$
 Tensioni: $\sigma_N=54.71$ $\sigma_M=311.75$ $\tau=47.16$ $\sigma_{max}=366.47$
 Tensioni: $\sigma_N=54.71$ $\sigma_M=-42.29$ $\tau=87.27$ $\tau_{max}=87.27$
 Tensioni: $\sigma_N=54.71$ $\sigma_M=305.71$ $\tau=64.51$ $\sigma_{ID,max}=377.35$

Asta n. 3837 (-6659 -9739) Tubo 80x120x5 mm - S355 Crit. 3

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: $N,Ed=-1556.54$ $M_y,Ed=-143.95$ $M_z,Ed=-178.85$
 Resistenze: $N_c,Rd=64238.10$ $M_y,c,Rd=2116.38$ $M_z,c,Rd=1670.05$ $L=21.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ $N_{cr,y}=17091400.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ $N_{cr,z}=8991280.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.02+0.05+0.10=0.18$
 Verifica ZZ: $0.02+0.04+0.10=0.17$

- Verifica in termini tensionali [4.2.4] - CC 54 SLU $X1=0.00$ - Classe 3
 Sollecitazioni: $N=1446.91$ $T_z=-582.22$ $M_y=-178.81$ $T_y=-289.06$ $M_z=-167.84$ $M_x=-79.95$
 Tensioni: $\sigma_N=76.15$ $\sigma_M=625.43$ $\tau=92.69$ $\sigma_{max}=701.58$
 Tensioni: $\sigma_N=76.15$ $\sigma_M=-297.31$ $\tau=151.82$ $\tau_{max}=151.82$
 Tensioni: $\sigma_N=76.15$ $\sigma_M=625.43$ $\tau=92.69$ $\sigma_{ID,max}=719.72$

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=770.72$ $T_z=-257.95$ $M_y=-78.93$ $T_y=-147.41$ $M_z=-79.20$ $M_x=-38.97$
 Tensioni: $\sigma_N=40.56$ $\sigma_M=286.44$ $\tau=45.18$ $\sigma_{max}=327.00$
 Tensioni: $\sigma_N=40.56$ $\sigma_M=-140.30$ $\tau=71.37$ $\tau_{max}=71.37$
 Tensioni: $\sigma_N=40.56$ $\sigma_M=286.44$ $\tau=45.18$ $\sigma_{ID,max}=336.24$

Asta n. 3838 (-2539 -2873) Tubo 60x80x5 mm - S355 Crit. 3

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
 Sollecitazioni: $N, Ed = -19.85$ $M_y, Ed = 67.86$ $M_z, Ed = -139.00$
 Resistenze: $N_c, Rd = 43952.40$ $M_y, c, Rd = 955.82$ $M_z, c, Rd = 801.10$ $L = 24.40$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 8.27$ $N_{cr, y} = 3935820.00$ $\lambda^*_y = 0.11$ Curva a: $\Phi_y = 0.00$ $\chi_y = 1.00$
 $\lambda_z = 10.44$ $N_{cr, z} = 2474030.00$ $\lambda^*_z = 0.14$ Curva a: $\Phi_z = 0.00$ $\chi_z = 1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00 + 0.07 + 0.16 = 0.23$
 Verifica ZZ: $0.00 + 0.05 + 0.16 = 0.22$

 - Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z, \phi} = 0.01$ (L/3603)

 - Verifica Freccia massima carichi totali - CC 46
 $f_{z, \phi} = 0.01$ (L/3377)

 - Verifica in termini tensionali [4.2.4] - CC 75 SLU $X1 = 0.00$ - Classe 3
 Sollecitazioni: $N = 1541.73$ $T_z = 973.95$ $M_y = 102.17$ $T_y = 606.31$ $M_z = -246.52$ $M_x = 72.33$
 Tensioni: $\sigma_N = 118.59$ $\sigma_M = 1401.81$ $\tau = 175.34$ $\sigma_{max} = 1520.40$
 Tensioni: $\sigma_N = 118.59$ $\sigma_M = -867.02$ $\tau = 325.19$ $\tau_{max} = 325.19$
 Tensioni: $\sigma_N = 118.59$ $\sigma_M = 1401.81$ $\tau = 175.34$ $\sigma_{ID, max} = 1550.44$

 - Verifica a taglio e torsione dir. Y [4.2.25] - CC 41 SLU $X1 = 0.11$
 Sollecitazioni: $N = 1046.09$ $T_z = 993.37$ $T_y = 532.10$ $M_z = -152.29$ $M_x = 92.40$
 $V, Ed = 532.10$ $V_c, Rd, Red = 9627.74$ $V, Ed/V_c, Rd, Red = 0.06$

 - Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed = 993.37$ $V_c, Rd, Red = 12837.00$ $V, Ed/V_c, Rd, Red = 0.08$

 - Verifica in termini tensionali [4.2.4] - CC 9 SND $X1 = 0.00$ - Classe 3
 Sollecitazioni: $N = 998.62$ $T_z = 538.78$ $M_y = 67.86$ $T_y = 340.62$ $M_z = -139.00$ $M_x = 46.30$
 Tensioni: $\sigma_N = 76.82$ $\sigma_M = 826.68$ $\tau = 112.23$ $\sigma_{max} = 903.50$
 Tensioni: $\sigma_N = 76.82$ $\sigma_M = -488.86$ $\tau = 195.13$ $\tau_{max} = 195.13$
 Tensioni: $\sigma_N = 76.82$ $\sigma_M = 826.68$ $\tau = 112.23$ $\sigma_{ID, max} = 924.18$
- Asta n. 3838 (-2873 -3969) Tubo 60x100x5 mm - S355 Crit. 3
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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
 Sollecitazioni: $N, Ed = -17.72$ $M_y, Ed = -179.34$ $M_z, Ed = -55.95$
 Resistenze: $N_c, Rd = 50714.30$ $M_y, c, Rd = 1327.02$ $M_z, c, Rd = 972.02$ $L = 21.45$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 5.93$ $N_{cr, y} = 8843590.00$ $\lambda^*_y = 0.08$ Curva a: $\Phi_y = 0.00$ $\chi_y = 1.00$
 $\lambda_z = 8.94$ $N_{cr, z} = 3886670.00$ $\lambda^*_z = 0.12$ Curva a: $\Phi_z = 0.00$ $\chi_z = 1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00 + 0.13 + 0.05 = 0.18$
 Verifica ZZ: $0.00 + 0.10 + 0.05 = 0.16$

 - Verifica Freccia massima per soli carichi accidentali - CC 46
 $f_{z, \phi} = 0.01$ (L/3569)

 - Verifica Freccia massima carichi totali - CC 46
 $f_{z, \phi} = 0.01$ (L/3407) $f_{z, L} = 0.00$ (L/12493)

 - Verifica in termini tensionali [4.2.4] - CC 89 SLU $X1 = 0.21$ - Classe 3
 Sollecitazioni: $N = 1015.37$ $T_z = 1006.69$ $M_y = -344.98$ $T_y = 532.73$ $M_z = 33.69$ $M_x = 98.02$
 Tensioni: $\sigma_N = 67.69$ $\sigma_M = 996.12$ $\tau = 187.60$ $\sigma_{max} = 1063.81$
 Tensioni: $\sigma_N = 67.69$ $\sigma_M = 97.66$ $\tau = 312.75$ $\tau_{max} = 312.75$
 Tensioni: $\sigma_N = 67.69$ $\sigma_M = 976.59$ $\tau = 272.53$ $\sigma_{ID, max} = 1146.01$

 - Verifica a taglio e torsione dir. Y [4.2.25] - CC 68 SLU $X1 = 0.16$
 Sollecitazioni: $N = 1023.00$ $T_z = 962.01$ $M_y = -282.69$ $T_y = 521.33$ $M_x = 83.73$
 $V, Ed = 521.33$ $V_c, Rd, Red = 10078.90$ $V, Ed/V_c, Rd, Red = 0.05$

 - Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed = 962.01$ $V_c, Rd, Red = 16798.20$ $V, Ed/V_c, Rd, Red = 0.06$

 - Verifica in termini tensionali [4.2.4] - CC 9 SND $X1 = 0.21$ - Classe 3
 Sollecitazioni: $N = 1003.12$ $T_z = 536.24$ $M_y = -179.34$ $T_y = 339.98$ $M_z = 19.62$ $M_x = 46.30$
 Tensioni: $\sigma_N = 66.87$ $\sigma_M = 525.17$ $\tau = 88.60$ $\sigma_{max} = 592.04$
 Tensioni: $\sigma_N = 66.87$ $\sigma_M = 56.87$ $\tau = 155.30$ $\tau_{max} = 155.30$
 Tensioni: $\sigma_N = 66.87$ $\sigma_M = 513.80$ $\tau = 142.80$ $\sigma_{ID, max} = 631.15$
- Asta n. 3838 (-3969 -6660) Tubo 80x120x5 mm - S355 Crit. 3
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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3

Sollecitazioni: N,Ed=-215.70 My,Ed=-316.21 Mz,Ed=102.67
 Resistenze: Nc,Rd=64238.10 My,c,Rd=2116.38 Mz,c,Rd=1670.05 L=21.34
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ Ncr,y=17091400.00 $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ Ncr,z=8991280.00 $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.12+0.06=0.18
 Verifica ZZ: 0.00+0.09+0.06=0.15

- Verifica in termini tensionali [4.2.4] - CC 75 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=1937.88 Tz=-754.61 My=-305.47 Ty=378.40 Mz=45.44 Mx=71.04
 Tensioni: $\sigma_N=101.99$ $\sigma_M=579.99$ $\tau=82.36$ $\sigma_{max}=681.99$
 Tensioni: $\sigma_N=101.99$ $\sigma_M=-80.49$ $\tau=159.00$ $\tau_{max}=159.00$
 Tensioni: $\sigma_N=101.99$ $\sigma_M=568.49$ $\tau=125.45$ $\sigma_{ID,max}=704.82$

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=1122.17 Tz=-391.44 My=-159.12 Ty=215.71 Mz=26.61 Mx=44.86
 Tensioni: $\sigma_N=59.06$ $\sigma_M=308.06$ $\tau=52.01$ $\sigma_{max}=367.12$
 Tensioni: $\sigma_N=59.06$ $\sigma_M=-47.13$ $\tau=91.76$ $\tau_{max}=91.76$
 Tensioni: $\sigma_N=59.06$ $\sigma_M=301.32$ $\tau=76.57$ $\sigma_{ID,max}=384.01$

Asta n. 3838 (-6660 -9741) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 49 SLU - Classe 3
 Sollecitazioni: N,Ed=-1595.06 My,Ed=-136.11 Mz,Ed=183.46
 Resistenze: Nc,Rd=64238.10 My,c,Rd=2116.38 Mz,c,Rd=1670.05 L=21.34
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.80$ Ncr,y=17091500.00 $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.62$ Ncr,z=8991320.00 $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.02+0.05+0.10=0.18
 Verifica ZZ: 0.02+0.04+0.10=0.17

- Verifica in termini tensionali [4.2.4] - CC 75 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=1436.04 Tz=-509.89 My=-160.95 Ty=317.17 Mz=157.01 Mx=65.23
 Tensioni: $\sigma_N=75.58$ $\sigma_M=574.98$ $\tau=75.63$ $\sigma_{max}=650.56$
 Tensioni: $\sigma_N=75.58$ $\sigma_M=-278.12$ $\tau=127.43$ $\tau_{max}=127.43$
 Tensioni: $\sigma_N=75.58$ $\sigma_M=574.98$ $\tau=75.63$ $\sigma_{ID,max}=663.62$

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=731.60 Tz=-277.76 My=-83.13 Ty=169.65 Mz=88.32 Mx=42.37
 Tensioni: $\sigma_N=38.51$ $\sigma_M=311.62$ $\tau=49.13$ $\sigma_{max}=350.12$
 Tensioni: $\sigma_N=38.51$ $\sigma_M=-156.46$ $\tau=77.34$ $\tau_{max}=77.34$
 Tensioni: $\sigma_N=38.51$ $\sigma_M=311.62$ $\tau=49.13$ $\sigma_{ID,max}=360.31$

Asta n. 3839 (-10251 -9747) Tubo 60x60x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 1
 Sollecitazioni: N,Ed=-1546.84 My,Ed=-2.77
 Resistenze: Nc,Rd=20053.30 My,c,Rd=421.84 L=153.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=66.75$ Ncr,y=41677.10 $\lambda^*_y=0.71$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=66.75$ Ncr,z=41677.10 $\lambda^*_z=0.71$ Curva a: $\Phi_z=0.81$ $\chi_z=0.84$
 Kyy, Kyz, Kzy, Kzz=0.99, 0.60, 0.00, 0.99
 Verifica YY: 0.08+0.01=0.08
 Verifica ZZ: 0.08=0.08

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,g}=0.01$ (L/28609)

- Verifica a compressione [4.2.9] - CC 45 SLU Xl=1.53 - Classe 1
 Sollecitazioni: N=-1546.84 Tz=-7.25 Mx=-3.86
 N,Ed=-1546.84 Nc,Rd=-20053.30 N,Ed/Nc,Rd=0.08

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 49 SLU Xl=0.00
 Sollecitazioni: N=-1094.04 Tz=7.25 Mx=-3.91
 V,Ed=7.25 Vc,Rd,Red=5719.27 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.77 - Classe 3
 Sollecitazioni: N=-366.81 My=-2.05 Mx=-2.06
 Tensioni: $\sigma_N=-40.94$ $\sigma_M=-13.08$ $\tau=8.21$ $\sigma_{max}=-54.02$
 Tensioni: $\sigma_N=-40.94$ $\sigma_M=13.08$ $\tau=8.21$ $\tau_{max}=8.21$
 Tensioni: $\sigma_N=-40.94$ $\sigma_M=-13.08$ $\tau=8.21$ $\sigma_{ID,max}=55.86$

Asta n. 3840 (-10249 -9734) Tubo 60x60x4 mm - S235 Crit. 2

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 1
 Sollecitazioni: $N, Ed = -1540.84$ My, Ed = -2.77
 Resistenze: $N_c, Rd = 20053.30$ My, c, Rd = 421.84 L = 153.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 66.75$ Ncr, $y = 41677.10$ $\lambda_y^* = 0.71$ Curva a: $\Phi_y = 0.81$ $\chi_y = 0.84$
 $\lambda_z = 66.75$ Ncr, $z = 41677.10$ $\lambda_z^* = 0.71$ Curva a: $\Phi_z = 0.81$ $\chi_z = 0.84$
 Kyy, Kyz, Kzy, Kzz = 0.99, 0.60, 0.00, 0.99
 Verifica YY: $0.08 + 0.01 = 0.08$
 Verifica ZZ: $0.08 = 0.08$

- Verifica Freccia massima carichi totali - CC 46
 $f_{z,6} = 0.01$ (L/29397)

- Verifica a compressione [4.2.9] - CC 45 SLU Xl = 1.53 - Classe 1
 Sollecitazioni: $N = -1540.84$ $T_z = -7.25$ $M_x = 3.84$
 $N, Ed = -1540.84$ $N_c, Rd = -20053.30$ $N, Ed / N_c, Rd = 0.08$

- Verifica a taglio e torsione dir. Z [4.2.25] - CC 49 SLU Xl = 0.00
 Sollecitazioni: $N = -1086.30$ $T_z = 7.25$ $M_x = 3.88$
 $V, Ed = 7.25$ $V_c, Rd, Red = 5719.77$ $V, Ed / V_c, Rd, Red = 0.00$

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl = 0.77 - Classe 3
 Sollecitazioni: $N = -366.04$ $M_y = -2.05$ $M_x = 2.06$
 Tensioni: $\sigma_N = -40.85$ $\sigma_M = -13.08$ $\tau = 8.20$ $\sigma_{max} = -53.93$
 Tensioni: $\sigma_N = -40.85$ $\sigma_M = 13.08$ $\tau = 8.20$ $\tau_{max} = 8.20$
 Tensioni: $\sigma_N = -40.85$ $\sigma_M = -13.08$ $\tau = 8.20$ $\sigma_{ID, max} = 55.77$

Asta n. 3997 (-4538 -4540) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N, Ed = -209.68$ My, Ed = -96.26 Mz, Ed = -0.54
 Resistenze: $N_c, Rd = 30796.20$ My, c, Rd = 951.93 Mz, c, Rd = 632.38 L = 14.09
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 3.27$ Ncr, $y = 26643900.00$ $\lambda_y^* = 0.03$ Curva a: $\Phi_y = 0.00$ $\chi_y = 1.00$
 $\lambda_z = 5.68$ Ncr, $z = 8849970.00$ $\lambda_z^* = 0.06$ Curva a: $\Phi_z = 0.00$ $\chi_z = 1.00$
 Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
 Verifica YY: $0.01 + 0.10 + 0.00 = 0.10$
 Verifica ZZ: $0.01 + 0.08 + 0.00 = 0.08$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl = 0.01 - Classe 3
 Sollecitazioni: $N = -1701.26$ $T_z = 199.65$ $M_y = 31.08$ $T_y = -38.93$ $M_z = -1.42$ $M_x = -24.77$
 Tensioni: $\sigma_N = -123.64$ $\sigma_M = -78.10$ $\tau = 47.66$ $\sigma_{max} = -201.74$
 Tensioni: $\sigma_N = -123.64$ $\sigma_M = 4.36$ $\tau = 73.54$ $\tau_{max} = 73.54$
 Tensioni: $\sigma_N = -123.64$ $\sigma_M = -77.43$ $\tau = 55.37$ $\sigma_{ID, max} = 222.77$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU Xl = 0.00
 Sollecitazioni: $N = 181.44$ $T_z = 268.37$ $M_y = -27.75$ $T_y = 4.21$ $M_x = -41.69$
 $V, Ed = 4.21$ $V_c, Rd, Red = 5558.96$ $V, Ed / V_c, Rd, Red = 0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V, Ed = 268.37$ $V_c, Rd, Red = 11117.90$ $V, Ed / V_c, Rd, Red = 0.02$

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl = 0.14 - Classe 3
 Sollecitazioni: $N = 340.39$ $T_z = 179.63$ $M_y = -96.26$ $T_y = -4.32$ $M_x = -29.59$
 Tensioni: $\sigma_N = 24.74$ $\sigma_M = 226.32$ $\tau = 56.93$ $\sigma_{max} = 251.06$
 Tensioni: $\sigma_N = 24.74$ $\sigma_M = 0.00$ $\tau = 80.22$ $\tau_{max} = 80.22$
 Tensioni: $\sigma_N = 24.74$ $\sigma_M = 226.32$ $\tau = 57.96$ $\sigma_{ID, max} = 270.39$

Asta n. 3997 (-4531 -4538) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
 Sollecitazioni: $N, Ed = -2052.65$ My, Ed = 71.99 Mz, Ed = -4.03
 Resistenze: $N_c, Rd = 30796.20$ My, c, Rd = 951.93 Mz, c, Rd = 632.38 L = 14.09
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 3.27$ Ncr, $y = 26644100.00$ $\lambda_y^* = 0.03$ Curva a: $\Phi_y = 0.00$ $\chi_y = 1.00$
 $\lambda_z = 5.68$ Ncr, $z = 8850040.00$ $\lambda_z^* = 0.06$ Curva a: $\Phi_z = 0.00$ $\chi_z = 1.00$
 Kyy, Kyz, Kzy, Kzz = 0.95, 0.95, 0.76, 0.95
 Verifica YY: $0.07 + 0.06 + 0.01 = 0.13$
 Verifica ZZ: $0.07 + 0.05 + 0.01 = 0.12$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU Xl = 0.00 - Classe 3
 Sollecitazioni: $N = -2052.65$ $T_z = 208.26$ $M_y = 71.99$ $T_y = -8.29$ $M_z = -2.86$ $M_x = -23.65$
 Tensioni: $\sigma_N = -149.18$ $\sigma_M = -179.39$ $\tau = 45.51$ $\sigma_{max} = -328.56$
 Tensioni: $\sigma_N = -149.18$ $\sigma_M = 8.79$ $\tau = 72.51$ $\tau_{max} = 72.51$

Tensioni: $\sigma_N=-149.18$ $\sigma_M=-179.39$ $\tau=45.51$ $\sigma_{ID,max}=337.89$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X_1=0.00$
Sollecitazioni: $N=235.03$ $T_z=277.97$ $M_y=23.69$ $T_y=1.43$ $M_x=-39.83$
 $V,Ed=1.43$ $Vc,Rd,Red=5575.37$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=277.97$ $Vc,Rd,Red=11150.70$ $V,Ed/Vc,Rd,Red=0.02$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.14$ - Classe 3
Sollecitazioni: $N=336.93$ $T_z=182.37$ $M_y=-63.46$ $T_y=2.01$ $M_x=-28.49$
Tensioni: $\sigma_N=24.49$ $\sigma_M=149.21$ $\tau=54.82$ $\sigma_{max}=173.69$
Tensioni: $\sigma_N=24.49$ $\sigma_M=0.00$ $\tau=78.46$ $\tau_{max}=78.46$
Tensioni: $\sigma_N=24.49$ $\sigma_M=139.26$ $\tau=67.26$ $\sigma_{ID,max}=200.96$

Asta n. 3997 (-4527 -4531) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
Sollecitazioni: $N,Ed=-2504.12$ $M_y,Ed=117.76$ $M_z,Ed=-15.30$
Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=14.09$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=3.27$ $N_{cr,y}=26643900.00$ $\lambda^*_y=0.03$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=5.68$ $N_{cr,z}=8849970.00$ $\lambda^*_z=0.06$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.08+0.09+0.02=0.20$
Verifica ZZ: $0.08+0.08+0.02=0.18$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X_1=0.00$ - Classe 3
Sollecitazioni: $N=-2504.12$ $T_z=251.72$ $M_y=117.76$ $T_y=77.30$ $M_z=-15.30$ $M_x=-21.26$
Tensioni: $\sigma_N=-181.99$ $\sigma_M=-331.00$ $\tau=40.92$ $\sigma_{max}=-512.99$
Tensioni: $\sigma_N=-181.99$ $\sigma_M=46.92$ $\tau=73.55$ $\tau_{max}=73.55$
Tensioni: $\sigma_N=-181.99$ $\sigma_M=-331.00$ $\tau=40.92$ $\sigma_{ID,max}=517.86$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X_1=0.08$
Sollecitazioni: $N=296.38$ $T_z=331.42$ $M_y=59.34$ $T_y=-8.51$ $M_x=-36.18$
 $V,Ed=-8.51$ $Vc,Rd,Red=5607.54$ $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=331.42$ $Vc,Rd,Red=11215.10$ $V,Ed/Vc,Rd,Red=0.03$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3
Sollecitazioni: $N=315.39$ $T_z=218.75$ $M_y=62.51$ $T_y=-6.55$ $M_x=-26.47$
Tensioni: $\sigma_N=22.92$ $\sigma_M=146.97$ $\tau=50.94$ $\sigma_{max}=169.90$
Tensioni: $\sigma_N=22.92$ $\sigma_M=-0.00$ $\tau=79.30$ $\tau_{max}=79.30$
Tensioni: $\sigma_N=22.92$ $\sigma_M=137.18$ $\tau=65.86$ $\sigma_{ID,max}=196.58$

Asta n. 3999 (-4525 -4527) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3
Sollecitazioni: $N,Ed=-3366.36$ $M_y,Ed=160.98$ $M_z,Ed=38.60$
Resistenze: $Nc,Rd=30796.20$ $M_y,c,Rd=951.93$ $M_z,c,Rd=632.38$ $L=13.86$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=3.22$ $N_{cr,y}=27515900.00$ $\lambda^*_y=0.03$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=5.59$ $N_{cr,z}=9139600.00$ $\lambda^*_z=0.06$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.11+0.13+0.06=0.30$
Verifica ZZ: $0.11+0.10+0.06=0.27$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X_1=0.00$ - Classe 3
Sollecitazioni: $N=-3366.36$ $T_z=216.80$ $M_y=160.98$ $T_y=-454.52$ $M_z=38.60$ $M_x=3.00$
Tensioni: $\sigma_N=-244.65$ $\sigma_M=-515.11$ $\tau=5.78$ $\sigma_{max}=-759.75$
Tensioni: $\sigma_N=-244.65$ $\sigma_M=353.25$ $\tau=114.01$ $\tau_{max}=114.01$
Tensioni: $\sigma_N=-244.65$ $\sigma_M=-515.11$ $\tau=5.78$ $\sigma_{ID,max}=759.82$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X_1=0.09$
Sollecitazioni: $N=413.16$ $T_z=283.86$ $M_y=120.86$ $T_y=59.16$ $M_x=-18.92$
 $V,Ed=59.16$ $Vc,Rd,Red=5759.89$ $V,Ed/Vc,Rd,Red=0.01$

- Verifica a taglio e torsione dir. Z [4.2.25]
 $V,Ed=283.86$ $Vc,Rd,Red=11519.80$ $V,Ed/Vc,Rd,Red=0.02$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3
Sollecitazioni: $N=335.04$ $T_z=194.19$ $M_y=65.79$ $T_y=40.11$ $M_z=-4.86$ $M_x=-25.08$
Tensioni: $\sigma_N=24.35$ $\sigma_M=171.88$ $\tau=48.25$ $\sigma_{max}=196.23$
Tensioni: $\sigma_N=24.35$ $\sigma_M=14.91$ $\tau=73.43$ $\tau_{max}=73.43$

Tensioni: $\sigma_N=24.35$ $\sigma_M=169.58$ $\tau=56.20$ $\sigma_{ID,max}=216.99$

Asta n. 3999 (-4524 -4525) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 45 SLU - Classe 3

Sollecitazioni: $N, Ed=-3464.21$ $M_y, Ed=146.03$ $M_z, Ed=31.03$

Resistenze: $N_c, Rd=30796.20$ $M_y, c, Rd=951.93$ $M_z, c, Rd=632.38$ $L=13.86$

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=3.22$ $N_{cr,y}=27515800.00$ $\lambda^*_y=0.03$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$

$\lambda_z=5.59$ $N_{cr,z}=9139590.00$ $\lambda^*_z=0.06$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$

$K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$

Verifica YY: $0.11+0.12+0.05=0.28$

Verifica ZZ: $0.11+0.09+0.05=0.25$

- Verifica in termini tensionali [4.2.4] - CC 45 SLU $X1=0.14$ - Classe 3

Sollecitazioni: $N=-3464.21$ $T_z=-383.81$ $M_y=146.03$ $T_y=-159.89$ $M_z=8.86$ $M_x=-10.30$

Tensioni: $\sigma_N=-251.76$ $\sigma_M=-374.71$ $\tau=19.83$ $\sigma_{max}=-626.47$

Tensioni: $\sigma_N=-251.76$ $\sigma_M=27.19$ $\tau=69.61$ $\tau_{max}=69.61$

Tensioni: $\sigma_N=-251.76$ $\sigma_M=-370.53$ $\tau=51.52$ $\sigma_{ID,max}=628.65$

- Verifica a taglio e torsione dir. Y [4.2.25] - CC 54 SLU $X1=0.00$

Sollecitazioni: $N=33.28$ $T_z=79.50$ $M_y=151.93$ $T_y=-18.00$ $M_x=-45.72$

$V, Ed=-18.00$ $V_c, Rd, Red=5523.40$ $V, Ed/V_c, Rd, Red=0.00$

- Verifica a taglio e torsione dir. Z [4.2.25]

$V, Ed=79.50$ $V_c, Rd, Red=11046.80$ $V, Ed/V_c, Rd, Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3

Sollecitazioni: $N=71.51$ $T_z=152.73$ $M_y=68.85$ $T_y=42.40$ $M_z=3.93$ $M_x=-26.34$

Tensioni: $\sigma_N=5.20$ $\sigma_M=175.78$ $\tau=50.69$ $\sigma_{max}=180.98$

Tensioni: $\sigma_N=5.20$ $\sigma_M=-12.05$ $\tau=70.49$ $\tau_{max}=70.49$

Tensioni: $\sigma_N=5.20$ $\sigma_M=173.93$ $\tau=59.09$ $\sigma_{ID,max}=206.31$

Membratura

Asta n. 2066 (-2477 1901 -2442 -2426 -2363) Tubo circolare $d=101.6 \times 6$ mm - S355 Crit. 3

- Verifica di stabilità (4.2.4.1.3.1) - CC 45 SLU

Sollecitazioni: $N=-3298.66$ $L=416.47$

$\lambda=122.97$ $N_{cr}=24697.30$ $\lambda^*=1.61$

Curva a: $\Phi=1.94$ $\chi, \min=0.33$ $N, Ed=-3298.66$ $N_b, Rd=20094.90$ $N, Ed/N_b, Rd=0.16$

- Verifica Freccia massima per soli carichi accidentali - CC 116

$f_{z,L}=1.33$ (L/312) $f_{z,G}=1.26$ (L/329)

- Verifica Freccia massima carichi totali - CC 46

$f_{z,G}=1.31$ (L/317)

Membratura

Asta n. 2066 (-2363 -2360 -2356 -2351) Tubo circolare $d=114.3 \times 6$ mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 56

$f_{z,L}=0.91$ (L/343) $f_{z,G}=0.88$ (L/355)

- Verifica Freccia massima carichi totali - CC 56

$f_{z,L}=0.97$ (L/321) $f_{z,G}=0.92$ (L/338)

Membratura

Asta n. 2590 (-2351 -2408 -2437 -2463) Tubo circolare $d=114.3 \times 6$ mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 56

$f_{z,G}=1.34$ (L/233)

- Verifica Freccia massima carichi totali - CC 56

$f_{z,G}=1.38$ (L/225)

Membratura

Asta n. 2590 (-2463 -2486 -2541 2401) Tubo circolare $d=101.6 \times 6$ mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 56

$f_{z,L}=0.48$ (L/646) $f_{z,G}=0.20$ (L/1545)

- Verifica Freccia massima carichi totali - CC 56

$f_{z,L}=0.66$ (L/472) $f_{z,G}=0.18$ (L/1758)

Membratura

Asta n. 2597 (-2352 -2409 -2438 -2464) Tubo circolare $d=114.3 \times 6$ mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 26
 $f_{z,L}=1.45$ (L/214)

- Verifica Freccia massima carichi totali - CC 26
 $f_{z,L}=1.49$ (L/208)

Membratura

Asta n. 2597 (-2464 -2487 -2539 2402) Tubo circolare d=101.6x6 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 62
 $f_{z,L}=0.41$ (L/769) $f_{z,G}=0.35$ (L/882)

- Verifica Freccia massima carichi totali - CC 26
 $f_{z,L}=0.41$ (L/753) $f_{z,G}=0.35$ (L/888)

Membratura

Asta n. 2819 (1901 -2497 -2643) Tubo 80x100x(2x5+6) mm - S355 (32) Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 56
 $f_{z,L}=0.04$ (L/983) $f_{z,G}=0.02$ (L/2081)

- Verifica Freccia massima carichi totali - CC 56
 $f_{z,L}=0.06$ (L/605) $f_{z,G}=0.03$ (L/1275)

Membratura

Asta n. 2819 (-2643 -3198 2901) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 56
 $f_{z,L}=0.07$ (L/579) $f_{z,G}=0.00$ (L/16969)

- Verifica Freccia massima carichi totali - CC 56
 $f_{z,L}=0.12$ (L/352) $f_{z,G}=0.00$ (L/11402)

Membratura

Asta n. 2819 (-2478 1902 -2441 -2427 -2405) Tubo circolare d=101.6x6 mm - S355 Crit. 3

- Verifica di stabilità (4.2.4.1.3.1) - CC 45 SLU
Sollecitazioni: N=-3394.48 L=416.44
 $\lambda=122.97$ Ncr=24701.10 $\lambda^*=1.61$

Curva a: $\Phi=1.94$ $\chi_{\min}=0.33$ N,Ed=-3394.48 Nb,Rd=20097.60 N,Ed/Nb,Rd=0.17

- Verifica Freccia massima per soli carichi accidentali - CC 26
 $f_{z,L}=1.08$ (L/386) $f_{z,G}=0.81$ (L/513)

- Verifica Freccia massima carichi totali - CC 26
 $f_{z,L}=1.21$ (L/345) $f_{z,G}=0.74$ (L/566)

Membratura

Asta n. 2819 (-2405 -2361 -2357 -2352) Tubo circolare d=114.3x6 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 26
 $f_{z,L}=1.47$ (L/211) $f_{z,G}=1.44$ (L/215)

- Verifica Freccia massima carichi totali - CC 26
 $f_{z,L}=1.53$ (L/202) $f_{z,G}=1.49$ (L/209)

Membratura

Asta n. 2820 (1902 -2498 -2644) Tubo 80x100x(2x5+6) mm - S355 (32) Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 56
 $f_{z,L}=0.03$ (L/1127) $f_{z,G}=0.02$ (L/2329)

- Verifica Freccia massima carichi totali - CC 56
 $f_{z,L}=0.06$ (L/652) $f_{z,G}=0.03$ (L/1358)

Membratura

Asta n. 2820 (-2644 -3199 2902) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 56
 $f_{z,L}=0.07$ (L/622) $f_{z,G}=0.00$ (L/37296)

- Verifica Freccia massima carichi totali - CC 56
 $f_{z,L}=0.12$ (L/367) $f_{z,G}=0.00$ (L/17213)

Membratura

Asta n. 3457 (2401 -3082 -3442 -4235) Tubo 80x100x(2x5+6) mm - S355 (32) Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 56
 $f_{z,L}=0.01$ (L/6757) $f_{z,G}=0.00$ (L/14107)

- Verifica Freccia massima carichi totali - CC 56
 $f_{z,L}=0.01$ (L/4311) $f_{z,G}=0.00$ (L/8746)

Membratura

Asta n. 3457 (-4235 -7091 3301) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 56
 $f_{z,L}=0.00$ (L/10001)

- Verifica Freccia massima carichi totali - CC 56
 $f_{z,L}=0.01$ (L/5831) $f_{z,G}=0.00$ (L/40687)

Membratura

Asta n. 3458 (2402 -3090 -3448 -4236) Tubo 80x100x(2x5+6) mm - S355 (32) Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 26
 $f_{z,L}=0.00$ (L/8410) $f_{z,G}=0.00$ (L/16637)

- Verifica Freccia massima carichi totali - CC 26
 $f_{z,L}=0.01$ (L/4843) $f_{z,G}=0.00$ (L/9749)

Membratura

Asta n. 3458 (-4236 -7092 3302) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 26
 $f_{z,L}=0.00$ (L/10593)

- Verifica Freccia massima carichi totali - CC 26
 $f_{z,L}=0.01$ (L/5927) $f_{z,G}=0.00$ (L/40687)

Membratura

Asta n. 3556 (-4659 -4678 -4682) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica Freccia massima per soli carichi accidentali - CC 55
 $f_{z,L}=0.02$ (L/1744)

- Verifica Freccia massima carichi totali - CC 55
 $f_{z,L}=0.03$ (L/1250) $f_{z,G}=0.00$ (L/27070)

Membratura

Asta n. 3556 (-4682 -4741 -4798 -4853 -4916 -4991 -5037 -5113 -5198 -5263 -5314 -5368 -5430 -5493 -5588 -5657 -5725 -5789 -5835 -5877 -5986) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità (4.2.4.1.3.1) - CC 45 SLU

Sollecitazioni: $N=-3616.21$ $L=345.63$

$\lambda_y=80.26$ $N_{cr,y}=44275.40$ $\lambda^*_y=0.85$

Curva a: $\Phi_y=0.93$ $\chi_y=0.76$

$\lambda_z=139.26$ $N_{cr,z}=14706.40$ $\lambda^*_z=1.48$

Curva a: $\Phi_z=1.73$ $\chi_z=0.38$

$\chi_{,min}=0.38$ $N_{,Ed}=-3616.21$ $N_{b,Rd}=11695.70$ $N_{,Ed/Nb,Rd}=0.31$

- Verifica Freccia massima per soli carichi accidentali - CC 56
 $f_{z,G}=0.29$ (L/1187)

- Verifica Freccia massima carichi totali - CC 56
 $f_{z,G}=0.48$ (L/720)

Membratura

Asta n. 3556 (-5986 -6059 -6127 -6184 -6234 -6295 -6363 -6476 -6535 -6613 -6666 -6741 -6826 -6900 -6991 -7050 -7130 -7193 -7256 -7290 -7340) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità (4.2.4.1.3.1) - CC 45 SLU

Sollecitazioni: $N=-5431.41$ $L=345.64$

$\lambda_y=80.26$ $N_{cr,y}=44274.90$ $\lambda^*_y=0.85$

Curva a: $\Phi_y=0.93$ $\chi_y=0.76$

$\lambda_z=139.26$ $N_{cr,z}=14706.20$ $\lambda^*_z=1.48$

Curva a: $\Phi_z=1.73$ $\chi_z=0.38$

$\chi_{,min}=0.38$ $N_{,Ed}=-5431.41$ $N_{b,Rd}=11695.60$ $N_{,Ed/Nb,Rd}=0.46$

- Verifica Freccia massima per soli carichi accidentali - CC 56
 $f_{z,L}=0.14$ (L/2434) $f_{z,G}=0.12$ (L/2863)

- Verifica Freccia massima carichi totali - CC 56
 $f_{z,L}=0.24$ (L/1436) $f_{z,G}=0.20$ (L/1692)

Membratura

Asta n. 3556 (-7340 -7456 -7492 -7567 -7654 -7697 -7800 -7921 -7967 -8021 -8147 -8221 -8309 -8370 -8417 -8468 -8530 -8615 -8712 -8801 -8901) Tubo 60x120x4 mm - S235 Crit. 2

-
- Verifica di stabilità (4.2.4.1.3.1) - CC 45 SLU
Sollecitazioni: $N=-5539.46$ $L=345.64$
 $\lambda_y=80.26$ $N_{cr,y}=44274.90$ $\lambda^*_y=0.85$
Curva a: $\Phi_y=0.93$ $\chi_y=0.76$
 $\lambda_z=139.26$ $N_{cr,z}=14706.20$ $\lambda^*_z=1.48$
Curva a: $\Phi_z=1.73$ $\chi_z=0.38$
 $\chi_{,min}=0.38$ $N_{,Ed}=-5539.46$ $N_{b,Rd}=11695.60$ $N_{,Ed/Nb,Rd}=0.47$
 - Verifica Freccia massima per soli carichi accidentali - CC 56
 $f_{z,g}=0.09$ (L/3787)
 - Verifica Freccia massima carichi totali - CC 56
 $f_{z,t}=0.15$ (L/2235)

Membratura

Asta n. 3556 (-8901 -8975 -9068 -9142 -9200 -9276 -9367 -9433 -9502 -9543 -9591 -9633 -9734 -9846 -9941 -10027 -10119 -10188 -10243) Tubo 60x120x4 mm - S235 Crit. 2

-
- Verifica di stabilità (4.2.4.1.3.1) - CC 45 SLU
Sollecitazioni: $N=-3995.09$ $L=311.07$
 $\lambda_y=72.23$ $N_{cr,y}=54660.50$ $\lambda^*_y=0.77$
Curva a: $\Phi_y=0.86$ $\chi_y=0.81$
 $\lambda_z=125.33$ $N_{cr,z}=18155.90$ $\lambda^*_z=1.33$
Curva a: $\Phi_z=1.51$ $\chi_z=0.45$
 $\chi_{,min}=0.45$ $N_{,Ed}=-3995.09$ $N_{b,Rd}=13901.50$ $N_{,Ed/Nb,Rd}=0.29$
 - Verifica Freccia massima per soli carichi accidentali - CC 26
 $f_{z,g}=0.06$ (L/5373)
 - Verifica Freccia massima carichi totali - CC 26
 $f_{z,g}=0.10$ (L/3037)

Membratura

Asta n. 3562 (-4660 -4681 -4698) Tubo 60x120x4 mm - S235 Crit. 2

-
- Verifica Freccia massima per soli carichi accidentali - CC 70
 $f_{z,t}=0.02$ (L/1418)
 - Verifica Freccia massima carichi totali - CC 70
 $f_{z,t}=0.03$ (L/1072) $f_{z,g}=0.00$ (L/29424)

Membratura

Asta n. 3562 (-4698 -4757 -4814 -4869 -4934 -4997 -5051 -5129 -5214 -5279 -5330 -5384 -5446 -5509 -5604 -5673 -5744 -5805 -5851 -5893 -5972) Tubo 60x120x4 mm - S235 Crit. 2

-
- Verifica di stabilità (4.2.4.1.3.1) - CC 45 SLU
Sollecitazioni: $N=-3565.29$ $L=345.63$
 $\lambda_y=80.26$ $N_{cr,y}=44275.40$ $\lambda^*_y=0.85$
Curva a: $\Phi_y=0.93$ $\chi_y=0.76$
 $\lambda_z=139.26$ $N_{cr,z}=14706.40$ $\lambda^*_z=1.48$
Curva a: $\Phi_z=1.73$ $\chi_z=0.38$
 $\chi_{,min}=0.38$ $N_{,Ed}=-3565.29$ $N_{b,Rd}=11695.70$ $N_{,Ed/Nb,Rd}=0.30$
 - Verifica Freccia massima per soli carichi accidentali - CC 42
 $f_{z,g}=0.28$ (L/1230)
 - Verifica Freccia massima carichi totali - CC 42
 $f_{z,g}=0.47$ (L/732)

Membratura

Asta n. 3562 (-5972 -6075 -6143 -6200 -6252 -6311 -6379 -6492 -6556 -6629 -6693 -6757 -6842 -6901 -7007 -7066 -7146 -7209 -7272 -7306 -7356) Tubo 60x120x4 mm - S235 Crit. 2

-
- Verifica di stabilità (4.2.4.1.3.1) - CC 45 SLU
Sollecitazioni: $N=-5402.74$ $L=345.64$
 $\lambda_y=80.26$ $N_{cr,y}=44274.90$ $\lambda^*_y=0.85$
Curva a: $\Phi_y=0.93$ $\chi_y=0.76$
 $\lambda_z=139.26$ $N_{cr,z}=14706.20$ $\lambda^*_z=1.48$
Curva a: $\Phi_z=1.73$ $\chi_z=0.38$
 $\chi_{,min}=0.38$ $N_{,Ed}=-5402.74$ $N_{b,Rd}=11695.60$ $N_{,Ed/Nb,Rd}=0.46$

- Verifica Freccia massima per soli carichi accidentali - CC 42
 $f_{z,L}=0.14$ (L/2527) $f_{z,G}=0.12$ (L/2969)

- Verifica Freccia massima carichi totali - CC 42
 $f_{z,L}=0.24$ (L/1465) $f_{z,G}=0.20$ (L/1722)

Membratura

Asta n. 3562 (-7356 -7472 -7508 -7586 -7671 -7723 -7813 -7937 -7983 -8037 -8163 -8237 -8325 -8386 -8433 -8486 -8546 -8635 -8728 -8809 -8917) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità (4.2.4.1.3.1) - CC 45 SLU
Sollecitazioni: N=-5524.99 L=345.64

$\lambda_y=80.26$ Ncr, $y=44274.90$ $\lambda_y^*=0.85$

Curva a: $\Phi_y=0.93$ $\chi_y=0.76$

$\lambda_z=139.26$ Ncr, $z=14706.20$ $\lambda_z^*=1.48$

Curva a: $\Phi_z=1.73$ $\chi_z=0.38$

$\chi_{,min}=0.38$ N, Ed=-5524.99 Nb, Rd=11695.60 N, Ed/Nb, Rd=0.47

- Verifica Freccia massima per soli carichi accidentali - CC 42
 $f_{z,G}=0.09$ (L/3857)

- Verifica Freccia massima carichi totali - CC 42
 $f_{z,G}=0.15$ (L/2265)

Membratura

Asta n. 3562 (-8917 -8991 -9100 -9158 -9216 -9292 -9383 -9449 -9507 -9559 -9607 -9649 -9747 -9863 -9974 -10043 -10135 -10201 -10257) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica di stabilità (4.2.4.1.3.1) - CC 45 SLU
Sollecitazioni: N=-3995.24 L=311.07

$\lambda_y=72.23$ Ncr, $y=54660.50$ $\lambda_y^*=0.77$

Curva a: $\Phi_y=0.86$ $\chi_y=0.81$

$\lambda_z=125.33$ Ncr, $z=18155.90$ $\lambda_z^*=1.33$

Curva a: $\Phi_z=1.51$ $\chi_z=0.45$

$\chi_{,min}=0.45$ N, Ed=-3995.24 Nb, Rd=13901.50 N, Ed/Nb, Rd=0.29

- Verifica Freccia massima per soli carichi accidentali - CC 26
 $f_{z,G}=0.06$ (L/5124)

- Verifica Freccia massima carichi totali - CC 26
 $f_{z,G}=0.11$ (L/2903)

Membratura

Asta n. 3566 (-4524 -4526 -4528) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica Freccia massima per soli carichi accidentali - CC 91
 $f_{z,L}=0.03$ (L/853)

- Verifica Freccia massima carichi totali - CC 91
 $f_{z,L}=0.04$ (L/649) $f_{z,G}=0.00$ (L/18758)

Membratura

Asta n. 3568 (-4528 -4532 -4539 -4541) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica Freccia massima per soli carichi accidentali - CC 91
 $f_{z,L}=0.03$ (L/1351)

- Verifica Freccia massima carichi totali - CC 91
 $f_{z,L}=0.05$ (L/926)

Membratura

Asta n. 3570 (-4541 -4554 -4569 -4579) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica Freccia massima per soli carichi accidentali - CC 91
 $f_{z,L}=0.03$ (L/1854) $f_{z,G}=0.00$ (L/14536)

- Verifica Freccia massima carichi totali - CC 91
 $f_{z,L}=0.04$ (L/1188) $f_{z,G}=0.01$ (L/8745)

Membratura

Asta n. 3571 (-4540 -4553 -4568 -4578) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica Freccia massima per soli carichi accidentali - CC 56
 $f_{z,L}=0.02$ (L/2279) $f_{z,G}=0.00$ (L/13970)

- Verifica Freccia massima carichi totali - CC 56

$f_{z,l}=0.04$ (L/1311) $f_{z,g}=0.01$ (L/8404)

Membratura

Asta n. 3574 (-4579 -4594 -4611 -4626) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica Freccia massima per soli carichi accidentali - CC 77
 $f_{z,l}=0.01$ (L/4271) $f_{z,g}=0.00$ (L/16612)

- Verifica Freccia massima carichi totali - CC 77
 $f_{z,l}=0.02$ (L/2646) $f_{z,g}=0.00$ (L/8625)

Membratura

Asta n. 3575 (-4578 -4593 -4610 -4612) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica Freccia massima per soli carichi accidentali - CC 77
 $f_{z,l}=0.01$ (L/3477) $f_{z,g}=0.00$ (L/17590)

- Verifica Freccia massima carichi totali - CC 77
 $f_{z,l}=0.02$ (L/2177) $f_{z,g}=0.00$ (L/8882)

Membratura

Asta n. 3579 (-4626 -4628 -4643 -4660) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica Freccia massima per soli carichi accidentali - CC 69
 $f_{z,l}=0.02$ (L/3081) $f_{z,g}=0.00$ (L/17927)

- Verifica Freccia massima carichi totali - CC 69
 $f_{z,l}=0.02$ (L/2428) $f_{z,g}=0.01$ (L/8725)

Membratura

Asta n. 3580 (-4612 -4627 -4642 -4659) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica Freccia massima per soli carichi accidentali - CC 55
 $f_{z,l}=0.01$ (L/4040) $f_{z,g}=0.00$ (L/12324)

- Verifica Freccia massima carichi totali - CC 55
 $f_{z,l}=0.01$ (L/3319) $f_{z,g}=0.01$ (L/7196)

Membratura

Asta n. 3595 (-2592 -3079 -4692) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 55
 $f_{z,l}=0.02$ (L/1847)

- Verifica Freccia massima carichi totali - CC 55
 $f_{z,l}=0.03$ (L/1313) $f_{z,g}=0.00$ (L/39783)

Membratura

Asta n. 3596 (-2591 -3078 -3569 -4688) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 70
 $f_{z,l}=0.03$ (L/1526)

- Verifica Freccia massima carichi totali - CC 70
 $f_{z,l}=0.04$ (L/1075)

Membratura

Asta n. 3642 (-2698 -3322 -5436) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 42
 $f_{z,l}=0.04$ (L/1118)

- Verifica Freccia massima carichi totali - CC 42
 $f_{z,l}=0.05$ (L/943) $f_{z,g}=0.00$ (L/42123)

Membratura

Asta n. 3643 (-2699 -3323 -5440) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 91
 $f_{z,l}=0.04$ (L/1167) $f_{z,g}=0.00$ (L/22661)

- Verifica Freccia massima carichi totali - CC 55
 $f_{z,l}=0.04$ (L/1092) $f_{z,g}=0.00$ (L/17381)

Membratura

Asta n. 3662 (-2755 -3450 -5841) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 91

$f_{z,l}=0.06$ (L/745)

- Verifica Freccia massima carichi totali - CC 55
 $f_{z,l}=0.07$ (L/628) $f_{z,g}=0.00$ (L/27124)

Membratura

Asta n. 3663 (-2756 -3451 -5845) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 91
 $f_{z,l}=0.09$ (L/492)
- Verifica Freccia massima carichi totali - CC 91
 $f_{z,l}=0.11$ (L/380) $f_{z,g}=0.00$ (L/24864)

Membratura

Asta n. 3683 (-2812 -3697 -6247) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 42
 $f_{z,l}=0.12$ (L/365)
- Verifica Freccia massima carichi totali - CC 42
 $f_{z,l}=0.16$ (L/273) $f_{z,g}=0.00$ (L/28874)

Membratura

Asta n. 3684 (-2811 -3696 -6244) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 91
 $f_{z,l}=0.08$ (L/568)
- Verifica Freccia massima carichi totali - CC 55
 $f_{z,l}=0.10$ (L/406) $f_{z,g}=0.00$ (L/36912)

Membratura

Asta n. 3703 (-2879 -3985 -6670) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 91
 $f_{z,l}=0.09$ (L/492)
- Verifica Freccia massima carichi totali - CC 55
 $f_{z,l}=0.12$ (L/354)

Membratura

Asta n. 3704 (-2880 -3986 -6673) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 42
 $f_{z,l}=0.13$ (L/320)
- Verifica Freccia massima carichi totali - CC 42
 $f_{z,l}=0.18$ (L/240) $f_{z,g}=0.00$ (L/41633)

Membratura

Asta n. 3723 (-2965 -4251 -7136) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 91
 $f_{z,l}=0.09$ (L/457)
- Verifica Freccia massima carichi totali - CC 55
 $f_{z,l}=0.12$ (L/347)

Membratura

Asta n. 3724 (-2966 -4252 -7140) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 42
 $f_{z,l}=0.14$ (L/306)
- Verifica Freccia massima carichi totali - CC 42
 $f_{z,l}=0.18$ (L/232)

Membratura

Asta n. 3739 (-3065 -4493 -7502) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 42
 $f_{z,l}=0.14$ (L/308)
- Verifica Freccia massima carichi totali - CC 42
 $f_{z,l}=0.18$ (L/235)

Membratura

Asta n. 3740 (-3064 -4492 -7498) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 91
 $f_{z,l}=0.09$ (L/451)

- Verifica Freccia massima carichi totali - CC 55
 $f_{z,l}=0.12$ (L/351)

Membratura

Asta n. 3756 (-3189 -5014 -7977) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 42
 $f_{z,l}=0.14$ (L/314)

- Verifica Freccia massima carichi totali - CC 42
 $f_{z,l}=0.18$ (L/237)

Membratura

Asta n. 3757 (-3193 -5013 -7973) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 91
 $f_{z,l}=0.09$ (L/477)

- Verifica Freccia massima carichi totali - CC 55
 $f_{z,l}=0.12$ (L/351)

Membratura

Asta n. 3775 (-3309 -5418 -8423) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 91
 $f_{z,l}=0.08$ (L/537)

- Verifica Freccia massima carichi totali - CC 56
 $f_{z,l}=0.12$ (L/364)

Membratura

Asta n. 3776 (-3317 -5397 -8427) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 42
 $f_{z,l}=0.13$ (L/337)

- Verifica Freccia massima carichi totali - CC 42
 $f_{z,l}=0.17$ (L/250)

Membratura

Asta n. 3795 (-3441 -5817 -8911) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 42
 $f_{z,l}=0.11$ (L/394)

- Verifica Freccia massima carichi totali - CC 42
 $f_{z,l}=0.15$ (L/286)

Membratura

Asta n. 3796 (-3440 -5807 -8907) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 56
 $f_{z,l}=0.07$ (L/653)

- Verifica Freccia massima carichi totali - CC 56
 $f_{z,l}=0.11$ (L/406)

Membratura

Asta n. 3815 (-3674 -6221 -9373) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 56
 $f_{z,l}=0.05$ (L/857)

- Verifica Freccia massima carichi totali - CC 56
 $f_{z,l}=0.08$ (L/526) $f_{z,e}=0.00$ (L/32256)

Membratura

Asta n. 3816 (-3675 -6230 -9377) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 42
 $f_{z,l}=0.08$ (L/531)

- Verifica Freccia massima carichi totali - CC 42

$f_{z,l}=0.11$ (L/379) $f_{z,g}=0.00$ (L/33778)

Membratura

Asta n. 3837 (-3956 -6659 -9739) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 91
 $f_{z,l}=0.02$ (L/2007)

- Verifica Freccia massima carichi totali - CC 50
 $f_{z,l}=0.03$ (L/1289) $f_{z,g}=0.00$ (L/13931)

Membratura

Asta n. 3838 (-3969 -6660 -9741) Tubo 80x120x5 mm - S355 Crit. 3

- Verifica Freccia massima per soli carichi accidentali - CC 42
 $f_{z,l}=0.04$ (L/1160) $f_{z,g}=0.00$ (L/22951)

- Verifica Freccia massima carichi totali - CC 42
 $f_{z,l}=0.05$ (L/843) $f_{z,g}=0.00$ (L/13163)

Membratura

Asta n. 3997 (-4540 -4538 -4531 -4527) Tubo 60x120x4 mm - S235 Crit. 2

- Verifica Freccia massima per soli carichi accidentali - CC 56
 $f_{z,l}=0.02$ (L/2162)

- Verifica Freccia massima carichi totali - CC 56
 $f_{z,l}=0.03$ (L/1286)

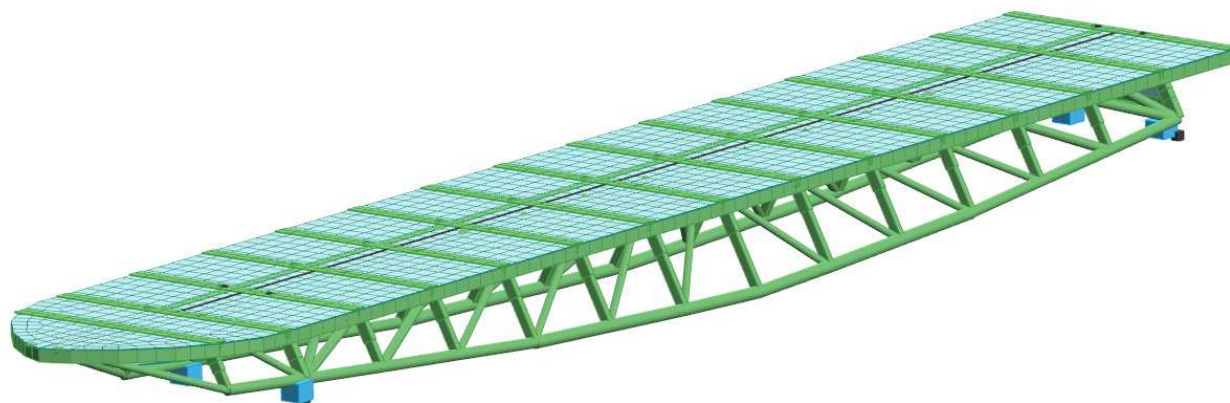
Membratura

Asta n. 3999 (-4527 -4525 -4524) Tubo 60x120x4 mm - S235 Crit. 2

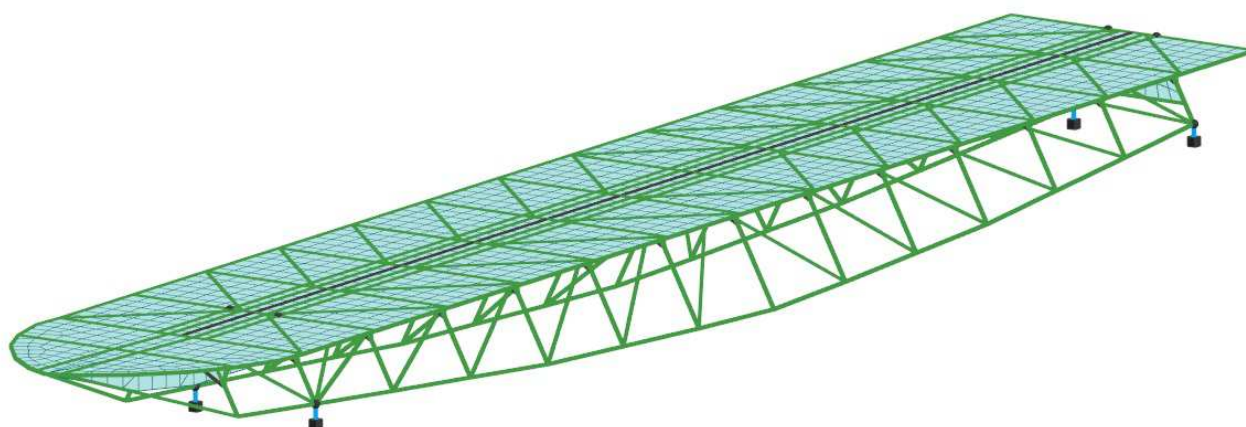
- Verifica Freccia massima per soli carichi accidentali - CC 91
 $f_{z,l}=0.02$ (L/1303)

- Verifica Freccia massima carichi totali - CC 56
 $f_{z,l}=0.02$ (L/1226) $f_{z,g}=0.00$ (L/14910)

DIAGRAMMI ESPLICATIVI DEL MODELLO F.E.M.
(struttura in acciaio)



Vista del modello assonometrico – Vista tridimensionale



Vista del modello assonometrico – Vista assonometrica unifilare

Verifica profili dei cavalletti in acciaio

(NTC - p.to 4.2.4.1.2-3)

Puntelli diagonali dei cavalletti di sostegno dell'impalcato (estremità inf. - Posiz. appoggio spalla)

Dati geometrici e caratteristiche d'inerzia della sezione

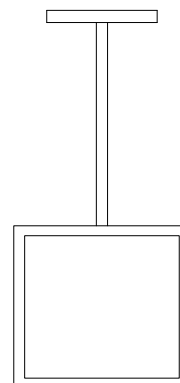
Profilo della sezione: **Tubo 120x80x5 + piatto 10 mm nervato**

Lato maggiore sezione: h (mm) =	120	H (mm) =	303.0
Lato minore sezione: b (mm) =	80	x (mm) =	144.3
Spessore del tubo: $t_w = a$ (mm) =	5		
Rapporto: c/t =	22.0		
Lunghezza ala di rinforzo: L (mm) =	177		
Spessore ala di rinforzo: t (mm) =	10		
Larghezza nervatura: b' (mm) =	50		
Spessore nervatura: t' (mm) =	6		

Area della sezione del profilo: A (cm ²) =	39.7
Area resistente netta: A _{net} (cm ²) =	39.7
Momento d'inerzia max.: J _y (cm ⁴) =	3 644.8
Momento d'inerzia min.: J _z (cm ⁴) =	205.3
Modulo di resistenza max.: W _y (cm ³) =	229.7
Modulo di resistenza min.: W _z (cm ³) =	51.3
Area a taglio: A _t (cm ²) =	10.4

Geometria profili

Luce dei profili: L (cm) =	42
Peso del profilo: p _{prof} (kg/m) =	31.2



Materiali della sezione

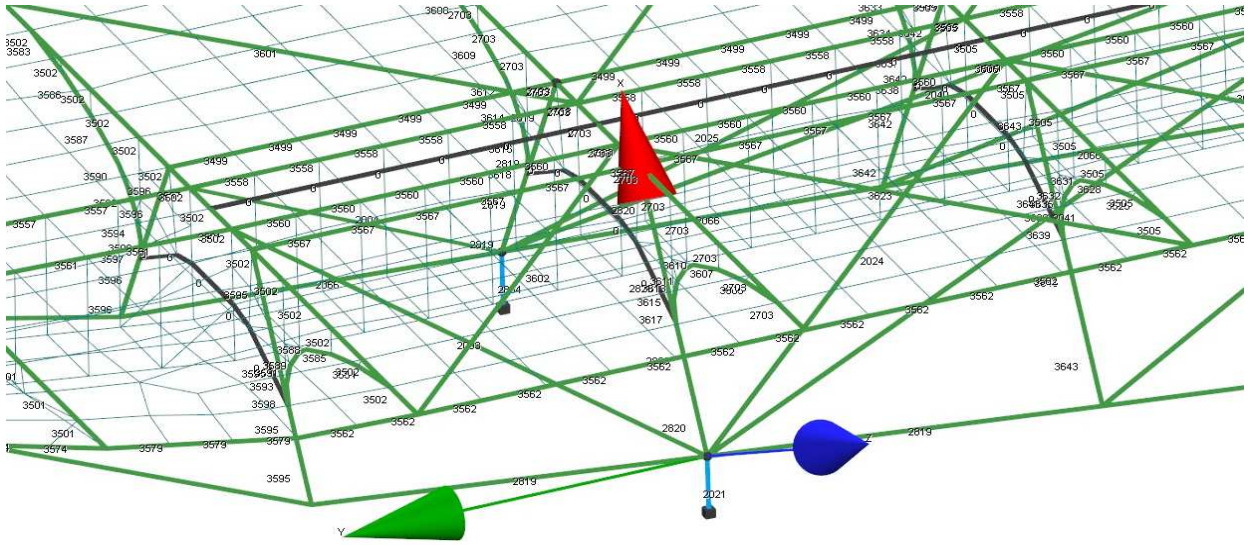
Classe dell'acciaio:	S 275 J0	Coeff. sicur. resistenza: γ_{M0} =	1.05
Tensione di rottura: f _{tk} (N/mm ²) =	430	Coeff. sicur. instabilità: γ_{M1} =	1.05
Tensione di snervam.: f _{yk} (N/mm ²) =	275	Coeff. sicur. frattura: γ_{M2} =	1.25
Parametro di classificaz.: ϵ =	0.924		
Classe della sezione:	1		
Coeff. di adattam. plastico sezione: ψ =	1.000		
Modulo elastico acciaio: E _s (N/mm ²) =	210 000		
Coefficiente di Poisson: ν =	0.3		

Sollecitazioni (da analisi F.E.M.)

	SLU (1)	SLV (1)	SLV (2)
Momento sollecit. asse y: M _{y,Ed} (kgm) =	2 589	1 807	3 317
Momento sollecit. asse z: M _{z,Ed} (kgm) =	711	518	94
Taglio sollecitante asse y: V _{y,Ed} (kg) =	1 364	182	980
Taglio sollecitante asse z: V _{z,Ed} (kg) =	7 674	8 782	4 849
Sforzo normale: N _{Ed} (kg) =	-3 320	-8 385	9 311
Torsione: T _{Ed} (kgm) =	0.0	0.0	0.0

Sollecitaz. prevalente: **N**

Coeff. incremento permanenti: γ_p =	1.30
Coeff. incremento variabili: γ_q =	1.50



Verif. di resistenza [4.2.4.1.2]

	SLU		
Momento resist. asse y: $M_{y,c,Rd}$ (kgm) =	6 017	>	2 589
Momento resist. asse z: $M_{z,c,Rd}$ (kgm) =	1 344	>	711
Taglio sollecitante asse y: $V_{y,Rd}$ (kg) =	60 031	>	1 364
Taglio sollecitante asse z: $V_{z,Rd}$ (kg) =	60 031	>	7 674
Sforzo normale resistente: $N_{pl,Rd}$ (kg) =	103 976	>	3 320

A_v (cm ²)	ρ
39.7	0.0
39.7	0.0
n =	0.032

	M+V	M+V+N		
Momento ridotto asse y: $M_{y,V,Rd}$ (kgm) =	6 017	6 017	>	2 589
Momento ridotto asse z: $M_{z,V,Rd}$ (kgm) =	1 344	1 344	>	710.9
[4.2.39-4.2.40]: $M_y + M_z + N + V =$		0.9591	<	1.00

Verifiche tensionali

Caso 1 SLU (1)

$\sigma_{s,N+M}$ (N/mm ²) =	259.5	<	261.9
$\tau_{s,Vz}$ (N/mm ²) =	25.8	<	151.2
$\sigma_{id,V+M+N}$ (N/mm ²) =	129.0	<	261.9

Caso 2 SLV (1)

$\sigma_{s,N+M}$ (N/mm ²) =	200.7	<	261.9
$\tau_{s,Vz}$ (N/mm ²) =	29.5	<	151.2
$\sigma_{id,V+M+N}$ (N/mm ²) =	112.1	<	261.9

Caso 3 SLV (2)

$\sigma_{s,N+M}$ (N/mm ²) =	186.2	<	261.9
$\tau_{s,Vz}$ (N/mm ²) =	16.3	<	151.2
$\sigma_{id,V+M+N}$ (N/mm ²) =	170.2	<	261.9

Verifiche di stabilità a compressione [4.2.4.1.3.1]

Lungh. di calcolo del profilo: L (cm) = 42

Nel seguito si fa riferimento alle seguenti grandezze:

Coefficiente di vincolo di estremità: β

Lunghezza di calcolo del profilo: L_0

Raggi d'inerzia (assi y e z): i_y, i_z

Snellezze (assi y e z): λ_y, λ_z

Carico critico euleriano (assi y e z): $N_{cr,y}, N_{cr,z}$

Snellezze adimensionali (assi y e z): λ^*_y, λ^*_z

Fattori di imperfezione (Tab. 4.2.VI): α_y, α_z

Fattore [4.2.45]: $\Phi = 0.5 [1 + \alpha (\lambda^* - 0.2) + \lambda^{*2}]$

Coefficiente di riduzione [4.2.45]: $\chi = 1 / [\Phi + (\Phi^2 - \lambda^{*2})^{0.5}] < 1.0$

Resistenza all'instabilità dell'asta compressa: $N_{b,Rd}$

Rapporto lati: h/b = 1.00 (Tab. 4.2.VI)

Asse	β	L_0 (cm)	i (cm)	λ	λ_{lim}	N_{cr} (kg)	λ^*	Curva	α
y-y	2.0	84	9.58	8.8	200	10 706 210	0.101	a	0.21
z-z	2.0	84	2.27	36.9	200	603 069	0.425	a	0.21

Φ	χ	$N_{b,Rd}$ (kg)		N_{Ed} (kg)	0.04 N_{cr} (kg)
0.495	1.000	103 976	>	8 385	428 248
0.614	0.946	98 357	>	8 385	24 123

Verifiche di stabilità a tenso-pressoflessione [4.2.4.1.3.3]

- Metodo "A"

Momento variabile linearmente lungo l'asta (asse di flessione y-y): no
 Momento variabile linearmente lungo l'asta (asse di flessione z-z): no
 Verifica di instabilità flessio-torsionale: si

	y-y	z-z
Momento massimo: $M_{max,Ed}$ (kgm) =	2 589	710.9
Momento all'estremità A: M_A (kgm) =	0.0	0.0
Momento all'estremità B: M_B (kgm) =	0.0	0.0
Sforzo normale nell'asta: N (kg) =	-3 320	

Nel seguito si fa riferimento alle seguenti grandezze:

Carico critico euleriano (assi y e z): $N_{cr,y}$, $N_{cr,z}$

Coefficiente di riduzione minimo (assi y e z): χ_{min}

Coefficiente di riduzione [4.2.51]: $\chi_{LT} = (1/f) [1 / (\Phi_{LT} + (\Phi_{LT}^2 - \lambda_{LT}^{*2})^{0.5})] < 1.0$

Momento equivalente da considerare nella verifica (assi y e z) [C4.2.4.1.3.3.1]: $M_{y,eq,Ed}$, $M_{z,eq,Ed}$

Asse	N_{cr} (kg)	χ_{min}	$M_{m,Ed}$	$1.3 M_{m,Ed}$	M_{max}	$M_{eq,Ed}$	$M_{eq,Ed,lin}$	N	My-Mz
y-y	10 706 210	0.946	1 726	2 244	2 589	2 244	0.0	0.034	0.373
z-z	603 069	\	473.9	616.1	710.9	616.1	0.0	\	0.461
Verifica di stabilità [C4.2.32]: $N+My+Mz =$			0.868	<	1.00				

Verifica profili dei cavalletti in acciaio

(NTC - p.to 4.2.4.1.2-3)

Puntelli diagonali dei cavalletti di sostegno dell'impalcato (estremità sup. - Posiz. appoggio spalla)

Dati geometrici e caratteristiche d'inerzia della sezione

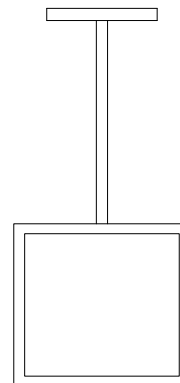
Profilo della sezione: **Tubo 120x80x5 + piatto 10 mm nervato**

Lato maggiore sezione: h (mm) =	120	H (mm) =	391.0
Lato minore sezione: b (mm) =	80	x (mm) =	185.5
Spessore del tubo: $t_w = a$ (mm) =	5		
Rapporto: c/t =	22.0		
Lunghezza ala di rinforzo: L (mm) =	265		
Spessore ala di rinforzo: t (mm) =	10		
Larghezza nervatura: b' (mm) =	50		
Spessore nervatura: t' (mm) =	6		

Area della sezione del profilo: A (cm ²) =	48.5
Area resistente netta: A _{net} (cm ²) =	48.5
Momento d'inerzia max.: J _y (cm ⁴) =	7 338.8
Momento d'inerzia min.: J _z (cm ⁴) =	206.0
Modulo di resistenza max.: W _y (cm ³) =	357.1
Modulo di resistenza min.: W _z (cm ³) =	51.5
Area a taglio: A _t (cm ²) =	10.4

Geometria profili

Luce dei profili: L (cm) =	42
Peso del profilo: p _{prof} (kg/m) =	38.1



Materiali della sezione

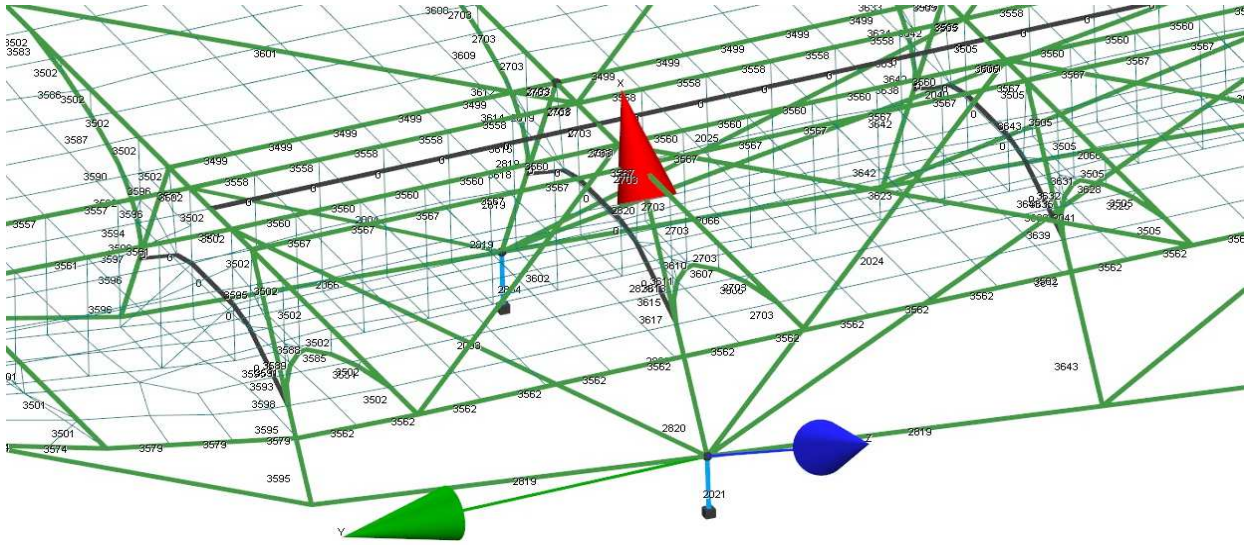
Classe dell'acciaio:	S 275 J0	Coeff. sicur. resistenza: γ_{M0} =	1.05
Tensione di rottura: f _{tk} (N/mm ²) =	430	Coeff. sicur. instabilità: γ_{M1} =	1.05
Tensione di snervam.: f _{yk} (N/mm ²) =	275	Coeff. sicur. frattura: γ_{M2} =	1.25
Parametro di classificaz.: ϵ =	0.924		
Classe della sezione:	1		
Coeff. di adattam. plastico sezione: ψ =	1.000		
Modulo elastico acciaio: E _s (N/mm ²) =	210 000		
Coefficiente di Poisson: ν =	0.3		

Sollecitazioni (da analisi F.E.M.)

	SLU (1)	SLV (1)	SLV (2)
Momento sollecit. asse y: M _{y,Ed} (kgm) =	1 621	1 133	2 091
Momento sollecit. asse z: M _{z,Ed} (kgm) =	520	381	69
Taglio sollecitante asse y: V _{y,Ed} (kg) =	1 363	181	979
Taglio sollecitante asse z: V _{z,Ed} (kg) =	7 672	8 780	4 850
Sforzo normale: N _{Ed} (kg) =	-3 320	-8 385	9 311
Torsione: T _{Ed} (kgm) =	0.0	0.0	0.0

Sollecitaz. prevalente: **N**

Coeff. incremento permanenti: γ_p =	1.30
Coeff. incremento variabili: γ_q =	1.50



Verif. di resistenza [4.2.4.1.2]

	SLU		
Momento resist. asse y: $M_{y,c,Rd}$ (kgm) =	9 352	>	1 621
Momento resist. asse z: $M_{z,c,Rd}$ (kgm) =	1 349	>	520
Taglio sollecitante asse y: $V_{y,Rd}$ (kg) =	73 337	>	1 363
Taglio sollecitante asse z: $V_{z,Rd}$ (kg) =	73 337	>	7 672
Sforzo normale resistente: $N_{pl,Rd}$ (kg) =	127 024	>	3 320

A_v (cm ²)	ρ
48.5	0.0
48.5	0.0
n = 0.026	

	M+V	M+V+N		
Momento ridotto asse y: $M_{y,V,Rd}$ (kgm) =	9 352	9 352	>	1 621
Momento ridotto asse z: $M_{z,V,Rd}$ (kgm) =	1 349	1 349	>	519.5
[4.2.39-4.2.40]: $M_y + M_z + N + V =$		0.5584	<	1.00

Verifiche tensionali

Caso 1 SLU (1)

$\sigma_{s,N+M}$ (N/mm ²) =	153.1	<	261.9
$\tau_{s,Vz}$ (N/mm ²) =	21.1	<	151.2
$\sigma_{id,V+M+N}$ (N/mm ²) =	63.7	<	261.9

Caso 2 SLV (1)

$\sigma_{s,N+M}$ (N/mm ²) =	122.9	<	261.9
$\tau_{s,Vz}$ (N/mm ²) =	24.1	<	151.2
$\sigma_{id,V+M+N}$ (N/mm ²) =	64.4	<	261.9

Caso 3 SLV (2)

$\sigma_{s,N+M}$ (N/mm ²) =	91.1	<	261.9
$\tau_{s,Vz}$ (N/mm ²) =	13.3	<	151.2
$\sigma_{id,V+M+N}$ (N/mm ²) =	81.1	<	261.9

Verifiche di stabilità a compressione [4.2.4.1.3.1]

Lungh. di calcolo del profilo: L (cm) = 42

Nel seguito si fa riferimento alle seguenti grandezze:

Coefficiente di vincolo di estremità: β

Lunghezza di calcolo del profilo: L_0

Raggi d'inerzia (assi y e z): i_y, i_z

Snellezze (assi y e z): λ_y, λ_z

Carico critico euleriano (assi y e z): $N_{cr,y}, N_{cr,z}$

Snellezze adimensionali (assi y e z): λ^*_y, λ^*_z

Fattori di imperfezione (Tab. 4.2.VI): α_y, α_z

Fattore [4.2.45]: $\Phi = 0.5 [1 + \alpha (\lambda^* - 0.2) + \lambda^{*2}]$

Coefficiente di riduzione [4.2.45]: $\chi = 1 / [\Phi + (\Phi^2 - \lambda^{*2})^{0.5}] < 1.0$

Resistenza all'instabilità dell'asta compressa: $N_{b,Rd}$

Rapporto lati: h/b = 1.00 (Tab. 4.2.VI)

Asse	β	L_0 (cm)	i (cm)	λ	λ_{lim}	N_{cr} (kg)	λ^*	Curva	α
y-y	2.0	84	12.30	6.8	200	21 556 846	0.079	a	0.21
z-z	2.0	84	2.06	40.8	200	605 223	0.469	a	0.21

Φ	χ	$N_{b,Rd}$ (kg)		N_{Ed} (kg)	0.04 N_{cr} (kg)
0.490	1.000	127 024	>	8 385	862 274
0.638	0.934	118 577	>	8 385	24 209

Verifiche di stabilità a tenso-pressoflessione [4.2.4.1.3.3]

- Metodo "A"

Momento variabile linearmente lungo l'asta (asse di flessione y-y): no
 Momento variabile linearmente lungo l'asta (asse di flessione z-z): no
 Verifica di instabilità flesso-torsionale: si

	y-y	z-z
Momento massimo: $M_{max,Ed}$ (kgm) =	1 621	519.5
Momento all'estremità A: M_A (kgm) =	0.0	0.0
Momento all'estremità B: M_B (kgm) =	0.0	0.0
Sforzo normale nell'asta: N (kg) =	-3 320	

Nel seguito si fa riferimento alle seguenti grandezze:

Carico critico euleriano (assi y e z): $N_{cr,y}$, $N_{cr,z}$

Coefficiente di riduzione minimo (assi y e z): χ_{min}

Coefficiente di riduzione [4.2.51]: $\chi_{LT} = (1/f) [1 / (\Phi_{LT} + (\Phi_{LT}^2 - \lambda_{LT}^{*2})^{0.5})] < 1.0$

Momento equivalente da considerare nella verifica (assi y e z) [C4.2.4.1.3.3.1]: $M_{y,eq,Ed}$, $M_{z,eq,Ed}$

Asse	N_{cr} (kg)	χ_{min}	$M_{m,Ed}$	$1.3 M_{m,Ed}$	M_{max}	$M_{eq,Ed}$	$M_{eq,Ed,lin}$	N	My-Mz
y-y	21 556 846	0.934	1 081	1 405	1 621	1 405	0.0	0.028	0.150
z-z	605 223	\	346.4	450.3	519.5	450.3	0.0	\	0.336
Verifica di stabilità [C4.2.32]: $N+My+Mz =$			0.514	<	1.00				

Verifica profili dei cavalletti in acciaio

(NTC - p.to 4.2.4.1.2-3)

Puntelli diagonali dei cavalletti di sostegno dell'impalcato (estremità inf. - Posiz. appoggio spalla)

Dati geometrici e caratteristiche d'inerzia della sezione

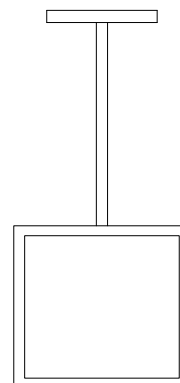
Profilo della sezione: **Tubo 120x80x5 + piatto 10 mm nervato**

Lato maggiore sezione: h (mm) =	120	H (mm) =	303.0
Lato minore sezione: b (mm) =	80	x (mm) =	144.3
Spessore del tubo: $t_w = a$ (mm) =	5		
Rapporto: c/t =	22.0		
Lunghezza ala di rinforzo: L (mm) =	177		
Spessore ala di rinforzo: t (mm) =	10		
Larghezza nervatura: b' (mm) =	50		
Spessore nervatura: t' (mm) =	6		

Area della sezione del profilo: A (cm ²) =	39.7
Area resistente netta: A _{net} (cm ²) =	39.7
Momento d'inerzia max.: J _y (cm ⁴) =	3 644.8
Momento d'inerzia min.: J _z (cm ⁴) =	205.3
Modulo di resistenza max.: W _y (cm ³) =	229.7
Modulo di resistenza min.: W _z (cm ³) =	51.3
Area a taglio: A _t (cm ²) =	10.4

Geometria profili

Luce dei profili: L (cm) =	42
Peso del profilo: p _{prof} (kg/m) =	31.2



Materiali della sezione

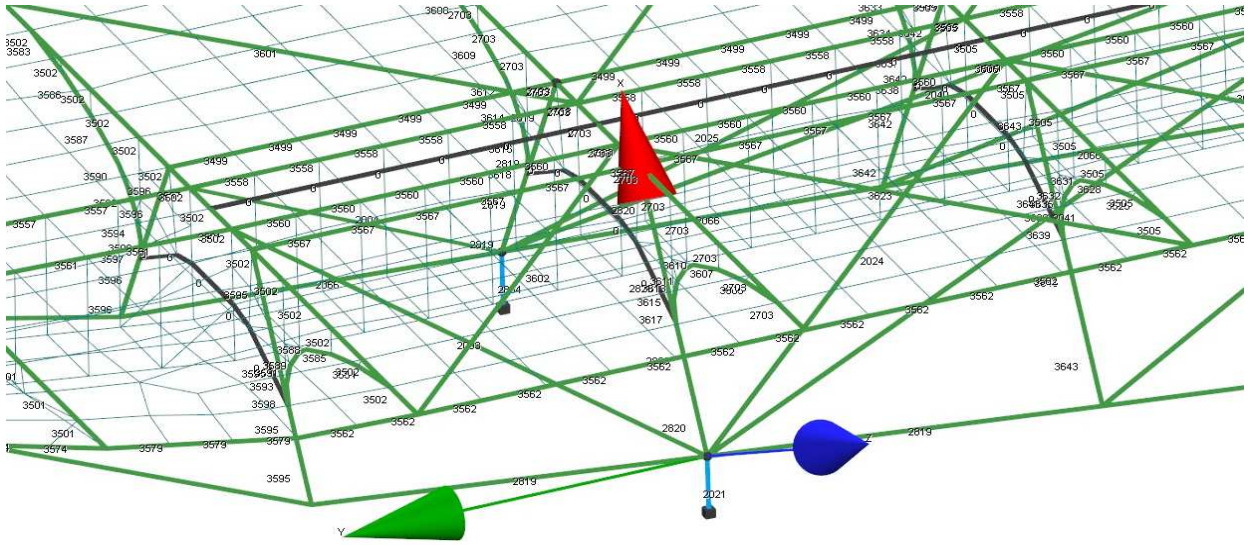
Classe dell'acciaio:	S 275 J0	Coeff. sicur. resistenza: γ_{M0} =	1.05
Tensione di rottura: f _{tk} (N/mm ²) =	430	Coeff. sicur. instabilità: γ_{M1} =	1.05
Tensione di snervam.: f _{yk} (N/mm ²) =	275	Coeff. sicur. frattura: γ_{M2} =	1.25
Parametro di classificaz.: ϵ =	0.924		
Classe della sezione:	1		
Coeff. di adattam. plastico sezione: ψ =	1.000		
Modulo elastico acciaio: E _s (N/mm ²) =	210 000		
Coefficiente di Poisson: ν =	0.3		

Sollecitazioni (da analisi F.E.M.)

	SLU (1)	SLV (1)	SLV (2)
Momento sollecit. asse y: M _{y,Ed} (kgm) =	2 638	813	2 350
Momento sollecit. asse z: M _{z,Ed} (kgm) =	636	80	469
Taglio sollecitante asse y: V _{y,Ed} (kg) =	1 214	874	131
Taglio sollecitante asse z: V _{z,Ed} (kg) =	6 728	5 123	1 047
Sforzo normale: N _{Ed} (kg) =	-4 893	-8 385	9 311
Torsione: T _{Ed} (kgm) =	0.0	0.0	0.0

Sollecitaz. prevalente: **N**

Coeff. incremento permanenti: γ_p =	1.30
Coeff. incremento variabili: γ_q =	1.50



Verif. di resistenza [4.2.4.1.2]

	SLU		
Momento resist. asse y: $M_{y,c,Rd}$ (kgm) =	6 017	>	2 638
Momento resist. asse z: $M_{z,c,Rd}$ (kgm) =	1 344	>	636
Taglio sollecitante asse y: $V_{y,Rd}$ (kg) =	60 031	>	1 214
Taglio sollecitante asse z: $V_{z,Rd}$ (kg) =	60 031	>	6 728
Sforzo normale resistente: $N_{pl,Rd}$ (kg) =	103 976	>	4 893

A_v (cm ²)	ρ
39.7	0.0
39.7	0.0
n =	0.047

	M+V	M+V+N		
Momento ridotto asse y: $M_{y,V,Rd}$ (kgm) =	6 017	6 017	>	2 638
Momento ridotto asse z: $M_{z,V,Rd}$ (kgm) =	1 344	1 344	>	636.3
[4.2.39-4.2.40]: $M_y + M_z + N + V =$		0.9118	<	1.00

Verifiche tensionali

Caso 1 SLU (1)

$\sigma_{s,N+M}$ (N/mm ²) =	251.1	<	261.9
$\tau_{s,Vz}$ (N/mm ²) =	22.6	<	151.2
$\sigma_{id,V+M+N}$ (N/mm ²) =	133.1	<	261.9

Caso 2 SLV (1)

$\sigma_{s,N+M}$ (N/mm ²) =	72.1	<	261.9
$\tau_{s,Vz}$ (N/mm ²) =	17.2	<	151.2
$\sigma_{id,V+M+N}$ (N/mm ²) =	63.9	<	261.9

Caso 3 SLV (2)

$\sigma_{s,N+M}$ (N/mm ²) =	217.0	<	261.9
$\tau_{s,Vz}$ (N/mm ²) =	3.5	<	151.2
$\sigma_{id,V+M+N}$ (N/mm ²) =	125.9	<	261.9

Verifiche di stabilità a compressione [4.2.4.1.3.1]

Lungh. di calcolo del profilo: L (cm) = 42

Nel seguito si fa riferimento alle seguenti grandezze:

Coefficiente di vincolo di estremità: β

Lunghezza di calcolo del profilo: L_0

Raggi d'inerzia (assi y e z): i_y, i_z

Snellezze (assi y e z): λ_y, λ_z

Carico critico euleriano (assi y e z): $N_{cr,y}, N_{cr,z}$

Snellezze adimensionali (assi y e z): λ^*_y, λ^*_z

Fattori di imperfezione (Tab. 4.2.VI): α_y, α_z

Fattore [4.2.45]: $\Phi = 0.5 [1 + \alpha (\lambda^* - 0.2) + \lambda^{*2}]$

Coefficiente di riduzione [4.2.45]: $\chi = 1 / [\Phi + (\Phi^2 - \lambda^{*2})^{0.5}] < 1.0$

Resistenza all'instabilità dell'asta compressa: $N_{b,Rd}$

Rapporto lati: h/b = 1.00 (Tab. 4.2.VI)

Asse	β	L_0 (cm)	i (cm)	λ	λ_{lim}	N_{cr} (kg)	λ^*	Curva	α
y-y	2.0	84	9.58	8.8	200	10 706 210	0.101	a	0.21
z-z	2.0	84	2.27	36.9	200	603 069	0.425	a	0.21

Φ	χ	$N_{b,Rd}$ (kg)		N_{Ed} (kg)	0.04 N_{cr} (kg)
0.495	1.000	103 976	>	8 385	428 248
0.614	0.946	98 357	>	8 385	24 123

Verifiche di stabilità a tenso-pressoflessione [4.2.4.1.3.3]

- Metodo "A"

Momento variabile linearmente lungo l'asta (asse di flessione y-y): no
 Momento variabile linearmente lungo l'asta (asse di flessione z-z): no
 Verifica di instabilità flessio-torsionale: si

	y-y	z-z
Momento massimo: $M_{max,Ed}$ (kgm) =	2 638	636.3
Momento all'estremità A: M_A (kgm) =	0.0	0.0
Momento all'estremità B: M_B (kgm) =	0.0	0.0
Sforzo normale nell'asta: N (kg) =	-4 893	

Nel seguito si fa riferimento alle seguenti grandezze:

Carico critico euleriano (assi y e z): $N_{cr,y}$, $N_{cr,z}$

Coefficiente di riduzione minimo (assi y e z): χ_{min}

Coefficiente di riduzione [4.2.51]: $\chi_{LT} = (1/f) [1 / (\Phi_{LT} + (\Phi_{LT}^2 - \lambda_{LT}^{*2})^{0.5})] < 1.0$

Momento equivalente da considerare nella verifica (assi y e z) [C4.2.4.1.3.3.1]: $M_{y,eq,Ed}$, $M_{z,eq,Ed}$

Asse	N_{cr} (kg)	χ_{min}	$M_{m,Ed}$	$1.3 M_{m,Ed}$	M_{max}	$M_{eq,Ed}$	$M_{eq,Ed,lin}$	N	My-Mz
y-y	10 706 210	0.946	1 759	2 287	2 638	2 287	0.0	0.050	0.380
z-z	603 069	\	424.2	551.4	636.3	551.4	0.0	\	0.414

Verifica di stabilità [C4.2.32]: $N+My+Mz = 0.844 < 1.00$

Verifica profili dei cavalletti in acciaio

(NTC - p.to 4.2.4.1.2-3)

Puntelli diagonali dei cavalletti di sostegno dell'impalcato (estremità sup. - Posiz. appoggio spalla)

Dati geometrici e caratteristiche d'inerzia della sezione

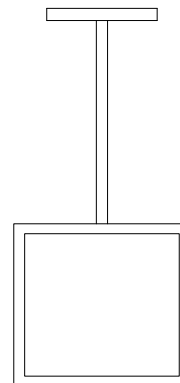
Profilo della sezione: **Tubo 120x80x5 + piatto 10 mm nervato**

Lato maggiore sezione: h (mm) =	120	H (mm) =	391.0
Lato minore sezione: b (mm) =	80	x (mm) =	185.5
Spessore del tubo: $t_w = a$ (mm) =	5		
Rapporto: c/t =	22.0		
Lunghezza ala di rinforzo: L (mm) =	265		
Spessore ala di rinforzo: t (mm) =	10		
Larghezza nervatura: b' (mm) =	50		
Spessore nervatura: t' (mm) =	6		

Area della sezione del profilo: A (cm ²) =	48.5
Area resistente netta: A _{net} (cm ²) =	48.5
Momento d'inerzia max.: J _y (cm ⁴) =	7 338.8
Momento d'inerzia min.: J _z (cm ⁴) =	206.0
Modulo di resistenza max.: W _y (cm ³) =	357.1
Modulo di resistenza min.: W _z (cm ³) =	51.5
Area a taglio: A _t (cm ²) =	10.4

Geometria profili

Luce dei profili: L (cm) =	42
Peso del profilo: p _{prof} (kg/m) =	38.1



Materiali della sezione

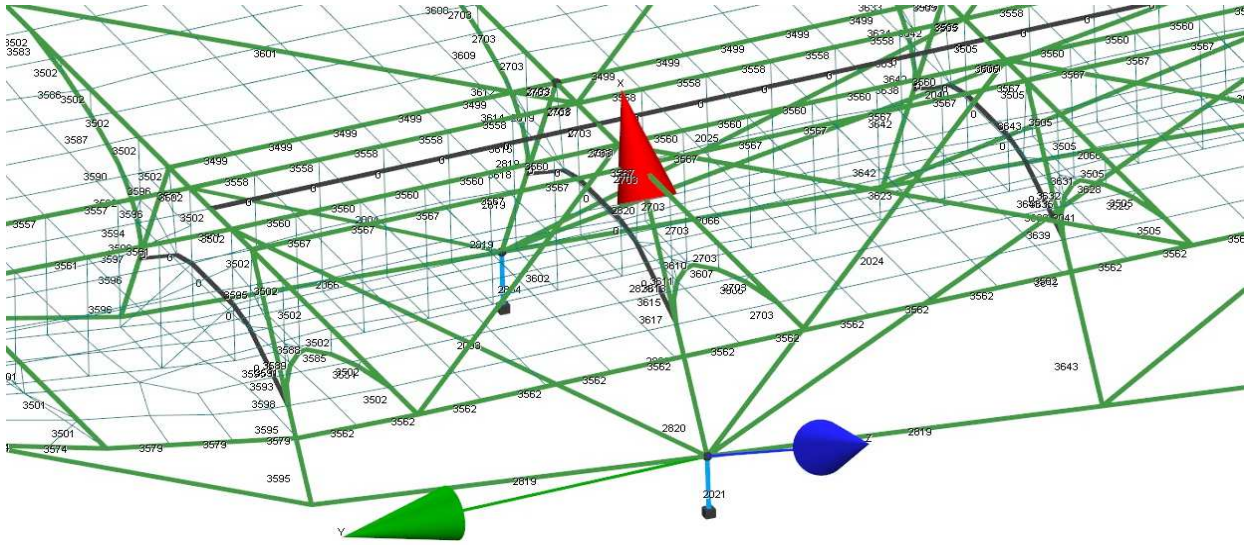
Classe dell'acciaio:	S 275 J0	Coeff. sicur. resistenza: γ_{M0} =	1.05
Tensione di rottura: f _{tk} (N/mm ²) =	430	Coeff. sicur. instabilità: γ_{M1} =	1.05
Tensione di snervam.: f _{yk} (N/mm ²) =	275	Coeff. sicur. frattura: γ_{M2} =	1.25
Parametro di classificaz.: ϵ =	0.924		
Classe della sezione:	1		
Coeff. di adattam. plastico sezione: ψ =	1.000		
Modulo elastico acciaio: E _s (N/mm ²) =	210 000		
Coefficiente di Poisson: ν =	0.3		

Sollecitazioni (da analisi F.E.M.)

	SLU (1)	SLV (1)	SLV (2)
Momento sollecit. asse y: M _{y,Ed} (kgm) =	1 526	668	1 634
Momento sollecit. asse z: M _{z,Ed} (kgm) =	466	62	346
Taglio sollecitante asse y: V _{y,Ed} (kg) =	1 214	872	130
Taglio sollecitante asse z: V _{z,Ed} (kg) =	6 726	5 123	1 050
Sforzo normale: N _{Ed} (kg) =	-3 320	-8 385	9 311
Torsione: T _{Ed} (kgm) =	0.0	0.0	0.0

Sollecitaz. prevalente: **N**

Coeff. incremento permanenti: γ_p =	1.30
Coeff. incremento variabili: γ_q =	1.50



Verif. di resistenza [4.2.4.1.2]

	SLU		
Momento resist. asse y: $M_{y,c,Rd}$ (kgm) =	9 352	>	1 526
Momento resist. asse z: $M_{z,c,Rd}$ (kgm) =	1 349	>	466
Taglio sollecitante asse y: $V_{y,Rd}$ (kg) =	73 337	>	1 214
Taglio sollecitante asse z: $V_{z,Rd}$ (kg) =	73 337	>	6 726
Sforzo normale resistente: $N_{pl,Rd}$ (kg) =	127 024	>	3 320

A_v (cm ²)	ρ
48.5	0.0
48.5	0.0
n =	0.026

	M+V	M+V+N		
Momento ridotto asse y: $M_{y,V,Rd}$ (kgm) =	9 352	9 352	>	1 526
Momento ridotto asse z: $M_{z,V,Rd}$ (kgm) =	1 349	1 349	>	465.9
[4.2.39-4.2.40]: $M_y + M_z + N + V =$		0.5086	<	1.00

Verifiche tensionali

Caso 1 SLU (1)

$\sigma_{s,N+M}$ (N/mm ²) =	140.0	<	261.9
$\tau_{s,Vz}$ (N/mm ²) =	18.5	<	151.2
$\sigma_{id,V+M+N}$ (N/mm ²) =	59.0	<	261.9

Caso 2 SLV (1)

$\sigma_{s,N+M}$ (N/mm ²) =	48.1	<	261.9
$\tau_{s,Vz}$ (N/mm ²) =	14.1	<	151.2
$\sigma_{id,V+M+N}$ (N/mm ²) =	43.5	<	261.9

Caso 3 SLV (2)

$\sigma_{s,N+M}$ (N/mm ²) =	132.2	<	261.9
$\tau_{s,Vz}$ (N/mm ²) =	2.9	<	151.2
$\sigma_{id,V+M+N}$ (N/mm ²) =	65.2	<	261.9

Verifiche di stabilità a compressione [4.2.4.1.3.1]

Lungh. di calcolo del profilo: L (cm) = 42

Nel seguito si fa riferimento alle seguenti grandezze:

Coefficiente di vincolo di estremità: β

Lunghezza di calcolo del profilo: L_0

Raggi d'inerzia (assi y e z): i_y, i_z

Snellezze (assi y e z): λ_y, λ_z

Carico critico euleriano (assi y e z): $N_{cr,y}, N_{cr,z}$

Snellezze adimensionali (assi y e z): λ^*_y, λ^*_z

Fattori di imperfezione (Tab. 4.2.VI): α_y, α_z

Fattore [4.2.45]: $\Phi = 0.5 [1 + \alpha (\lambda^* - 0.2) + \lambda^{*2}]$

Coefficiente di riduzione [4.2.45]: $\chi = 1 / [\Phi + (\Phi^2 - \lambda^{*2})^{0.5}] < 1.0$

Resistenza all'instabilità dell'asta compressa: $N_{b,Rd}$

Rapporto lati: h/b = 1.00 (Tab. 4.2.VI)

Asse	β	L_0 (cm)	i (cm)	λ	λ_{lim}	N_{cr} (kg)	λ^*	Curva	α
y-y	2.0	84	12.30	6.8	200	21 556 846	0.079	a	0.21
z-z	2.0	84	2.06	40.8	200	605 223	0.469	a	0.21

Φ	χ	$N_{b,Rd}$ (kg)		N_{Ed} (kg)	0.04 N_{cr} (kg)
0.490	1.000	127 024	>	8 385	862 274
0.638	0.934	118 577	>	8 385	24 209

Verifiche di stabilità a tenso-pressoflessione [4.2.4.1.3.3]

- Metodo "A"

Momento variabile linearmente lungo l'asta (asse di flessione y-y): no
 Momento variabile linearmente lungo l'asta (asse di flessione z-z): no
 Verifica di instabilità flessio-torsionale: si

	y-y	z-z
Momento massimo: $M_{max,Ed}$ (kgm) =	1 526	465.9
Momento all'estremità A: M_A (kgm) =	0.0	0.0
Momento all'estremità B: M_B (kgm) =	0.0	0.0
Sforzo normale nell'asta: N (kg) =	-3 320	

Nel seguito si fa riferimento alle seguenti grandezze:

Carico critico euleriano (assi y e z): $N_{cr,y}$, $N_{cr,z}$

Coefficiente di riduzione minimo (assi y e z): χ_{min}

Coefficiente di riduzione [4.2.51]: $\chi_{LT} = (1/f) [1 / (\Phi_{LT} + (\Phi_{LT}^2 - \lambda_{LT}^{*2})^{0.5})] < 1.0$

Momento equivalente da considerare nella verifica (assi y e z) [C4.2.4.1.3.3.1]: $M_{y,eq,Ed}$, $M_{z,eq,Ed}$

Asse	N_{cr} (kg)	χ_{min}	$M_{m,Ed}$	$1.3 M_{m,Ed}$	M_{max}	$M_{eq,Ed}$	$M_{eq,Ed,lin}$	N	My-Mz
y-y	21 556 846	0.934	1 017	1 322	1 526	1 322	0.0	0.028	0.141
z-z	605 223	\	310.6	403.8	465.9	403.8	0.0	\	0.301
Verifica di stabilità [C4.2.32]: $N+My+Mz =$			0.470	<	1.00				

Verifica profili dei cavalletti in acciaio

(NTC - p.to 4.2.4.1.2-3)

Puntelli diagonali dei cavalletti di sostegno dell'impalcato (estremità inf. - Posiz. appoggio pila)

Dati geometrici e caratteristiche d'inerzia della sezione

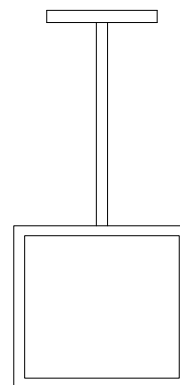
Profilo della sezione: **Tubo 120x80x5 + piatto 10 mm nervato**

Lato maggiore sezione: h (mm) =	120	H (mm) =	303.0
Lato minore sezione: b (mm) =	80	x (mm) =	144.3
Spessore del tubo: $t_w = a$ (mm) =	5		
Rapporto: c/t =	22.0		
Lunghezza ala di rinforzo: L (mm) =	177		
Spessore ala di rinforzo: t (mm) =	10		
Larghezza nervatura: b' (mm) =	50		
Spessore nervatura: t' (mm) =	6		

Area della sezione del profilo: A (cm ²) =	39.7
Area resistente netta: A _{net} (cm ²) =	39.7
Momento d'inerzia max.: J _y (cm ⁴) =	3 644.8
Momento d'inerzia min.: J _z (cm ⁴) =	205.3
Modulo di resistenza max.: W _y (cm ³) =	229.7
Modulo di resistenza min.: W _z (cm ³) =	51.3
Area a taglio.: A _t (cm ²) =	10.4

Geometria profili

Luce dei profili: L (cm) =	42
Peso del profilo: p _{prof} (kg/m) =	31.2



Materiali della sezione

Classe dell'acciaio:	S 275 J0	Coeff. sicur. resistenza: γ_{M0} =	1.05
Tensione di rottura: f _{tk} (N/mm ²) =	430	Coeff. sicur. instabilità: γ_{M1} =	1.05
Tensione di snervam.: f _{yk} (N/mm ²) =	275	Coeff. sicur. frattura: γ_{M2} =	1.25
Parametro di classificaz.: ϵ =	0.924		
Classe della sezione:	1		
Coeff. di adattam. plastico sezione: ψ =	1.000		
Modulo elastico acciaio: E _s (N/mm ²) =	210 000		
Coefficiente di Poisson: ν =	0.3		

Sollecitazioni (da analisi F.E.M.)

	SLU (1)	SLV (1)	SLV (2)
Momento sollecit. asse y: M _{y,Ed} (kgm) =	707	184	543
Momento sollecit. asse z: M _{z,Ed} (kgm) =	698	0	380
Taglio sollecitante asse y: V _{y,Ed} (kg) =	930	631	112
Taglio sollecitante asse z: V _{z,Ed} (kg) =	7 182	5 948	2 400
Sforzo normale: N _{Ed} (kg) =	-3 065	-8 385	9 311
Torsione: T _{Ed} (kgm) =	0.0	0.0	0.0

Sollecitaz. prevalente: **N**

Coeff. incremento permanenti: γ_p =	1.30
Coeff. incremento variabili: γ_q =	1.50

Verif. di resistenza [4.2.4.1.2]

	SLU		
Momento resist. asse y: $M_{y,c,Rd}$ (kgm) =	6 017	>	707
Momento resist. asse z: $M_{z,c,Rd}$ (kgm) =	1 344	>	698
Taglio sollecitante asse y: $V_{y,Rd}$ (kg) =	60 031	>	930
Taglio sollecitante asse z: $V_{z,Rd}$ (kg) =	60 031	>	7 182
Sforzo normale resistente: $N_{pl,Rd}$ (kg) =	103 976	>	3 065

A_v (cm ²)	ρ
39.7	0.0
39.7	0.0
n =	0.029

	M+V	M+V+N		
Momento ridotto asse y: $M_{y,V,Rd}$ (kgm) =	6 017	6 017	>	707
Momento ridotto asse z: $M_{z,V,Rd}$ (kgm) =	1 344	1 344	>	697.9
[4.2.39-4.2.40]: $M_y + M_z + N + V =$		0.6366	<	1.00

Verifiche tensionali

Caso 1 SLU (1)

$\sigma_{s,N+M}$ (N/mm ²) =	174.5	<	261.9
$\tau_{s,Vz}$ (N/mm ²) =	24.1	<	151.2
$\sigma_{id,V+M+N}$ (N/mm ²) =	56.8	<	261.9

Caso 2 SLV (1)

$\sigma_{s,N+M}$ (N/mm ²) =	29.1	<	261.9
$\tau_{s,Vz}$ (N/mm ²) =	20.0	<	151.2
$\sigma_{id,V+M+N}$ (N/mm ²) =	45.2	<	261.9

Caso 3 SLV (2)

$\sigma_{s,N+M}$ (N/mm ²) =	121.2	<	261.9
$\tau_{s,Vz}$ (N/mm ²) =	8.1	<	151.2
$\sigma_{id,V+M+N}$ (N/mm ²) =	49.1	<	261.9

Verifiche di stabilità a compressione [4.2.4.1.3.1]

Lungh. di calcolo del profilo: L (cm) = 42

Nel seguito si fa riferimento alle seguenti grandezze:

Coefficiente di vincolo di estremità: β

Lunghezza di calcolo del profilo: L_0

Raggi d'inerzia (assi y e z): i_y, i_z

Snellezze (assi y e z): λ_y, λ_z

Carico critico euleriano (assi y e z): $N_{cr,y}, N_{cr,z}$

Snellezze adimensionali (assi y e z): λ^*_y, λ^*_z

Fattori di imperfezione (Tab. 4.2.VI): α_y, α_z

Fattore [4.2.45]: $\Phi = 0.5 [1 + \alpha (\lambda^* - 0.2) + \lambda^{*2}]$

Coefficiente di riduzione [4.2.45]: $\chi = 1 / [\Phi + (\Phi^2 - \lambda^{*2})^{0.5}] < 1.0$

Resistenza all'instabilità dell'asta compressa: $N_{b,Rd}$

Rapporto lati: h/b = 1.00 (Tab. 4.2.VI)

Asse	β	L_0 (cm)	i (cm)	λ	λ_{lim}	N_{cr} (kg)	λ^*	Curva	α
y-y	2.0	84	9.58	8.8	200	10 706 210	0.101	a	0.21
z-z	2.0	84	2.27	36.9	200	603 069	0.425	a	0.21

Φ	χ	$N_{b,Rd}$ (kg)		N_{Ed} (kg)	0.04 N_{cr} (kg)
0.495	1.000	103 976	>	8 385	428 248
0.614	0.946	98 357	>	8 385	24 123

Verifiche di stabilità a tenso-pressoflessione [4.2.4.1.3.3]

- Metodo "A"

Momento variabile linearmente lungo l'asta (asse di flessione y-y): no
 Momento variabile linearmente lungo l'asta (asse di flessione z-z): no
 Verifica di instabilità flessio-torsionale: si

	y-y	z-z
Momento massimo: $M_{max,Ed}$ (kgm) =	707	697.9
Momento all'estremità A: M_A (kgm) =	0.0	0.0
Momento all'estremità B: M_B (kgm) =	0.0	0.0
Sforzo normale nell'asta: N (kg) =	-3 065	

Nel seguito si fa riferimento alle seguenti grandezze:

Carico critico euleriano (assi y e z): $N_{cr,y}$, $N_{cr,z}$

Coefficiente di riduzione minimo (assi y e z): χ_{min}

Coefficiente di riduzione [4.2.51]: $\chi_{LT} = (1/f) [1 / (\Phi_{LT} + (\Phi_{LT}^2 - \lambda_{LT}^{*2})^{0.5})] < 1.0$

Momento equivalente da considerare nella verifica (assi y e z) [C4.2.4.1.3.3.1]: $M_{y,eq,Ed}$, $M_{z,eq,Ed}$

Asse	N_{cr} (kg)	χ_{min}	$M_{m,Ed}$	$1.3 M_{m,Ed}$	M_{max}	$M_{eq,Ed}$	$M_{eq,Ed,lin}$	N	My-Mz
y-y	10 706 210	0.946	471	612	707	612	0.0	0.031	0.102
z-z	603 069	\	465.3	604.9	697.9	604.9	0.0	\	0.452

Verifica di stabilità [C4.2.32]: $N+My+Mz = 0.585 < 1.00$

Verifica profili dei cavalletti in acciaio

(NTC - p.to 4.2.4.1.2-3)

Puntelli diagonali dei cavalletti di sostegno dell'impalcato (estremità sup. - Posiz. appoggio pila)

Dati geometrici e caratteristiche d'inerzia della sezione

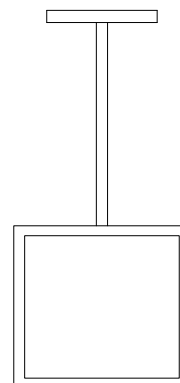
Profilo della sezione: **Tubo 120x80x5 + piatto 10 mm nervato**

Lato maggiore sezione: h (mm) =	120	H (mm) =	391.0
Lato minore sezione: b (mm) =	80	x (mm) =	185.5
Spessore del tubo: $t_w = a$ (mm) =	5		
Rapporto: c/t =	22.0		
Lunghezza ala di rinforzo: L (mm) =	265		
Spessore ala di rinforzo: t (mm) =	10		
Larghezza nervatura: b' (mm) =	50		
Spessore nervatura: t' (mm) =	6		

Area della sezione del profilo: A (cm ²) =	48.5
Area resistente netta: A _{net} (cm ²) =	48.5
Momento d'inerzia max.: J _y (cm ⁴) =	7 338.8
Momento d'inerzia min.: J _z (cm ⁴) =	206.0
Modulo di resistenza max.: W _y (cm ³) =	357.1
Modulo di resistenza min.: W _z (cm ³) =	51.5
Area a taglio: A _t (cm ²) =	10.4

Geometria profili

Luce dei profili: L (cm) =	42
Peso del profilo: p _{prof} (kg/m) =	38.1



Materiali della sezione

Classe dell'acciaio:	S 275 J0	Coeff. sicur. resistenza: γ_{M0} =	1.05
Tensione di rottura: f _{tk} (N/mm ²) =	430	Coeff. sicur. instabilità: γ_{M1} =	1.05
Tensione di snervam.: f _{yk} (N/mm ²) =	275	Coeff. sicur. frattura: γ_{M2} =	1.25
Parametro di classificaz.: ϵ =	0.924		
Classe della sezione:	1		
Coeff. di adattam. plastico sezione: ψ =	1.000		
Modulo elastico acciaio: E _s (N/mm ²) =	210 000		
Coefficiente di Poisson: ν =	0.3		

Sollecitazioni (da analisi F.E.M.)

	SLU (1)	SLV (1)	SLV (2)
Momento sollecit. asse y: M _{y,Ed} (kgm) =	1 621	1 133	2 091
Momento sollecit. asse z: M _{z,Ed} (kgm) =	520	381	69
Taglio sollecitante asse y: V _{y,Ed} (kg) =	1 363	181	979
Taglio sollecitante asse z: V _{z,Ed} (kg) =	7 672	8 780	4 850
Sforzo normale: N _{Ed} (kg) =	-3 320	-8 385	9 311
Torsione: T _{Ed} (kgm) =	0.0	0.0	0.0

Sollecitaz. prevalente: **N**

Coeff. incremento permanenti: γ_p =	1.30
Coeff. incremento variabili: γ_q =	1.50

Verif. di resistenza [4.2.4.1.2]

	SLU		
Momento resist. asse y: $M_{y,c,Rd}$ (kgm) =	9 352	>	1 621
Momento resist. asse z: $M_{z,c,Rd}$ (kgm) =	1 349	>	520
Taglio sollecitante asse y: $V_{y,Rd}$ (kg) =	73 337	>	1 363
Taglio sollecitante asse z: $V_{z,Rd}$ (kg) =	73 337	>	7 672
Sforzo normale resistente: $N_{pl,Rd}$ (kg) =	127 024	>	3 320

A_v (cm ²)	ρ
48.5	0.0
48.5	0.0
n = 0.026	

	M+V	M+V+N		
Momento ridotto asse y: $M_{y,V,Rd}$ (kgm) =	9 352	9 352	>	1 621
Momento ridotto asse z: $M_{z,V,Rd}$ (kgm) =	1 349	1 349	>	519.5
[4.2.39-4.2.40]: $M_y + M_z + N + V =$		0.5584	<	1.00

Verifiche tensionali

Caso 1 SLU (1)

$\sigma_{s,N+M}$ (N/mm ²) =	153.1	<	261.9
$\tau_{s,Vz}$ (N/mm ²) =	21.1	<	151.2
$\sigma_{id,V+M+N}$ (N/mm ²) =	63.7	<	261.9

Caso 2 SLV (1)

$\sigma_{s,N+M}$ (N/mm ²) =	122.9	<	261.9
$\tau_{s,Vz}$ (N/mm ²) =	24.1	<	151.2
$\sigma_{id,V+M+N}$ (N/mm ²) =	64.4	<	261.9

Caso 3 SLV (2)

$\sigma_{s,N+M}$ (N/mm ²) =	91.1	<	261.9
$\tau_{s,Vz}$ (N/mm ²) =	13.3	<	151.2
$\sigma_{id,V+M+N}$ (N/mm ²) =	81.1	<	261.9

Verifiche di stabilità a compressione [4.2.4.1.3.1]

Lungh. di calcolo del profilo: L (cm) = 42

Nel seguito si fa riferimento alle seguenti grandezze:

Coefficiente di vincolo di estremità: β

Lunghezza di calcolo del profilo: L_0

Raggi d'inerzia (assi y e z): i_y, i_z

Snellezze (assi y e z): λ_y, λ_z

Carico critico euleriano (assi y e z): $N_{cr,y}, N_{cr,z}$

Snellezze adimensionali (assi y e z): λ^*_y, λ^*_z

Fattori di imperfezione (Tab. 4.2.VI): α_y, α_z

Fattore [4.2.45]: $\Phi = 0.5 [1 + \alpha (\lambda^* - 0.2) + \lambda^{*2}]$

Coefficiente di riduzione [4.2.45]: $\chi = 1 / [\Phi + (\Phi^2 - \lambda^{*2})^{0.5}] < 1.0$

Resistenza all'instabilità dell'asta compressa: $N_{b,Rd}$

Rapporto lati: h/b = 1.00 (Tab. 4.2.VI)

Asse	β	L_0 (cm)	i (cm)	λ	λ_{lim}	N_{cr} (kg)	λ^*	Curva	α
y-y	2.0	84	12.30	6.8	200	21 556 846	0.079	a	0.21
z-z	2.0	84	2.06	40.8	200	605 223	0.469	a	0.21

Φ	χ	$N_{b,Rd}$ (kg)		N_{Ed} (kg)	0.04 N_{cr} (kg)
0.490	1.000	127 024	>	8 385	862 274
0.638	0.934	118 577	>	8 385	24 209

Verifiche di stabilità a tenso-pressoflessione [4.2.4.1.3.3]

- Metodo "A"

Momento variabile linearmente lungo l'asta (asse di flessione y-y): no
 Momento variabile linearmente lungo l'asta (asse di flessione z-z): no
 Verifica di instabilità flesso-torsionale: si

	y-y	z-z
Momento massimo: $M_{max,Ed}$ (kgm) =	1 621	519.5
Momento all'estremità A: M_A (kgm) =	0.0	0.0
Momento all'estremità B: M_B (kgm) =	0.0	0.0
Sforzo normale nell'asta: N (kg) =	-3 320	

Nel seguito si fa riferimento alle seguenti grandezze:

Carico critico euleriano (assi y e z): $N_{cr,y}$, $N_{cr,z}$

Coefficiente di riduzione minimo (assi y e z): χ_{min}

Coefficiente di riduzione [4.2.51]: $\chi_{LT} = (1/f) [1 / (\Phi_{LT} + (\Phi_{LT}^2 - \lambda_{LT}^{*2})^{0.5})] < 1.0$

Momento equivalente da considerare nella verifica (assi y e z) [C4.2.4.1.3.3.1]: $M_{y,eq,Ed}$, $M_{z,eq,Ed}$

Asse	N_{cr} (kg)	χ_{min}	$M_{m,Ed}$	$1.3 M_{m,Ed}$	M_{max}	$M_{eq,Ed}$	$M_{eq,Ed,lin}$	N	My-Mz
y-y	21 556 846	0.934	1 081	1 405	1 621	1 405	0.0	0.028	0.150
z-z	605 223	\	346.4	450.3	519.5	450.3	0.0	\	0.336
Verifica di stabilità [C4.2.32]: $N+My+Mz =$			0.514	<	1.00				

Verifica profili dei cavalletti in acciaio

(NTC - p.to 4.2.4.1.2-3)

Puntelli diagonali dei cavalletti di sostegno dell'impalcato (estremità inf. - Posiz. appoggio pila)

Dati geometrici e caratteristiche d'inerzia della sezione

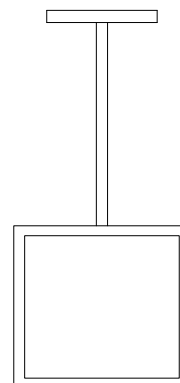
Profilo della sezione: **Tubo 120x80x5 + piatto 10 mm nervato**

Lato maggiore sezione: h (mm) =	120	H (mm) =	303.0
Lato minore sezione: b (mm) =	80	x (mm) =	144.3
Spessore del tubo: $t_w = a$ (mm) =	5		
Rapporto: c/t =	22.0		
Lunghezza ala di rinforzo: L (mm) =	177		
Spessore ala di rinforzo: t (mm) =	10		
Larghezza nervatura: b' (mm) =	50		
Spessore nervatura: t' (mm) =	6		

Area della sezione del profilo: A (cm ²) =	39.7
Area resistente netta: A _{net} (cm ²) =	39.7
Momento d'inerzia max.: J _y (cm ⁴) =	3 644.8
Momento d'inerzia min.: J _z (cm ⁴) =	205.3
Modulo di resistenza max.: W _y (cm ³) =	229.7
Modulo di resistenza min.: W _z (cm ³) =	51.3
Area a taglio: A _t (cm ²) =	10.4

Geometria profili

Luce dei profili: L (cm) =	42
Peso del profilo: p _{prof} (kg/m) =	31.2



Materiali della sezione

Classe dell'acciaio:	S 275 J0	Coeff. sicur. resistenza: γ_{M0} =	1.05
Tensione di rottura: f _{tk} (N/mm ²) =	430	Coeff. sicur. instabilità: γ_{M1} =	1.05
Tensione di snervam.: f _{yk} (N/mm ²) =	275	Coeff. sicur. frattura: γ_{M2} =	1.25
Parametro di classificaz.: ϵ =	0.924		
Classe della sezione:	1		
Coeff. di adattam. plastico sezione: ψ =	1.000		
Modulo elastico acciaio: E _s (N/mm ²) =	210 000		
Coefficiente di Poisson: ν =	0.3		

Sollecitazioni (da analisi F.E.M.)

	SLU (1)	SLV (1)	SLV (2)
Momento sollecit. asse y: M _{y,Ed} (kgm) =	621	7	369
Momento sollecit. asse z: M _{z,Ed} (kgm) =	767	471	11
Taglio sollecitante asse y: V _{y,Ed} (kg) =	1 054	65	665
Taglio sollecitante asse z: V _{z,Ed} (kg) =	6 189	3 852	256
Sforzo normale: N _{Ed} (kg) =	-3 008	-8 385	9 311
Torsione: T _{Ed} (kgm) =	0.0	0.0	0.0

Sollecitaz. prevalente: **N**

Coeff. incremento permanenti: γ_p =	1.30
Coeff. incremento variabili: γ_q =	1.50

Verif. di resistenza [4.2.4.1.2]

	SLU		
Momento resist. asse y: $M_{y,c,Rd}$ (kgm) =	6 017	>	621
Momento resist. asse z: $M_{z,c,Rd}$ (kgm) =	1 344	>	767
Taglio sollecitante asse y: $V_{y,Rd}$ (kg) =	60 031	>	1 054
Taglio sollecitante asse z: $V_{z,Rd}$ (kg) =	60 031	>	6 189
Sforzo normale resistente: $N_{pl,Rd}$ (kg) =	103 976	>	3 008

A_v (cm ²)	ρ
39.7	0.0
39.7	0.0
n =	0.029

	M+V	M+V+N		
Momento ridotto asse y: $M_{y,V,Rd}$ (kgm) =	6 017	6 017	>	621
Momento ridotto asse z: $M_{z,V,Rd}$ (kgm) =	1 344	1 344	>	767.0
[4.2.39-4.2.40]: $M_y + M_z + N + V =$		0.6737	<	1.00

Verifiche tensionali

Caso 1 SLU (1)

$\sigma_{s,N+M}$ (N/mm ²) =	184.0	<	261.9
$\tau_{s,Vz}$ (N/mm ²) =	20.8	<	151.2
$\sigma_{id,V+M+N}$ (N/mm ²) =	49.9	<	261.9

Caso 2 SLV (1)

$\sigma_{s,N+M}$ (N/mm ²) =	113.1	<	261.9
$\tau_{s,Vz}$ (N/mm ²) =	12.9	<	151.2
$\sigma_{id,V+M+N}$ (N/mm ²) =	31.0	<	261.9

Caso 3 SLV (2)

$\sigma_{s,N+M}$ (N/mm ²) =	41.6	<	261.9
$\tau_{s,Vz}$ (N/mm ²) =	0.9	<	151.2
$\sigma_{id,V+M+N}$ (N/mm ²) =	39.5	<	261.9

Verifiche di stabilità a compressione [4.2.4.1.3.1]

Lungh. di calcolo del profilo: L (cm) = 42

Nel seguito si fa riferimento alle seguenti grandezze:

Coefficiente di vincolo di estremità: β

Lunghezza di calcolo del profilo: L_0

Raggi d'inerzia (assi y e z): i_y, i_z

Snellezze (assi y e z): λ_y, λ_z

Carico critico euleriano (assi y e z): $N_{cr,y}, N_{cr,z}$

Snellezze adimensionali (assi y e z): λ^*_y, λ^*_z

Fattori di imperfezione (Tab. 4.2.VI): α_y, α_z

Fattore [4.2.45]: $\Phi = 0.5 [1 + \alpha (\lambda^* - 0.2) + \lambda^{*2}]$

Coefficiente di riduzione [4.2.45]: $\chi = 1 / [\Phi + (\Phi^2 - \lambda^{*2})^{0.5}] < 1.0$

Resistenza all'instabilità dell'asta compressa: $N_{b,Rd}$

Rapporto lati: h/b = 1.00 (Tab. 4.2.VI)

Asse	β	L_0 (cm)	i (cm)	λ	λ_{lim}	N_{cr} (kg)	λ^*	Curva	α
y-y	2.0	84	9.58	8.8	200	10 706 210	0.101	a	0.21
z-z	2.0	84	2.27	36.9	200	603 069	0.425	a	0.21

Φ	χ	$N_{b,Rd}$ (kg)		N_{Ed} (kg)	0.04 N_{cr} (kg)
0.495	1.000	103 976	>	8 385	428 248
0.614	0.946	98 357	>	8 385	24 123

Verifiche di stabilità a tenso-pressoflessione [4.2.4.1.3.3]

- Metodo "A"

Momento variabile linearmente lungo l'asta (asse di flessione y-y): no
 Momento variabile linearmente lungo l'asta (asse di flessione z-z): no
 Verifica di instabilità flesso-torsionale: si

	y-y	z-z
Momento massimo: $M_{max,Ed}$ (kgm) =	621	767.0
Momento all'estremità A: M_A (kgm) =	0.0	0.0
Momento all'estremità B: M_B (kgm) =	0.0	0.0
Sforzo normale nell'asta: N (kg) =	-3 008	

Nel seguito si fa riferimento alle seguenti grandezze:

Carico critico euleriano (assi y e z): $N_{cr,y}$, $N_{cr,z}$

Coefficiente di riduzione minimo (assi y e z): χ_{min}

Coefficiente di riduzione [4.2.51]: $\chi_{LT} = (1/f) [1 / (\Phi_{LT} + (\Phi_{LT}^2 - \lambda_{LT}^{*2})^{0.5})] < 1.0$

Momento equivalente da considerare nella verifica (assi y e z) [C4.2.4.1.3.3.1]: $M_{y,eq,Ed}$, $M_{z,eq,Ed}$

Asse	N_{cr} (kg)	χ_{min}	$M_{m,Ed}$	$1.3 M_{m,Ed}$	M_{max}	$M_{eq,Ed}$	$M_{eq,Ed,lin}$	N	My-Mz
y-y	10 706 210	0.946	414	538	621	538	0.0	0.031	0.089
z-z	603 069	\	511.3	664.7	767.0	664.7	0.0	\	0.497
Verifica di stabilità [C4.2.32]: $N+My+Mz =$			0.617	<	1.00				

Verifica profili dei cavalletti in acciaio

(NTC - p.to 4.2.4.1.2-3)

Puntelli diagonali dei cavalletti di sostegno dell'impalcato (estremità sup. - Posiz. appoggio pila)

Dati geometrici e caratteristiche d'inerzia della sezione

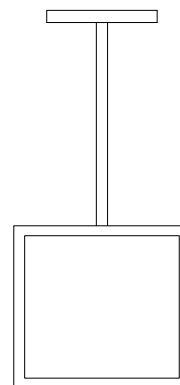
Profilo della sezione: **Tubo 120x80x5 + piatto 10 mm nervato**

Lato maggiore sezione: h (mm) =	120	H (mm) =	391.0
Lato minore sezione: b (mm) =	80	x (mm) =	185.5
Spessore del tubo: $t_w = a$ (mm) =	5		
Rapporto: c/t =	22.0		
Lunghezza ala di rinforzo: L (mm) =	265		
Spessore ala di rinforzo: t (mm) =	10		
Larghezza nervatura: b' (mm) =	50		
Spessore nervatura: t' (mm) =	6		

Area della sezione del profilo: A (cm ²) =	48.5
Area resistente netta: A _{net} (cm ²) =	48.5
Momento d'inerzia max.: J _y (cm ⁴) =	7 338.8
Momento d'inerzia min.: J _z (cm ⁴) =	206.0
Modulo di resistenza max.: W _y (cm ³) =	357.1
Modulo di resistenza min.: W _z (cm ³) =	51.5
Area a taglio: A _t (cm ²) =	10.4

Geometria profili

Luce dei profili: L (cm) =	42
Peso del profilo: p _{prof} (kg/m) =	38.1



Materiali della sezione

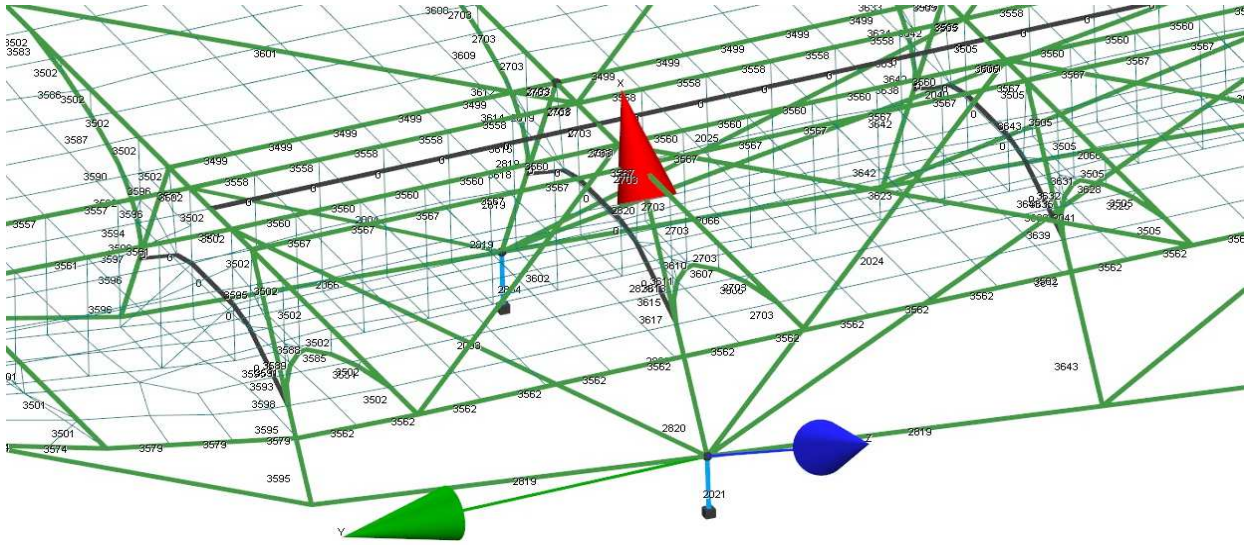
Classe dell'acciaio:	S 275 J0	Coeff. sicur. resistenza: γ_{M0} =	1.05
Tensione di rottura: f _{tk} (N/mm ²) =	430	Coeff. sicur. instabilità: γ_{M1} =	1.05
Tensione di snervam.: f _{yk} (N/mm ²) =	275	Coeff. sicur. frattura: γ_{M2} =	1.25
Parametro di classificaz.: ϵ =	0.924		
Classe della sezione:	1		
Coeff. di adattam. plastico sezione: ψ =	1.000		
Modulo elastico acciaio: E _s (N/mm ²) =	210 000		
Coefficiente di Poisson: ν =	0.3		

Sollecitazioni (da analisi F.E.M.)

	SLU (1)	SLV (1)	SLV (2)
Momento sollecit. asse y: M _{y,Ed} (kgm) =	1 526	668	1 634
Momento sollecit. asse z: M _{z,Ed} (kgm) =	466	62	346
Taglio sollecitante asse y: V _{y,Ed} (kg) =	1 214	872	130
Taglio sollecitante asse z: V _{z,Ed} (kg) =	6 726	5 123	1 050
Sforzo normale: N _{Ed} (kg) =	-3 320	-8 385	9 311
Torsione: T _{Ed} (kgm) =	0.0	0.0	0.0

Sollecitaz. prevalente: **N**

Coeff. incremento permanenti: γ_p =	1.30
Coeff. incremento variabili: γ_q =	1.50



Verif. di resistenza [4.2.4.1.2]

	SLU		
Momento resist. asse y: $M_{y,c,Rd}$ (kgm) =	9 352	>	1 526
Momento resist. asse z: $M_{z,c,Rd}$ (kgm) =	1 349	>	466
Taglio sollecitante asse y: $V_{y,Rd}$ (kg) =	73 337	>	1 214
Taglio sollecitante asse z: $V_{z,Rd}$ (kg) =	73 337	>	6 726
Sforzo normale resistente: $N_{pl,Rd}$ (kg) =	127 024	>	3 320

A_v (cm ²)	ρ
48.5	0.0
48.5	0.0
n =	0.026

	M+V	M+V+N		
Momento ridotto asse y: $M_{y,V,Rd}$ (kgm) =	9 352	9 352	>	1 526
Momento ridotto asse z: $M_{z,V,Rd}$ (kgm) =	1 349	1 349	>	465.9
[4.2.39-4.2.40]: $M_y + M_z + N + V =$		0.5086	<	1.00

Verifiche tensionali

Caso 1 SLU (1)

$\sigma_{s,N+M}$ (N/mm ²) =	140.0	<	261.9
$\tau_{s,Vz}$ (N/mm ²) =	18.5	<	151.2
$\sigma_{id,V+M+N}$ (N/mm ²) =	59.0	<	261.9

Caso 2 SLV (1)

$\sigma_{s,N+M}$ (N/mm ²) =	48.1	<	261.9
$\tau_{s,Vz}$ (N/mm ²) =	14.1	<	151.2
$\sigma_{id,V+M+N}$ (N/mm ²) =	43.5	<	261.9

Caso 3 SLV (2)

$\sigma_{s,N+M}$ (N/mm ²) =	132.2	<	261.9
$\tau_{s,Vz}$ (N/mm ²) =	2.9	<	151.2
$\sigma_{id,V+M+N}$ (N/mm ²) =	65.2	<	261.9

Verifiche di stabilità a compressione [4.2.4.1.3.1]

Lungh. di calcolo del profilo: L (cm) = 42

Nel seguito si fa riferimento alle seguenti grandezze:

Coefficiente di vincolo di estremità: β

Lunghezza di calcolo del profilo: L_0

Raggi d'inerzia (assi y e z): i_y, i_z

Snellezze (assi y e z): λ_y, λ_z

Carico critico euleriano (assi y e z): $N_{cr,y}, N_{cr,z}$

Snellezze adimensionali (assi y e z): λ^*_y, λ^*_z

Fattori di imperfezione (Tab. 4.2.VI): α_y, α_z

Fattore [4.2.45]: $\Phi = 0.5 [1 + \alpha (\lambda^* - 0.2) + \lambda^{*2}]$

Coefficiente di riduzione [4.2.45]: $\chi = 1 / [\Phi + (\Phi^2 - \lambda^{*2})^{0.5}] < 1.0$

Resistenza all'instabilità dell'asta compressa: $N_{b,Rd}$

Rapporto lati: h/b = 1.00 (Tab. 4.2.VI)

Asse	β	L_0 (cm)	i (cm)	λ	λ_{lim}	N_{cr} (kg)	λ^*	Curva	α
y-y	2.0	84	12.30	6.8	200	21 556 846	0.079	a	0.21
z-z	2.0	84	2.06	40.8	200	605 223	0.469	a	0.21

Φ	χ	$N_{b,Rd}$ (kg)		N_{Ed} (kg)	0.04 N_{cr} (kg)
0.490	1.000	127 024	>	8 385	862 274
0.638	0.934	118 577	>	8 385	24 209

Verifiche di stabilità a tenso-pressoflessione [4.2.4.1.3.3]

- Metodo "A"

Momento variabile linearmente lungo l'asta (asse di flessione y-y): no
 Momento variabile linearmente lungo l'asta (asse di flessione z-z): no
 Verifica di instabilità flessio-torsionale: si

	y-y	z-z
Momento massimo: $M_{max,Ed}$ (kgm) =	1 526	465.9
Momento all'estremità A: M_A (kgm) =	0.0	0.0
Momento all'estremità B: M_B (kgm) =	0.0	0.0
Sforzo normale nell'asta: N (kg) =	-3 320	

Nel seguito si fa riferimento alle seguenti grandezze:

Carico critico euleriano (assi y e z): $N_{cr,y}$, $N_{cr,z}$

Coefficiente di riduzione minimo (assi y e z): χ_{min}

Coefficiente di riduzione [4.2.51]: $\chi_{LT} = (1/f) [1 / (\Phi_{LT} + (\Phi_{LT}^2 - \lambda_{LT}^{*2})^{0.5})] < 1.0$

Momento equivalente da considerare nella verifica (assi y e z) [C4.2.4.1.3.3.1]: $M_{y,eq,Ed}$, $M_{z,eq,Ed}$

Asse	N_{cr} (kg)	χ_{min}	$M_{m,Ed}$	$1.3 M_{m,Ed}$	M_{max}	$M_{eq,Ed}$	$M_{eq,Ed,lin}$	N	My-Mz
y-y	21 556 846	0.934	1 017	1 322	1 526	1 322	0.0	0.028	0.141
z-z	605 223	\	310.6	403.8	465.9	403.8	0.0	\	0.301
Verifica di stabilità [C4.2.32]: $N+My+Mz =$			0.470	<	1.00				

APPOGGI TRAVI DI IMPALCATO

Campata sud - spalla sud

Appoggio su struttura in c.a. - Verifica SLU a presso-flessione

Caratteristiche dei materiali

- Calcestruzzo

Classe calcestruzzo della struttura di base: R_{ck} (N/mm ²) =	14.2	Carota	C2
Resistenza cilindrica caratteristica del materiale base: f_{ck} (N/mm ²) =	11.8		
Resistenza a taglio caratteristica del materiale base: f_{ctk} (N/mm ²) =	1.09		
Coefficiente di sicurezza parziale del materiale: γ_c =	1.50		
Fattore di confidenza: FC =	1.00	<i>(struttura esistente con prova diretta su campione)</i>	
Resist. a compressione di progetto del materiale base: f_{cd} (N/mm ²) =	6.67		
Resistenza a taglio di progetto del materiale base: f_{ctd} (N/mm ²) =	0.72		

- Barre in acciaio

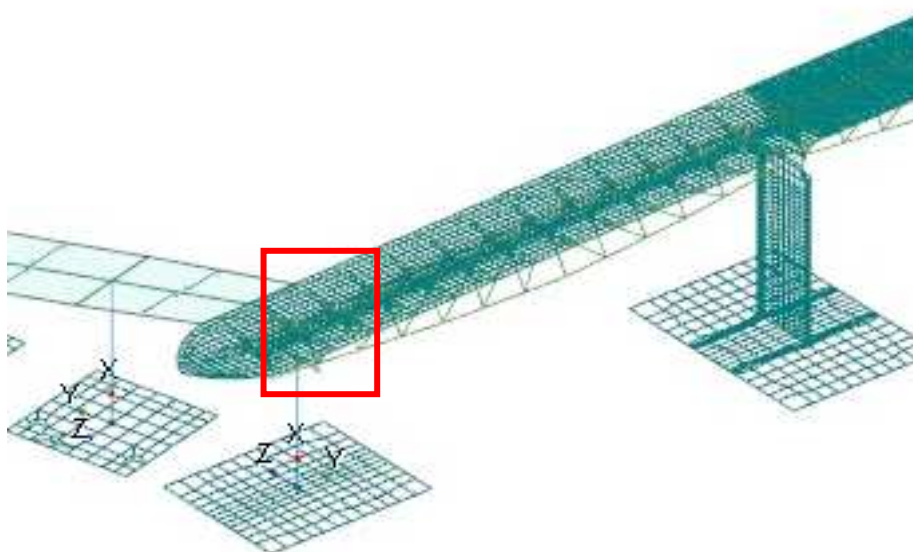
Acciaio a snervamento: f_{yk} (MPa) =	469	Spezz.	1
Acciaio a rottura: f_{tk} (MPa) =	674		

Si assumono i valori di un acciaio FeB44k

Resistenza a rottura caratteristica delle barre: f_{tk} (N/mm ²) =	674	FeB44k	
Resistenza a snervamento caratteristica delle barre: f_{yk} (N/mm ²) =	469		
Coefficiente parziale di sicurezza del materiale: γ_M =	1.15		
Fattore di confidenza: FC =	1.00	<i>(struttura esistente con prova diretta su campione)</i>	
Resistenza a trazione di progetto delle barre di nodo: $f_{s,yd}$ (N/mm ²) =	407.8		

- Materiali dell'ancoraggio

f_{yk} (N/mm ²) =	640
Classe dell'acciaio:	cl. 8.8
f_{yd} (N/mm ²) =	512
Tensione di rottura: f_{tk} (N/mm ²) =	800
Coeff. sicur. parziale: γ_s =	1.25



Posizione dell'appoggio sulla struttura in c.a.

Verifica a pressoflessione dell'appoggio

Definizione della sezione resistente e delle sollecitazioni.

Titolo : Spalla sud - Appoggio

N° Vertici **Zoom** **N° barre** **Zoom**

N°	x [cm]	y [cm]
1	0	0
2	0	30
3	33	30
4	33	0

N°	As [cm²]	x [cm]	y [cm]
2	2.01	3.2	26.8
3	2.01	3.2	15
4	2.01	29.8	3.2
5	2.01	29.8	26.8
6	2.01	29.8	15

Tipo Sezione
 Rettan.re Trapezi
 a T Circolare
 Rettangoli Coord.

Sollecitazioni
 S.L.U. Metodo n

N_{Ed} kN
M_{xEd} kNm
M_{yEd}

P.to applicazione N
 Centro Baricentro cls
 Coord.[cm] xN yN

Tipo rottura
 Lato calcestruzzo - Acciaio snervato

Metodo di calcolo
 S.L.U.+ S.L.U.-
 Metodo n

Tipo flessione
 Retta Deviata

N* rett.

Calcola MRd **Dominio Mx-My**

angolo asse neutro θ°

Precompresso

Materiali
 cl. 8.8 Carota 2
 ϵ_{su} ‰ ϵ_{c2} ‰
 f_{yd} N/mm² ϵ_{cu} ‰
 E_s N/mm² f_{cd} ‰
 E_s/E_c f_{cc}/f_{cd} ?
 ϵ_{syd} ‰ $\sigma_{c,adm}$
 $\sigma_{s,adm}$ N/mm² τ_{co}
 τ_{c1}

M_{xRd} kN m
M_{yRd} kN m
 σ_c N/mm²
 σ_s N/mm²
 ϵ_c ‰
 ϵ_s ‰
 d cm
 x x/d
 δ

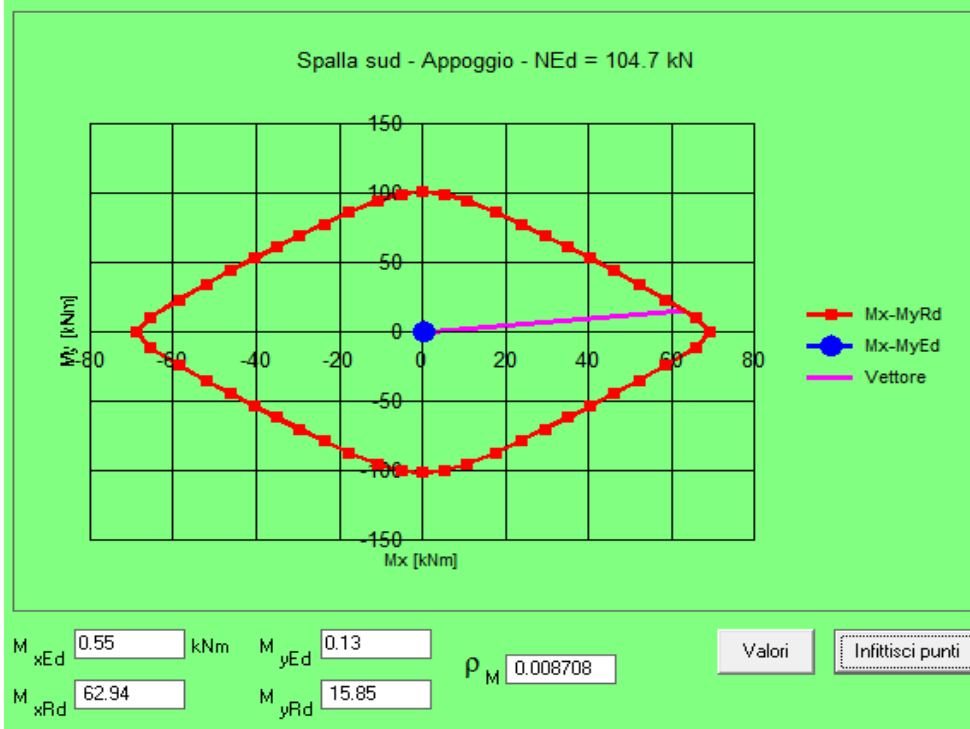
Si considera l'altezza del tacco di riscontro (piano di trasferimento dell'azione sollecitante) dalla sezione di verifica del collegamento sul calcestruzzo di base.

Altezza del dispositivo di appoggio: h' (cm) =

Sollecitazioni e verifiche

- SISMA direzione X

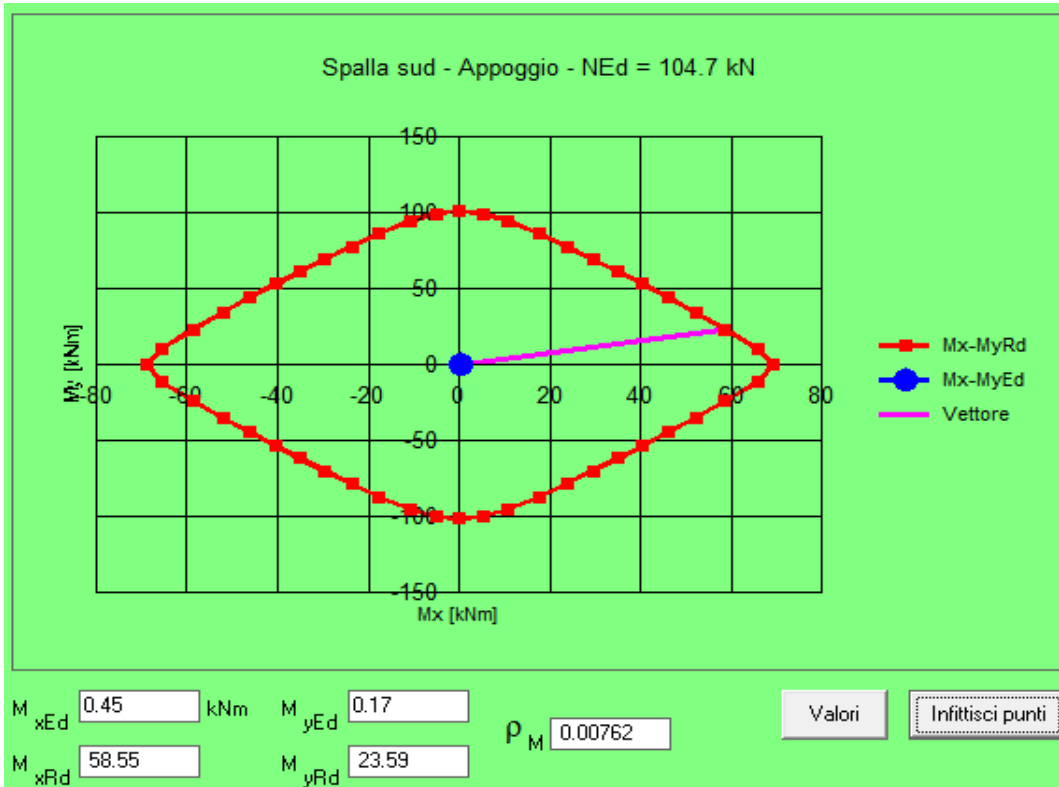
Momento sollecitante massimo asse Y: $M_{Ed,y}$ (kNm) = 0.55
 Momento sollecitante corrispondente asse X: $M_{Ed,x}$ (kNm) = 0.13
 Sforzo normale corrispondente: $N_{Ed,1}$ (kN) = 104.7
 Taglio sollecitante lungo asse X: $V_{Ed,x}$ (kN) = 110.2
 Taglio sollecitante lungo asse Y: $V_{Ed,y}$ (kN) = 26.8



Rapporto di verifica a pressoflessione: ρ_M =

- SISMA direzione Y

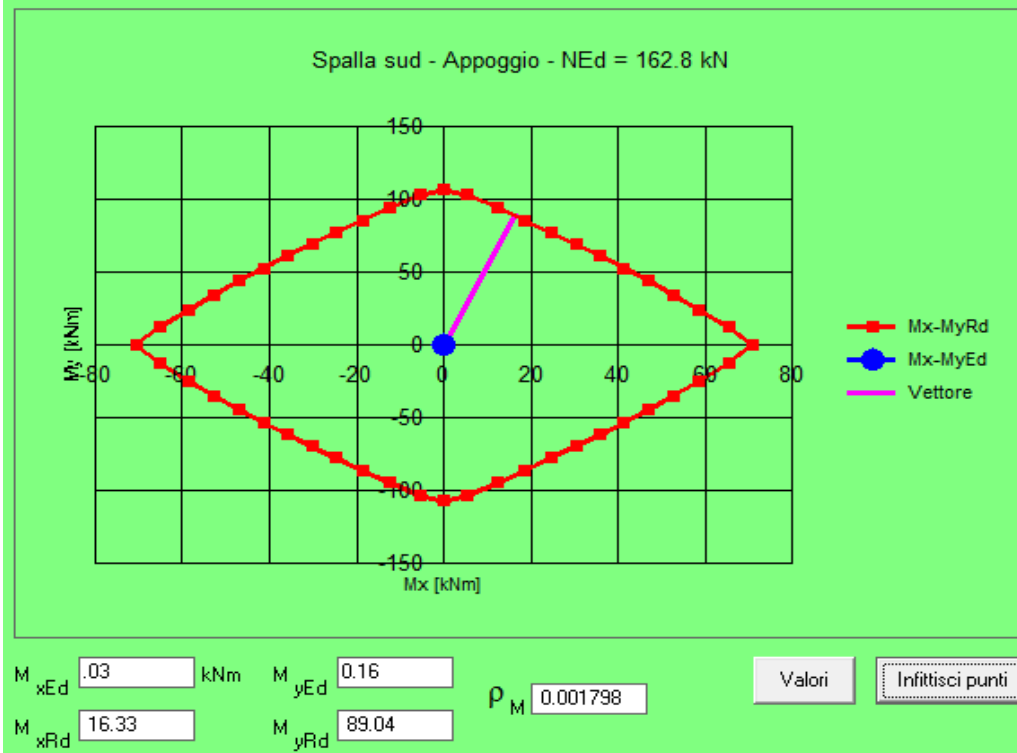
Momento sollecitante massimo asse Y: $M_{Ed,y}$ (kNm) = 0.17
 Momento sollecitante corrispondente asse X: $M_{Ed,x}$ (kNm) = 0.45
 Sforzo normale corrispondente: $N_{Ed,1}$ (kN) = 104.7
 Taglio sollecitante lungo asse X: $V_{Ed,x}$ (kN) = 33.1
 Taglio sollecitante lungo asse Y: $V_{Ed,y}$ (kN) = 89.3



Rapporto di verifica a pressoflessione: $\rho_M =$

- STATICA + VENTO

Momento sollecitante massimo asse Y: $M_{Ed,y}$ (kNm) = 0.16
 Momento sollecitante corrispondente asse X: $M_{Ed,x}$ (kNm) = 0.03
 Sforzo normale corrispondente: $N_{Ed,1}$ (kN) = 162.8
 Taglio sollecitante lungo asse X: $V_{Ed,x}$ (kN) = 32.2
 Taglio sollecitante lungo asse Y: $V_{Ed,y}$ (kN) = 5.8



Rapporto di verifica a pressoflessione: ρ_M = 0.002

Rapporto di verifica massimo: ρ_M = 0.009 < 1.00

Verifica SLU a taglio (Vy-Vz)

Campata sud - spalla sud

- Materiali del dispositivo di appoggio

Classe dell'acciaio:	S355J0
Tensione di rottura: f_{tk} (N/mm ²) =	510
Tensione di snervamento: f_{yk} (N/mm ²) =	355
Coefficiente di sicurezza parziale: γ_s =	1.05
Resistenza di progetto: f_{yd} (N/mm ²) =	338

- Piatti di contenimento dell'appoggio in neoprene

- Geometria del vassoio di contenimento del neoprene

Spessore del piatto di riscontro: t (mm) =	10
Altezza del piatto di riscontro: h (mm) =	35
Lunghezza del piatto di riscontro: l (mm) =	170
Num. di piatti di riscontro per ciascuna direz.: n =	2
Area resistente a taglio: A_v (mm ²) =	3 400
Momento d'inerzia dei piatti: J_s (mm ⁴) =	28 333
Modulo di resistenza dei piatti: W_s (mm ³) =	56 667

- Sollecitazioni

Azione di taglio nei piatti di riscontro: V_s (kN) =	141.9
Momento massimo nei piatti: M (kNm) =	5.0

- Verifica del vassoio di contenimento del neoprene

Tensione normale massima nei piatti: σ_s (N/mm ²) =	88	<	338
Tensione tangenziale max. nei piatti: ρ_s (N/mm ²) =	63	<	195

- Nervature verticali di raccordo sulle travi di impalcato

- Geometria del piatto nervato verticale

Num. di piatti di raccordo (pinne nervate): n =	2	
Altezza del piatto verticale: h (mm) =	100	
Spessore del piatto verticale: t (mm) =	15	
Larghezza del piatto verticale: b (mm) =	260	(base)
Spessore della nervatura: t' (mm) =	8	
Altezza della nervatura: h' (mm) =	100	
Larghezza di base della nervatura: b' (mm) =	65	
Numero di nervature di rinforzo: n' =	2	(per ciascuna pinna verticale)

Area totale della sezione composta: A_s (mm ²) =	9 880
Area resistente a taglio: A_v (mm ²) =	2 080
Posiz. asse neutro della sez. composta: x (mm) =	15.9
Momento d'inerzia del piatto nervato: J_s (cm ⁴) =	350.6
Modulo di resist. del piatto nervato: W_s (cm ³) =	54.7

- Sollecitazioni

Altezza di applicazione dell'azione orizz. H' (mm) =	66.7
Azione di taglio nei piatti di riscontro: V_s (kN) =	141.9
Momento massimo nei piatti: M (kNm) =	9.5

- Verifica del vassoio di contenimento del neoprene

Tensione normale massima nei piatti: σ_s (N/mm ²) =	173	<	338
Tensione tangenziale max. nei piatti: ρ_s (N/mm ²) =	102	<	195

Verifica ancoraggi sulla struttura in c.a.

Trazione massima nei tirafondi: N (kN) =	-10.8 sisma
Taglio massimo nei tirafondi: V (kN) =	141.9 sisma

Trazione massima nei tirafondi: N (kN) =	0.0 statico
Taglio massimo nei tirafondi: V (kN) =	32.7 statico

Le verifiche di resistenza dell'ancoraggio sono svolte nelle pagine seguenti.

VERIFICA DELL'ANCORAGGIO SULLA STRUTTURA IN C.A.

Campata sud - spalla sud

Riferimento del nodo: **Appoggio della trave di impalcato**

Si verifica l'ancoraggio della struttura di base. L'azione massima è trasferita al piatto di base dal tacco di riscontro a taglio interno al dispositivo di appoggio.

Tipo di ancorante		HILTI HIT-HY 200A
Diametro della barra	d	16 mm
Classe acciaio barra		Classe 8.8
Area della barra di ancoraggio	A_b	201.1 mm ²
Numero di barre di ancoraggio	n.	6
Trazione di progetto - SLU	N_{Sd}	0.00 kN
Taglio di progetto - SLU	V_{Sd}	32.70 kN

Si considera un ancoraggio con barra inclinata di un angolo β rispetto alla normale alla superficie di ancoraggio (materiale base).

Angolo di infissione della barra di ancoraggio β 0 °

Componente di trazione di progetto - SLU	N'_{Sd}	0.00 kN
Componente di taglio di progetto - SLU	V'_{Sd}	32.70 kN

Calcolo della trazione resistente

Rottura di progetto lato calcestruzzo (classe C20/25)	$N_{0Rd,c}$	33.2 kN
Profondità nominale di ancoraggio	h_{nom}	120 mm
Profondità effettiva di ancoraggio	h_{act}	200 mm
Fattore di influenza della profondità	f_T	1.667
Resistenza cubica a comp. cls	R_{ck}	14.2 MPa
Fattore di confidenza	FC	1.00
Fattore classe di resistenza	$f_{b,N}$	0.89
Interasse di posa	s	118 mm
Interasse minimo di posa	s_{min}	80 mm
	s / s_{min}	1.48 > 1.0
Fattore interasse di posa	$f_{A,N}$	0.75
Distanza dal bordo	c	80 mm
Distanza minima di posa dai bordi	c_{min}	80 mm
	c / c_{min}	1.00 > 1.0
Fattore distanza dal bordo - sp	$f_{R,N}$	0.76
Cedimento cono cls	$N_{Rd,c}$	28.0 kN
Resistenza a trazione (materiale base - resina)	N_{Rd}	28.0 kN
Resistenza a trazione (lato acciaio)	N_{Rd}	86.9 kN

Calcolo della resistenza a taglio

Rottura di progetto lato calcestruzzo (classe C20/25)	$V_{Rd,c}$	36.7 kN
Fattore classe di resistenza	$f_{b,V}$	0.75
Resistenza a taglio (materiale base)	V_{Rd}	27.6 kN
Resistenza a compressione caratt. materiale base	f_{ck}	11.78 N/mm ²
Spessore della struttura di base	t	1000 mm
Diametro di rottura del cono della soletta	d'	26 mm
Resistenza a taglio (rifollam. materiale base)	V_{Rd}	30.6 kN
Resistenza a taglio (lato acciaio)	V_{Rd}	57.9 kN

Verifiche di resistenza

Resistenza totale a trazione	$N_{Rd,tot}$	167.85 kN
Resistenza totale a taglio	$V_{Rd,tot}$	165.90 kN
verifica di resistenza a trazione		0.00 < 1.0
verifica di resistenza a taglio		0.20 < 1.0
Carico combinato sollecitante	F_{Sd}	32.70 kN
Inclinazione del carico combinato	α	1.57 rad
Capacità di carico combinato	F_{Rd}	165.90 kN
verifica di resistenza a taglio / trazione		0.20 < 1.0

VERIFICA DELL'ANCORAGGIO SULLA STRUTTURA IN C.A.

Campata sud - spalla sud

Riferimento del nodo: **Appoggio della trave di impalcato (condiz. di sollevamento)**

Si verifica l'ancoraggio della struttura di base. L'azione massima è trasferita al piatto di base dal tacco di riscontro a taglio interno al dispositivo di appoggio.

Tipo di ancorante		HILTI HIT-HY 200A
Diametro della barra	d	16 mm
Classe acciaio barra		Classe 8.8
Area della barra di ancoraggio	A_b	201.1 mm ²
Numero di barre di ancoraggio	n.	6
Trazione di progetto - SLU	N_{Sd}	10.84 kN
Taglio di progetto - SLU	V_{Sd}	141.89 kN

Si considera un ancoraggio con barra inclinata di un angolo β rispetto alla normale alla superficie di ancoraggio (materiale base).

Angolo di infissione della barra di ancoraggio β 0 °

Componente di trazione di progetto - SLU	N'_{Sd}	10.84 kN
Componente di taglio di progetto - SLU	V'_{Sd}	141.89 kN

Calcolo della trazione resistente

Rottura di progetto lato calcestruzzo (classe C20/25)	$N_{0Rd,c}$	33.2 kN
Profondità nominale di ancoraggio	h_{nom}	120 mm
Profondità effettiva di ancoraggio	h_{act}	200 mm
Fattore di influenza della profondità	f_T	1.667
Resistenza cubica a comp. cls	R_{ck}	14.19 MPa
Fattore di confidenza	FC	1.00
Fattore classe di resistenza	$f_{b,N}$	0.89
Interasse di posa	s	118 mm
Interasse minimo di posa	s_{min}	80 mm
	s / s_{min}	1.48 > 1.0
Fattore interasse di posa	$f_{A,N}$	0.75
Distanza dal bordo	c	80 mm
Distanza minima di posa dai bordi	c_{min}	80 mm
	c / c_{min}	1.00 > 1.0
Fattore distanza dal bordo - sp	$f_{R,N}$	0.76
Cedimento cono cls	$N_{Rd,c}$	28.0 kN
Resistenza a trazione (materiale base - resina)	N_{Rd}	28.0 kN
Resistenza a trazione (lato acciaio)	N_{Rd}	86.9 kN

Calcolo della resistenza a taglio

Rottura di progetto lato calcestruzzo (classe C20/25)	$V_{Rd,c}$	36.7 kN
Fattore classe di resistenza	$f_{b,V}$	0.75
Resistenza a taglio (materiale base)	V_{Rd}	27.6 kN
Resistenza a compressione caratt. materiale base	f_{ck}	11.78 N/mm ²
Spessore della struttura di base	t	1000 mm
Diametro di rottura del cono della soletta	d'	26 mm
Resistenza a taglio (rifollam. materiale base)	V_{Rd}	30.6 kN
Resistenza a taglio (lato acciaio)	V_{Rd}	57.9 kN

Verifiche di resistenza

Resistenza totale a trazione	$N_{Rd,tot}$	167.85 kN
Resistenza totale a taglio	$V_{Rd,tot}$	165.90 kN
verifica di resistenza a trazione		0.06 < 1.0
verifica di resistenza a taglio		0.86 < 1.0
Carico combinato sollecitante	F_{Sd}	142.30 kN
Inclinazione del carico combinato	α	1.49 rad
Capacità di carico combinato	F_{Rd}	164.12 kN
verifica di resistenza a taglio / trazione		0.87 < 1.0

APPOGGI TRAVI DI IMPALCATO

Campata sud - spalla sud

Appoggio su struttura in c.a. - Verifica SLU a presso-flessione

Caratteristiche dei materiali

- Calcestruzzo

Classe calcestruzzo della struttura di base: R_{ck} (N/mm ²) =	14.2	Carota	C2
Resistenza cilindrica caratteristica del materiale base: f_{ck} (N/mm ²) =	11.8		
Resistenza a taglio caratteristica del materiale base: f_{ctk} (N/mm ²) =	1.09		
Coefficiente di sicurezza parziale del materiale: γ_c =	1.50		
Fattore di confidenza: FC =	1.00	<i>(struttura esistente con prova diretta su campione)</i>	
Resist. a compressione di progetto del materiale base: f_{cd} (N/mm ²) =	6.67		
Resistenza a taglio di progetto del materiale base: f_{ctd} (N/mm ²) =	0.72		

- Barre in acciaio

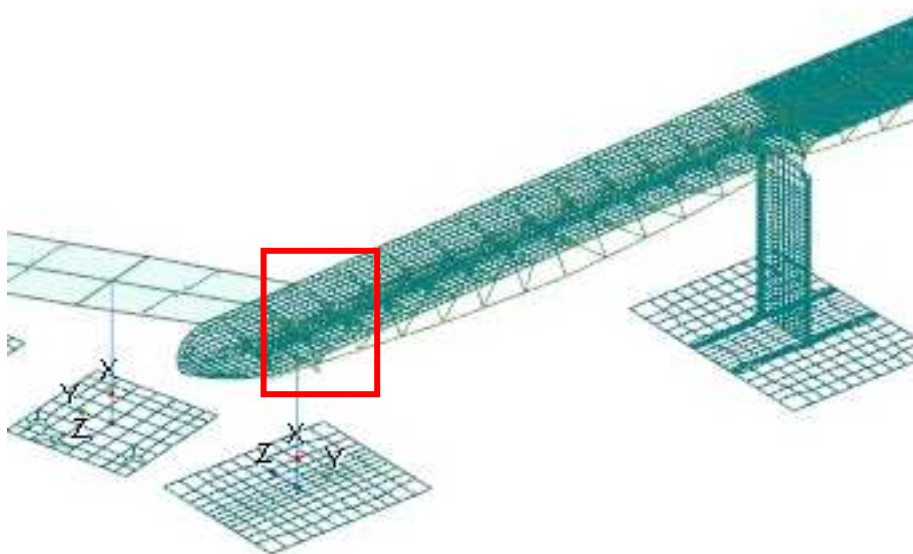
Acciaio a snervamento: f_{yk} (MPa) =	469	Spezz.	1
Acciaio a rottura: f_{tk} (MPa) =	674		

Si assumono i valori di un acciaio FeB44k

Resistenza a rottura caratteristica delle barre: f_{tk} (N/mm ²) =	674	FeB44k	
Resistenza a snervamento caratteristica delle barre: f_{yk} (N/mm ²) =	469		
Coefficiente parziale di sicurezza del materiale: γ_M =	1.15		
Fattore di confidenza: FC =	1.00	<i>(struttura esistente con prova diretta su campione)</i>	
Resistenza a trazione di progetto delle barre di nodo: $f_{s,yd}$ (N/mm ²) =	407.8		

- Materiali dell'ancoraggio

		f_{yk} (N/mm ²) =	640
Classe dell'acciaio:	cl. 8.8	f_{yd} (N/mm ²) =	512
Tensione di rottura: f_{tk} (N/mm ²) =	800	Coeffic. sicur. parziale: γ_s =	1.25



Posizione dell'appoggio sulla struttura in c.a.

Verifica a pressoflessione dell'appoggio

Definizione della sezione resistente e delle sollecitazioni.

Titolo : Spalla sud - Appoggio

N° Vertici **Zoom** **N° barre** **Zoom**

N°	x [cm]	y [cm]
1	0	0
2	0	30
3	33	30
4	33	0

N°	As [cm²]	x [cm]	y [cm]
2	2.01	3.2	26.8
3	2.01	3.2	15
4	2.01	29.8	3.2
5	2.01	29.8	26.8
6	2.01	29.8	15

Tipo Sezione
 Rettan.re Trapezi
 a T Circolare
 Rettangoli Coord.

Sollecitazioni
 S.L.U. Metodo n

N_{Ed} kN
M_{xEd} kNm
M_{yEd}

P.to applicazione N
 Centro Baricentro cls
 Coord.[cm] xN yN

Tipo rottura
 Lato calcestruzzo - Acciaio snervato

Metodo di calcolo
 S.L.U.+ S.L.U.-
 Metodo n

Tipo flessione
 Retta Deviata

N* rett.
Calcola MRd **Dominio Mx-My**

angolo asse neutro θ°

Precompresso

Materiali
 cl. 8.8 Carota 2
 ϵ_{su} ‰ ϵ_{c2} ‰
 f_{yd} N/mm² ϵ_{cu} ‰
 E_s N/mm² f_{cd} ‰
 E_s/E_c f_{cc}/f_{cd} ?
 ϵ_{syd} ‰ $\sigma_{c,adm}$
 $\sigma_{s,adm}$ N/mm² τ_{co}
 τ_{c1}

M_{xRd} kN m
M_{yRd} kN m
 σ_c N/mm²
 σ_s N/mm²
 ϵ_c ‰
 ϵ_s ‰
 d cm
 x x/d
 δ

Si considera l'altezza del tacco di riscontro (piano di trasferimento dell'azione sollecitante) dalla sezione di verifica del collegamento sul calcestruzzo di base.

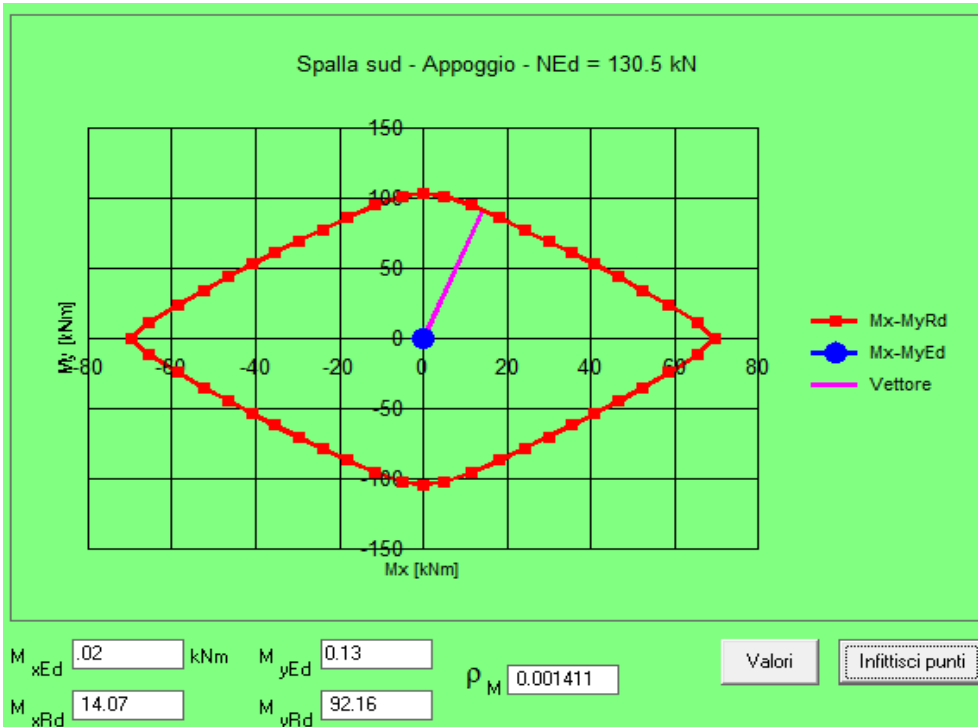
Altezza del dispositivo di appoggio: h' (cm) =

5.0

Sollecitazioni e verifiche

- SISMA direzione X

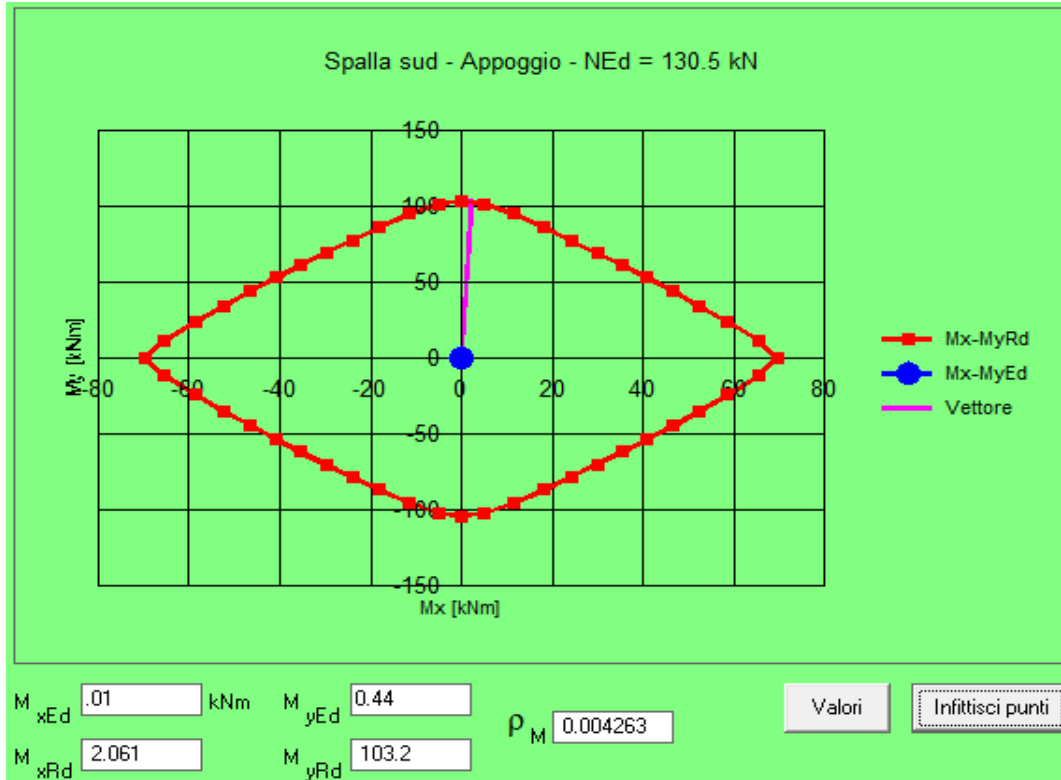
Momento sollecitante massimo asse Y: $M_{Ed,y}$ (kNm) =	0.02
Momento sollecitante corrispondente asse X: $M_{Ed,x}$ (kNm) =	0.13
Sforzo normale corrispondente: $N_{Ed,1}$ (kN) =	130.5
Taglio sollecitante lungo asse X: $V_{Ed,x}$ (kN) =	3.6
Taglio sollecitante lungo asse Y: $V_{Ed,y}$ (kN) =	26.5



Rapporto di verifica a pressoflessione: $\rho_M =$ 0.001

- SISMA direzione Y

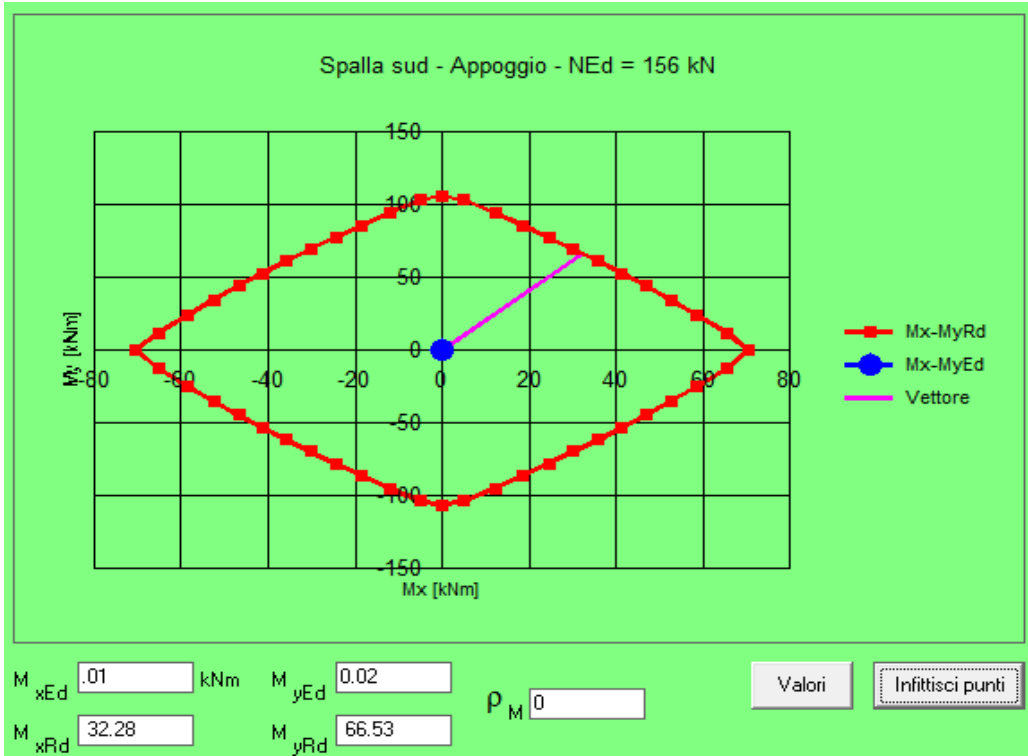
Momento sollecitante massimo asse Y: $M_{Ed,y}$ (kNm) =	0.01
Momento sollecitante corrispondente asse X: $M_{Ed,x}$ (kNm) =	0.44
Sforzo normale corrispondente: $N_{Ed,1}$ (kN) =	130.5
Taglio sollecitante lungo asse X: $V_{Ed,x}$ (kN) =	1.1
Taglio sollecitante lungo asse Y: $V_{Ed,y}$ (kN) =	88.4



Rapporto di verifica a pressoflessione: $\rho_M =$ 0.004

- STATICA + VENTO

Momento sollecitante massimo asse Y: $M_{Ed,y}$ (kNm) = 0.01
 Momento sollecitante corrispondente asse X: $M_{Ed,x}$ (kNm) = 0.02
 Sforzo normale corrispondente: $N_{Ed,1}$ (kN) = 156.0
 Taglio sollecitante lungo asse X: $V_{Ed,x}$ (kN) = 2.6
 Taglio sollecitante lungo asse Y: $V_{Ed,y}$ (kN) = 4.9



Rapporto di verifica a pressoflessione: $\rho_M =$ 0.002

Rapporto di verifica massimo: $\rho_M =$ 0.004 < 1.00

Verifica SLU a taglio (Vy-Vz)

Campata sud - spalla sud

- Materiali del dispositivo di appoggio

Classe dell'acciaio:	S355J0
Tensione di rottura: f_{tk} (N/mm ²) =	510
Tensione di snervamento: f_{yk} (N/mm ²) =	355
Coefficiente di sicurezza parziale: γ_s =	1.05
Resistenza di progetto: f_{yd} (N/mm ²) =	338

- Piatti di contenimento dell'appoggio in neoprene

- Geometria del vassoio di contenimento del neoprene

Spessore del piatto di riscontro: t (mm) =	10
Altezza del piatto di riscontro: h (mm) =	35
Lunghezza del piatto di riscontro: l (mm) =	170
Num. di piatti di riscontro per ciascuna direz.: n =	2
Area resistente a taglio: A_v (mm ²) =	3 400
Momento d'inerzia dei piatti: J_s (mm ⁴) =	28 333
Modulo di resistenza dei piatti: W_s (mm ³) =	56 667

- Sollecitazioni

Azione di taglio nei piatti di riscontro: V_s (kN) =	88.4
Momento massimo nei piatti: M (kNm) =	3.1

- Verifica del vassoio di contenimento del neoprene

Tensione normale massima nei piatti: σ_s (N/mm ²) =	55	<	338
Tensione tangenziale max. nei piatti: ρ_s (N/mm ²) =	39	<	195

- Nervature verticali di raccordo sulle travi di impalcato

- Geometria del piatto nervato verticale

Num. di piatti di raccordo (pinne nervate): n =	2	
Altezza del piatto verticale: h (mm) =	100	
Spessore del piatto verticale: t (mm) =	15	
Larghezza del piatto verticale: b (mm) =	260	(base)
Spessore della nervatura: t' (mm) =	8	
Altezza della nervatura: h' (mm) =	100	
Larghezza di base della nervatura: b' (mm) =	65	
Numero di nervature di rinforzo: n' =	2	(per ciascuna pinna verticale)

Area totale della sezione composta: A_s (mm ²) =	9 880
Area resistente a taglio: A_v (mm ²) =	2 080
Posiz. asse neutro della sez. composta: x (mm) =	15.9
Momento d'inerzia del piatto nervato: J_s (cm ⁴) =	350.6
Modulo di resist. del piatto nervato: W_s (cm ³) =	54.7

- Sollecitazioni

Altezza di applicazione dell'azione orizz. H' (mm) =	66.7
Azione di taglio nei piatti di riscontro: V_s (kN) =	88.4
Momento massimo nei piatti: M (kNm) =	5.9

- Verifica del vassoio di contenimento del neoprene

Tensione normale massima nei piatti: σ_s (N/mm ²) =	108	<	338
Tensione tangenziale max. nei piatti: ρ_s (N/mm ²) =	64	<	195

Verifica ancoraggi sulla struttura in c.a.

Trazione massima nei tirafondi: N (kN) =	-34.6 sisma
Taglio massimo nei tirafondi: V (kN) =	88.4 sisma
Trazione massima nei tirafondi: N (kN) =	0.0 statico
Taglio massimo nei tirafondi: V (kN) =	5.6 statico

Le verifiche di resistenza dell'ancoraggio sono svolte nelle pagine seguenti.

VERIFICA DELL'ANCORAGGIO SULLA STRUTTURA IN C.A.

Campata sud - spalla sud

Riferimento del nodo: **Appoggio della trave di impalcato**

Si verifica l'ancoraggio della struttura di base. L'azione massima è trasferita al piatto di base dal tacco di riscontro a taglio interno al dispositivo di appoggio.

Tipo di ancorante		HILTI HIT-HY 200A
Diametro della barra	d	16 mm
Classe acciaio barra		Classe 8.8
Area della barra di ancoraggio	A_b	201.1 mm ²
Numero di barre di ancoraggio	n.	6
Trazione di progetto - SLU	N_{Sd}	0.00 kN
Taglio di progetto - SLU	V_{Sd}	5.55 kN

Si considera un ancoraggio con barra inclinata di un angolo β rispetto alla normale alla superficie di ancoraggio (materiale base).

Angolo di infissione della barra di ancoraggio β 0 °

Componente di trazione di progetto - SLU	N'_{Sd}	0.00 kN
Componente di taglio di progetto - SLU	V'_{Sd}	5.55 kN

Calcolo della trazione resistente

Rottura di progetto lato calcestruzzo (classe C20/25)	$N_{0Rd,c}$	33.2 kN
Profondità nominale di ancoraggio	h_{nom}	120 mm
Profondità effettiva di ancoraggio	h_{act}	200 mm
Fattore di influenza della profondità	f_T	1.667
Resistenza cubica a comp. cls	R_{ck}	14.2 MPa
Fattore di confidenza	FC	1.00
Fattore classe di resistenza	$f_{b,N}$	0.89
Interasse di posa	s	118 mm
Interasse minimo di posa	s_{min}	80 mm
	s / s_{min}	1.48 > 1.0
Fattore interasse di posa	$f_{A,N}$	0.75
Distanza dal bordo	c	80 mm
Distanza minima di posa dai bordi	c_{min}	80 mm
	c / c_{min}	1.00 > 1.0
Fattore distanza dal bordo - sp	$f_{R,N}$	0.76
Cedimento cono cls	$N_{Rd,c}$	28.0 kN
Resistenza a trazione (materiale base - resina)	N_{Rd}	28.0 kN
Resistenza a trazione (lato acciaio)	N_{Rd}	86.9 kN

Calcolo della resistenza a taglio

Rottura di progetto lato calcestruzzo (classe C20/25)	$V_{Rd,c}$	36.7 kN
Fattore classe di resistenza	$f_{b,V}$	0.75
Resistenza a taglio (materiale base)	V_{Rd}	27.6 kN
Resistenza a compressione caratt. materiale base	f_{ck}	11.78 N/mm ²
Spessore della struttura di base	t	1000 mm
Diametro di rottura del cono della soletta	d'	26 mm
Resistenza a taglio (rifollam. materiale base)	V_{Rd}	30.6 kN
Resistenza a taglio (lato acciaio)	V_{Rd}	57.9 kN

Verifiche di resistenza

Resistenza totale a trazione	$N_{Rd,tot}$	167.85 kN
Resistenza totale a taglio	$V_{Rd,tot}$	165.90 kN
verifica di resistenza a trazione		0.00 < 1.0
verifica di resistenza a taglio		0.03 < 1.0
Carico combinato sollecitante	F_{Sd}	5.55 kN
Inclinazione del carico combinato	α	1.57 rad
Capacità di carico combinato	F_{Rd}	165.90 kN
verifica di resistenza a taglio / trazione		0.03 < 1.0

VERIFICA DELL'ANCORAGGIO SULLA STRUTTURA IN C.A.

Campata sud - spalla sud

Riferimento del nodo: **Appoggio della trave di impalcato (condiz. di sollevamento)**

Si verifica l'ancoraggio della struttura di base. L'azione massima è trasferita al piatto di base dal tacco di riscontro a taglio interno al dispositivo di appoggio.

Tipo di ancorante		HILTI HIT-HY 200A
Diametro della barra	d	16 mm
Classe acciaio barra		Classe 8.8
Area della barra di ancoraggio	A_b	201.1 mm ²
Numero di barre di ancoraggio	n.	6
Trazione di progetto - SLU	N_{Sd}	34.62 kN
Taglio di progetto - SLU	V_{Sd}	88.44 kN

Si considera un ancoraggio con barra inclinata di un angolo β rispetto alla normale alla superficie di ancoraggio (materiale base).

Angolo di infissione della barra di ancoraggio β 0 °

Componente di trazione di progetto - SLU	N'_{Sd}	34.62 kN
Componente di taglio di progetto - SLU	V'_{Sd}	88.44 kN

Calcolo della trazione resistente

Rottura di progetto lato calcestruzzo (classe C20/25)	$N_{0Rd,c}$	33.2 kN
Profondità nominale di ancoraggio	h_{nom}	120 mm
Profondità effettiva di ancoraggio	h_{act}	200 mm
Fattore di influenza della profondità	f_T	1.667
Resistenza cubica a comp. cls	R_{ck}	14.19 MPa
Fattore di confidenza	FC	1.00
Fattore classe di resistenza	$f_{b,N}$	0.89
Interasse di posa	s	118 mm
Interasse minimo di posa	s_{min}	80 mm
	s / s_{min}	1.48 > 1.0
Fattore interasse di posa	$f_{A,N}$	0.75
Distanza dal bordo	c	80 mm
Distanza minima di posa dai bordi	c_{min}	80 mm
	c / c_{min}	1.00 > 1.0
Fattore distanza dal bordo - sp	$f_{R,N}$	0.76
Cedimento cono cls	$N_{Rd,c}$	28.0 kN
Resistenza a trazione (materiale base - resina)	N_{Rd}	28.0 kN
Resistenza a trazione (lato acciaio)	N_{Rd}	86.9 kN

Calcolo della resistenza a taglio

Rottura di progetto lato calcestruzzo (classe C20/25)	$V_{Rd,c}$	36.7 kN
Fattore classe di resistenza	$f_{b,V}$	0.75
Resistenza a taglio (materiale base)	V_{Rd}	27.6 kN
Resistenza a compressione caratt. materiale base	f_{ck}	11.78 N/mm ²
Spessore della struttura di base	t	1000 mm
Diametro di rottura del cono della soletta	d'	26 mm
Resistenza a taglio (rifollam. materiale base)	V_{Rd}	30.6 kN
Resistenza a taglio (lato acciaio)	V_{Rd}	57.9 kN

Verifiche di resistenza

Resistenza totale a trazione	$N_{Rd,tot}$	167.85 kN
Resistenza totale a taglio	$V_{Rd,tot}$	165.90 kN
verifica di resistenza a trazione		0.21 < 1.0
verifica di resistenza a taglio		0.53 < 1.0
Carico combinato sollecitante	F_{Sd}	94.98 kN
Inclinazione del carico combinato	α	1.20 rad
Capacità di carico combinato	F_{Rd}	154.30 kN
verifica di resistenza a taglio / trazione		0.62 < 1.0

Apparecchi d'appoggio - Neoprene

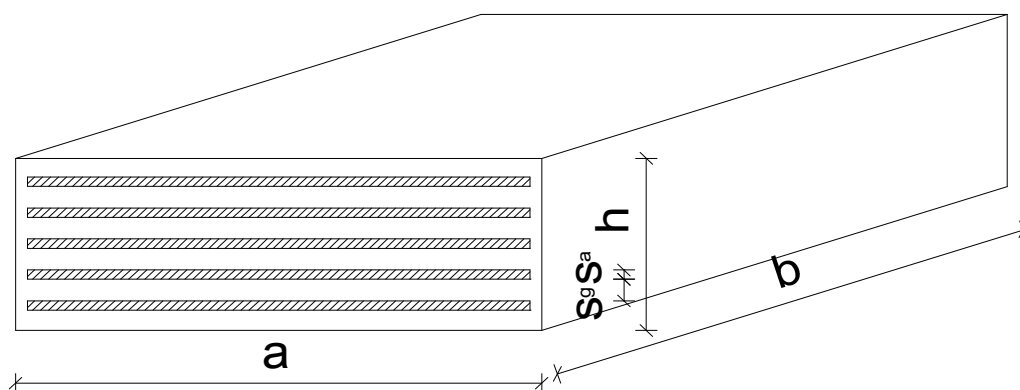
Appoggio dell'impalcato Campata sud - spalla sud

Sollecitazioni di progetto - Appoggio tipo

Condizioni di esercizio - SLE

Forza verticale totale: F_z (kg) =	4 794
Forza verticale per carichi permanenti: F_z (p) (kg) =	2 397
Forza verticale per azioni di breve durata (variabili): F_z (q) (kg) =	2 397
Forza orizzontale totale: F_{xy} (kg) =	40
Forza orizzontale per carichi permanenti: F_{xy} (p) (kg) =	18
Forza orizzontale per carichi di breve durata (variabili): F_{xy} (q) (kg) =	22
	$\Psi_{2j} =$ 0.60

Si assume che le azioni orizzontali per sisma e vento siano assorbite dai ritegni in acciaio.



Caratteristiche geometriche dell'appoggio

Lato trasversale appoggio: a (cm) =	18
Lato longitudinale appoggio: b (cm) =	18
Spessore singolo strato di gomma: s_g (cm) =	2.0
Numero di strati di gomma interni ai lamierini: n_g =	1
Spessore strato di gomma esterno: s_e (cm) =	0
Spessore totale della gomma interna ai lamierini: h_g (cm) =	2
Numero di lamierini di armatura in acciaio: n_a =	0
Spessore singolo lamierino: s_a (cm) =	0

Spessore totale dell'appoggio: h (cm) =	2
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Caratteristiche della gomma, per durezza 60 gradi Shore A3:

Modulo di elasticità tangenziale della gomma: G (kg/cm ²) (= E/3) =	9.0
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Area di appoggio: A_c (cm ²) =	324.0
Area di appoggio ridotta: A_r (cm ²) =	323.8
Coefficiente di forma: $S = \mu$ =	2.250

Tensioni e deformazioni nell'appoggio

Tensione tangenziale prodotta da F_{xy} (p) e F_{xy} (q): τ_H (kg/cm ²) =	0.06
Scorrimento elastico dovuto a F_{xy} (p) e F_{xy} (q): $\tan \gamma$ =	0.01
Spostamento orizzontale elastico longitudinale: u_a (cm) =	0.012
Spostamento orizzontale elastico trasversale: u_b (cm) =	0
Tensione normale prodotta dal carico F_z : σ_V (kg/cm ²) =	14.81
Tensione normale prodotta dal carico permanente F_z (p): σ_V' (kg/cm ²) =	7.40
Tensione tangenziale prodotta da F_z : τ_V (kg/cm ²) =	9.87
Rotaz. all'app. in direz. y (nel piano della strutt.) - Cond. statiche: α (rad) =	0.00602
Rotaz. all'appoggio in direz. x (fuori dal piano della struttura): α_x (rad) =	0.00005
Tensione tangenziale prodotta dalla rotazione α : $\tau_{\alpha y}$ (kg/cm ²) =	2.19
Rotaz. all'app. in direz. y (nel piano della strutt.) - Cond. sismiche: α (rad) =	0.00551
Rotaz. all'appoggio in direz. x (fuori dal piano della struttura): α_x (rad) =	0.00005
Tensione tangenziale prodotta dalla rotazione α : $\tau_{\alpha y}$ (kg/cm ²) =	2.01
Accorciamento elastico dell'appoggio dovuto a F_z : Δh (cm) =	0.0659

Verifiche appoggio elastomerico non armato

Verifiche di resistenza

σ_V (kg/cm ²) =	14.81	<	24.3	kg/cm ²
σ_V' (kg/cm ²) =	7.40	<	50.0	kg/cm ²
$\sigma_{V''}$ (kg/cm ²) =	7.40	<	24.3	kg/cm ²
Cond. statiche: Δh (cm) =	0.0659	>	$(a/2) \tan \alpha =$	0.0546 cm
Cond. sism: Δh (cm) =	0.0659	>	$(a/6) \tan \alpha =$	0.0167 cm

Verifiche di stabilità

h (cm) =	2.00	<	$a / 5 =$	3.60 cm
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APPOGGI TRAVI DI IMPALCATO

Campata sud - pila

Appoggio su struttura in c.a. - Verifica SLU a presso-flessione

Caratteristiche dei materiali

- Calcestruzzo

Classe calcestruzzo della struttura di base: R_{ck} (N/mm ²) =	29.3	Carota	C4
Resistenza cilindrica caratteristica del materiale base: f_{ck} (N/mm ²) =	24.3		
Resistenza a taglio caratteristica del materiale base: f_{ctk} (N/mm ²) =	1.76		
Coefficiente di sicurezza parziale del materiale: γ_c =	1.50		
Fattore di confidenza: FC =	1.20		
Resist. a compressione di progetto del materiale base: f_{cd} (N/mm ²) =	11.48		
Resistenza a taglio di progetto del materiale base: f_{ctd} (N/mm ²) =	0.98		

- Barre in acciaio

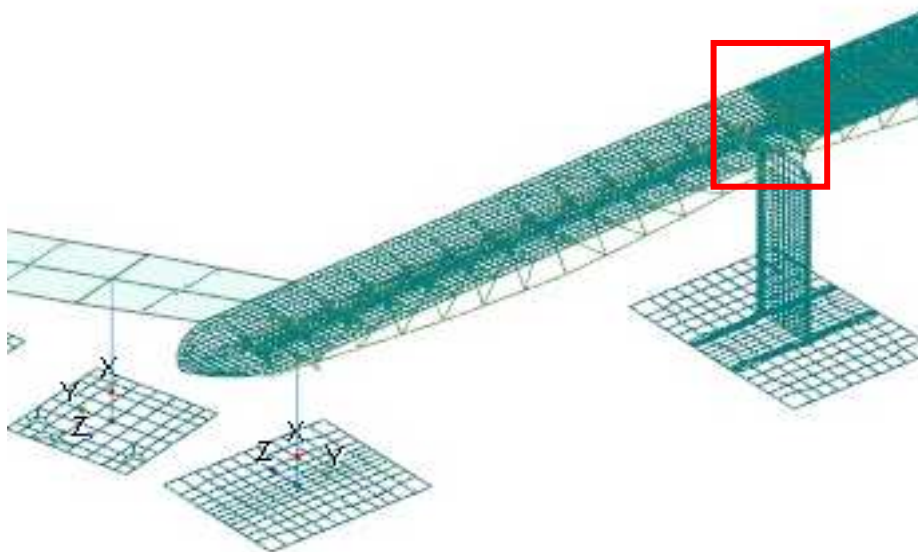
Acciaio a snervamento: f_{yk} (MPa) =	460	Spezz.	2
Acciaio a rottura: f_{tk} (MPa) =	681		

Si assumono i valori di un acciaio FeB44k

Resistenza a rottura caratteristica delle barre: f_{tk} (N/mm ²) =	681	FeB44k
Resistenza a snervamento caratteristica delle barre: f_{yk} (N/mm ²) =	460	
Coefficiente parziale di sicurezza del materiale: γ_M =	1.15	
Fattore di confidenza: FC =	1.00	
Resistenza a trazione di progetto delle barre di nodo: $f_{s,yd}$ (N/mm ²) =	400.0	

- Materiali dell'ancoraggio

	f_{yk} (N/mm ²) =	640
Classe dell'acciaio:	f_{yd} (N/mm ²) =	512
Tensione di rottura: f_{tk} (N/mm ²) =	800	
	Coeff. sicur. parziale: γ_s =	1.25



Posizione dell'appoggio sulla struttura in c.a.

Verifica a pressoflessione dell'appoggio

Definizione della sezione resistente e delle sollecitazioni.

Titolo : Pila sud - Appoggio

N° Vertici **Zoom** **N° barre** **Zoom**

N°	x [cm]	y [cm]
1	0	0
2	0	31
3	31	31
4	31	0

N°	As [cm²]	x [cm]	y [cm]
1	2.01	4	3.2
2	2.01	4	27.8
3	2.01	4	15.5
4	2.01	27	3.2
5	2.01	27	27.8
6	2.01	27	15.5

Sollecitazioni
 S.L.U. Metodo n

N_{Ed} kN
M_{xEd} kNm
M_{yEd}

P.to applicazione N
 Centro Baricentro cls
 Coord.[cm] xN yN

Tipo rottura
 Lato calcestruzzo - Acciaio snervato

Metodo di calcolo
 S.L.U.+ S.L.U.-
 Metodo n

Tipo flessione
 Retta Deviata

N° rett.

angolo asse neutro θ°
 Precompresso

Materiali

 ϵ_{su} ‰ ϵ_{c2} ‰
 f_{yd} N/mm² ϵ_{cu} ‰
 E_s N/mm² f_{cd} ‰
 E_s/E_c f_{cc}/f_{cd} ?
 ϵ_{syd} ‰ $\sigma_{c,adm}$ ‰
 $\sigma_{s,adm}$ N/mm² τ_{co}
 τ_{c1}

M_{xRd} kN m
M_{yRd} kN m
 σ_c N/mm²
 σ_s N/mm²
 ϵ_c ‰
 ϵ_s ‰
d cm
x **x/d**
 δ

Si considera l'altezza del tacco di riscontro (piano di trasferimento dell'azione sollecitante) dalla sezione di verifica del collegamento sul calcestruzzo di base.

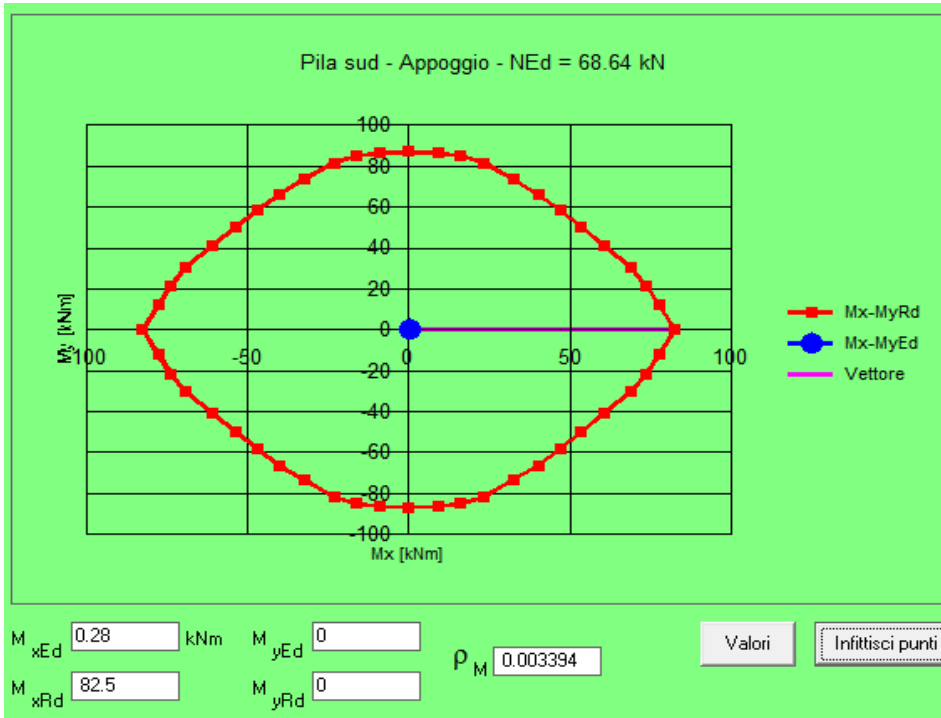
Altezza del dispositivo di appoggio: h' (cm) =

5.0

Sollecitazioni e verifiche

- SISMA direzione X

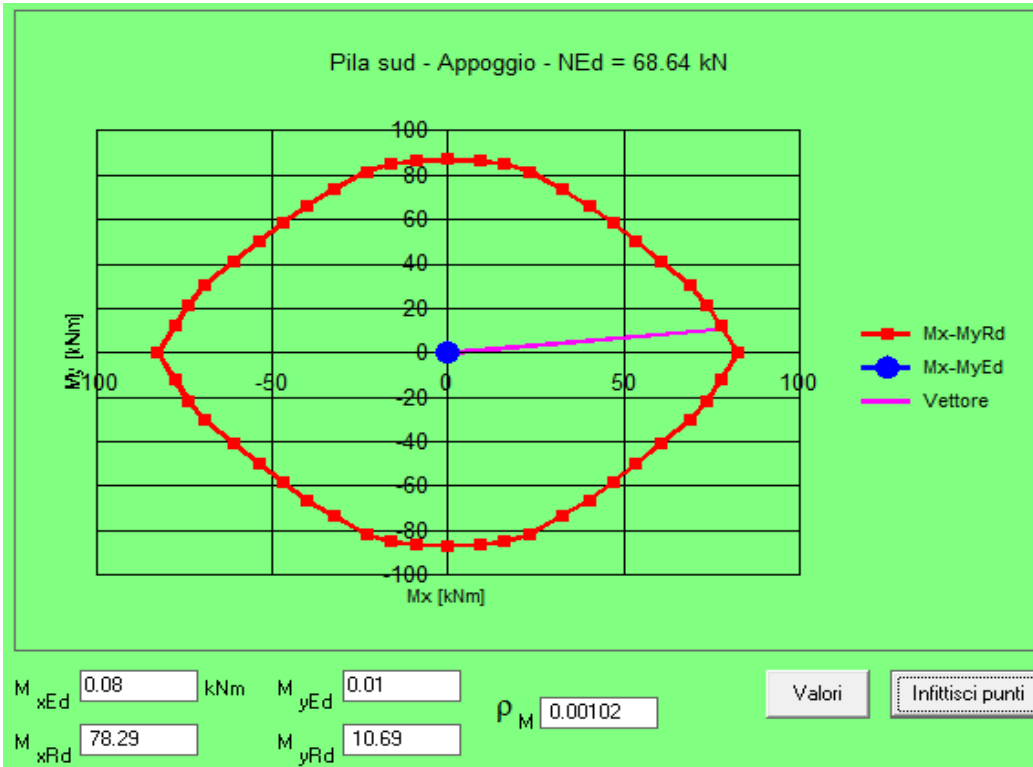
Momento sollecitante massimo asse Y: $M_{Ed,y}$ (kNm) =	0.28
Momento sollecitante corrispondente asse X: $M_{Ed,x}$ (kNm) =	0.00
Sforzo normale corrispondente: $N_{Ed,1}$ (kN) =	68.6
Taglio sollecitante lungo asse X: $V_{Ed,x}$ (kN) =	56.3
Taglio sollecitante lungo asse Y: $V_{Ed,y}$ (kN) =	0.3



Rapporto di verifica a pressoflessione: $\rho_M =$

- SISMA direzione Y

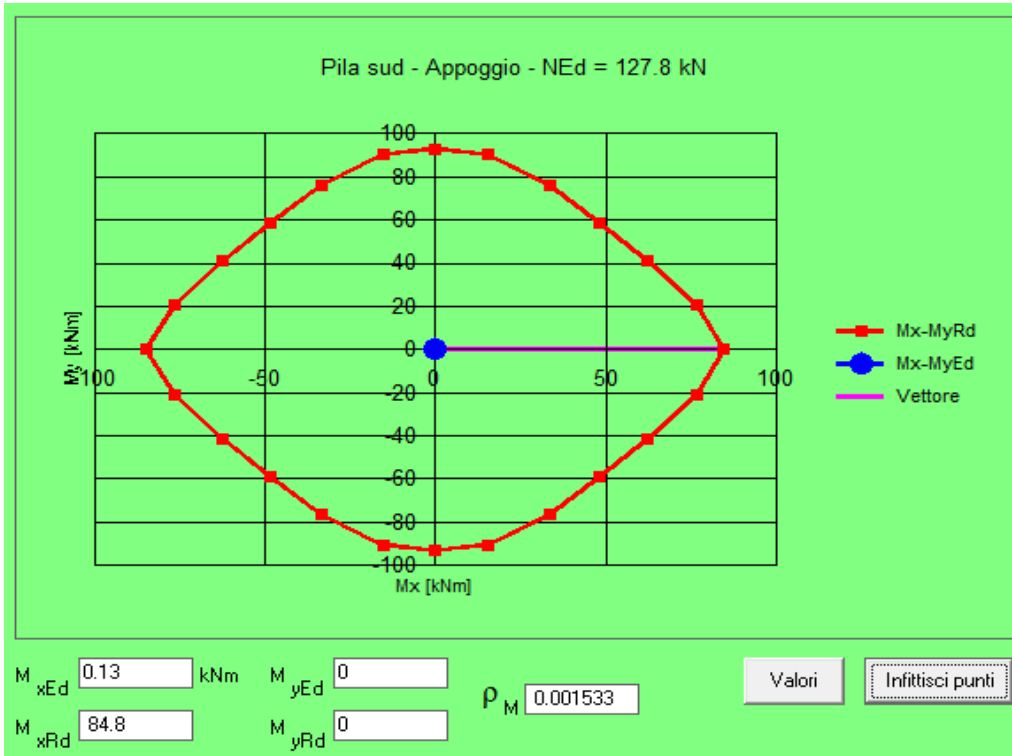
Momento sollecitante massimo asse Y: $M_{Ed,y}$ (kNm) = 0.08
 Momento sollecitante corrispondente asse X: $M_{Ed,x}$ (kNm) = 0.01
 Sforzo normale corrispondente: $N_{Ed,1}$ (kN) = 68.6
 Taglio sollecitante lungo asse X: $V_{Ed,x}$ (kN) = 16.9
 Taglio sollecitante lungo asse Y: $V_{Ed,y}$ (kN) = 1.1



Rapporto di verifica a pressoflessione: ρ_M =

- STATICA + VENTO

Momento sollecitante massimo asse Y: $M_{Ed,y}$ (kNm) = 0.13
 Momento sollecitante corrispondente asse X: $M_{Ed,x}$ (kNm) = 0.00
 Sforzo normale corrispondente: $N_{Ed,1}$ (kN) = 127.8
 Taglio sollecitante lungo asse X: $V_{Ed,x}$ (kN) = 26.4
 Taglio sollecitante lungo asse Y: $V_{Ed,y}$ (kN) = 0.7



Rapporto di verifica a pressoflessione: ρ_M = 0.002

Rapporto di verifica massimo: ρ_M = 0.003 < 1.00

Verifica SLU a taglio (Vy-Vz)

Campata sud - pila

- Materiali del dispositivo di appoggio

Classe dell'acciaio:	S355J0
Tensione di rottura: f_{tk} (N/mm ²) =	510
Tensione di snervamento: f_{yk} (N/mm ²) =	355
Coefficiente di sicurezza parziale: γ_s =	1.05
Resistenza di progetto: f_{yd} (N/mm ²) =	338

- Piatti di contenimento dell'appoggio in neoprene

- Geometria del vassoio di contenimento del neoprene

Spessore del piatto di riscontro: t (mm) =	10
Altezza del piatto di riscontro: h (mm) =	35
Lunghezza del piatto di riscontro: l (mm) =	170
Num. di piatti di riscontro per ciascuna direz.: n =	2
Area resistente a taglio: A_v (mm ²) =	3 400
Momento d'inerzia dei piatti: J_s (mm ⁴) =	28 333
Modulo di resistenza dei piatti: W_s (mm ³) =	56 667

- Sollecitazioni

Azione di taglio nei piatti di riscontro: V_s (kN) =	56.3
Momento massimo nei piatti: M (kNm) =	2.0

- Verifica del vassoio di contenimento del neoprene

Tensione normale massima nei piatti: σ_s (N/mm ²) =	35	<	338
Tensione tangenziale max. nei piatti: ρ_s (N/mm ²) =	25	<	195

- Nervature verticali di raccordo sulle travi di impalcato

- Geometria del piatto nervato verticale

Num. di piatti di raccordo (pinne nervate): n =	2	
Altezza del piatto verticale: h (mm) =	220	
Spessore del piatto verticale: t (mm) =	20	
Larghezza del piatto verticale: b (mm) =	270	(base)
Spessore della nervatura: t' (mm) =	8	
Altezza della nervatura: h' (mm) =	220	
Larghezza di base della nervatura: b' (mm) =	60	
Numero di nervature di rinforzo: n' =	2	(per ciascuna pinna verticale)

Area totale della sezione composta: A_s (mm ²) =	12 720
Area resistente a taglio: A_v (mm ²) =	1 920
Posiz. asse neutro della sez. composta: x (mm) =	16.0
Momento d'inerzia del piatto nervato: J_s (cm ⁴) =	354.4
Modulo di resist. del piatto nervato: W_s (cm ³) =	55.4

- Sollecitazioni

Altezza di applicazione dell'azione orizz. H' (mm) =	146.7
Azione di taglio nei piatti di riscontro: V_s (kN) =	56.3
Momento massimo nei piatti: M (kNm) =	8.3

- Verifica del vassoio di contenimento del neoprene

Tensione normale massima nei piatti: σ_s (N/mm ²) =	149	<	338
Tensione tangenziale max. nei piatti: ρ_s (N/mm ²) =	44	<	195

Verifica ancoraggi sulla struttura in c.a.

Trazione massima nei tirafondi: N (kN) =	3.4 sisma
Taglio massimo nei tirafondi: V (kN) =	56.3 sisma

Trazione massima nei tirafondi: N (kN) =	0.0 statico
Taglio massimo nei tirafondi: V (kN) =	26.4 statico

Le verifiche di resistenza dell'ancoraggio sono svolte nelle pagine seguenti.

VERIFICA DELL'ANCORAGGIO SULLA STRUTTURA IN C.A.

Campata sud - pila

Riferimento del nodo: **Appoggio della trave di impalcato**

Si verifica l'ancoraggio della struttura di base. L'azione massima è trasferita al piatto di base dal tacco di riscontro a taglio interno al dispositivo di appoggio.

Tipo di ancorante		HILTI HIT-HY 200A
Diametro della barra	d	16 mm
Classe acciaio barra		Classe 8.8
Area della barra di ancoraggio	A_b	201.1 mm ²
Numero di barre di ancoraggio	n.	6
Trazione di progetto - SLU	N_{Sd}	0.00 kN
Taglio di progetto - SLU	V_{Sd}	26.38 kN

Si considera un ancoraggio con barra inclinata di un angolo β rispetto alla normale alla superficie di ancoraggio (materiale base).

Angolo di infissione della barra di ancoraggio β 0 °

Componente di trazione di progetto - SLU	N'_{Sd}	0.00 kN
Componente di taglio di progetto - SLU	V'_{Sd}	26.38 kN

Calcolo della trazione resistente

Rottura di progetto lato calcestruzzo (classe C20/25)	$N_{0Rd,c}$	33.2 kN
Profondità nominale di ancoraggio	h_{nom}	120 mm
Profondità effettiva di ancoraggio	h_{act}	200 mm
Fattore di influenza della profondità	f_T	1.667
Resistenza cubica a comp. cls	R_{ck}	29.3 MPa
Fattore di confidenza	FC	1.20
Fattore classe di resistenza	$f_{b,N}$	0.99
Interasse di posa	s	118 mm
Interasse minimo di posa	s_{min}	80 mm
	s / s_{min}	1.48 > 1.0
Fattore interasse di posa	$f_{A,N}$	0.75
Distanza dal bordo	c	80 mm
Distanza minima di posa dai bordi	c_{min}	80 mm
	c / c_{min}	1.00 > 1.0
Fattore distanza dal bordo - sp	$f_{R,N}$	0.76
Cedimento cono cls	$N_{Rd,c}$	31.2 kN
Resistenza a trazione (materiale base - resina)	N_{Rd}	31.2 kN
Resistenza a trazione (lato acciaio)	N_{Rd}	86.9 kN

Calcolo della resistenza a taglio

Rottura di progetto lato calcestruzzo (classe C20/25)	$V_{Rd,c}$	36.7 kN
Fattore classe di resistenza	$f_{b,V}$	0.99
Resistenza a taglio (materiale base)	V_{Rd}	36.3 kN
Resistenza a compressione caratt. materiale base	f_{ck}	24.30 N/mm ²
Spessore della struttura di base	t	1000 mm
Diametro di rottura del cono della soletta	d'	26 mm
Resistenza a taglio (rifollam. materiale base)	V_{Rd}	52.7 kN
Resistenza a taglio (lato acciaio)	V_{Rd}	57.9 kN

Verifiche di resistenza

Resistenza totale a trazione	$N_{Rd,tot}$	187.06 kN
Resistenza totale a taglio	$V_{Rd,tot}$	217.54 kN
verifica di resistenza a trazione		0.00 < 1.0
verifica di resistenza a taglio		0.12 < 1.0
Carico combinato sollecitante	F_{Sd}	26.38 kN
Inclinazione del carico combinato	α	1.57 rad
Capacità di carico combinato	F_{Rd}	217.54 kN
verifica di resistenza a taglio / trazione		0.12 < 1.0

VERIFICA DELL'ANCORAGGIO SULLA STRUTTURA IN C.A.

Campata sud - pila

Riferimento del nodo: **Appoggio della trave di impalcato (condiz. di sollevamento)**

Si verifica l'ancoraggio della struttura di base. L'azione massima è trasferita al piatto di base dal tacco di riscontro a taglio interno al dispositivo di appoggio.

Tipo di ancorante		HILTI HIT-HY 200A
Diametro della barra	d	16 mm
Classe acciaio barra		Classe 8.8
Area della barra di ancoraggio	A_b	201.1 mm ²
Numero di barre di ancoraggio	n.	5
Trazione di progetto - SLU	N_{Sd}	3.39 kN
Taglio di progetto - SLU	V_{Sd}	56.30 kN

Si considera un ancoraggio con barra inclinata di un angolo β rispetto alla normale alla superficie di ancoraggio (materiale base).

Angolo di infissione della barra di ancoraggio β 0 °

Componente di trazione di progetto - SLU	N'_{Sd}	3.39 kN
Componente di taglio di progetto - SLU	V'_{Sd}	56.30 kN

Calcolo della trazione resistente

Rottura di progetto lato calcestruzzo (classe C20/25)	$N_{0Rd,c}$	33.2 kN
Profondità nominale di ancoraggio	h_{nom}	120 mm
Profondità effettiva di ancoraggio	h_{act}	200 mm
Fattore di influenza della profondità	f_T	1.667
Resistenza cubica a comp. cls	R_{ck}	29.28 MPa
Fattore di confidenza	FC	1.20
Fattore classe di resistenza	$f_{b,N}$	0.99
Interasse di posa	s	118 mm
Interasse minimo di posa	s_{min}	80 mm
	s / s_{min}	1.48 > 1.0
Fattore interasse di posa	$f_{A,N}$	0.75
Distanza dal bordo	c	80 mm
Distanza minima di posa dai bordi	c_{min}	80 mm
	c / c_{min}	1.00 > 1.0
Fattore distanza dal bordo - sp	$f_{R,N}$	0.76
Cedimento cono cls	$N_{Rd,c}$	31.2 kN
Resistenza a trazione (materiale base - resina)	N_{Rd}	31.2 kN
Resistenza a trazione (lato acciaio)	N_{Rd}	86.9 kN

Calcolo della resistenza a taglio

Rottura di progetto lato calcestruzzo (classe C20/25)	$V_{Rd,c}$	36.7 kN
Fattore classe di resistenza	$f_{b,V}$	0.99
Resistenza a taglio (materiale base)	V_{Rd}	36.3 kN
Resistenza a compressione caratt. materiale base	f_{ck}	24.30 N/mm ²
Spessore della struttura di base	t	1000 mm
Diametro di rottura del cono della soletta	d'	26 mm
Resistenza a taglio (rifollam. materiale base)	V_{Rd}	52.7 kN
Resistenza a taglio (lato acciaio)	V_{Rd}	57.9 kN

Verifiche di resistenza

Resistenza totale a trazione	$N_{Rd,tot}$	155.88 kN
Resistenza totale a taglio	$V_{Rd,tot}$	181.28 kN
verifica di resistenza a trazione		0.02 < 1.0
verifica di resistenza a taglio		0.31 < 1.0
Carico combinato sollecitante	F_{Sd}	56.40 kN
Inclinazione del carico combinato	α	1.51 rad
Capacità di carico combinato	F_{Rd}	179.41 kN
verifica di resistenza a taglio / trazione		0.31 < 1.0

Apparecchi d'appoggio - Neoprene

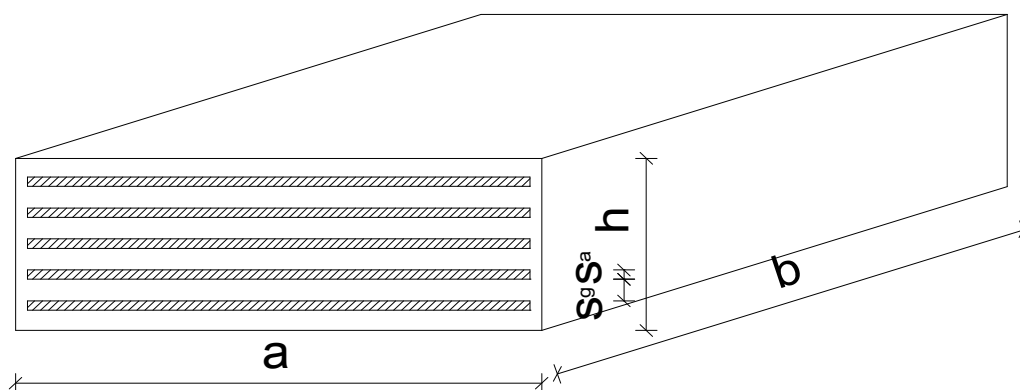
Appoggio dell'impalcato Campata sud - pila

Sollecitazioni di progetto - Appoggio tipo

Condizioni di esercizio - SLE

Forza verticale totale: F_z (kg) =	4 185
Forza verticale per carichi permanenti: F_z (p) (kg) =	2 092
Forza verticale per azioni di breve durata (variabili): F_z (q) (kg) =	2 092
Forza orizzontale totale: F_{xy} (kg) =	1 866
Forza orizzontale per carichi permanenti: F_{xy} (p) (kg) =	840
Forza orizzontale per carichi di breve durata (variabili): F_{xy} (q) (kg) =	1 026
	$\psi_{2j} =$ 0.60

Si assume che le azioni orizzontali per sisma e vento siano assorbite dai ritegni in acciaio.



Caratteristiche geometriche dell'appoggio

Lato trasversale appoggio: a (cm) =	15
Lato longitudinale appoggio: b (cm) =	18
Spessore singolo strato di gomma: s_g (cm) =	2.0
Numero di strati di gomma interni ai lamierini: n_g =	1
Spessore strato di gomma esterno: s_e (cm) =	0
Spessore totale della gomma interna ai lamierini: h_g (cm) =	2
Numero di lamierini di armatura in acciaio: n_a =	0
Spessore singolo lamierino: s_a (cm) =	0

Spessore totale dell'appoggio: h (cm) =	2
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Caratteristiche della gomma, per durezza 60 gradi Shore A3:

Modulo di elasticità tangenziale della gomma: G (kg/cm ²) (= E/3) =	9.0
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Area di appoggio: A_c (cm ²) =	270.0
Area di appoggio ridotta: A_r (cm ²) =	257.6
Coefficiente di forma: $S = \mu$ =	2.045

Tensioni e deformazioni nell'appoggio

Tensione tangenziale prodotta da F_{xy} (p) e F_{xy} (q): τ_H (kg/cm ²) =	3.11
Scorrimento elastico dovuto a F_{xy} (p) e F_{xy} (q): $\tan \gamma$ =	0.35
Spostamento orizzontale elastico longitudinale: u_a (cm) =	0.691
Spostamento orizzontale elastico trasversale: u_b (cm) =	0
Tensione normale prodotta dal carico F_z : σ_V (kg/cm ²) =	16.25
Tensione normale prodotta dal carico permanente F_z (p): σ_V' (kg/cm ²) =	8.12
Tensione tangenziale prodotta da F_z : τ_V (kg/cm ²) =	11.92
Rotaz. all'app. in direz. y (nel piano della strutt.) - Cond. statiche: α (rad) =	0.00602
Rotaz. all'appoggio in direz. x (fuori dal piano della struttura): α_x (rad) =	0.00005
Tensione tangenziale prodotta dalla rotazione α : $\tau_{\alpha y}$ (kg/cm ²) =	1.52
Rotaz. all'app. in direz. y (nel piano della strutt.) - Cond. sismiche: α (rad) =	0.00551
Rotaz. all'appoggio in direz. x (fuori dal piano della struttura): α_x (rad) =	0.00005
Tensione tangenziale prodotta dalla rotazione α : $\tau_{\alpha y}$ (kg/cm ²) =	1.39
Accorciamento elastico dell'appoggio dovuto a F_z : Δh (cm) =	0.0779

Verifiche appoggio elastomerico non armato

Verifiche di resistenza

σ_V (kg/cm ²) =	16.25	<	22.1	kg/cm ²
σ_V' (kg/cm ²) =	8.12	<	50.0	kg/cm ²
$\sigma_{V''}$ (kg/cm ²) =	8.12	<	22.1	kg/cm ²
Cond. statiche: Δh (cm) =	0.0779	>	$(a/2) \tan \alpha =$	0.0456 cm
Cond. sism: Δh (cm) =	0.0779	>	$(a/6) \tan \alpha =$	0.0139 cm

Verifiche di stabilità

h (cm) =	2.00	<	$a / 5 =$	3.00 cm
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VERIFICA DEGLI SPOSTAMENTI

Campata sud - pila

Luce teorica di calcolo	L	12.326 m
Variazione termica di progetto	$\Delta T =$	25 °C
Dilatazione termica massima attesa	$\Delta L =$	3.70 mm

- Condizioni statiche

Spostamento massimo in direzione longitudinale	d	8.5 mm
Asolatura nei piatti	d'	20.0 mm
verifica di spostamento ammesso		0.43 < 1.0

- Condizioni sismiche

Spostamento massimo in direzione longitudinale	d	17.5 mm
Asolatura nei piatti	d'	20.0 mm
verifica di spostamento ammesso		0.88 < 1.0